

**Bending strain-driven modification of surface reconstructions: Au(111)**U. Tartaglino,<sup>1,2,\*</sup> E. Tosatti,<sup>1,2,3</sup> D. Passerone,<sup>1,2,4</sup> and F. Ercolessi<sup>1,2,5</sup><sup>1</sup>SISSA, Via Beirut 2, I-34014 Trieste, Italy<sup>2</sup>Unità INFN/SISSA<sup>3</sup>ICTP, Strada Costiera 11, I-34100 Trieste, Italy<sup>4</sup>CSCS, Galleria 2, CH-6928, Manno, Switzerland<sup>5</sup>Dipartimento di Fisica, Università di Udine, Via delle Scienze 208, I-33100 Udine, Italy

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Strain can affect the morphology of a crystal surface, and cause modifications of its reconstruction even when weak, as in the case of mechanical bending. We carried out calculations of strain-dependent surface free energy and direct bending simulations demonstrating the change of incommensurate reconstruction in Au(111) under strain, in good agreement with recent data. Time-dependent strain should cause a sliding of the topmost layer over the second, suggesting an interesting case of nanofriction. Bending strain could also be used to fine tune the spacing of selectively absorbed nanoclusters.

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Crystal surfaces often break their ideal bulklike symmetry, even in the absence of adsorbates, to lower their free energy through so-called reconstructions. Temperature, adsorbate coverage, and (in electrolytes) electrochemical potential<sup>1</sup> cause these reconstructions to evolve, either continuously or through two-dimensional phase transitions.<sup>2</sup> Work on semiconductor surfaces<sup>3-5</sup> indicated that external strain can also drive changes in surface reconstruction. In this paper we present theory and simulations indicating that reconstruction changes at an incommensurate metal surface like Au(111) can be provoked by application of strain, even with the weak strains attainable by bending a platelet or slab. When compared with very recent data, which appeared while this paper was being reviewed, the quantitative agreement is remarkable. We propose a possible application of this fine effect to selective adsorption of nanostructures on this surface. Because the strain-induced reconstruction changes involve a continuous change of first-layer lateral atom density, time-dependent bending strain will also drive a kind of incommensurate nanofriction.

In a semi-infinite crystal we introduce a uniform strain  $\lambda \varepsilon_{\alpha\beta}$ ,  $\lambda$  increasing from 0 to 1. The surface free-energy change, equalling the surface work, is obtained through thermodynamic integration,

$$\Delta(\gamma A) = W_s = \int_A dA \int_0^1 \tau_{\alpha\beta}^{\text{surf}}(\lambda) \varepsilon_{\alpha\beta} d\lambda,$$

where  $\gamma$  is the surface free energy per unit area,  $A$  is the area,  $\tau_{\alpha\beta}^{\text{surf}}$  the (strain dependent) surface stress, and  $\alpha$  and  $\beta$  span the  $(x, y)$  in-plane coordinates. If the surface free energies (per unit area) of two different reconstructions 1 and 2 satisfy  $\gamma_1^0 < \gamma_2^0$ , then in the absence of strain state 1 prevails over 2. However, their respective surface stress tensors generally differ, and free energies will thus vary with different slopes under strain, possibly leading to  $\gamma_1 > \gamma_2$ . We are interested in a detectable modification of reconstruction periodicity, particularly if it is obtainable even with the weak strains provided by mechanical bending.

