

## Study of the resonance modes of a magnetic tunnel junction-like system

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The ferromagnetic resonance (FMR) modes of a magnetic tunnel junction-like system are investigated. Such a system consists of an interfacial (F/AF) interaction described by an exchange anisotropy field  $H_E$  and a magnetic coupling of two ferromagnetic layers separated by a nonmagnetic interlayer. The latter interaction is accounted for by bilinear  $J_1$  and biquadratic  $J_2$  coupling strengths. The dispersion relation, the resonant frequency,  $f$ , as well as the corresponding mode intensity,  $I$ , versus applied field  $H$  curves, have been studied. Analytical formulas for the resonance condition and intensity have been derived for the low magnetic coupling/high exchange anisotropy case. In this situation, the system is found to behave as two *uncoupled* layers with magnetic characteristics different from those of the initial layers; the effect of the low coupling is to modify the different anisotropies:  $J_1$  contributes to the exchange anisotropy while  $J_2$  modifies the magnetocrystalline anisotropies. For very strong coupling, the system behaves as a single (F/AF) system with effective exchange and magnetocrystalline anisotropy fields; these fields have been derived as a function of the individual layer magnetic parameters.

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### I. INTRODUCTION

Ferromagnetic resonance (FMR) is a powerful method which has been widely used to investigate a variety of magnetic system.<sup>1-9</sup> The present work deals with the ferromagnetic resonance modes (position and intensity) of a magnetic tunnel junction-like system. Such a system may consist of a stacking of an antiferromagnetic layer (AF) and two ferromagnetic layers (A and B) separated by a nonmagnetic interlayer.<sup>10-12</sup> The interaction at the interface of layer A with AF gives rise to a unidirectional anisotropy called exchange anisotropy.<sup>13-21</sup> This anisotropy can be modeled as a magnetic field  $\mathbf{H}_E$ , the exchange anisotropy field. The layer A magnetization  $\mathbf{M}_A$  is subjected to  $\mathbf{H}_E$  and is thus pinned. Layers A and B are magnetically coupled. The magnetic coupling can be described by the bilinear  $J_1$  and the biquadratic  $J_2$  coupling parameters.<sup>22-27</sup> The former may favor a parallel alignment (ferromagnetic coupling) or an antiparallel alignment (antiferromagnetic coupling) of  $\mathbf{M}_A$  and  $\mathbf{M}_B$  while the latter one ( $J_2$ ) may lead to a perpendicular configuration of the magnetizations.

The geometry of the system and the energy will be displayed in Sec. II. The relations giving the mode positions (resonance frequency) and the FMR intensity will be derived (Sec. III) and discussed as a function of the coupling strengths  $J_1$  and  $J_2$  and of the exchange anisotropy field  $H_E$ : for zero coupling (Sec. IV), for low magnetic coupling/high exchange anisotropy (Sec. V), and for very strong magnetic coupling (Sec. VI).

### II. THE MAGNETIC SYSTEM

The magnetic tunnel junction, the system under consideration here, is shown in Fig. 1. It consists of an antiferromagnetic layer (noted AF) on top of which is deposited a first ferromagnetic layer (labeled A). Layer A is separated from a second ferromagnetic layer B by a nonmagnetic interlayer.

All the thin film layers are assumed to lie in the  $x$ - $y$  plane, with the  $z$  axis normal to the film planes. The magnetization  $\mathbf{M}_A$  of layer A is defined, in spherical coordinates, by the angles  $\theta_A$  and  $\phi_A$ ; and similarly  $\mathbf{M}_B$  (layer B) by the angles  $\theta_B$  and  $\phi_B$ . Two magnetic phenomenon arise in this system. First, the exchange anisotropy at the interface AF-A, is modeled as a magnetic field  $\mathbf{H}_E$ , the exchange anisotropy field. The field  $\mathbf{H}_E$  is taken to be along the  $x$  axis (see Fig. 1). Second, we have the magnetic coupling between two ferromagnetic layers separated by a nonmagnetic interlayer. This interaction will be described by the bilinear  $J_1$  and biquadratic  $J_2$  coupling parameters. Moreover, layer A is supposed to have an in-plane uniaxial magnetocrystalline anisotropy, with the easy axis taken to be along the  $x$  axis. On the other hand, no in-plane magnetocrystalline anisotropy is included

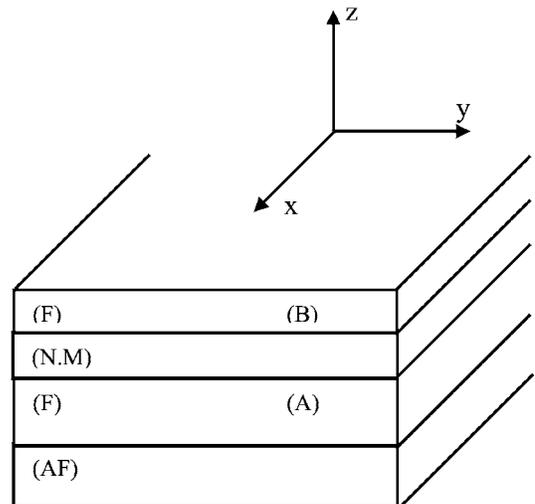


FIG. 1. The magnetic tunnel junction-like system. AF: antiferromagnetic layer. F: ferromagnetic layers (A and B). (N.M): nonmagnetic interlayer.

for layer  $B$ , i.e., the layer  $B$  magnetization is free to rotate within the plane in the absence of magnetic coupling. The external applied magnetic field  $\mathbf{H}$  is taken to be in the plane of the films, making an  $\alpha$  angle with the  $x$  axis. The microwave field  $\mathbf{h}$  is along the  $y$  axis. With all these considerations, the total free energy of the system per unit area can be explicitly written as

$$\begin{aligned}
 E = & t_A[-M_A H \sin \theta_A \cos(\alpha - \phi_A) + K_{\text{eff}A} \sin^2 \theta_A \\
 & + K_A \sin^2 \theta_A \sin^2 \phi_A - M_A H_E \sin \theta_A \cos \phi_A] \\
 & + t_B[-M_B H \sin \theta_B \cos(\alpha - \phi_B) + K_{\text{eff}B} \sin^2 \theta_B] \\
 & - J_1[\sin \theta_A \sin \theta_B \cos(\phi_A - \phi_B) + \cos \theta_A \cos \theta_B] \\
 & - J_2[\sin \theta_A \sin \theta_B \cos(\phi_A - \phi_B) + \cos \theta_A \cos \theta_B]^2.
 \end{aligned} \tag{1}$$

