# Nonlinear dynamics of vortices in easy flow channels along grain boundaries in superconductors

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A theory of nonlinear dynamics of mixed Abrikosov vortices with Josephson cores (AJ vortices) on lowangle grain boundaries (GB) in superconductors is proposed. As the misorientation angle  $\vartheta$  increases, vortices on low-angle GBs evolve from the Abrikosov vortices with normal cores to intermediate AJ vortices with Josephson cores, whose length l along GB is smaller that the London penetration depth  $\lambda$ , but larger than the coherence length  $\xi$ . Dynamics and pinning of the AJ vortex structures determine the in-field current transport through GB and the microwave response of polycrystal in the crucial misorientation range  $\vartheta < 20-30^\circ$  of the exponential drop of the local critical current density  $J_b(\vartheta)$  through GB. An exact solution for an overdamped periodic AJ vortex structure driven along GB by an arbitrary time-dependent transport current in a dc magnetic field  $H > H_{c1}$  is obtained. It is shown that the dynamics of the AJ vortex chain is parametrized by solutions of two coupled first-order nonlinear differential equations which describe self-consistently the time dependence of the vortex velocity and the AJ core length. Exact formulas for the dc flux flow resistivity  $R_{f}(H)$ , and the nonlinear voltage-current characteristics are obtained. Dynamics of the AJ vortex chain driven by superimposed ac and dc currents is considered, and general expressions for a linear complex resistivity  $R(\omega)$  and dissipation of the ac field are obtained. A flux flow resonance is shown to occur at large dc vortex velocities vfor which the imaginary part of  $R(\omega)$  has peaks at the "washboard" as frequency  $\omega_0 = 2\pi v/a$ , where a is the intervortex spacing. This resonance can cause peaks and portions with negative differential conductivity on the averaged dc voltage-current (V-I) characteristics. ac currents of large amplitude cause generation of higher voltage harmonics and phase locking effects which manifest themselves in steps on the averaged dc I-V curves at the Josephson voltages,  $n\hbar \omega/2e$  with  $n = 1.2, \ldots$ 

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### I. INTRODUCTION

Mechanisms of current transport through grain boundaries (GB) in high-temperature superconductors (HTS) have attracted much attention because they reveal the *d*-wave symmetry of the HTS pairing<sup>1</sup> and determine the currentcarrying capability of HTS materials.<sup>2</sup> Unlike low- $T_c$ superconductors, GBs in HTS exhibit weak-link behavior due to the exponential drop of the local critical current density of a GB,  $J_b = J_0 \exp(-\vartheta/\vartheta_0)$ , as the misorientation angle  $\vartheta$  between the neighboring crystallites increases above  $\vartheta_0$  $\simeq 5-6^{\circ}$ . The strong dependence of  $J_{h}(\vartheta)$  on  $\vartheta$  makes highangle GBs crucial current-limiting defects in HTS polycrystals.<sup>2</sup> Since pioneering experiments of the IBM group,<sup>3</sup> much progress has been made in understanding the multiscale microstructure of GBs and its effect on their weak-link behavior,4-7 but primarily in the absence of a strong magnetic field H. Detailed atomic structure of GBs revealed by high-resolution electron microscopy has been used to determine local underdoped states of GB, defectinduced suppression of superconducting properties at the nanoscale and controlled increase of  $J_b$  by overdoping of GB.<sup>8–11</sup> Recent models have also pointed out the importance of charging and strain effects which drive the HTS state at GB toward the metal-insulator transition as  $\vartheta$  increases.<sup>12,13</sup>

At the same time, little is known about vortices on lowangle GBs, although it is the dynamics and pinning of the GB vortices, which mostly limit critical currents of HTS polycrystal in a magnetic field,<sup>2</sup> and determine a microwave response of HTS films.<sup>14–18</sup> Generally, pinning of vortices along GBs is weaker than in the grains, so GBs form a natural percolating network for preferential motion of vortices through a superconductor.<sup>19–27</sup> Such percolating networks are not only characteristic of polycrystals, but represent a rather generic feature of vortex dynamics and pinning in superconductors. For instance, networks of easy flow vortex channels have been suggested by Kramer in early shear models of flux pinning<sup>28</sup> and later discovered in moleculardynamics simulation of vortices in random pinning potential,<sup>29,30</sup> numerical simulations of time-dependent Ginzburg-Landau equations that describe moving vortex structure near twin boundaries<sup>31</sup> and observed by decoration<sup>32</sup> and Lorentz microscopy.<sup>33</sup> Matching effects in dynamics and pinning of mesoscopic vortex flow channels in artificial thin film superconducting structures have been extensively studied by Kes and co-workers.<sup>34,35</sup> Many observable features of global current-voltage characteristics, magnetization, rf response, and flux creep of HTS polycrystal may be due to dynamics and pinning of vortices in easy-flow channels, rather than stronger pinned vortices in the grains.<sup>36–40</sup> By contrast, GBs in low- $T_c$  materials do not block macroscopic currents, but can enhance flux pinning<sup>41,42</sup> and play the role of "hidden" weak links that strongly affect the vortex mass and viscosity<sup>19</sup> crucial for transport and microwave response of superconductors,<sup>14,15</sup>

The behavior of vortices in easy flow channels on GBs in polycrystal is mostly determined by the structure of vortex cores which depends on the local depairing current density  $J_b$  through a GB at the nanoscale of few current channels between the dislocations. The extreme sensitivity of  $J_b(\vartheta)$  to the misorientation angle  $\vartheta$  makes GBs in HTS a unique tool to trace a fundamental transition between the Abrikosov (A)

and Josephson (J) vortices. As  $\vartheta$  increases,  $J_b(\vartheta)$  rapidly decreases, from the bulk depairing current density  $J_d$  at  $\vartheta$  $\ll \vartheta_0$  down to much lower values  $J_b \ll J_d$  at  $\vartheta \gg \vartheta_0$ . In turn, vortices on a GB evolve from the A vortices with normal cores at  $\vartheta \ll \vartheta_0$  to intermediate Abrikosov vortices with Josephson cores (AJ vortices)<sup>19</sup> and then to the J vortices at higher  $\vartheta$ . There is no order parameter suppression in the AJ core, which is a phase kink whose length l along GB is greater than the coherence length  $\xi$ , but shorter than the scale of circulating screening currents set by the London penetration depth  $\lambda$ . As  $\vartheta$  increases further, the AJ vortices turn into J vortices in which both the Josephson currents and the magnetic field H(x) vary on the same scale along GB set by the Josephson penetration depth  $\lambda_J$ .<sup>43,44</sup> This continuous *A* to AJ vortex transition occurs as the spacing between GB dislocation cores becomes shorter than  $\xi$ , giving rise to a suppression of the amplitude  $\Delta$  of the order parameter  $\Psi$  $=\Delta \exp(i\varphi)$  in current channels between dislocations.<sup>12</sup> Thus, a low-angle GB behaves as a high- $J_b$  superconductingnormal-superconducting (SNS) Josephson contact, for which the Josephson cores of the AJ vortices do not cause pair breaking effects responsible for the suppression of  $\Delta$  in the normal A cores. Such contacts are described by integral equations of a nonlocal Josephson electrodynamics (NJE),<sup>19,21,44-50</sup> which account for the variations of phase difference  $\theta(x) = \varphi_1 - \varphi_2$  along a GB on any length scale greater than  $\xi$ . If  $\theta(x)$  varies slowly on the scales  $\sim \lambda$ , the NJE equations reduce to the usual sine-Gordon equation for long Josephson junctions.<sup>44,43</sup> The key difference of the nonlocal approach from the local sine-Gordon theory is that the NJE equations can describe the AJ vortex core in the region of parameters where  $J_b > J_d \xi / \lambda$ , and  $\theta(x)$  varies on the scale  $l = \lambda_J^2 / \lambda \simeq \xi J_d / J_b$  much shorter than the decay length  $\lambda$  of the circulating supercurrents.

The importance of the Josephson nonlocality for thin films has been recognized long ago.<sup>44,45</sup> Because the penetration depth  $\tilde{\lambda} = 2\lambda^2/d$  increases as the film thickness d decreases, the nonlocality condition  $\lambda_I < \tilde{\lambda}$  can be fulfilled even for comparatively low- $J_b$  junctions. Independently, the NJE approach was developed for bulk superconductors to describe mixed AJ vortices on high- $J_b$  "hidden weak links," such as low-angle GBs in HTS and thin  $\alpha$ -Ti ribbons in NbTi<sup>19</sup>. A nonlocal generalization of the sine-Gordon equation was also considered in Ref. 46. It turns out that, in the strong nonlocality limit, the NJE equation reduces to the well-studied Peierls equation of dislocation theory, thus, the AJ single vortex solution<sup>19</sup> is similar to that for the core of an edge dislocation.<sup>51</sup> The NJE equations have other exact solutions<sup>19,46,51–53</sup> for static and dynamic AJ vortex structures. Recently, the existence of AJ vortices in low-angle YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7</sub> bicrystals was proven by transport measurements, using an exact expression for the flux flow resistivity of AJ vortices.<sup>53</sup> The good agreement between the theory and experiment made it possible to extract the core length l(T)and the intrinsic depairing current density  $J_b(\vartheta)$  of a GB on a nanoscale of few dislocation spacings. The temperature dependence of  $J_b \propto (T_c - T)^2$  extracted from these measurements does indicate the SNS coupling on GBs in HTS, in

agreement with the model of Ref. 12.

This paper presents a theory of a nonlinear flux flow of AJ vortices driven by dc and ac currents in a magnetic field. An exactly solvable model that describes a chain of AJ vortices moving along a GB through the strongly pinned A vortex lattice in the grains, is proposed. This model of the overdamped vortex dynamics describes self-consistently both nonlinear dissipative processes in the AJ vortex cores and magnetic interaction between AJ vortices, showing how the distributions of circulating superconducting and quasiparticle currents change as a function of the vortex velocity. The AJ vortices exhibit many characteristic features of the dynamics of the periodic A vortex lattice, for example, viscous flux flow,<sup>54</sup> static and dynamic matching effects, and Josephsonlike voltage oscillations.35,55,56 At the same time, the AJ vortices can also exhibit effects characteristic of the dynamics of short Josephson contacts in ac field, or J vortices in long Josephson junctions, for example, flux flow resonance,<sup>5</sup> phase locking in ac field,<sup>43,58</sup> etc. Pronounced resonance effects occur if the strongly overdamped AJ structure is driven by superimposed ac and dc currents  $J(t) = J_0 + J_a \cos \omega t$  at  $J_0 > J_b$ . It is shown that all this rich AJ vortex dynamics is described by two coupled first-order nonlinear ordinary differential equations for the vortex velocity and the core size, for any time dependent J(t). These equations have the form of a complex resistively-shunted junction (RSJ) equation for a short Josephson contact.