To explore that, we choose the promising example of Au(111) as our test case. Au(111) displays a well-documented  $(L \times \sqrt{3})$  reconstruction,<sup>6</sup> ( $L \approx 22.5$  in ordinary conditions). It is promising because its long incommensurate period  $L$  should readily be changeable by a small but detectable amount. The  $(L \times \sqrt{3})$  pattern, commensurate along  $\langle 112 \rangle$ , is incommensurate in the orthogonal  $\langle 110 \rangle$  direction, where the reconstruction consists of a succession of hcp and fcc stripes, separated by sharp solitonlike boundaries, due to an extra row of atoms for each period  $L$  of reconstruction. X-ray-diffraction experiments<sup>7</sup> show, as temperature is raised from 300 to 800 K, a *continuous* shift of the periodicity  $L$  from about 22.5 to 20.9, which confirms the incommensurability. It also indicates a denser and denser surface at higher temperatures, a kind of negative expansion coefficient [probably arising, as in the case of Au(100),<sup>8,9</sup> to compensate for a large outward thermal relaxation of the first layer]. Here we shall describe how an external strain can also change the periodicity  $L$  of Au(111).

To describe the initial  $(L \times \sqrt{3})$  reconstruction we use an empirical many-body classical potential, the glue model,<sup>10</sup> known to describe reasonably well all the gold surfaces. In the glue model, the ground state of Au(111) is properly reconstructed, though with a somewhat shorter  $T=0$  periodicity  $L=11$ .<sup>11</sup> The difference between this and the experimental  $L=22.5$  is a purely numerical discrepancy that can be corrected for, and of no fundamental significance. The long-range “herringbone” secondary superstructure, also well known on this surface,<sup>7</sup> is much more delicate involving far smaller energies, and will not concern us any further here. All calculations and simulations are conducted for thin crystal slabs where strain is introduced by simulated bending,<sup>12</sup> as in real-life experiments<sup>1</sup> (although of course our theoretical slabs are far thinner).

Calculations of the surface free energy change under strain start with an  $N$ -layer fcc (111) slab, its two faces  $(L \times \sqrt{3})$  reconstructed with different periodicities  $L$  and  $L'$ . This is obtained by the addition of one extra  $[11\bar{2}]$  row of surface atoms every  $L$ , followed by relaxation.<sup>11</sup> We carry out molecular dynamics simulations of about 1 ns at 100 K, to obtain by standard methods<sup>13</sup> the average stress tensor

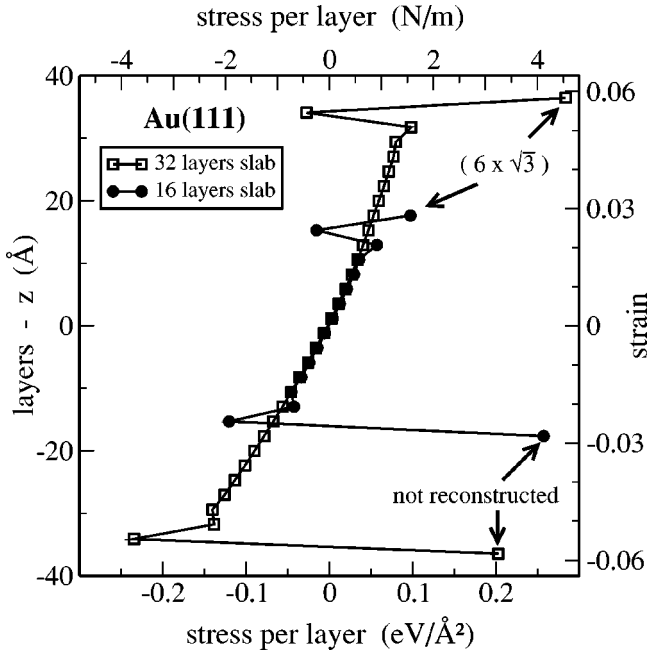


FIG. 1. Layer-resolved stress profiles of two Au(111) slabs with 16 and 32 layers, subjected to the same bending curvature. Note the large surface stress and the subsurface oscillations. The nonlinear bulk stress profile is due to anharmonicity.