In the two first terms of Eq. (1),  $t_A$  and  $t_B$  are the thicknesses of layers  $A$  and  $B$ , respectively. The total energy  $E$  consists for layer  $A$  (the first term) of the Zeemann energy (interaction of the external magnetic field  $\mathbf{H}$  with the magnetizations),  $-\mathbf{M}_A \mathbf{H}$ , the shape and any out-of-plane uniaxial anisotropy with effective constant  $K_{\text{eff}A}$  ( $K_{\text{eff}A} = K_u - 2\pi M_A^2$ ,  $K_u$  being the uniaxial magnetocrystalline constant), the in-plane magnetocrystalline anisotropy with constant  $K_A$ , and the exchange anisotropy with exchange anisotropy field  $H_E$ . For layer  $B$  [the second term in Eq. (1)], the Zeeman energy and the effective uniaxial anisotropy term (shape and magnetocrystalline) are displayed. The interlayer coupling energy is given by the two last terms. The nature and the strength of the coupling are described by the sign and the magnitude of  $J_1$  and  $J_2$ . When  $J_1$  dominates and if it is positive the energy is minimal when  $\mathbf{M}_A$  and  $\mathbf{M}_B$  are parallel (ferromagnetic coupling), while if it is negative, then the lowest energy is achieved when  $\mathbf{M}_A$  and  $\mathbf{M}_B$  are antiparallel (antiferromagnetic coupling). If, on the other hand,  $J_2$  dominates and is negative (which was experimentally observed), then the minimum energy occurs when the magnetizations are oriented perpendicularly to each other (the  $90^\circ$ -type coupling).

At equilibrium, the magnetizations  $\mathbf{M}_A$  and  $\mathbf{M}_B$  must lie in the film plane, i.e.,  $\theta_A = \theta_B = 90^\circ$ , due to the strong demagnetizing field of the thin films and to the fact that the applied magnetic field is in-plane. Then, the angles  $\phi_{A,B}$  are given by the following two coupled equations (the equilibrium conditions):

$$\begin{aligned}
 H \sin(\alpha - \phi_A) = & \frac{H_A}{2} \sin 2\phi_A + H_E \sin \phi_A + \frac{J_1}{a} \sin(\phi_A - \phi_B) \\
 & + \frac{J_2}{a} \sin 2(\phi_A - \phi_B)
 \end{aligned} \tag{2a}$$

and

$$H \sin(\alpha - \phi_B) = -\frac{J_1}{b} \sin(\phi_A - \phi_B) - \frac{J_2}{b} \sin 2(\phi_A - \phi_B), \tag{2b}$$

where  $H_A = 2K_A/M_A$  is the planar anisotropy field for layer  $A$ ,  $a = t_A M_A$  and  $b = t_B M_B$ .

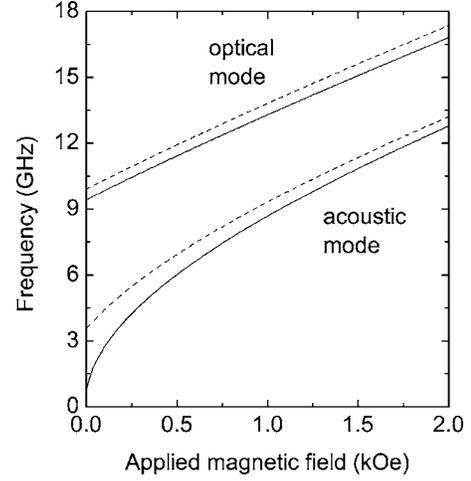


FIG. 2. Resonant frequency vs. applied field  $H$ . Ferromagnetic coupling:  $J_1 = 0.5$  erg cm $^{-2}$ ,  $J_2 = 0$ .  $H_E = 0$  (solid line),  $H_E = 250$  Oe (dashed line). Layer  $A$ :  $4\pi M_A = 10$  kG,  $H_{\text{keff}A} = -10$  kOe,  $H_A = 10$  Oe,  $t_A = 200$  Å,  $\gamma_A/2\pi = 2.8$  GHz kOe $^{-1}$ . Layer  $B$ :  $4\pi M_B = 6$  kG,  $H_{\text{keff}B} = -6$  kOe,  $H_{\text{in}B} = 0$  Oe,  $t_B = 100$  Å,  $\gamma_B/2\pi = 2.8$  GHz kOe $^{-1}$ .

### III. RESONANT MODE POSITION AND INTENSITY

#### A. The mode position

The normal modes of the system can be found by the use of the method based on the energy, in this case the equations coupling  $\Delta\theta_i$ ,  $\Delta\phi_i$  ( $i=A,B$ ); the excursions during oscillations about the equilibrium position can be written in a matrix form.<sup>28–30</sup> The matrix elements consist of the second derivatives of the energy  $E$  with respect to  $\theta_i$  and  $\phi_i$  ( $i=A,B$ ). A solution of the form  $\exp(i\omega t)$  will be taken;  $\omega$  is the (angular) frequency of precession. The solutions (normal modes) of the system will be found by setting the determinant of the matrix to zero. If one is using a variable frequency setup (frequency sweeper) and a fixed dc field, then one may solve for the frequency. One will then find a fourth-order equation in  $\omega$  (the resonant frequency) with at most two meaningful solutions (real and positive numbers) for given coupling strength parameters and dc field intensity and direction values.<sup>28–30</sup> Thus computing the second derivatives of the energy (evaluated at the equilibrium positions), setting the determinant to zero, and rearranging the terms, one will obtain the following fourth-order equation in  $\omega$ :