The paper is organized as follows. In Sec. II a qualitative description of length scales of vortices on a GB and their evolution with  $\vartheta$  is given. In Sec. III the NJE equations and an exact solution that describes a chain of AJ vortices driven by an arbitrary ac current in a dc magnetic field are presented. In Sec. IV, the nonlinear *V*-*J* characteristics and the flux flow resistivity of a GB in a magnetic field are calculated. In Sec. V a linear complex resistivity and rf dissipation are calculated for a chain of AJ vortices driven by superimposed ac and dc currents. A flux flow resonance is predicted. Section VI is devoted to nonlinear effects caused by superimposed ac and dc currents, in particular the averaged dc *V*-*J* characteristics in the presence of an ac signal, generation of higher harmonics and phase locking effects. Section VII concludes with a discussion of the obtained results.

### II. VORTEX LENGTH SCALES ON GRAIN BOUNDARIES IN A MAGNETIC FIELD

The results of this paper are independent of the detailed atomic structure of GB,<sup>3-5</sup> so we consider a simplest planar [001] tilt GB between two crystallites misoriented by the angle  $\vartheta$ . Such low-angle GB can be regarded as a periodic chain of edge dislocations spaced by  $d_0 = b/2 \sin(\vartheta/2)$ , where *b* is the Burgers vector.<sup>5</sup> Because of the proximity of the HTS state to the antiferromagnetic metal-insulator transition, regions of size  $\approx b$  near dislocation cores are driven into insulating state by local nonstoichiometry, strains, and charging effects.<sup>12</sup> As  $\vartheta$  increases, the spacing  $d_0(\vartheta)$  decreases, becoming smaller than the zero-*T* coherence length  $\xi_0$  and the in-plane Debye screening length at the angle  $\vartheta_0$  $\approx 4-6^\circ$ . For  $\vartheta > \vartheta_0$ , the proximity effect, strain and charge coupling cause suppression of  $\Delta$  between dislocation cores, which becomes more pronounced as  $\vartheta$  increases. In this model a GB thus behaves as a SNS Josephson contact, whose critical current density  $J_b(\vartheta)$  decreases nearly exponentially as  $\vartheta$  increases with  $J_b(\vartheta) \sim J_d$  at  $\vartheta < \vartheta_0$ .

A magnetic field H above the lower critical field  $H_{c1}$  produces A vortices in the grain, and vortices of different character on the GB, depending on the ratio  $\xi/d_0$ . For  $\theta \ll \theta_0$ , the GB vortices are A vortices with normal cores pinned by GB dislocations.<sup>22</sup> As  $\vartheta$  further increases, a GB exhibits a continuous transition from metallic to tunneling behavior above  $\vartheta > \vartheta_0$ , similar to high- $J_b$  SNS Josephson junction<sup>59</sup> for which the normal core of A vortices disappears if  $\Delta$  on the junction drops below a critical value.<sup>44</sup> For vortices on a GB, the normal core disappears quite naturally because of the exponential decrease of  $J_b(\vartheta)$ . Since vortex currents must cross the GB which can only sustain  $J_b$  much smaller than the depairing current density  $J_d$ , the modulus  $\Delta$  of the order parameter is unaffected by vortex cores. As a result, the normal A core turns into a Josephson core in which the phase difference  $\theta(x,t)$  on GB varies by  $2\pi$  over the length l along GB, but the amplitude  $\Delta$  is independent of x. The phase core length  $l \simeq \xi J_d / J_b$  is greater then  $\xi$ , but smaller then the London penetration depth  $\lambda$ , if  $J_b > J_d / \kappa$ , where  $\kappa = \lambda / \xi \simeq 10^2$  is the Ginzburg-Landau parameter.<sup>19</sup> As  $\vartheta$  increases, the core length  $l(\vartheta) \simeq \xi J_d / J_b(\vartheta)$  increases, so the GB vortices evolve from A vortices for  $\vartheta \ll \vartheta_0$  to mixed AJ vortices at  $J_d < J_b(\vartheta) < J_d/\kappa$ . The AJ vortices turn into J vortices at higher angles, for which *l* becomes greater than  $\lambda$  if

$$\vartheta > \vartheta_J \simeq \vartheta_0 \ln(\tilde{\lambda}/\xi),$$
 (1)

where  $\tilde{\lambda}$  is the magnetic screening length. In bulk samples  $\tilde{\lambda}$  is the London penetration depth  $\lambda$ , while a thin film of thickness  $d < \lambda$  the magnetic screening length is  $\tilde{\lambda} = 2\lambda^2/d$ . For bulk samples, Eq. (1) yields  $\theta_J \approx 23^\circ$  if  $\theta_0 = 5^\circ$ ,  $\kappa = 100$ , and  $J_0 = J_d$ . For a film with  $d \ll \lambda$ , the AJ region expands considerably, for example, if  $d = 0.1\lambda$ , then  $\vartheta_J \approx 38^\circ$ . Therefore, the AJ vortices exist in a rather wide range of misorientations,  $\vartheta_0 < \vartheta < \vartheta_J \approx 22-40^\circ$ , which comprises the crucial region of the exponential drop of  $J_b(\vartheta)$ . In this region the in-field current transport through GBs in HTS is determined by dynamics and pinning of AJ vortices.

Due to the lack of the order parameter suppression in the AJ cores, AJ vortices can be described by the NJE theory which regards the GB as a Josephson contact whose  $J_b(\vartheta)$  can be tuned in a very broad range by varying the misorientation angle  $\vartheta$ . Once the AJ core size  $l = \xi J_d / J_b$  exceeds the scales set by the coherence length, the Debye screening length and the dislocation spacing, the structure of AJ vortices is entirely determined by the electrodynamics of currents circulating around the cores, regardless of the atomic structure of GB, pairing mechanisms and the symmetry of the order parameter. The current distribution in the AJ vortex is described by the universal Josephson and London equations, while the GB imposes a boundary condition of current continuity for the sum of the Josephson, quasiparticle, and displacements current densities  $J = J_b \sin \theta(x,t) + V/R + C\dot{V}$ 

crossing the GB, where V is the voltage on a GB, R, and C are the quasiparticle resistance and capacitance per unit area of a GB, respectively.

The structure of a vortex on a GB is determined by the ratio  $\kappa_b = \tilde{\lambda}/l$  reminiscent of the GL parameter  $\kappa = \lambda/\xi$  for the A vortices. Here  $\kappa_b = (\lambda/\lambda_J)^2 \simeq \kappa J_b/J_d$  for a bulk sample,  $\kappa_b = d\lambda^3 / \lambda_I^2 d$  for a film of thickness  $d < \lambda$ . The case  $\kappa_b \ll 1$  corresponds to the local relation  $H(x) = \phi_0 \partial_x \theta / 4\pi \lambda$ characteristic of low- $J_b$  high-angle GB, for which both  $\theta(x)$ and H(x) vary on the same spatial scale. Such GBs exhibit the J vortices of length  $\lambda_J$  described by the sine-Gordon equation.43 However, the low-angle GB (especially in thin films) correspond to  $\kappa_b > 1$  in which case the relation between  $\theta(x)$  and H(x) is nonlocal, and  $\theta(x)$  and H(x) vary on essentially different spatial scales  $l = \xi J_d / J_b$  and  $\lambda$ , respectively. This gives rise to the mixed AJ vortices described by integral NJE equations<sup>19,21,44–46,49,47,48,50</sup> which reduce to the sine-Gordon equation if  $\theta(x)$  varies weakly on the scales  $\sim \lambda$ . The NJE equations provide a universal description of vortex structures on GB for which all microscopic details are hidden in the intrinsic parameters  $J_h$  and R of a GB. These parameters are very difficult to calculate, given the present state of the microscopic theory of HTS, but they can be extracted from resistive measurements on HTS bicrystrals with the help of exact NJE solutions that describe the flux flow resistance of moving AJ vortices.<sup>53</sup>

In a strong magnetic field  $H \ge H_{c1}$ , the *A* vortex spacing  $a = (\phi_0/H)^{1/2}$  is shorter than  $\lambda$ , thus the relation between  $\theta(x,t)$  and H(x,y) is always nonlocal, regardless of the value of  $J_b$ . The AJ vortex chain is then has two length scales: the core size  $l > \xi$  and the inter vortex spacing a(H). Both lengths *a* and *l* become comparable at a characteristic field  $H_0 \sim \phi_0/l^2 \sim (J_b/J_d)^2 H_{c2}$  much smaller then the upper critical field  $H_{c2}$ . Thus, unlike the *A* lattices, there is a wide field region  $H_0 < H < H_{c2}$  in which the AJ vortex cores overlap, but the bulk superconductivity persists.

The larger core of AJ vortices leads to their weaker pinning along a GB, which thus becomes a channel for motion of AJ vortices between pinned A vortices in the grains<sup>19</sup> (Fig. 1). This gives rise to an extended linear region in the V-Icharacteristic of a polycrystalline HTS that is dominated by motion of AJ vortices along GBs.<sup>10,22-27</sup> Pinning of AJ vortices results from interaction of the AJ phase core with structural inhomogeneities of GB and the magnetic interaction of AJ vortices with more strongly pinned A vortices in the grains. If the periods of the AJ vortices and bulk A vortices are slightly different, the AJ vortex chain breaks into commensurate domains (in which A and AJ periods coincide) separated by domain walls. This behavior, characteristic of commensurate-incommensurate transitions,60,61 was observed in molecular-dynamics simulations of A vortices in artificial flux flow channels<sup>35</sup> for which the width of the domain walls (dislocations) considerably exceeds the intervortex spacing. In this case the pinning of domain walls by the intrinsic Peierls potential is exponentially weak, so the depinning critical current  $I_{gh}(H)$  is most likely due to macroscopic variations of superconducting properties along GB, for example, facet structures that cause significant peaks in



FIG. 1. Current streamlines around AJ vortices on a GB (dashed line) and the bulk A vortices in the grains, calculated from Eq. (18) for l=0.2a.

 $I_{gb}(H)$  if the A vortex spacing is commensurate with the facet period,<sup>62</sup> strains and local nonstoichiometry along GB,<sup>2</sup> etc.

At low field, only a single AJ vortex row moves along GB, while the A vortices in the grains remain pinned.<sup>21</sup> At higher field the moving AJ vortices start dragging neighboring rows of A vortices in a flux flow channel along GB. The field  $H_1$  below which only a single AJ vortex row moves along the GB, can be estimated from the condition that the pinning force  $f_m$  of AJ vortices due to their magnetic interaction with fixed A vortices equals the intergrain pinning force  $\phi_0 J_c/c$ . The pinning force of AJ vortices is the maximum gradient of the magnetic energy f(x) $= -\phi_0 \partial_x H(x)/4\pi$ , where  $H(x) = B + \Delta H \cos(2\pi x/a)$  is the local field produced by the fixed A vortex lattice along GB,  $\Delta H = \phi_0 e^{-2\pi u/a} / \pi \lambda^2$  is the amplitude of the oscillating part of the local field H(x) due to the periodicity of the A lattice, and  $u \sim a$  is the spacing of the first A vortex row from GB.<sup>63</sup> Therefore,

$$H_1 \simeq \left[\frac{2\pi\lambda^2 J_c}{c\sqrt{\phi_0}}\right]^2 \exp\left(\frac{4\pi u}{a}\right). \tag{2}$$

For u=a,  $\lambda = 2000$  Å, and  $J_c = 10^5 - 10^6$  A/cm<sup>2</sup>, Eq. (2) yields  $H_1 \approx 0.1 - 10$  T. Note that the essential dependence of the transition field  $H_1$  on the bulk  $J_c$  indicates that the region  $0 < H < H_1$  can be significantly widened by irradiation which increases  $J_c$  while weakly affecting GB properties.<sup>53</sup> In addition,  $H_1$  is very sensitive to the position u of the first vortex row that can be strongly affected by the GB microstructure, facets, long-range  $T_c$  variations due to strains, etc.