$\sigma_{\alpha\beta}$ . From the same simulation we also extract a *layer-resolved* stress profile  $\tau_{\alpha\beta}(z_l)$ , defined as the force per unit length acting in layer  $l$ :

$$\tau_{\alpha\beta}(z_l) = -\frac{1}{A} \left\langle \sum_{i \in l} \left( \frac{p_{\alpha i} p_{\beta i}}{m_i} + \frac{1}{2} \sum_j \frac{\partial U}{\partial r_{ij}} \frac{r_{ij, \alpha} r_{ij, \beta}}{r_{ij}} \right) \right\rangle,$$

where  $i$  runs over the atoms of layer  $l$ ,  $j$  spans all the atoms, and  $U$  is the potential energy, a function of the interatomic distances (this formula is easily modified for application to a bent slab<sup>14</sup>). The elastic bending work is done in our case by  $\tau_{yy}$ ,  $y \equiv [1\bar{1}0]$  being the strained direction, orthogonal to the solitons.

The bent slab stress profile obtained for  $L=6$ ,  $L'=\infty$  (at  $T=100$  K) is shown in Fig. 1. The smoothly varying bulk-like stress in the interior of the slab develops a sharp oscillation at the surface, swinging from compressive in the second layer to tensile in the first layer. As shown by a comparison of two different slabs with the same curvature but different thicknesses,  $N=16$  and 32, the surface stress of the thinner slab can be immediately computed by subtracting the corresponding bulklike stress of the thicker slab. The bulk stress  $\tau_{yy}^{(\text{bulk})}(z)$  deviates from linearity for increasing strain in a way that is very well described by a parabolic fit; the nonlinearity is due to anharmonicity. The layer-resolved surface stress is then obtained as  $\tau_{yy}^s(z_l) = \tau_{yy}(z_l) - \tau_{yy}^{(\text{bulk})}(z_l)$ . Repeating calculations for increasing curvature  $k$ , we obtain the curvature-dependent surface stress. This approach, we note, will give free-energy differences, fully inclusive of the entropic term. Finally the free-energy change as a function of strain is obtained by integrating<sup>14</sup>

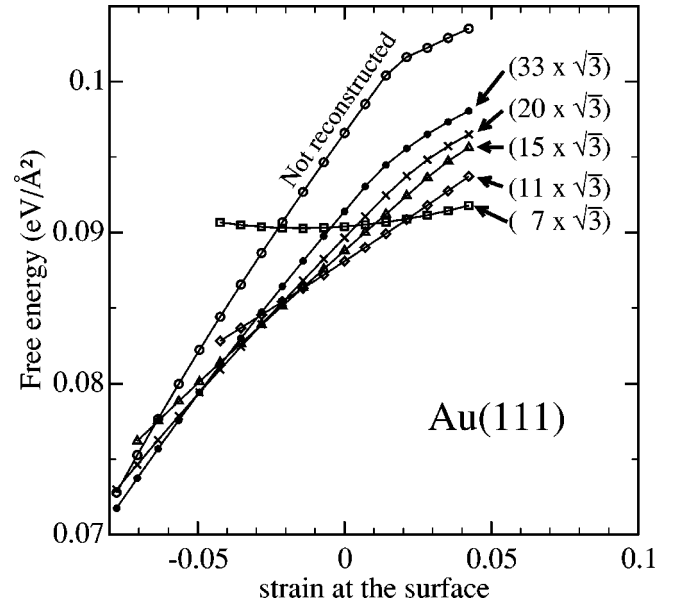


FIG. 2. Free energies at 100 K of various  $(L \times \sqrt{3})$  Au(111) surface reconstructions calculated as the strain is changed through bending. (The free energy values at zero strain are arbitrarily set at their independently obtained  $T=0$  values.) The predicted strain induced drift of  $L$  can be extracted from the lowest envelope of these curves.

$$W_s = \sum_{l \in \text{layers}} \int_0^k d\kappa \tau_{yy}^s(\kappa, z_l) \frac{d\varepsilon_{yy}(z_l)}{d\kappa}.$$

Likewise, the total surface stress can be obtained as  $\tau_{\alpha\beta}^{\text{surf}}(k) = \sum_{l \in \text{layers}} \tau_{\alpha\beta}^s(k, z_l)$ .