$$\begin{aligned}
 \omega^4 - \omega^2 \left[ \gamma_A^2 H_1^A H_2^A + \gamma_B^2 H_1^B H_2^B + c_1 \left( \frac{\gamma_B^2 H_2^B}{b} + \frac{\gamma_A^2 H_2^A}{a} \right) \right. \\
 \left. + c_2 \left( \frac{\gamma_B^2 H_1^B}{b} + \frac{\gamma_A^2 H_1^A}{a} \right) + c_1 c_2 \left( \frac{\gamma_A^2}{a^2} + \frac{\gamma_B^2}{b^2} \right) + \frac{2c_0 c_2 \gamma_A \gamma_B}{ab} \right] \\
 + \gamma_A^2 \gamma_B^2 \left[ H_2^A H_2^B + c_2 \left( \frac{H_2^B}{a} + \frac{H_2^A}{b} \right) \right] \left[ H_1^A H_1^B + c_1 \left( \frac{H_1^B}{a} \right. \right. \\
 \left. \left. + \frac{H_1^A}{b} \right) + \frac{c_1^2 - c_0^2}{ab} \right] = 0,
 \end{aligned} \tag{3}$$

where  $\gamma_A$  and  $\gamma_B$  denote the gyromagnetic ratios of layers  $A$  and  $B$ , respectively. The parameters  $c_j$  contain the coupling

strength:  $c_0 = J_1 + 2J_2 \cos(\phi_A - \phi_B)$ ,  $c_1 = J_1 \cos(\phi_A - \phi_B) + 2J_2 \cos^2(\phi_A - \phi_B)$  and  $c_2 = J_1 \cos(\phi_A - \phi_B) + 2J_2 \cos(2\phi_A - \phi_B)$ , and

$$H_1^A = H \cos(\alpha - \phi_A) - H_{K_{effA}} - H_A \sin^2 \phi_A + H_E \cos \phi_A, \quad (4a)$$

$$H_2^A = H \cos(\alpha - \phi_A) + H_A \cos 2\phi_A + H_E \cos \phi_A, \quad (4b)$$

$$H_1^B = H \cos(\alpha - \phi_B) - H_{K_{effB}}, \quad (4c)$$

$$H_2^B = H \cos(\alpha - \phi_B), \quad (4d)$$

where  $H_{K_{effA}} = 2K_{ueffA}/M_A$  and  $H_{K_{effB}} = 2K_{ueffB}/M_B$ .

### B. The FMR intensity

The FMR mode intensity is defined as corresponding to the area under the absorption line. In the present study, the applied magnetic field  $\mathbf{H}$  is parallel to the film plane, along the  $x$  direction, and the microwave  $\mathbf{h}$  field is along the  $y$

direction, the magnetizations precess in an elliptical orbit; the precession orbit is the  $y$ - $z$  plane. The intensity is thus given by<sup>30,31</sup> (taking into account the fact that, in the more general case, the magnetization components  $m_i$  are complex quantities)

$$I = \frac{(t_A m_{Ay} + t_B m_{By})(t_A m_{Ay} + t_B m_{By})^*}{t_A(m_{Ay} m_{Ay}^* + m_{Az} m_{Az}^*)/2M_A + t_B(m_{By} m_{By}^* + m_{Bz} m_{Bz}^*)/2M_B}. \quad (5)$$

Here  $m$  denotes the time-dependent magnetization component for  $A$  and  $B$  (the asterisk denotes the complex conjugate expressions). The magnetization components,  $m$ , are assumed to be uniform throughout each individual layer. One can compute all the four rf magnetization components by the use of the  $4 \times 4$  matrix and through the derivation of  $\Delta\theta_A$ ,  $\Delta\phi_A$ ,  $\Delta\theta_B$ ,  $\Delta\phi_B$ . After some algebraic manipulations, the rf magnetizations are computed and substituted into the intensity  $I$  [Eq. (5)]. When the two magnetizations are pointing along the  $x$  axis (the  $H$  direction), the intensity can then be put into the following form:

$$I = \frac{2ab\omega^2(aq + b)^2}{ab\omega^2(aq^2 + b) + b\gamma_A^2[qaH_2^A + c_2(q-1)]^2 + a\gamma_B^2[bH_2^B - c_2(q-1)]^2}, \quad (6a)$$

where

$$q = \frac{\gamma_A^2 c_2 b (aH_1^A + c_1) + \gamma_A \gamma_B c_0 a (bH_2^B + c_2)}{\gamma_A^2 b (aH_1^A + c_1) (aH_2^A + c_2) + \gamma_A \gamma_B c_0 c_2 a - a^2 b \omega^2}. \quad (6b)$$

Equation (3) has been numerically solved to study the resonant frequency versus applied field  $H$ ; for  $\mathbf{H}$  in the forward direction, the direction of  $\mathbf{H}_E$  ( $\alpha = 0^\circ$ ).

For the ferromagnetic coupling case ( $J_1 > 0$ ),  $\mathbf{M}_A$  and  $\mathbf{M}_B$  are expected to be along  $\mathbf{H}$  for all  $H$  values,  $\phi_A = \phi_B = 0^\circ$ . From the resolution of Eq. (3), two solutions  $\omega_1$  and  $\omega_2$  are expected, corresponding to the acoustic mode (where the magnetizations precess in phase) and to the optical mode (out of phase). The optical mode intensity will decrease with increasing coupling and would disappear for very strong coupling, in this case only the acoustic mode would remain (see Sec. VI). For ferromagnetic coupling, the high-frequency mode is the optical mode while the low frequency mode corresponds to the acoustic mode (note that this is the opposite to a fixed frequency analysis where the lower resonant field corresponds to the optical mode for ferromagnetic coupling). Examples of dispersion relation curves are shown in Fig. 2 for  $J_1 = +0.5 \text{ erg/cm}^2$ , for  $H_E = 0$  (solid line) and  $H_E = 250 \text{ Oe}$  (dashed line); for other parameters used in the computation, see the caption of Fig. 2. The frequency of both modes increases with increasing field  $H$ . One can see that  $H_E$  induces a shift to higher frequency values for the two modes.

For the low  $H$  field values, the shift in the acoustic mode is more important than that of the optical mode. However, as  $H$  increases, the shift in both modes is of the same order of magnitude.