In this paper we neglect the pinning of vortices on a GB, assuming that the driving current J(t) is higher than the de-

pinning current of the AJ vortices, but lower than  $J_c$  of the A vortices in the grains. This behavior has been observed on HTS bicrystals in a wide region  $H \le H_1$  of magnetic fields.<sup>10,22–27,53</sup> Under the ac current, pinning effects in electromagnetic response weaken even more as the ac frequency  $\omega$  exceeds a characteristic depinning frequency.<sup>64,65</sup> Furthermore, low-angle GBs can be regarded as overdamped Josephson contacts for which the displacements currents can be neglected. Indeed, the overdamped state corresponds to  $\omega$  $\ll \omega_c = (CR)^{-1} \sim 4\pi/\delta\rho \delta\epsilon$ , where  $\delta\rho$  and  $\delta\epsilon$  are the excess resistivity and dielectric susceptibility on GB. Because for low-angle GB the dielectric dislocation cores do not overlap,  $\delta \rho \sim \rho_n$ , and  $\delta \epsilon \sim 1$ , where  $\rho_n$  is the normal state resistivity at  $T_c$ . Thus, the condition  $\omega \ll \omega_c$  always holds for  $\omega$  smaller than the superconducting gap (see also Refs. 16,17). We also neglect the time dispersion of the the GB resistance R and contribution of bulk quasiparticles, adopting the simplest, frequency independent R in the framework of a standard RSJ model.43

#### **III. GENERAL DYNAMIC EQUATIONS**

The NJE equations for current-driven vortex structures on an overdamped Josephson contact are<sup>19–21</sup>

$$H = \frac{\phi_0}{(2\pi\lambda)^2} \int_{-\infty}^{\infty} \theta'(u) K_0 \left[ \frac{\sqrt{y^2 + (x-u)^2}}{\lambda} \right] du + B_v, \quad (3)$$

$$\tau \dot{\theta} = \frac{l}{\pi} \int_{-\infty}^{\infty} \theta''(u) K_0 \left( \frac{x - u}{\lambda} \right) du - \sin \theta + \beta, \qquad (4)$$

$$l = c \phi_0 / 16 \pi^2 \lambda^2 J_b, \quad \tau = \phi_0 / 2 \pi c R J_b.$$
 (5)

Here the overdot and the prime denote differentiation with respect to time and the coordinate x along GB,  $\beta(x,t) = J(x,t)/J_b$ ,  $\mathbf{J} = (c/4\pi) \nabla \times \mathbf{B}_v$  is the current density across GB induced by bulk vortices,

$$B_{v}(x,y) = \frac{\phi_{0}}{2\pi\lambda^{2}} \sum_{n} K_{0} \left[ \frac{|\mathbf{r} - \mathbf{r_{n}}|}{\lambda} \right], \tag{6}$$

where  $\mathbf{r_n}$  is the position of the *n*th A vortex,  $K_0(x)$  is a modified Bessel function,  $\phi_0$  is the flux quantum, and c is the speed of light. The first term in the right-hand side of Eq. (3) describes the magnetic field produced by all currents circulating near GB, and the second term represents the contribution of bulk vortices without GB. To provide the boundary condition for  $\mathbf{J}(x,y)$  on a GB, the phase difference  $\theta(x,t)$ must satisfy Eq. (4), which results from the current continuity condition,  $cH'/4\pi = J_b \sin \theta + \hbar \dot{\theta}/2eR$ . Equations (3) and (4) describe spatial variation of  $\theta(x,t)$  and H(x,y,t) on any scale greater than  $\xi$ , irrespective of the microscopic mechanisms of current transport through the GB. The only assumption  $J_h \ll J_d$  behind Eqs. (3) and (4) ensures the lack of the order parameter suppression by currents flowing through GB. The geometry of the sample manifests itself in the longrange asymptotics of the kernel in Eq. (4) at  $|\mathbf{r}-\mathbf{r}'| > \lambda$ . For instance, Eqs. (3) and (4) correspond to an infinite GB in a parallel field. More complicated expressions for the kernel  $\tilde{K}[(x-u)/\tilde{\lambda}]$  have been obtained for thin films in a perpendicular field, <sup>45,47,48</sup> and slabs in parallel<sup>49</sup> and perpendicular<sup>50</sup> fields.

In the vicinity of the AJ cores,  $r \ll \lambda$ , and also in the highfield limit,  $H \gg H_{c1}$ , Eq. (4) acquires a simple universal form independent of the sample geometry. This universality results from the fact that for  $H \gg H_{c1}$ , the derivative  $\theta''(u)$  in Eq. (4) rapidly oscillates over the intervortex spacing  $(\phi_0/H)^{1/2}$  $\ll \lambda$ . In this case the main contribution to the integral comes from the region  $|x-u| < \lambda$ , where the Bessel function  $K_0(x)$ in Eq. (4) can be replaced by its expansion  $K_0(x) \simeq -\ln(x)$  at small *x*. Thus, the equation for  $\theta$  becomes

$$\tau \dot{\theta} = \frac{l}{\pi} \int_{-\infty}^{\infty} \frac{\theta'(u)du}{u-x} - \sin\theta + \beta, \tag{7}$$

For other geometries,  $K_0[(x-u)/\lambda]$  in Eq. (4) should be replaced with the appropriate kernel  $\tilde{K}[(x-u)/\tilde{\lambda}]$  which always has a logarithmic singularity at x=u, and a geometrydependent nonsingular part,  $\tilde{K}_{reg}(x,u)$ ,

$$\widetilde{K}(|x-u|/\widetilde{\lambda}) = -\ln|(x-u)/\widetilde{\lambda}| + \widetilde{K}_{reg}[(x-u)/\widetilde{\lambda}].$$
(8)

This general behavior of  $\tilde{K}[(x-u)/\tilde{\lambda}]$  is illustrated in Appendix A where  $\tilde{K}[(x-u)/\tilde{\lambda}]$  for a thin film  $(d \ll \lambda)$ , is considered. Because of the rapid oscillations of  $\theta''(u)$  at H  $\gg H_{c1}$ , the main contribution to the integral in Eq. (4) comes from the narrow region around u=x, so neither  $\tilde{K}_{reg}[(x + x)]$  $(-u)/\tilde{\lambda}$ , nor the screening length  $\tilde{\lambda}$  contribute to Eq. (7). This feature of Eq. (7) reflects the physical fact that the distribution of currents near the AJ cores is unaffected by the London screening. Indeed, the Green function  $\tilde{K}[(x-u)/\tilde{\lambda}]$ is proportional to the single-vortex London solution H(r), so the difference between  $\tilde{K}[(x-u)/\tilde{\lambda}]$  for bulk samples and thin films is basically the same as between H(r) for the A vortex and the Pearl vortex,<sup>66</sup> respectively. Both vortices have the same distributions of currents J(r) near the core,  $r < \lambda$ , but very different asymptotics of J(r) for  $r > \lambda$ . Thus, the universal Eq. (7) describes the distributions of the phase difference  $\theta(x)$  in the AJ vortex cores and circulating supercurrents on the scales  $< \tilde{\lambda}$  away from the cores where the London screening is inessential.

The driving parameter  $\beta = \beta_0 + \delta\beta(x)$  is a sum of the constant transport current  $\beta_0$  due to the gradient of the *A* vortex density in the grains, and an oscillating component  $\delta\beta(x)$  due to the discreteness of the *A* vortex lattice. The term  $\delta\beta(x)$  gives rise to a critical current  $\beta_c$  through GB due to pinning of AJ vortices by *A* vortices in the grains.<sup>21</sup> In this paper we consider a rapidly moving AJ structure in the flux flow state,  $\beta \ge \beta_c$ , for which the pinning term  $\delta\beta(x) \ll 1$  can be neglected, and  $\beta(x)$  be replaced by  $\beta_0(t)$ . As shown in Appendix B, the nonlinear Eq. (7) then has the following *exact* solution that describes a stable periodic vortex structure:

where  $\gamma(t)$ , M(t), and the vortex velocity  $v(t) = \dot{x}_0$  depend only on t and obey the following equations:

$$\tau \dot{\alpha} + \sinh \alpha \cos \gamma = \sqrt{h},$$
 (10)

$$\tau \dot{\gamma} + \sin \gamma \cosh \alpha = \beta_0(t),$$
 (11)

$$k\tau v = -\sin\gamma\sinh\alpha. \tag{12}$$

Here  $h = (kl)^2$  is the dimensionless magnetic field, the wave vector  $k = 2\pi/a$  defines the period *a* of the AJ structure, and

$$\sinh \alpha = 2M/(M^2 - 1).$$
 (13)

Using the complex variables  $z = \gamma + i\alpha$  and  $f = \beta_0 + i\sqrt{h}$ , Eqs. (10)–(12) can be written in a more compact form

$$\dot{\tau z} + \sin z = f, \quad k \tau v = \operatorname{Im} \cos z.$$
 (14)

The equation for the complex "phase" z(t) has the same form as the usual RSJ equation for the phase difference on an overdamped point contact.

Equations (9)-(12) were obtained in Appendix B by the Hilbert transform, which was used to obtain static periodic solutions of the Peierls equation (7) in the dislocation theory,<sup>51</sup> and then employed to describe AJ structures.<sup>52</sup> It is instructive to derive Eqs. (9)-(12) using a more transparent approach, starting from the basic London equation

$$H - \lambda^2 \nabla^2 H = \phi_0 \theta(x) \,\delta(y) / 2\pi, \tag{15}$$

where  $\theta(x)$  is determined by a particular vortex structure on a GB. Since screening does not affect the AJ cores and current distribution on the scales  $<\lambda$  away from GB, Eq. (15) reduces to the Laplace equation  $\nabla^2 H=0$  supplemented by the boundary condition for the tangential and normal components of the current density on GB.

$$\partial_{y}H(x,+0) - \partial_{y}H(x,-0) = -\phi_{0}\theta'(x)/(2\pi\lambda^{2}), \quad (16)$$

$$J_{y}(x,\pm 0) = -\frac{c}{4\pi}H'(x,\pm 0) = J_{b}\sin\theta + \frac{\phi_{0}\dot{\theta}}{2\pi cR} - J. \quad (17)$$