Figure 2 displays our main result: the strain-induced free energy variation of several different  $(L \times \sqrt{3})$  reconstructions of Au(111) at  $T=100$  K. The strain dependence found for free energy is relatively large, of order 2 meV/Å (about 1% of the total surface free energy) for 1% strain. By comparison with the absolute zero-temperature surface energy differences at zero strain, independently calculated (and used in Fig. 2 to fix the unknown relative position of curves, thus neglecting an entropy term, hopefully small at low temperatures) we find that 0.18 meV/Å is roughly the surface free energy difference between periodicities  $L$  and  $L+1$  for  $L$  around 20 in Au(111). By interpolating Fig. 2 we find that a change of periodicity from, say,  $L=23$  to 24 can in principle be provoked by a compressive surface strain of order 0.2%. More generally, strain will cause a periodicity drift determined by the lower envelope of all the curves: positive (tensile) strain decreasing  $L$ , negative (compressive) strain increasing it. Eventually for a theoretically very large strain  $L=\infty$  would be reached, where the reconstruction itself disappears. That strain, of order  $-2\%$  in Au(111) (see below), might however be too large to be achieved by bending.

Our predictions, based on free energies, find a first confirmation in a computer experiment, consisting of a realistic molecular-dynamics simulation, based on introducing a bending strain in the same slab geometry previously used for the surface stress calculation. If we start out with two iden-

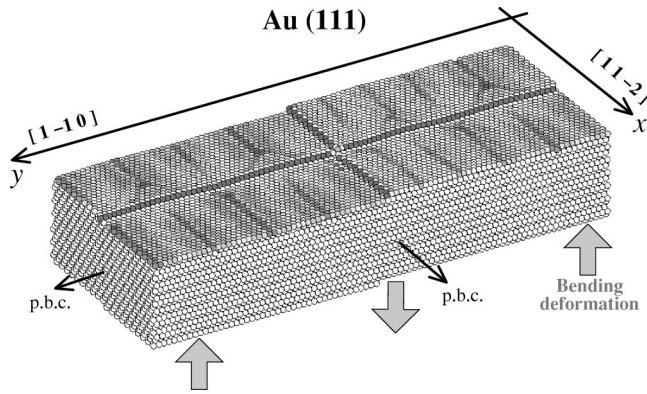


FIG. 3. The upper half of the simulation slab, with two orthogonal steps. Periodic boundary conditions require no extra steps at the boundaries. The grayscale reflects atomic coordination: atoms at the solitons between fcc and bcc regions appear darker.

tically reconstructed surfaces, bending strain should cause  $L$  to spontaneously increase on the concave face, and decrease on the convex one. However, the simulation must overcome a technical problem, connected with particle conservation. A change of the reconstruction periodicity  $L$  implies a change of the first-layer lateral surface density, equal to  $(1 + 1/L)$  times the density of an unreconstructed layer. The initially flat, defect-free reconstructed surface should, under bending, spontaneously expel atoms from the top layer to form islands on the concave face, while opening craters that expose a portion of the layer below on the convex face.<sup>15</sup> Such phenomena are slow, needing times much longer than the typical simulation nanosecond. Because of this, it would seem that the molecular-dynamics simulation should be abandoned. A