The corresponding intensities are plotted in Fig. 3. The effect of  $\mathbf{H}_E$  is to increase (decrease) the intensity of the optical (acoustic) mode by practically the same amount.

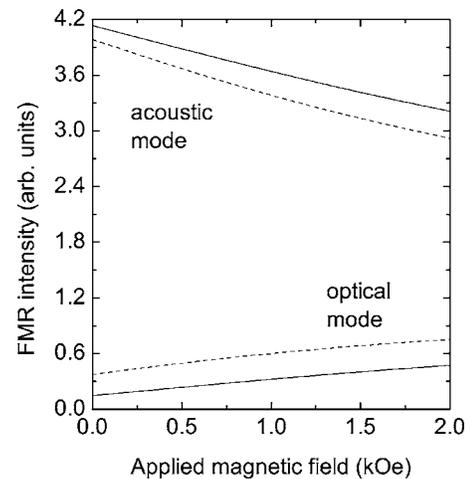


FIG. 3. FMR intensity vs. applied field  $H$ . Ferromagnetic coupling:  $J_1 = 0.5 \text{ erg cm}^{-2}$ ,  $J_2 = 0$ .  $H_E = 0$  (solid line),  $H_E = 250 \text{ Oe}$  (dashed line). Other parameters as for Fig. 2.

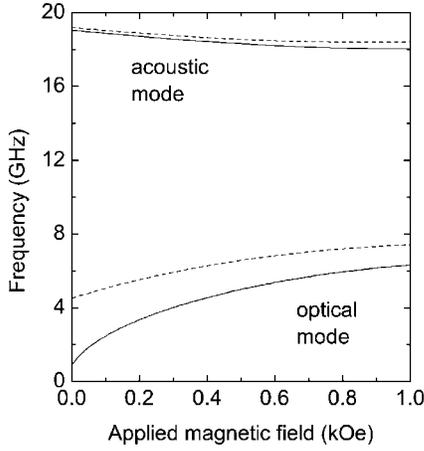


FIG. 4. Resonant frequency vs. applied field  $H$ . Antiferromagnetic coupling:  $J_1 = -2 \text{ erg cm}^{-2}$ ,  $J_2 = 0$ .  $H_E = 0$  (solid line),  $H_E = 250 \text{ Oe}$  (dashed line). Other parameters as for Fig. 2.

When the coupling is antiferromagnetic ( $J_1 < 0$ ) and if the coupling is strong enough to overcome the effect of the applied field  $H$ , then  $\mathbf{M}_A$  and  $\mathbf{M}_B$  are antiparallel, i.e.,  $\phi_A = 0$ ,  $\phi_B = \pi$  (assuming  $a > b$ ). This case is displayed in Figs. 4 and 5 for  $J_1 = -2 \text{ erg/cm}^{-2}$  and  $H$  between 0 and 1 kOe. Note that, for the antiferromagnetic coupling, the lower frequency mode (the higher magnetic field) is the optical mode (this is the reversed situation compared to the ferromagnetic coupling). The mode behavior is different, here, from that observed in the ferromagnetic case. The acoustic mode (the higher frequency mode) slightly decreases with increasing applied field  $H$  while the optical mode frequency increases with  $H$ . The exchange anisotropy field  $H_E$  seems to affect more the optical than the acoustic modes, i.e., the shift to higher frequency value is more important for the optical than the acoustic modes. The FMR intensity is shown in Fig. 5; the increase of  $H_E$  leads to an increase (decrease) of the intensity of the acoustic (optical) mode which is the opposite of what was seen in the ferromagnetic coupling case.

In the following sections, some cases of interest will be studied. In particular, it will be shown that, when the mag-

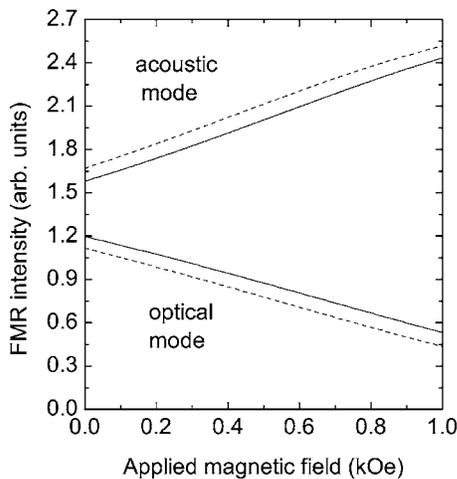


FIG. 5. FMR intensity vs. applied field  $H$ . Antiferromagnetic coupling:  $J_1 = -2 \text{ erg cm}^{-2}$ ,  $J_2 = 0$ .  $H_E = 0$  (solid line),  $H_E = 250 \text{ Oe}$  (dashed line). Other parameters as for Fig. 2.

netic coupling is zero, very low and strong compared to the exchange anisotropy effect, the resonance modes (frequency and intensity) can be described by analytical formula.

#### IV. THE ZERO COUPLING CASE

When the layers are not coupled ( $J_1 = J_2 = 0$ ) then  $c_j = 0$  and Eq. (3) will reduce to  $(\omega^2 - \gamma_A^2 H_1^A H_2^A)(\omega^2 - \gamma_B^2 H_1^B H_2^B) = 0$ , which, upon substituting the  $H_j^i$  by their expressions [Eqs. (4a)–(4d)] will lead to the following two uncoupled equations:

$$\frac{\omega_A^2}{\gamma_A^2} = [H \cos(\alpha - \phi_A) - H_{KeffA} - H_A \sin^2 \phi_A + H_E \cos \phi_A] \times [H \cos(\alpha - \phi_A) + H_A \cos 2\phi_A + H_E \cos \phi_A] \quad (7)$$

and

$$\frac{\omega_B^2}{\gamma_B^2} = H(H - H_{KeffB}). \quad (8)$$

Equation (7) is the resonance condition for a single layer with in-plane and exchange anisotropies,<sup>20,21</sup> while Eq. (8) is the well-known resonance condition for a ferromagnetic thin film with an in-plane applied field and where all the directions within the plane are equivalent (no in-plane anisotropy, i.e.,  $\alpha = \phi_B$ ). Thus in this uncoupled case, two peaks are expected to be observed in the FMR spectra whose positions are given by the resonance conditions [Eqs. (7) and (8)].