If screening is inessential, H(x,y) becomes a potential field, which in some cases can be found directly using the theory of analytic functions. For instance, H(x,y) from a periodic AJ vortex structure in the *upper* half-plane y > 0, is given by the following ansatz:

$$H = \frac{\phi_0}{2\pi\lambda^2} \operatorname{Re}\ln\sin\{x - x_0(t) + i[|y| + y_0(t)]\}\frac{k}{2}, \quad (18)$$

which describes the field produced by a chain of fictitious *A* vortices displaced by  $y = -y_0$  away from GB in the *lower* half-plane (we omit a constant term in H(x,y), inessential for  $|y| < \lambda$ ). Equation (18) is an exact solution of the Laplace equation  $\nabla^2 H = 0$ . It turns out that  $y_0(t)$  can be chosen such that H(x,y) also satisfies the boundary conditions (16) and (17) provided that  $\theta(x,t)$  is given by Eq. (9) while  $\gamma$ ,  $\alpha$ , and  $x_0(t)$  obey Eqs. (10)–(12). To show that we first observe that

$$\partial_x H = \frac{k\phi_0}{4\pi\lambda^2} \frac{\sin\zeta}{\left[\cosh k(y-y_0) - \cos\zeta\right]},\tag{19}$$

$$\partial_{y}H = -\frac{k\phi_{0}}{4\pi\lambda^{2}}\frac{\operatorname{sign}(y)\operatorname{sinh}\alpha}{[\cosh k(y-y_{0}) - \cos\zeta]},\qquad(20)$$

where  $\zeta = [x - x_0(t)]k$ . In turn, Eqs. (9) and (13) yield

$$\theta' = \frac{k \sinh \alpha}{\cosh \alpha - \cos \zeta},\tag{21}$$

$$\dot{\theta} = \dot{\gamma} - \frac{\alpha \sin \zeta + kx_0 \sinh \alpha}{\cosh \alpha - \cos \zeta}, \qquad (22)$$

$$\sin \theta = \frac{(1 - \cosh \alpha \cos \zeta) \sin \gamma - \sinh \alpha \sin \zeta \cos \gamma}{(\cosh \alpha - \cos \zeta)}.$$
(23)

Now  $y_0$  can be chosen such that the denominators of Eqs. (19)–(23) would coincide at y=0,

$$ky_0 = \alpha = \ln[(M+1)/(M-1)].$$
(24)

Equations (20) and (21) with  $ky_0 = \alpha$  automatically satisfy the first boundary condition (16). Furthermore, substituting Eqs. (19)–(24) into the second boundary condition (17) reduces the latter to the form:  $C_1(t)\cos k\zeta + C_2(t)\sin k\zeta + C_3(t)$ =0. The self-consistency conditions  $C_i(t) = 0$  are satisfied only if  $\theta(t)$ ,  $\alpha(t)$ , and  $x_0(t)$  do obey the dynamic equations (10)–(12).

Figure 1 shows the current streamlines calculated from Eq. (18), which has a clear interpretation similar to that of a single AJ vortex.<sup>19</sup> Namely, the current streamlines described by Eq. (18) in the upper half-plane y > 0 coincide with those produced by a chain of moving fictitious A vortices displaced by  $y = -\alpha(t)/k$  away from GB. Likewise, the current streamlines in the lower half-plane y < 0 coincide with those produced by a chain of fictitious A vortices displaced by y  $= \alpha(t)/k$  away from GB. The resulting nonsingular field distribution H(x,y) is an exact solution for moving AJ vortices, where the transverse displacement  $y_0$  determines the AJ core size along GB. The time-dependent Cartesian coordinates  $x_0(t)$  and  $y_0(t) = \alpha(t)/k$  of these fictitious A chains obey Eqs. (10)–(12). The transition from AJ to A vortices occurs as  $J_b$  increases, reaching  $J_b \simeq J_d$ , while  $y_0$  decreases down to  $y_0 \simeq \xi$ . Likewise, the transition from AJ to J vortices occurs as  $J_b$  decreases below  $J_d/\kappa$ , in which case  $y_0$  becomes greater than  $\lambda$ .

The set of coupled ordinary differential equations (10)-(12) describe the evolution of the AJ phase core length, the phase shift  $\gamma(t)$ , and the vortex velocity  $\dot{x}_0(t)$  for any time-dependent transport current  $\beta_0(t)$ . These equations along with Eqs. (9) and (18) determine distributions of the phase difference  $\theta(x,t)$  and screening currents for an interacting moving AJ vortex chain, including nonlinear dissipative dynamic states caused by ac and dc driving currents of large amplitude,  $J(t) \sim J_b$ . Equations (10)–(12) considerably sim-

plify in the low-field limit,  $a \rightarrow \infty$  for which Eq. (9) reduces to a superposition of independent single AJ vortex solutions<sup>19</sup>

$$\theta(x,t) = \gamma(t) + \sum_{n} \left[ \pi + 2 \tan^{-1} \frac{x - na - x_0(t)}{L(t)} \right].$$
 (25)

Here  $k = 2\pi/a \rightarrow 0$ ,  $\alpha \rightarrow 2/M \rightarrow 0$ , so the AJ core length  $L(t) = \alpha/k$  is independent of the magnetic field, while  $\alpha = Lk \rightarrow 0$ . If  $\alpha \rightarrow 0$ , Eqs. (10)–(12) turn into the following equations that describe a single AJ vortex<sup>20</sup>

$$\tau \dot{\gamma} + \sin \gamma = \beta_0, \qquad (26)$$

$$\tau \dot{L} + L \cos \gamma = l, \qquad (27)$$

$$\tau \dot{x}_0 = -L \sin \gamma. \tag{28}$$

Unlike Eqs. (10)–(12), the equation for  $\gamma$  is *decoupled*, from Eqs. (27) and (28). Thus, in the limit  $a \ge L$ , the dynamics of the core length L(t) and the vortex velocity  $\dot{x}_0$  is integrable for any given  $\gamma(t)$ , which in turn is determined by Eq. (26) for any time–dependent  $\beta_0(t)$ . This result is no longer valid if the interaction between AJ vortices at a finite H is taken into account, when both  $\gamma(t)$  and  $\alpha(t)$  are determined self-consistently by Eqs. (10)–(12).

Contribution of each AJ vortex to the "staircase" solution (25) gives a  $2\pi$  phase shift along GB, thus the AJ vortex carries exactly one flux quantum  $\phi_0$ .<sup>21</sup> Generally, the intervortex spacing a(H) on GB is different from the period  $(\phi_0/H)^{1/2}$  of the bulk *A* lattice, because of the reduced  $H_{c1}$  on a GB.<sup>19</sup> In the low-field region,  $H \sim H_{c1}$ , the magnetic induction *B* is very different from *H*, which causes a significant mismatch in the periods of AJ and bulk *A* vortex lattices. However, for strong fields  $H \gg H_{c1}$  considered in this paper, the difference between *B* and *H* is negligible, so the AJ spacing a(H) nearly coincides with the bulk one,  $(\phi_0/H)^{1/2}$  as both are fixed by the same flux quantization condition.

The averaged voltage V on a GB produced by the moving AJ vortex structure is given by

$$V = \frac{\phi_0}{2\pi ca} \int_0^a \dot{\theta} dx.$$
 (29)

Substituting Eq. (22) into Eq. (29), we see that the term proportional to  $\dot{\alpha}$  vanishes after integration, while the part of  $\dot{\theta}(x-x_0)$  proportional to  $\dot{x}_0$  reduces to the full derivative  $-\dot{x}_0\theta'$ . Integration of  $\theta'$  from 0 to *a* gives  $2\pi$  due to the flux quantization condition,  ${}^{21}\theta(x+a) - \theta(x) = 2\pi$ , thus

$$V = \frac{\phi_0}{2\pi c} (\dot{\gamma} - kv). \tag{30}$$

Here the first term in the parentheses describes the quasiparticle component of V, and the second term results from vortex motion. Equation (30), along with Eqs. (10)-(12), determine the nonlinear electromagnetic response of the moving AJ vortex chain. These equations can be presented in different forms, depending on the way the external drive is applied. For example, the solutions of Eqs. (10)-(12) determine the voltage (30) for any time-dependent current J(t).

Another regime corresponds to the rf response, when it is the voltage V(t) [rather than the current density J(t)] on a GB which is fixed by an external rf source. In this case it is convenient to express the vortex velocity via V from Eq. (30) and subtract Eq. (11) from Eq. (32). Then the equations for  $\alpha(t)$ ,  $\gamma(t)$  and  $\beta(t)$  in the fixed voltage mode take the form

$$\tau \dot{\alpha} + \sinh \alpha \cos \gamma = \sqrt{h},$$
 (31)

$$\tau \dot{\gamma} + \sin \gamma \sinh \alpha = u,$$
 (32)

$$\beta = u + e^{-\alpha} \sin \gamma, \tag{33}$$

where  $u = V/RJ_h$  is the dimensionless voltage on a GB.

### IV. NONLINEAR STEADY-STATE FLUX FLOW

The steady-state velocity v of the AJ vortex chain driven by the constant current  $\beta_0$  is described by Eq. (9) and Eqs. (10)–(12) with  $\dot{\alpha} = \dot{\gamma} = 0$ , whence  $\tanh \alpha = -s\sqrt{h}/\beta_0$ ,  $\tan \gamma$ = -s, and  $s\sqrt{h} = -\sin\gamma\sinh\alpha$ . These equations give the dimensionless propagation velocity  $s(\beta_0) = v/v_0$  in the form

$$s^{2} = \left[\sqrt{(1-\beta_{0}^{2}+h)^{2}+4\beta_{0}^{2}h}-1-h+\beta_{0}^{2}\right]/2h.$$
 (34)

Here  $v_0 = l/\tau$ ,  $h = (2\pi l/a)^2$  is a dimensionless magnetic field. The limit  $h \rightarrow 0$  corresponds to a single AJ vortex, for which both Eq. (34) and the steady-state Eqs. (26)-(28)  $(L \cos \gamma = l, \sin \gamma = \beta_0, \text{ and } \tau v = -L \cos \gamma), \text{ give } v$  $=v_0\beta_0/\sqrt{1-\beta_0^2}$ . The so-obtained single vortex velocity v(J) diverges at  $J \rightarrow J_b$ , because the AJ core size L  $= l/\sqrt{1-\beta_0^2}$  expands as  $\beta_0$  increases.<sup>19</sup> The core expansion as the velocity v(J) increases is characteristic of both AJ (Ref. 19) and J (Ref. 44) vortices in the overdamped limit, unlike the Lorentz contraction of J vortices in the underdamped limit. However, as the AJ cores expand, they start overlapping, so the interaction between vortices at  $J > J_h$ cannot be neglected even at low fields,  $h \ll 1$ . The importance of the interaction is apparent form the exact Eq. (34), which shows that the velocity  $s(\beta_0)$  smoothly increases as  $\beta_0$  increases and has no singularity for any nonzero h.

The dc V-J characteristic due to viscous motion of AJ vortices follows from Eq. (30) in which  $\dot{\gamma}=0$ , and v(J) is given by Eq. (34). Hence

$$V = \frac{V_0}{\sqrt{2}} \left[ \sqrt{(1 - \beta_0^2 + h)^2 + 4\beta_0^2 h} - 1 - h + \beta_0^2 \right]^{1/2}, \quad (35)$$

where  $V_0 = RJ_b$ . Equation (35) can also be written in a more transparent form

$$J = \frac{V}{R} \left[ 1 + \frac{1}{H/H_0 + (V/V_0)^2} \right]^{1/2}.$$
 (36)

The V-J curve shown in Fig. 2 has two linear portions: a flux



FIG. 2. The *V-J* curves calculated from Eq. (35) for different magnetic fields  $h=H/H_0$ : 0.01(1), 0.05(2), 0.1(3), 0.5(4), 10(5). Inset shows the field dependence of the flux flow resistance  $R_f(B)$  given by Eq. (37).

flow part,  $V = R_f J$  at  $J \ll J_b$ , and the quasiparticle Ohmic part, V = RJ for  $J \gg J_b$ . In the crossover region,  $J \sim J_b$ , the V-J curve becomes nonlinear, because of the AJ core expansion as J increases. Since the AJ vortex core overlap at J $> J_b$ , the GB resistance approaches its maximum value R at  $J \gg J_b$ .