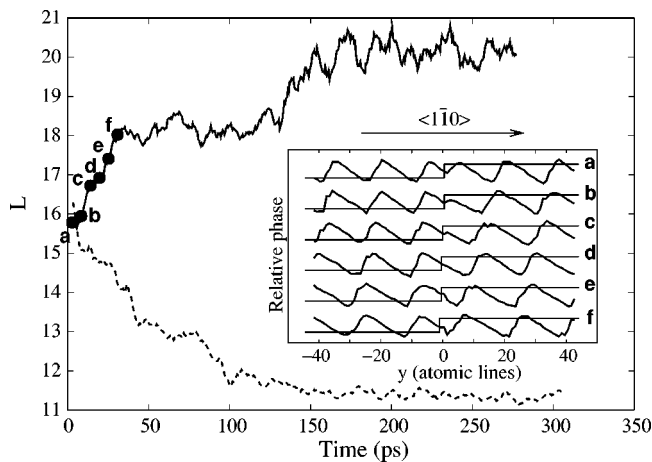


FIG. 4. Time evolution of the reconstruction periodicity, from a nonequilibrium starting point with  $L=16$ , toward equilibrium. Solid line: bent slab with a compressive surface strain of  $-4.7\%$ . Dashed line: flat slab with zero surface strain. Geometry as in Fig. 3,  $T=800$  K. Inset: details of the phase difference between the atoms of the first two layers, at selected instants of time during the bending. Note that the step, indicated schematically at each of the instants, has moved slightly to the left in correspondence with the increase of  $L$  (decrease of lateral density). The excess soliton is absorbed at the step upper rim between instants (a) and (c).

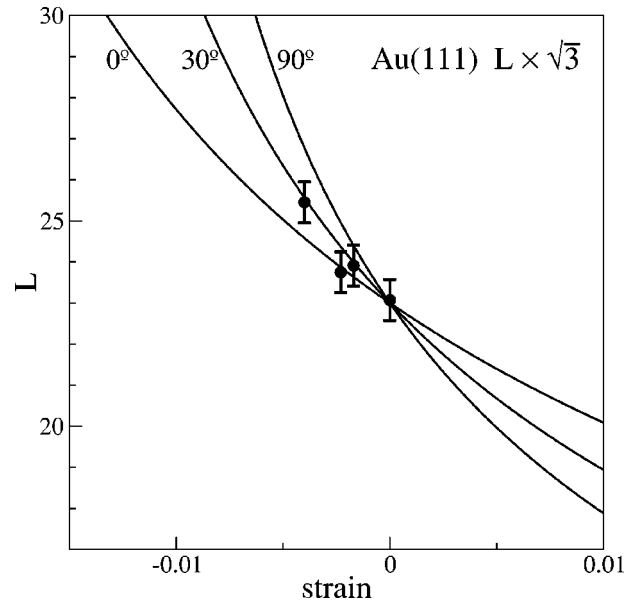


FIG. 5. Change of Au(111) reconstruction period  $L$  as a function of applied strain. Solid lines, are theoretical predictions, in the form  $L = K(\varepsilon - \varepsilon_d)^{-1/2}$ , for strains orthogonal ( $\theta=90^\circ$ ,  $K=2.84$ ,  $\varepsilon_d=-0.0153$ ), oblique ( $\theta=30^\circ$ ,  $K=3.34$ ,  $\varepsilon_d=-0.0210$ ), and parallel ( $\theta=0^\circ$ ,  $K=4.12$ ,  $\varepsilon_d=-0.0323$ ) to the  $[11\bar{2}]$  oriented solitons. These parameters best fit our simulation results, with a shift in strain, to make the  $L=23$  point correspond to strain  $\varepsilon=0$ . Data points were extracted from the STM images of Ref. 18, where the strain direction was  $\theta=30^\circ$ .

practical way out of this problem<sup>16</sup> is to include a loose grid of steps in the starting configuration, which amounts to simulating a very close vicinal face rather than the original  $(1\ 1\ 1)$  surface.

Our realization, shown in Fig. 3, comprises four subterraces of heights 0, 1, 1, and 2, separated by steps, and connected one with another across suitably shifted boundary conditions.<sup>16</sup> No other steps occur at the boundaries; hence the four subterraces constitute in reality a single large terrace. The terrace size used is  $88d \times 20\sqrt{3}d$ , with  $d$  the nearest-neighbor distance. With this geometry we can carry out various simulations, bending an initially flat surface and unbending an initially bent surface. In order to speed up kinetics, the temperature is raised well above room temperature, up to about  $T=600$  K.