The corresponding intensities of these peaks have been evaluated. When the layers are uncoupled then  $c_j = 0$ . For the intensity of layer  $B$ , when  $c_j = 0$ , then  $q = 0$ . Substituting in Eq. (6a)  $q = 0$  and replacing  $\omega$  by  $\omega_B$  [Eq. (8)], one will find

$$I_B = \frac{2bH_1^B}{H_1^B + H_2^B}. \quad (9)$$

Since  $\alpha = 0$ , then  $\phi_B = 0$  for all  $H$  and Eq. (9) becomes

$$I_B = \frac{2I_B M_B (H - H_{KeffB})}{2H - H_{KeffB}}. \quad (10)$$

For the intensity,  $I_A$ , of layer  $A$ , it is easy to see that both numerator and denominator in  $q$  are equal to zero (the first and last terms in the denominator of  $q$  [Eq. (6b)] cancel because of the resonance condition [Eq. (7)], recall in this case that  $\omega^2 = \gamma_A^2 H_1^A H_2^A$ ). Due to this indetermination, the intensity of each layer is usually found separately. Alternatively, one can compute  $q$  and  $I$  for low coupling strengths, then let  $c_j$  go to zero [see Eq. (17) in Sec. V, below] to find the intensity of the uncoupled layers; this way will be shown later in the following section. Both methods will lead to the same result, for layer  $A$ :

$$I_A = \frac{2aH_1^A}{H_1^A + H_2^A}, \quad (11)$$

where  $H_1^A$  and  $H_2^A$  are given by Eqs. (4a) and (4b). Recall that in the present case  $\alpha = 0$ , therefore  $\mathbf{M}_A$  is expected to be along the  $x$  axis for all  $H$ , i.e.,  $\phi_A = 0$ . Thus substituting  $H_1^A$  and  $H_2^A$ , one will find

$$I_A = \frac{2t_A M_A (H - H_{K_{effA}} + H_E)}{2H - H_{K_{effA}} + H_A + 2H_E}. \quad (12)$$

Equations (10) and (12) giving the intensities of single layers with different anisotropies are quite known relations.<sup>31,32</sup> The terms multiplying  $2a$  and  $2b$  in Eqs. (9) and (11) are referred to as the “elliptic terms.”<sup>33</sup> Note that the ellipticity factor in Eq. (12) explicitly depends on the in-plane anisotropy field  $H_A$  and the exchange bias  $H_E$ .

In the case where, for layer  $A$ , the exchange and in-plane fields,  $H_E$  and  $H_A$ , are very small compared to  $(H - H_{K_{eff}})$  [this assumption is often true, for instance, in permalloy,  $(-H_{K_{eff}})$ , equal to  $4\pi M_S$ , is about 10 kOe, while  $H_E$  and  $H_A$  are around 20 and 5 Oe], the intensity  $I_A$  may be written as the sum of different contributions to the intensity. Making the above approximations, the intensity  $I_A$  will be

$$I_A = I_0 + I_{ex} + I_{in}, \quad (13a)$$

where

$$I_0 = \frac{2t_A M_A (H - H_{K_{effA}})}{2H - H_{K_{effA}}} \quad (13b)$$

would be the intensity of layer  $A$  if it did not have in-plane and exchange anisotropies [similar to Eq. (9) for layer  $B$ ],

$$I_{ex} = \frac{2t_A M_A H_{K_{effA}}}{(2H - H_{K_{effA}})^2} H_E \quad (13c)$$

is the contribution of the exchange anisotropy to the intensity of the layer, and

$$I_{in} = \frac{2t_A M_A (H_{K_{effA}} - H)}{(2H - H_{K_{effA}})^2} H_A \quad (13d)$$

is the intensity due to the in-plane anisotropy.

Note that, since  $H_{K_{effA}}$  is negative, both the exchange and the in-plane anisotropies will tend to decrease the intensity  $I_A$ . For a very strong applied field, it is easy to see that both  $I_{ex}$  and  $I_{in}$  vanish and the intensity  $I_A$  will be equal simply to the known result,  $I_A = t_A M_A$ . (This is in fact the intensity per unit area; experimentally, however, the total intensity is  $M \times V$ , where  $V$  is the volume of the sample.)

## V. LOW MAGNETIC COUPLING

For an arbitrary magnetic coupling, there is no analytical formula for the resonance modes. For the low magnetic coupling case, it will be shown in this section that the resonance modes, frequency, and intensity, found numerically from Eqs. (3) and (6a), can be described by analytical formula. Indeed, neglecting second-order terms of the magnetic coupling parameters ( $c_i c_k$ ) in Eq. (3) and solving for  $\omega$ , one will obtain the following two solutions:

$$\omega_1^2 = \omega_A^2 + \frac{c_1}{a} \gamma_A^2 H_2^A + \frac{c_2}{a} \gamma_A^2 H_1^A \quad (14a)$$

and

$$\omega_2^2 = \omega_B^2 + \frac{c_1}{b} \gamma_B^2 H_2^B + \frac{c_2}{b} \gamma_B^2 H_1^B, \quad (14b)$$

where  $\omega_A$  and  $\omega_B$  are given by the expressions in Eqs. (7) and (8) i.e., the uncoupled layer case;  $H_1^A$ ,  $H_2^A$ ,  $H_1^B$ , and  $H_2^B$  have been defined earlier in Eqs. (4a)–(4d). Note that in the limit where there is no coupling ( $c_1 = c_2 = 0$ ), then  $\omega_1$  and  $\omega_2$  correctly reduce to  $\omega_A$  and  $\omega_B$  as expected.

Furthermore, Eqs. (14a) and (14b) can also be written as

$$\omega_1^2 = \gamma_A^2 \left( H_1^A + \frac{c_1}{a} \right) \left( H_2^A + \frac{c_2}{a} \right) \quad (15a)$$

and

$$\omega_2^2 = \gamma_B^2 \left( H_1^B + \frac{c_1}{b} \right) \left( H_2^B + \frac{c_2}{b} \right), \quad (15b)$$

i.e., the above equations will lead to the previous ones [Eqs. (14a) and (14b)], if the second-order terms ( $c_1 c_2$ ) are neglected as was assumed in the beginning.