For  $J \ll J_b$ , Eq. (36) yields  $V = R_f J$ , where  $R_f = R\sqrt{h/(1+h)}$  is the flux flow resistivity of AJ vortices. If  $H \gg H_{c1}$ , then  $h = (2 \pi l/a)^2 = H/H_0$ , and

$$R_f = \frac{R\sqrt{H}}{\sqrt{H+H_0}}, \quad H_0 = \frac{\phi_0}{(2\pi l)^2}.$$
 (37)

At  $H \ll H_0$ , Eq. (37) describes a chain of AJ vortices whose cores do not overlap. In this case  $R_f(H)$  is similar to the one-dimensional (1D) Bardeen-Stephen formula,<sup>54</sup>  $R_{BS}$  $\approx R \sqrt{H/H_{c2}}$ , except that in Eq. (37) the core structure is taken into account exactly (see also Ref. 19). For  $H > H_0$  $\approx (J_b/J_d)^2 H_{c2} \ll H_{c2}$ , the AJ cores overlap, and Eq. (37) describes a crossover to a field-independent resistance *R*. This regime has no analogs for *A* vortices, whose normal overlap only at  $H_{c2}$ .

It is interesting to compare Eq. (37) to  $R_f(H)$  for *J* vortices at  $J \ll J_b$ . It is known<sup>67</sup> that for small density of *J* vortices,  $R_f(B) = RB/H_{c1J}$  is proportional to *B*, similar to the Bardeen-Stephen resistivity in which  $H_{c2}$  is replaced by the Josephson lower critical field  $H_{c1J} = \phi_0/\pi^2 \lambda \lambda_J$ . A general expression for  $R_f(H)$  can be written in the following form (see Appendix C):

$$R_f(H) = RB(H)/H. \tag{38}$$

Here B(H) is determined by the equilibrium magnetization the J vortex structure,<sup>68</sup>

$$B = \pi^2 H_{c1J}/4p K(p), \quad H = H_{c1J} E(p)/p,$$
 (39)

where K(p) and E(p) are the complete elliptic integrals of the first and the second kinds, respectively,<sup>69</sup> and 0 isa continuous parameter. As follows from Eqs. (38) and (39), $<math>R_f$  first increases linearly with B at  $B \ll H_{c1J}$  and then ap-

proaches the constant value R at  $H \ge H_{c1J}$  as the J vortices overlap, and  $B \rightarrow H$ . By contrast, the saturation of  $R_f(H)$  for the AJ vortices occurs at much higher fields  $\sim H_0 \gg H_{c1}$  for which the AJ vortex spacing  $a = (\phi_0/B)^{1/2}$  becomes of order the AJ core size l. The dependence of  $R_f(H)$  for J vortices looks rather different from the simple Eq. (37) mostly because of the complicated relation (39) between B and H at low fields  $H \simeq H_{c1I}$ . In fact, Eq. (37) also becomes more complicated at low H, of the order of the AJ lower critical field  $H_{c1b} = (\phi_0/4\pi\lambda^2) [\ln(\lambda/l) + 0.423]$ ,<sup>19</sup> for which *H* in Eq. (37) should be replaced by the corresponding B(H) dependence for AJ vortices.<sup>49</sup> For  $H \ge H_{c1b}$ , the induction B almost coincides with H, thus  $R_f(H)$  for AJ vortices acquires the universal form (37) independent of demagnetizing effects crucial at  $H \sim H_{c1}$ . The simplicity of Eq. (37) is very convenient to extract intrinsic properties of GBs at the nanoscale from transport measurements of  $R_f(H)$  in HTS bicrystals.<sup>53</sup>

#### **V. LINEAR ac RESPONSE**

To obtain the dynamic linear resistance  $R_{\omega}$  for a weak ac current,  $J_a \cos(\omega t) \ll J_b$  superimposed on the dc current J, we calculate the amplitude of the induced ac voltage,  $V_{\omega}$  from Eq. (30) in which  $\gamma(t)$  and v(t) are determined by Eqs. (10)–(12) with  $\beta = \beta_0 + \beta_a \exp(i\omega t)$ . Setting  $\alpha = \alpha_0 + \delta \alpha$ ,  $\gamma = \gamma_0 + \delta \gamma$  and calculating the perturbations  $\delta \alpha \ll 1$  and  $\delta \gamma \ll 1$  induced by the ac current from the linearized Eqs. (10)–(12) yields the following general expression for the ac complex resistivity  $R_{\omega} = V_{\omega}/J_a$  (see Appendix D):

$$\frac{R_{\omega}}{R} = \frac{\eta (h+u^2)/\sqrt{h} - \Omega^2 + i\Omega(\eta + \sqrt{h})}{\Omega_0^2 - \Omega^2 + 2i\eta\Omega}.$$
 (40)

Here  $u = V/J_b R$  is the dimensionless dc voltage on a GB,  $\Omega = \omega \tau$  is the normalized ac frequency,  $\Omega_0$  and  $\eta = \beta_0/s$  are the dimensionless flux flow resonance frequency and viscosity, respectively,

$$\eta = \sqrt{h + h/(h + u^2)}, \quad \Omega_0 = \sqrt{u^2 + \eta^2}.$$
 (41)

In the fixed current mode, it is convenient to express  $\Omega_0$  and  $\eta$  in terms of  $\beta_0$ ,

$$\Omega_0 = \left[ (1+h-\beta_0^2)^2 + 4h\beta_0^2 \right]^{1/4}, \tag{42}$$

$$\eta = \left[\sqrt{(1+h-\beta_0^2)^2 + 4h\beta_0^2} + 1 + h - \beta_0^2\right]^{1/2} / \sqrt{2}.$$
 (43)

The dependencies of  $\Omega_0$  and  $\eta$  on  $\beta_0$  are shown in Fig. 3. For  $J < J_b$ ,  $\Omega_0$  and  $\eta$  practically coincide, but for higher J, the frequency  $\Omega_0$  becomes much higher than the damping constant  $\eta$ . In the following subsections various dynamic regimes described by Eq. (40) are considered.

#### A. Small dc vortex velocities

For v = 0, Eq. (40) reduces to

$$R_{\omega} = R + \frac{R_f - R}{i\,\omega\,\tau_f + 1}.\tag{44}$$



FIG. 3. Dependencies of  $\Omega_0$  and  $\eta$  on the normalized dc current density  $\beta_0 = J/J_b$  for  $H = 0.05H_0$ .

Here  $R_f$  is the dc flux flow resistivity (37), and  $\tau_f$  is the flux flow relaxation time constant in the AJ vortex chain,

$$\tau_f = \frac{\tau}{\sqrt{1 + H/H_0}}.$$
(45)

The Drude-like frequency dependence of  $R_{\omega}$ , results in the following retarded relation between the induced voltage V(t) and the driving current J(t),

$$V(t) = RJ(t) + (R_f - R) \int_{-\infty}^{t} e^{(t'-t)/\tau_f} J(t') \frac{dt'}{\tau_f}.$$
 (46)

For example, after a jump-wise increase of J(t) from 0 to  $J_0$ , the steady-state flux flow sets in according to

$$V(t) = J_0[R_f + (R - R_f)e^{-t/\tau_f}], \quad t > 0,$$
(47)

and V=0 for t<0. The discontinuity in V(t) at t=0 disappears if a time dispersion of R, or a finite capacitance C of the GB are taken into account. In the latter case V(t) sharply increases from 0 to V(t) given by Eq. (47) during a short time  $\tau_i = RC$ .

The ac power  $Q = (1/2)J_a^2 Re(R_{\omega})$ , dissipated on a GB due to viscous flow of AJ vortices can be obtained from Eqs. (37), (44), and (45) in the form

$$Q = \frac{RJ_a^2[\sqrt{h(1+h)} + (\omega\tau)^2]}{2[1+h+(\omega\tau)^2]}.$$
 (48)

For a fixed frequency, Q(H) monotonically increases with H, approaching the quasiparticle limit  $RJ_a^2/2$  for  $H \gg H_0$ , as shown in Fig. 4. In the steady state,  $\omega \tau \rightarrow 0$ , the power  $Q(H) \propto \sqrt{h}/\sqrt{1+h}$  is simply proportional to  $R_f(H)$ . For finite frequencies, Q(H) becomes finite even with no vortices (H=0) due to quasiparticle ac Ohmic currents through GB.



FIG. 4. Field dependence of the ac dissipated power Q(H) for different dimensionless frequencies  $\Omega = \omega \tau$ .

# B. Flux flow resonance for moving AJ vortices

Interaction of the moving AJ chain with the ac field can cause a resonance, if  $\omega$  is close to the real part  $\omega_0$  of the complex eigenfrequency  $\omega_f$  which corresponds to the pole in  $R_{\omega}(\Omega)$ ,

$$\omega_f = \omega_0 + i \,\eta_0 \,, \tag{49}$$

where the flux flow resonance frequency  $\omega_0$  and the damping constant  $\eta_0$  are given by

$$\omega_0 = \sqrt{(kv)^2 + \eta_0^2},\tag{50}$$

$$\eta_0 = \frac{1}{\tau} \left[ \frac{H}{H_0} + \frac{1}{1 + (v/v_0)^2} \right]^{1/2}.$$
 (51)

For small dc velocity v, the AJ oscillations are strongly overdamped,  $\omega_0 \approx \eta_0$ , so no resonance peaks in  $R_{\omega}(\Omega)$  occur for  $J < J_b$ , as evident from Fig. 3. However, because the frequency  $\omega_0$  increases, while the damping constant  $\eta_0$  decrease as v(J) increases, the flux flow resonance emerges at high dc driving currents  $J > J_b$ , for which  $\omega_0 \ge \eta_0$ . For a given frequency  $\omega$ , the resonance occurs at the vortex velocity  $v_f$ , for which

$$\omega^2 = (kv_f)^2 + \eta_0^2(v_f).$$
 (52)

If  $kv \ge \eta_0$ , the resonance frequency  $\omega_0$  approaches the "washboard" frequency<sup>55</sup> for which the vortex velocity  $v_f$  equals the phase velocity of the electromagnetic wave  $\omega/k$  with the wave vector  $k = 2\pi/a$  of the AJ structure. Because  $\Omega_0(\beta_0)$  has a minimum at  $J \simeq J_b$  (see Fig. 3), the resonance condition (52) at a given frequency  $\omega$  can be satisfied either for one or two velocities  $v_f$ . From Eqs. (50), (51), and (52), it follows that

$$v_f = \left[\frac{\Omega^2 \pm \sqrt{\Omega^4 - 4h}}{2h} - 1\right]^{1/2} v_0.$$
 (53)



FIG. 5. Flux flow resonance line in Im  $R_{\omega}(\Omega)$  calculated from Eq. (40) for  $\beta = 4$  and different magnetic fields  $H/H_0$ : 0.05, 0.4, and 2 (from bottom to top curve, respectively).