Representative simulation results are illustrated in Fig. 4, where the continuous drift of reconstruction periodicity for a surface initially reconstructed with  $L$  around 16 is demonstrated for two different situations, a large compressive surface strain, and zero strain respectively, the former obtained through simulated bending. The periodicity drift from 16 to about 20 and from 16 to about 11 in the two cases is in good agreement with the free-energy prediction of Fig. 2. The inset details the behavior of the phase of the topmost atom layer lattice relative to the bulklike second layer (modulo  $2\pi$ ) as seen on the bent slab at selected instants of time. Data are averaged along the  $[11\bar{2}]$  direction to reduce the noise due to thermal excitation: averaging explains why the phase jumps around  $2\pi$  are replaced by a smooth behavior.

We find that the periodicity changes are actuated through the appearance (or disappearance) of solitons, nucleated preferentially at the upper rim of the surface step, where atoms possess the lowest coordination.

Experimentally, attempts by scanning tunneling microscopy (STM) to provoke and observe surface reconstruction modifications by bending, have been carried out recently, precisely on Au(111). Because the strains attained are small they were found to affect mostly the secondary structure. An early unpublished report by Huang *et al.*,<sup>17</sup> described strain-induced removal of the wrongly oriented domains of the secondary herringbone structure with strains as small as  $1.3 \times 10^{-5}$ , with occasional removal of the whole reconstruction. Newer data from Schaff *et al.*<sup>18</sup> showed that the secondary structure is again removed but the  $(L \times \sqrt{3})$  reconstruction survives at least up to a maximum compressive strain of 0.4%. By a closer examination of their data we note that, under strain, exerted at an angle of  $30^\circ$  with respect to the solitons, there is evidence of a drift of periodicity  $L$  from about 23 to about 25. We can directly compare this with our calculations. We find that the calculated  $L$ -dependent surface free energy for variable bending is well fitted by a Pokrovskii-Talapov form<sup>2</sup>  $\Delta E = -a/L + b/L^3$ , where  $a$  is the cost of solitons and  $b$  reflects their mutual interaction  $\propto 1/L^2$ . Here  $a(\varepsilon) = a'(\varepsilon - \varepsilon_c)$  will vanish at a critical strain  $\varepsilon_c$ , so that  $L = K(\varepsilon - \varepsilon_c)^{-1/2}$ , where  $K = \sqrt{3b/a'}$ . Based on our computed surface energies and anisotropic surface stress tensor, we derived  $K$  and  $\varepsilon_c$  for arbitrary strain direction, so as to compare the experimental drift with calculated periodicity changes (Fig. 5). The agreement obtained is very en-

couraging, fully supporting our qualitative expectations, and demonstrating the applicability of the proposed mechanism of surface modification under bending strain.

The strain-induced reconstruction changes described above can lead to potentially interesting consequences and applications. In a surface that is perturbed by a time-dependent strain, there will be as a consequence a sliding nanofriction of the incommensurate reconstructed top layer of Au(111) against the regular second layer. For example, an oscillatory bending would result according to Fig. 4 in a corresponding variation of  $L$ , driving an oscillatory sliding of the first layer onto the second. A pinned state of the top layer will imply a threshold strain magnitude to actuate the sliding. When the sliding occurs, a surface nanofrictional contribution should appear as a part of the mechanical damping of a Au(111) platelet. Among the applications, there could be the possibility to tune through bending strain the spacing between deposited nanoclusters. Recently, deposition of 1-nitronaphthalene nanoclusters on a stepped Au(111) surface has revealed<sup>19</sup> that, at low coverage, adsorption at the step is favored in the fcc zones of the  $(L \times \sqrt{3})$  reconstruction pattern and unfavored in the hcp zones; in this way, stripes can be produced. The distance among the stripes could in principle be changed upon bending, with interesting consequences in the field of miniature device fabrication.

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