Moreover, Eqs. (15a) and (15b) can be put in a very interesting form. For the case of a ferromagnetic coupling with  $\mathbf{H}$  in the forward direction, i.e.,  $\alpha = \phi_A = \phi_B = 0$  (or even in the antiferromagnetic coupling but in the saturated state), and if one substitutes the  $H_j^i$  by their expressions and rearranges the terms, then Eq. (15a) can be written as

$$\frac{\omega_1^2}{\gamma_A^2} = \left[ H - \left( H_{K_{effA}} - \frac{2J_2}{t_A M_A} \right) + \left( H_E + \frac{J_1}{t_A M_A} \right) \right] \times \left[ H + \left( H_A + \frac{2J_2}{t_A M_A} \right) + \left( H_E + \frac{J_1}{t_A M_A} \right) \right]. \quad (16a)$$

Comparing Eq. (16a) with Eq. (7) (for  $\alpha = \phi_A = 0$ ), one may regard the mode  $\omega_1$  as that of a single layer with an effective anisotropy field given by  $(H_{K_{effA}} - 2J_2/t_A M_A)$ , an in-plane anisotropy field  $(H_A + 2J_2/t_A M_A)$ , and an exchange anisotropy field  $(H_E + J_1/t_A M_A)$ . Note that the magnetogyric ratio  $\gamma_A$  is the same as that of layer  $A$ .

In the same manner, Eq. (15b) can be written as

$$\frac{\omega_2^2}{\gamma_B^2} = \left[ H - \left( H_{K_{effB}} - \frac{2J_2}{t_B M_B} \right) + \frac{J_1}{t_B M_B} \right] \left( H + \frac{2J_2}{t_B M_B} + \frac{J_1}{t_B M_B} \right). \quad (16b)$$

Similarly  $\omega_2$  can describe the resonant frequency of a layer with an effective anisotropy field given by  $(H_{K_{effB}} - 2J_2/t_B M_B)$ , an in-plane anisotropy field  $H_B = 2J_2/t_B M_B$ , and an exchange anisotropy field  $H_E^B = J_1/t_B M_B$ .

Note that  $\omega_1$  [in Eqs. (14a), (15a), and (16a)] depends only on the layer  $A$  parameters, while  $\omega_2$  contains only the layer  $B$  parameters. Thus, when the magnetic coupling is low, the system behaves as two *uncoupled* layers with magnetic characteristics different from those of layers  $A$  and  $B$ . The effect of the low coupling is to modify the different anisotropies; the bilinear coupling,  $J_1$ , contributes to the exchange anisotropy while the biquadratic coupling,  $J_2$ , modifies the magnetocrystalline anisotropies (uniaxial and in-plane). Note that one cannot experimentally separate the contributions of  $J_1$  and  $J_2$ ; generally a value of  $(J_1 + 2J_2)$

(when the magnetizations are parallel) is derived (see, for instance, Refs. 25 and 26). From the present analysis, it is inferred that physically  $J_1$  seems to be equivalent to an exchange anisotropy while  $J_2$  is equivalent to an in-plane anisotropy. In fact, the equivalence between  $J_2$  and the in-plane magnetic anisotropy (a case similar to the latter one) was explicitly worked out in coupled layers with in-plane magnetic anisotropies; it was shown that a small deviation of the in-plane easy axis direction of one layer with respect to the one of the second layer may be interpreted as a small biquadratic coupling.<sup>34</sup> Also, Eqs. (16a) and (16b) are valid for ferromagnetic (F) ( $J_1 > 0$ ) and antiferromagnetic (AF) ( $J_1 < 0$ ) coupling. For F (AF), the exchange anisotropy field  $H_E$  increases (decreases) for layer A. For layer B, which initially does not have in-plane and exchange anisotropies, the effect of the low coupling is to give to the layer a small exchange bias and an in-plane anisotropy. Moreover, these additional anisotropies vary as  $1/t$ , giving them a surface anisotropy character.

One should, now, compute the intensities of these modes and show that they correspond to two uncoupled layers.

Once again for ferromagnetic coupling, and  $\mathbf{H}$  in the forward direction,  $\alpha=0$ ,  $\phi_A=\phi_B$ , then  $c_0=c_1=c_2=J_1+2J_2=J_{eff}$ . For the mode corresponding to  $\omega_1$  the first and last terms of the denominator in  $q$  [Eq. (6b)] cancel because of the resonance condition [Eq. (15a)]; but it is easy to see that for low coupling ( $J_{eff}$  goes to zero),  $1/q$  goes to zero. Using this fact in Eq. (6a) and replacing  $\omega_1$  by its expression [Eq. (15a)], the intensity,  $I_1$ , is found to be

$$I_1 = \frac{2a \left( H_1^A + \frac{J_{eff}}{a} \right)}{H_1^A + H_2^A + \frac{2J_{eff}}{a}}. \quad (17)$$

Note that if  $J_{eff}=0$  (no coupling),  $I_1$  reduces to  $I_A$  as expected [in fact, this is a good way to find the intensity of the uncoupled layers from Eqs. (6a) and (6b)]. Substituting the  $H_j^A$  by their expressions, the intensity of mode 1 [Eq. (17)] in the forward direction can be written as

$$I_1 = \frac{2t_A M_A \left[ H - \left( H_{K_{effA}} - \frac{2J_2}{t_A M_A} \right) + \left( H_E + \frac{J_1}{t_A M_A} \right) \right]}{2H - \left( H_{K_{effA}} - \frac{2J_2}{t_A M_A} \right) + \left( H_A + \frac{2J_2}{t_A M_A} \right) + 2 \left( H_E + \frac{J_1}{t_A M_A} \right)}. \quad (18)$$

Comparing Eq. (18) with the intensity of a single layer [Eq. (12)], one can see that Eq. (18) is indeed the intensity of a single layer with these characteristics:  $(H_{K_{effA}} - 2J_2/t_A M_A)$ ,  $(H_A + 2J_2/t_A M_A)$ , and  $(H_E + J_1/t_A M_A)$ . So, the analysis of the FMR intensity and the mode position are coherent.