The solution for  $v_f$  exists above the threshold  $\Omega > (4h)^{1/4}$ , where the resonance can occur either at one or two different velocities  $v_f$ , depending on  $\Omega$ ,

$$(4h)^{1/4} < \Omega < (1+h)^{1/2}$$
 two  $v_f$ , (54)

$$\Omega > (1+h)^{1/2}$$
 one  $v_f$ . (55)

At  $\Omega = (1+h)^{1/2}$ , the smaller resonance velocities vanishes as  $v_f \propto (\sqrt{1+h}-\Omega)^{1/2}$ . For  $\Omega \gg h^{1/4}$ , the larger resonance velocity approaches the material-independent "washboard" value  $v_f = a \omega/2\pi$ .

Near the resonance,  $\omega \approx \omega_0$ , at high vortex velocities ( $s^2 \gg 1$ ,  $\Omega_0 \approx s \sqrt{h}$ ,  $\eta \approx \sqrt{h} \ll \Omega_0$ ), Eq. (40) yields

$$\frac{R_{\omega}}{R} = 1 + \frac{1}{4\Omega_0(i\,\eta - \Omega + \Omega_0)}.$$
(56)

Equation (56) describes a resonance line with a Lorentz peak in Im  $R_{\omega} = -R/4s[h + (\Omega - \Omega_0)^2]$ , as shown in Fig. 5. For  $s^2 \ge 1$ , the amplitude of the peak decreases as v(J) and Hincrease. The resonance is most pronounced if  $J > J_b$  and  $H \ll H_0$ , while at smaller J or higher H, the peak in Im  $R_{\omega}(\Omega)$  disappears as the linewidth  $\eta$  becomes of the order of the eigenfrequency  $\Omega_0$ .

# VI. NONLINEAR RESPONSE

# A. Flux flow resonances on the dc V-J curve

The flux flow resonance also manifests itself in the averaged dc voltage V as a function of the dc current density. To calculate V(J), it is convenient to use the complex representation (14) for  $z = \gamma + i\alpha$ , taking  $z = z_0 + \delta z_0 + \delta z$ , where  $z_0$ is the dc solution without the ac field for which  $\sin z_0 = \beta$  $+i\sqrt{h}$ , and the oscillating correction  $\delta z$  obeys the linearized equation

$$\tau \delta \dot{z} + \cos z_0 \delta z = \delta \beta. \tag{57}$$

Here  $\delta\beta(t) = \beta_a \cos \omega t$ , and  $\delta z_0$  is a dc correction to  $z_0$  due to the ac field, which is determined by Eq. (14) expanded to quadratic terms in  $\delta z$ ,

$$2\,\delta z_0 \cos z_0 = \langle\,\delta z^2\rangle \sin z_0,\tag{58}$$

where the angular brackets mean time averaging over the ac period  $2\pi/\omega$ . The averaged vortex velocity  $\langle v \rangle$  is given by the second of Eqs. (14) expanded to quadratic terms in  $\delta z$  and linear terms in  $\delta z_0$ ,

$$k \tau \langle v \rangle = \operatorname{Im} \left( \cos z_0 - \frac{\langle \delta z^2 \rangle}{2 \cos z_0} \right).$$
 (59)

The second term in the parentheses describes the correction due to the ac field. The value  $\langle \delta z^2 \rangle$  can be calculated using the solution of Eq. (57),

$$\delta z = \frac{\beta_a}{\Omega^2 + \cos^2 z_0} (\cos z_0 \cos \omega t + \Omega \sin \omega t), \qquad (60)$$

which yields  $\langle \delta z^2 \rangle = \beta_a^2 / 2[\Omega^2 + \cos^2 z_0]$ . Inserting this expression into Eq. (59) gives the averaged vortex velocity in the form

$$\sqrt{h}\langle s \rangle = -(1 + \Gamma_{\omega}) \sin \gamma_0 \sinh \alpha_0,$$
 (61)

where the parameter  $\Gamma_{\omega}$  quantifies the ac contribution

$$\Gamma_{\omega} = \frac{J_a^2 (4 \,\eta^2 + \Omega^2 - \Omega_0^2)}{(2J_b \Omega_0)^2 [(\Omega^2 - \Omega_0^2)^2 + 4 \,\eta^2 \Omega^2]}.$$
 (62)

Equation (61) for  $\langle s \rangle$  is identical to the dc relation,  $\tau kv = -\sin \gamma \sinh \alpha$ , if v is replaced by the effective velocity  $\tilde{v} = v/[1 + \Gamma_{\omega}(v)]$ . Therefore, the averaged *J*-V characteristics can be presented in the dc form (36) if V is replaced by the effective voltage  $\tilde{V}(V)$  as follows:

$$J = \frac{\tilde{V}}{R} \left[ 1 + \frac{1}{H/H_0 + (\tilde{V}/V_0)^2} \right]^{1/2},$$
 (63)

$$\tilde{V} = V/[1 + \Gamma_{\omega}(V)], \qquad (64)$$

where  $\Gamma(V)$  is determined by Eqs. (41) and (62). The *J*-*V* characteristics described by Eqs. (63) and (64)  $J_a$  are shown in Fig. 6 for different ac amplitudes  $J_a$ . For stronger ac signal, the *J*-*V* curves can exhibit two maxima at the resonance voltages  $V_f = \phi_0 v_f / ca$ , and portions with negative differential conductivity. As follows from Eqs. (54) and (55), there are either one or two resonance voltages, depending on the relation between *H* and  $\omega$ . The increase of the magnetic field broadens the peaks in J(V) which eventually disappear at higher *H*, because of the increase of the effective damping constant  $\eta_0$  in Eqs. (49)–(51).

### B. ac dissipation

The mean ac power  $Q = \langle JV \rangle$  dissipated per unit area of a GB due to the ac voltage  $V(t) = V_a \cos \omega t$  of large amplitude can be calculated by solving Eqs. (31)–(33) numerically. The



FIG. 6. Manifestation of the flux flow resonance on the averaged dc *J*-*V* characteristic for  $\omega \tau = 0.1$ ,  $H = 0.01H_0$ , and different ac amplitudes,  $(J_a/2J_b)^2$ : 0 (1), 0.05 (2), 0.1 (3).

situation simplifies for a low-frequency ac signal ( $\omega \tau \ll 1$ ) for which Q can be obtained using the quasistatic Eq. (36). For low fields  $h \ll 1$  and moderate ac amplitudes  $u_a = V_a/V_0 < 1$ , the unity under the square root in Eq. (36) can be neglected, giving

$$Q = \frac{\omega V_a^2}{2\pi R} \int_0^{2\pi/\omega} \frac{\cos^2 \omega t dt}{\sqrt{h + u_a^2 \cos^2 \omega t}}.$$
 (65)

This integral can be expressed in terms of the complete elliptic integrals K(m) and E(m),<sup>69</sup>

$$Q = \frac{2J_b^2 R_f}{\pi \sqrt{1+g^2}} [(1+g^2)E(m) - K(m)], \qquad (66)$$

$$m = g^2 / (1 + g^2), \quad g = V_a / R_f J_b.$$
 (67)

The power Q(g) is a function of only one dimensionless parameter g which includes both the ac amplitude and the magnetic field, as shown in Fig. 7. For a weak ac signal,  $V_a \ll J_b R \sqrt{h}$ , Eq. (66) yields the quadratic dependence of Q $= V_a^2/2R_f$  on  $V_a$ , where  $R_f = R \sqrt{h}$  is the dc flux flow resistivity at  $h \ll 1$ . However, for stronger ac signals,  $J_b R \sqrt{h}$  $\ll V_a \ll J_b R$ , Eqs. (65) and (66) yield the *linear* dependence

$$Q = 2V_a J_b / \pi, \tag{68}$$

which is independent of the GB resistance *R*. This behavior is due to the AJ core expansion at large vortex velocities. For very high ac amplitude  $V_a \ge RJ_b$ , the full Eq. (36) should be used instead of Eq. (65). In this case Eq. (36) yields V = J/R during most part of the ac cycle, thus the ac power dissipated on the GB becomes quadratic in  $V_a$ , approaching the normal state limit,  $Q \rightarrow V_a^2/2R$  (not shown in Fig. 7).



FIG. 7. The power Q dissipated on a GB as a function of the ac amplitude, where  $Q_a = 2J_b^2 R_f / \pi$ .

#### C. Generation of higher harmonics

The nonlinearity of the electromagnetic response of the AJ structure driven by harmonic ac current  $J(t) = J_a \cos \omega t$  gives rise to higher voltage harmonics

$$V(t) = \sum_{n=0}^{\infty} V_{2n+1}(\boldsymbol{\beta}, \boldsymbol{\omega}, h) \cos(2n+1) \, \boldsymbol{\omega} t, \qquad (69)$$

where the Fourier coefficients  $V_{2n+1}$  can in principle be calculated from Eqs. (10)–(12). The higher harmonics in V(t)are most pronounced if the amplitude of ac AJ vortex displacements is maximum. For the overdamped dynamics considered in this paper, the amplitude of the AJ vortex oscillations decreases with  $\omega$ , so the higher harmonics in V(t) are most pronounced for the quasistatic ac signal,  $\omega \tau \ll 1$ . In that case the coefficients

$$V_{2n+1} = \frac{2\omega}{\pi} \int_0^{\pi/\omega} dt V(\beta_a \cos \omega t) \cos(2n+1)\omega t \quad (70)$$

are independent of  $\omega$ , and  $V[\beta(t)]$  is given by Eq. (35). For instance, the amplitude of the third harmonics  $V_3$  for a small ac current  $\beta_a = J_a/J_b \ll 1$  is obtained by expanding Eq. (35) up to cubic terms in  $\beta$ . This yields  $V(t) \approx R_f J_a \cos \omega t$  $+V_3 \cos 3\omega t$ , where

$$V_3 = \frac{RJ_a^3}{8J_b^2} \frac{\sqrt{h}}{(1+h)^{5/2}}.$$
(71)

The amplitude of the third harmonics  $V_3(h)$  has a maximum at h=1/4, as shown in Fig. 8. This field dependence reflects the increase of  $V_3 \propto \sqrt{h}$  at small *h* proportional to the AJ vortex density, followed by the decrease of  $V_3(h)$  at higher fields, for which the AJ cores start overlapping, and the V(J)curve becomes Ohmic. This trend is characteristic of other higher order harmonics as well, whose amplitudes  $V_{2n+1}(h) \propto \beta_a^{2n+1}$  strongly decrease with *n* and *h* for h > 1.



FIG. 8. The field dependencies of the amplitude of the third harmonics  $V_3(H)$  normalized to  $V_n = RJ_a^3/16J_b^2$  and the flux flow resistance  $R_f(H)$ .

The maximum in  $V_3(h)$  could be used for extracting the field  $H_0$  and thus the AJ core size l on a GB from the ac measurements. In that case the ac measurements of  $V_3(H)$  may bring some advantages over the dc measurements of  $H_0$  from the flux flow resistivity  $R_f(H)$ ,<sup>53</sup> since the maximum in  $V_3(H)$  occurs at the field  $H_0/4$  independent of the quasiparticle resistivity R, while the extracting of l from  $R_f(H)$  requires a two-parameter fit for  $H_0$  and R.

#### D. Phase locking and quasisteps on J-V curves

AJ vortices in superimposed ac and dc fields can exhibit phase locking effects at ac large amplitudes  $\beta_a$  if the dc voltage V on a GB is commensurate to the Josephson voltage  $V_{\omega} = \hbar \omega/2e$ , where n is any integer, and e is the electron charge. The electromagnetic response of a GB biased by a dc voltage V superimposed on ac voltage  $V_a \cos \omega t$ , is described by Eqs. (31)–(33) with  $u(t)=u+u_a \cos \omega t$ , where u $= V/RJ_b$ , and  $u_a = V_a/RJ_b$ . To calculate the dc J-V characteristic averaged over the ac oscillations with the account of the phase locking of  $\gamma(t)$  onto the ac field, we use an approach similar to that for Shapiro current steps on J-V curves of small Josephson junctions.<sup>43,58</sup> In this case

$$\gamma = \psi + n\omega t + q\sin\omega t + \delta\gamma, \quad q = u_a/\Omega,$$
 (72)

where  $\psi$  is a constant phase shift, and  $\delta\gamma(t)$  is a nongrowing oscillating correction. Likewise,  $\alpha = \alpha_0 + \delta\alpha(t)$ , where  $\alpha_0$  is a constant to be determined, and  $\delta\alpha(t)$  is an oscillating correction. We consider here the high-frequency signals of large amplitude ( $\omega\tau \gg 1$ ,  $u_a > 1$ ), for which both  $\delta\alpha \sim 1/\omega\tau \ll 1$  and  $\delta\gamma \sim 1/\omega\tau \ll 1$  can be neglected. This situation differs from the nonlocked state (n=0) considered in the preceding section, for which the contribution of  $\delta\alpha$  and  $\delta\gamma$  entirely determine the effect of the ac field on the dc *V*-*J* curves.

Equation (72) and Eqs. (31)–(33) yield the following averaged dc equations:

$$\langle \cos \gamma \rangle \sinh \alpha_0 = \sqrt{h},$$
 (73)



FIG. 9. Quasistep on the averaged *J*-*V* characteristic at  $V \approx V_{\omega}$  for q = 3, n = 1,  $V_{\omega}/RJ_b = 1$ , and different magnetic fields  $H/H_0$ : 0 (1), 0.01 (2), and 0.1 (3).

$$\langle \sin \gamma \rangle \sinh \alpha_0 = u - n\Omega,$$
 (74)

$$\beta_0 = u + \langle \sin \gamma \rangle e^{-\alpha_0}. \tag{75}$$

Here the averages  $\langle \sin \gamma \rangle$  and  $\langle \cos \gamma \rangle$  were calculated in Appendix E,

$$\langle \sin \gamma \rangle = (-1)^n J_n(q) \sin \psi,$$
 (76)

$$\langle \cos \gamma \rangle = (-1)^n J_n(q) \cos \psi,$$
 (77)

where  $J_n(q)$  is the Bessel function. From Eqs. (73)–(77), it follows that

$$\tan\psi = (u - n\Omega)/\sqrt{h},\tag{78}$$

$$\sinh^2 \alpha_0 = [h + (u - n\Omega)^2] / J_n^2(q).$$
(79)

Equations (75), (78), and (79) give the following dc *J-V* characteristics at  $V \approx nV_{\omega}$ :

$$RJ = nV_{\omega} + (V - nV_{\omega}) \left[ 1 + \frac{J_n^2(q)}{h + (V - nV_{\omega})^2 / V_0^2} \right]^{1/2}.$$
(80)

The behavior of J(V) near the resonant voltage  $V \approx nV_{\omega}$  is shown in Fig. 9. For  $H \rightarrow H_0$ , the J(V) dependence approaches that of the Shapiro step for a small Josephson junction at zero field. For finite H, the contribution from the AJ vortex motion broadens the kink in J(V), whose width  $\Delta V$  $= V - V_{\omega}$  can be estimated from the condition that two terms in the denominator of Eq. (80) become comparable. This yields

$$\Delta V \simeq \frac{Rc \sqrt{\phi_0 H}}{8\pi\lambda^2}.$$
(81)

The value  $\Delta V$  is independent of  $J_b$  and goes to zero as  $T_c - T$  at  $T_c$ .

The evolution of the AJ core length  $L = l\alpha/\sqrt{h}$  as the dc voltage V sweeps through the resonance at  $V_{\omega}$  is described by Eq. (79) as follows:

$$L = \frac{l}{\sqrt{h}} \sinh^{-1} \left[ \frac{\sqrt{h} + (u - n\Omega)^2}{|J_n(q)|} \right].$$
(82)

The core length L(V) passes through minima at the resonance voltages  $n\hbar \omega/2e$ . Notice that there are specific values of the ac parameter  $q_n = u_a/\Omega$ , which correspond to zeros of the Bessel function  $J_n(q)$ . In this case the core length diverges logarithmically, so the above approximation, which neglects the ac corrections  $\delta\gamma \sim \delta\alpha \propto 1/\Omega$ , becomes invalid. The blowing up of the AJ core length above  $\lambda$  at  $q \rightarrow q_m$  may indicate a conversion of the AJ into the J vortex under the action of an ac field.

# VII. DISCUSSION

In this paper solutions that describe dc and ac driven mixed Abrikosov vortices with Josephson cores on high- $J_b$  grain boundaries in a magnetic field are obtained. These solutions give self-consistent distributions of currents circulating around moving AJ vortex structure in an exactly solvable model of the overdamped AJ vortex dynamics that describes both nonlinear dissipative processes in the vortex cores and magnetic interaction between AJ vortices along a GB. Unlike Josephson vortices whose overdamped nonlinear dynamics in the long junctions can be described only numerically, the dynamics of AJ vortices turned out to be integrable just in the overdamped limit that is most relevant to low-angle GBs. The analytic theory of the ac response developed in this paper could be used to describe high- $J_b$  flux flow oscillators based on HTS bicrystals.<sup>18</sup>

Based on the exact AJ dynamic solutions, both the dc flux flow resistivity and the V-J characteristics are obtained. The field dependence of the flux flow resistivity  $R_f(H)$  shows the characteristic  $\sqrt{H}$  behavior at low H, but then it approaches the quasiparticle limit *R* for  $H \ge H_0$  as the AJ cores overlap. The simplicity of Eq. (37) for  $R_f(H)$  gives a direct way of extracting the AJ core length l and thus the intrinsic depairing current density  $J_{h}$  and the quasiparticle resistance R averaged over few current channels from transport measurements. Such measurements have indeed proven the existence of AJ vortices on 7° irradiated and unirradiated YBCO bicrystals for which the AJ core lengths  $\simeq 100-200$  Å at 55-77 K is considerably greater than  $\xi(T)$ , but smaller than  $\lambda(T)$ .<sup>53</sup> In addition, the extracted temperature dependence of  $J_d(T)$ exhibited a clear SNS behavior  $J_{h} = J_{0}(1 - T/T_{c})^{2}$ , indicating a significant order parameter suppression between dislocation cores, even on a rather low-angle 7° GB, in accordance with the model of Ref. 12.

The fact that moving AJ vortex core can effectively probe local GB properties at the nanoscale of few GB dislocation spacings, makes standard transport measurements a very useful tool to clarify the structure of vortex core on GBs, mechanisms of current transport through GBs and the effect of local overdoping on  $J_b$  and R. This method implies measurements of flux flow resistance  $R_f(H)$  for bicrystals with the

same misorientation angle  $\vartheta$ , but different local doping level. In this way, the intrinsic depairing current density of a GB,  $J_b$  can be obtained as a function of the dopant concentration. Pinning of AJ vortices strongly affects the V-J curve near the depinning current density,  $J \approx J_{gb}$ , but for  $J \gg J_{gb}$ , the differential resistivity dV/dJ approaches the free flux flow resistivity.<sup>70</sup> Thus, measuring  $R_f(H)$  in the flux flow region at  $J > (2-3)J_{gb}$  enables one to avoid the analysis of multiple pinning mechanisms on real grain boundaries in HTS,<sup>2</sup> using instead an exact flux flow theory for the interpretation of the experimental data in the region  $J \gg J_{ob}$ , where pinning is a weak perturbation. This conclusion is consistent with the experimental fact that V-J curves observed on HTS bicrystals are rather straight above  $J_{gb}$  in a wide range of currents.<sup>10,22–27,53</sup> Thus, the intrinsic properties of grain boundaries can be extracted from the analysis of the differential resistance (but not V-J curves) measured at J $\gg J_{gb}$  using our solution for  $R_f$  which neglects pinning. A similar approach was used to measure the flux flow resistivity of pinned A vortices driven by strong current pulses well above  $J_c$ .<sup>71</sup> Since  $J_{gb}$  is by two to three orders of magnitudes below the intrinsic  $J_b$ , the pinning region is much smaller than the scale of Fig. 2, so the linear  $R_f$  can be used to fit the data.

Measuring the local ac response of a GB can bring additional advantages over the dc measurements in which the dc current acts both on AJ on GB and A vortices in the grains. Indeed, using a scanning localized microwave source,<sup>15</sup> it would be possible to probe the ac dynamics of AJ on GB, minimizing the effect of pinned A vortices. For instance, the AJ core size and thus the local  $J_b$  can be extracted from ac measurements of higher voltage harmonics, as described in the preceding section.

The behavior of AJ vortices in a strong dc field  $H \gg H_{c1}$ considered in this paper is most relevant for bulk HTS. However, of much interest for superconducting electronics is also the electromagnetic response of HTS polycrystaline films in comparatively weak rf fields for which vortices mostly penetrate the network of GBs. In equilibrium, this regime corresponds to the field range  $\hat{H}_{c1b} < H < H_{c1}$ , where  $H_{c1}$ = $(\phi_0/4\pi\lambda^2)(1-N)[\ln(\lambda/\xi)+0.5]$  is the lower critical field for intragrain A vortices,<sup>69</sup> and  $H_{c1b} = (\phi_0/4\pi\lambda^2)(1-N)$  $\times [\ln(\lambda/l) + 0.423]$  is the lower critical field of AJ vortices,<sup>19</sup> and N is the demagnetizing factor. For a film in a perpendicular field, the AJ vortex spacing  $a = (\phi_0/B)^{1/2}$  can now significantly vary along GB, since the normal component of the local magnetic induction B(x,y) is now determined by highly nonuniform distribution of the Meissner surface currents and a domelike vortex distribution due to the geometrical barrier.<sup>72,73</sup> In this case the results of this paper based on the solution (9) with constant  $k = 2\pi/a(B)$  may be used if B(x) varies slowly over the intervortex spacing a(x), thus the parameter h in the above formulas should be replaced by its local value  $h(x) = B(x)/H_0$ .