One can express  $I_1$  in term of  $I_A$ ; making the approximation that  $J_{eff}$  is small and using Eq. (12), Eq. (18) can be written as

$$I_1 = I_A \left[ 1 + \frac{J_1 + 2J_2}{t_A M_A} \times \frac{H_A + H_{K_{effA}}}{(H - H_{K_{effA}} + H_E)(2H - H_{K_{effA}} + 2H_E + H_A)} \right]. \quad (19)$$

Note that for very strong applied field  $H$ ,  $I_1$  will tend to  $I_A$ .

For the intensity of the second mode (corresponding to  $\omega_2$ ), it is easy to see that as  $J_{eff}$  goes to zero,  $q$  will go to zero. Using this limit in Eq. (6a) and replacing  $\omega_2$  by its expression [Eq. (15b)], the intensity  $I_2$  will be

$$I_2 = \frac{2b \left( H_1^B + \frac{J_{eff}}{b} \right)}{H_1^B + H_2^B + \frac{2J_{eff}}{b}} \quad (20)$$

or after replacing  $H_j^B$  by their expressions

$$I_2 = \frac{2t_B M_B \left[ H - \left( H_{K_{effB}} - \frac{2J_2}{t_B M_B} \right) + \frac{J_1}{t_B M_B} \right]}{2H - \left( H_{K_{effB}} - \frac{2J_2}{t_B M_B} \right) + \frac{2J_2}{t_B M_B} + \frac{2J_1}{t_B M_B}}. \quad (21)$$

The same remark can be made once again. Eq. (21) can be considered as the intensity of a layer (by comparison with the general formula) with an effective uniaxial anisotropy  $(H_{K_{effB}} - 2J_2/t_B M_B)$ , an in-plane anisotropy  $H_B = 2J_2/t_B M_B$ , and an exchange bias  $H_E^B = J_1/t_B M_B$ .

In terms of  $I_B$ , the combination of Eqs. (10) and (21) would give

$$I_2 = I_B \left( 1 + \frac{J_1 + 2J_2}{t_B M_B} \frac{H_{K_{effB}}}{(H - H_{K_{effB}})(2H - H_{K_{effB}})} \right). \quad (22)$$

## VI. STRONG MAGNETIC COUPLING

When the magnetic coupling is ferromagnetic and very strong, one expects  $\phi_A = \phi_B = \phi_F$  for all  $H$  values ( $\phi_F = 0$  for  $\alpha = 0$ ). In this case,  $c_0 = c_1 = c_2 = J_1 + 2J_2 = J_{eff}$  and the terms in  $J_{eff}^2$  dominate in Eq. (3). Keeping only the second-order terms in  $J_{eff}$  in Eq. (3), substituting the  $H_i^j$  by their expressions, and rearranging the terms will lead to the following resonance relation:

$$\frac{\omega^2}{\gamma_{eff}^2} = [H \cos(\alpha - \phi_F) - H_{K_{eff}}^F - H_A^{eqF} \sin^2 \phi_F + H_E^{eqF} \cos \phi_F] \times [H \cos(\alpha - \phi_F) + H_A^{eqF} \cos 2\phi_F + H_E^{eqF} \cos \phi_F]. \quad (23a)$$

Equation (23a) is the resonance relation of a single layer [compare with Eq. (7)] with the following magnetic characteristics: the effective magnetogyric ratio,  $\gamma_{eff}^F$ , is given by

$$\gamma_{eff}^F = \frac{t_A M_A + t_B M_B}{\frac{t_A M_A}{\gamma_A} + \frac{t_B M_B}{\gamma_B}}, \quad (23b)$$

the effective uniaxial anisotropy field,  $H_{K_{eff}}^F$ , is

$$H_{K_{eff}}^F = \frac{t_A M_A H_{K_{eff}A} + t_B M_B H_{K_{eff}B}}{t_A M_A + t_B M_B}, \quad (23c)$$

and equivalent exchange anisotropy field,  $H_E^{eqF}$ , and in-plane anisotropy field,  $H_A^{eqF}$ , are given, respectively, by

$$H_E^{eqF} = \frac{t_A M_A H_E}{t_A M_A + t_B M_B} \quad (23d)$$

and

$$H_A^{eqF} = \frac{t_A M_A H_A}{t_A M_A + t_B M_B}. \quad (23e)$$

Thus, in the strong ferromagnetic coupling, only one mode (the acoustic mode) will be seen in the FMR spectrum. The whole system behaves as a AF/F bilayer system with exchange bias  $H_E^{eqF}$  (lower than  $H_E$ ) and with effective magnetogyric ratio and effective anisotropy fields.

The intensity of this mode can be computed. For strong coupling ( $J_{eff}$  very large), it is easy to see that  $q$ , in Eq. (6b), will tend to 1, while  $J_{eff}(q-1)$  appearing in the denominator of  $I$  [Eq. (6a)] will reach the limiting value  $ab(\gamma_B H_2^B - \gamma_A H_2^A)/(a\gamma_B + b\gamma_A)$ . Substituting these values into  $I$  and replacing  $\omega$  by its expression for strong magnetic coupling [Eq. (23a)], one will find

$$I^F = \frac{2(a+b)(aH_1^A + bH_1^B)}{(aH_1^A + bH_1^B) + (aH_2^A + bH_2^B)}. \quad (24)$$

Once again,  $\phi_F = 0$  (i.e.,  $\alpha = 0$ ) will be considered; after substituting the  $H_i^j$  by their expressions and rearranging the terms, Eq. (24) may be written as

$$I^F = \frac{2(t_A M_A + t_B M_B)(H + H_E^{eqF} - H_{K_{eff}}^F)}{2H + 2H_E^{eqF} + H_A^{eqF} - H_{K_{eff}}^F}, \quad (25)$$

where  $H_{K_{eff}}^F$ ,  $H_E^{eqF}$  and  $H_A^{eqF}$  are given by Eqs. (23c)–(23e). Comparing Eqs. (25) and (12), one can see that Eq. (25) may

indeed represent the intensity of a ferromagnetic layer with an exchange anisotropy (given by  $H_E^{eqF}$ ) and in-plane magnetocrystalline anisotropy ( $H_A^{eqF}$ ) and effective uniaxial anisotropy ( $H_{K_{eff}}^F$ ). The intensity formula is thus in agreement with the interpretation of the resonance relation.

Furthermore, if one defines an effective magnetization of the whole system,  $M_{eff}$ , as the total magnetic moment per unit volume, i.e.,  $M_{eff} = (t_A M_A + t_B M_B)/(t_A + t_B)$ , then Eq. (25) will be

$$I^F = \frac{2(t_A + t_B)M_{eff}(H + H_E^{eqF} - H_{K_{eff}}^F)}{2H + 2H_E^{eqF} + H_A^{eqF} - H_{K_{eff}}^F}. \quad (26)$$

The term multiplying the elliptic factor is indeed magnetization times thickness (the total magnetic thickness), as in Eq. (12) (or multiplying by the surface  $S$ ,  $I$  will be proportional to  $M \times V$ ).

One may also study the strong antiferromagnetic coupling. If the applied magnetic field  $H$  is strong enough to overcome the effect of the antiferromagnetic coupling, i.e., the two magnetizations are parallel (in the direction of  $\mathbf{H}$ ), then the resonance modes are governed by the same equations as for the ferromagnetic coupling [Eqs. (23a)–(23e)]. On the other hand, when the effect of the strong antiferromagnetic coupling is greater than the effect of  $H$ , the magnetization will be antiparallel, i.e.,  $\phi_A = \phi_{AF}$  and  $\phi_B = \phi_{AF} + \pi$  (assuming  $a > b$ ) ( $\phi_{AF} = 0$  for  $\alpha = 0$ ). In this case,  $c_0 = J_1 - 2J_2 = J_{eff}^*$  and  $c_1 = c_2 = -J_{eff}^*$ . Following the same procedure as for the ferromagnetic coupling, i.e., keeping only the second-order terms in  $J_{eff}^*$ , and rearranging the terms, Eq. (3) will reduce to the following resonance condition:

$$\frac{\omega^2}{\gamma_{eff}^{AF2}} = [H \cos(\alpha - \phi_{AF}) - H_{K_{eff}}^{AF} - H_A^{eqAF} \sin^2 \phi_{AF} + H_E^{eqAF} \cos \phi_{AF}] [H \cos(\alpha - \phi_{AF}) + H_A^{eqAF} \cos 2\phi_{AF} + H_E^{eqAF} \cos \phi_{AF}], \quad (27a)$$

where

$$\gamma_{eff}^{AF} = \frac{t_A M_A - t_B M_B}{\frac{t_A M_A}{\gamma_A} - \frac{t_B M_B}{\gamma_B}} \quad (27b)$$

is an effective magnetogyric ratio,

$$H_{K_{eff}}^{AF} = \frac{t_A M_A H_{K_{eff}A} + t_B M_B H_{K_{eff}B}}{t_A M_A - t_B M_B} \quad (27c)$$

is the effective uniaxial anisotropy field,

$$H_E^{eqAF} = \frac{t_A M_A H_E}{t_A M_A - t_B M_B} \quad (27d)$$

is an equivalent exchange anisotropy field, and

$$H_A^{eqAF} = \frac{t_A M_A H_A}{t_A M_A - t_B M_B} \quad (27e)$$

is the in-plane anisotropy field of the whole system.

Once again the whole system behaves as a single ferromagnetic layer exchange coupled to an antiferromagnetic

layer F/AF with effective exchange anisotropy, in-plane, and uniaxial magnetocrystalline anisotropy fields and magneto-gyric ratio.

The intensity of this mode for the strong antiferromagnetic coupling can be computed by the same manner. Using Eqs. (6a) and (6b) and taking into account the fact that the magnetizations are antiparallel, the intensity is found to be

$$I^{AF} = \frac{2(t_A M_A - t_B M_B)^2 (H + H_E^{eqAF} - H_{Keff}^{AF})}{(t_A M_A + t_B M_B)(2H + 2H_E^{eqAF} + H_A^{eqAF} - H_{Keff}^{AF})}. \quad (28)$$

Once again, the intensity relation is in agreement with the resonance relation.

Note that in the strong ferromagnetic coupling case, the equivalent exchange and in-plane anisotropy fields of the whole system are lower than the  $H_E$  and  $H_A$  of layer A. However, in the antiferromagnetic coupling,  $H_E^{eqAF}$  and  $H_A^{eqAF}$  are larger than  $H_E$  and  $H_A$  respectively. Hence, in the latter case, one can increase the exchange bias of the equivalent system to any value by the right choice of  $(t_A M_A - t_B M_B)$ , i.e., by the choice of the ferromagnetic layer thicknesses and nature (through the magnetizations).

## VII. CONCLUSION

The ferromagnetic resonance (FMR) modes of a magnetic tunnel junction-like system are described. The dispersion relation, the resonant frequency  $f$  vs applied field, as well as the corresponding mode intensity,  $I$ , have been studied in different situations. The effect of the exchange anisotropy field  $H_E$  and magnetic coupling strengths ( $J_1$  and  $J_2$ ) on resonance mode behavior is investigated for arbitrary coupling ( $J_1$  and  $J_2$ ) parameters. Analytical formulas for the resonance condition and intensity have been derived for the low magnetic coupling/high exchange anisotropy case. In this situation, the system is found to behave as two *uncoupled* layers with magnetic characteristics different from those of the initial layers; the effect of the low coupling is to modify the different anisotropies,  $J_1$  contributes to the exchange anisotropy while  $J_2$  modifies the magnetocrystalline anisotropies. For very strong coupling, the system behaves as a single ferromagnetic layer exchange coupled to an antiferromagnetic one (F/AF system) with effective exchange and magnetocrystalline anisotropy fields; these fields have been derived as a function of the individual layer magnetic parameters. The exchange bias of this equivalent system is lower (higher) than  $H_E$  for ferromagnetic (antiferromagnetic) coupling.

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