*Note added.* After this manuscript was submitted, I became aware of the papers by  $Silin^{52(b)}$  in which equations analogous to Eqs. (10)–(12) had also been obtained.

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### APPENDIX A: DERIVATION OF EQ. (7)

To calculate the 2D current distribution around a planar Josephson contact in the *x*-*z* plane at *y*=0, it is convenient to use the scalar stream function  $\psi(x,y)$  so that  $J_x = \partial_y \psi$ ,  $J_y = -\partial_x \psi$ , whence

$$\frac{\partial \psi}{\partial y} = \frac{c}{4\pi\lambda^2} \left( \frac{\phi_0}{2\pi} \frac{\partial \varphi}{\partial x} - A_x \right), \tag{A1}$$

$$\frac{\partial \psi}{\partial x} = -\frac{c}{4\pi\lambda^2} \left( \frac{\phi_0}{2\pi} \frac{\partial \varphi}{\partial y} - A_y \right), \tag{A2}$$

where **A** is the vector potential, and  $\varphi$  is the phase of the order parameter. From Eq. (A1), it follows that the parallel component  $J_x(x,+0) - J_x(x,-0) = (c \phi_0/8\pi^2\lambda^2)\theta'$  is discontinuous for any nonuniform distribution of the phase difference  $\theta(x) = \varphi(x,+0) - \varphi(x,-0)$  along GB. This results in the following boundary condition for the stream function at a GB:

$$\partial_{\nu}\psi(x,+0) - \partial_{\nu}\psi(x,-0) = (c\phi_0/8\pi^2\lambda^2)\theta'.$$
(A3)

Excluding  $\varphi$  from Eqs. (A1) and (A2), we obtain

$$\nabla^2 \psi - \frac{cH}{4\pi\lambda^2} = \frac{c\phi_0\theta'}{8\pi^2\lambda^2} \,\delta(y),\tag{A4}$$

where the  $\delta$  function  $\delta(y)$  in the right-hand side provides the boundary condition (A3), and  $H = \nabla_z \times \mathbf{A}$  is the *z* component of the magnetic field, related to the stream function  $\psi$  by the Biot-Savart law,

$$H(\mathbf{r}) = \frac{1}{c} \int_{V[(x-x')^2 + (y-y')^2 + (z-z')^2]^{3/2}}^{[(x-x')^2 + (y-y')^2 + (y-y')^2 + (z-z')^2]^{3/2}}.$$
 (A5)

Equations (A4) and (A5) give an integrodifferential equation for  $\psi(x,y)$  which can be solved by the Fourier transform.

For an infinite (along **H**) sample, the local relation  $\psi(x,y) = cH(x,y)/4\pi$  holds, thus Eq. (A4) becomes the London equation (15) for H(x,y). For a thin film of thickness  $d \ll \lambda$ , one can put z = z' = 0 in Eq. (A5), then the integration over z' gives the factor d, and Eq. (A5) gives the following relation between the Fourier components of H and  $\psi$ :

$$H_q = (2\pi q d/c)\psi_q, \qquad (A6)$$

where  $q^2 = q_x^2 + q_y^2$ . The Fourier transform of Eq. (A4) yields

$$\psi_q = -\frac{c\,\phi_0\,\theta'(q_x)}{8\,\pi^2\lambda^2(q^2+q/\tilde{\lambda})},\tag{A7}$$

where  $\tilde{\lambda} = 2\lambda^2/d$ . Making the inverse Fourier transform of Eq. (A7) and using the boundary condition  $\psi'(x,0)$ 

= $J_b \sin \theta + \hbar \dot{\theta}/2eR$ , we arrive at the nonlocal Eq. (4) for  $\theta(x,t)$  in which  $K_0(|x-u|/\lambda)$  should be replaced by the kernel  $\tilde{K}(|x-u|/\lambda)$ , where<sup>47,48</sup>

$$\widetilde{K}(s) = \int_0^\infty \frac{e^{-sp}dp}{\sqrt{1+p^2}}.$$
(A8)

Despite different behaviors of  $K_0(|x-u|/\lambda)$  and  $\tilde{K}(|x-u|/\lambda)$ , at large distances, they both have the same logarithmic singularity at x=u, because at short distances  $|u-x| \ll \lambda$ , screening is inessential so the vector potential **A** in Eqs. (A1) and (A2) and the field *H* in Eq. (A4) can be neglected. Then Eq. (A4) becomes a 2D Poisson equation whose solution is

$$\psi(x,y) = \frac{c \phi_0}{32\pi^3 \lambda^2} \int_{-\infty}^{\infty} \theta'(u) \ln[y^2 + (x-u)^2] du, \quad (A9)$$

both for thin films and bulk samples.

# APPENDIX B: EXACT SOLUTION

To show that Eq. (9) is indeed an exact solution of Eq. (7), we substitute Eq. (21)–(23) into Eq. (7) in which the integral is evaluated using the Hilbert transform<sup>51,52</sup>

$$\int_{-\infty}^{\infty} \frac{\sinh \alpha dy}{(x-y)(\cosh \alpha - \cos ky)} = \frac{\pi \sin kx}{\cosh \alpha - \cos kx}.$$
 (B1)

Equation (7) then reduces to the algebraic form  $C_1 \cos \zeta + C_2 \sin \zeta + C_3 = 0$ , where the coefficients  $C_i$  depend only on time via  $\alpha(t)$ ,  $\gamma(t)$ , and  $\dot{x}_0(t)$ . Equating all  $C_i$  to zero, we arrive at Eqs. (10)–(12).

Useful relations for the steady-state vortex propagation can be obtained from Eqs. (10)–(12) with  $\dot{\gamma} = \dot{\alpha} = 0$ ,

$$\sinh \alpha \cos \gamma = \sqrt{h}, \tag{B2}$$

$$\sin\gamma\cosh\alpha = \beta_0(t), \tag{B3}$$

$$s\sqrt{h} = -\sin\gamma\sinh\alpha.$$
 (B4)

Adding squared Eqs. (B2) and (B4) yields

$$\sinh^2 \alpha = (1+s^2)h. \tag{B5}$$

Subtracting squared Eqs. (B3) and (B4) yields

$$\sin^2 \gamma = \beta_0^2 - s^2 h, \tag{B6}$$

Substituting Eqs. (B5) and (B6) back to Eq. (B4) gives the following equation for s:

$$\beta_0^2 = hs^2 + \frac{s^2}{1+s^2}.$$
 (B7)

The use of the relation  $s\sqrt{h} = V/J_bR$  reduces Eq. (B7) to Eq. (36). Substituting Eq. (B7) into Eq. (B6) yields

$$\sin \gamma = \frac{s}{\sqrt{1+s^2}}, \quad \cos \gamma = \frac{1}{\sqrt{1+s^2}}.$$
 (B8)

These results can also be obtained from the complex representation of the dc equations (14),

$$\sin z_0 = \beta_0 + i\sqrt{h}. \tag{B9}$$

The vortex velocity is given by the second Eq. (14),

$$s\sqrt{h} = \text{Im}[1 - (\beta_0 + i\sqrt{h})]^{1/2},$$
 (B10)

from which Eq. (34) readily follows.

# APPENDIX C: $R_f$ FOR J VORTICES

The sine-Gordon equation for a periodic J vortex structure moving with a constant velocity v has the form

$$\lambda_J^2 \partial_{\zeta\zeta} \theta + v \,\tau \partial_{\zeta} \theta - \sin \theta + \beta = 0, \tag{C1}$$

where the  $\zeta = x - vt$ . Multiplying Eq. (C1) by  $\partial_{\zeta} \theta$  and then integrating from  $\zeta = 0$  to  $\zeta = a$ , using the flux quantization condition  $\theta(\zeta + a) - \theta(\zeta) = 2\pi$ , and the periodicity condition  $\partial_{\zeta}\theta(\zeta + a) = \partial_{\zeta}\theta(\zeta)$  for  $H(\zeta)$ , we arrive at the following equation for v:

$$2\pi\beta = -v\,\tau \int_0^a (\partial_\zeta \theta)^2 d\zeta. \tag{C2}$$

Expressing the vortex velocity v(J) in Eq. (C2) via the dc voltage V from Eq. (30) yields the flux flow resistivity  $R_f = V/J$  in the form

$$R_f = 4 \,\pi^2 R / \left[ a \int_0^a (\partial_{\zeta} \theta)^2 d\zeta \right]. \tag{C3}$$

For the linear flux flow state at  $\beta \leq 1$ ,  $\theta(\zeta)$  in Eq. (C3) can be replaced with static  $\theta_0(x)$  for which

$$\lambda_J^2 \theta_0'' - \sin \theta_0 = 0, \qquad (C4)$$

The first integral of Eq. (C4) has the form

$$(\lambda_J \theta_0')^2 = 4[p^{-2} - \cos^2 \theta_0/2].$$
 (C5)

The periodic solutions of Eq. (C5) can be expressed in terms of the Jacobi elliptic function,  $\theta_0(x) = \pi + 2am(x/p\lambda_J)$ , where 0 is a parameter that is related to the appliedmagnetic field*H*and the magnetic induction*B*by Eqs.(39).<sup>68</sup> The period*a*of the*J*structure is given by

$$a = 2\lambda_J p K(p), \quad 2\lambda a B = \phi_0, \tag{C6}$$

where K(p) and E(p) are the complete elliptic integrals,<sup>69</sup>

$$K(p) = \int_0^{\pi/2} (1 - p^2 \sin^2 \theta)^{-1/2} d\theta, \qquad (C7)$$

$$E(p) = \int_0^{\pi/2} (1 - p^2 \sin \theta^2)^{1/2} d\theta.$$
 (C8)

Substituting Eq. (C5) into Eq. (C3) and changing integration  $\int_0^a dx \rightarrow \int_0^{2\pi} d\theta / \theta'$ , we obtain

$$R_f = \frac{\pi^2 R p \lambda_J}{2aE(p)}.$$
 (C9)

Equations (C6), (C9), and (39) give Eq. (38).

### APPENDIX D: LINEAR RESPONSE

Linearized Eqs. (10)-(12) have the form

$$\tau \dot{\delta \alpha} + \delta \alpha \cosh \alpha \cos \gamma - \delta \gamma \sinh \alpha \sin \gamma = 0, \quad (D1)$$

$$\tau \dot{\delta \gamma} + \delta \gamma \cos \gamma \cosh \alpha + \delta \alpha \sin \gamma \sinh \alpha = \beta_{\omega} e^{i\omega t}, \qquad (D2)$$

$$k\tau\delta v = -\delta\gamma\cos\gamma\sinh\alpha - \delta\alpha\sin\gamma\cosh\alpha.$$
 (D3)

These equations give the following Fourier components of  $\delta \alpha$ ,  $\delta \gamma$ , and  $\delta s$ :

$$\delta \alpha_{\omega} = \frac{\sinh \alpha \sin \gamma \delta \beta_{\omega}}{(i\Omega + \cosh \alpha \cos \gamma)^2 + \sinh^2 \alpha \sin^2 \gamma}, \quad (D4)$$

$$\delta \gamma_{\omega} = \frac{(i\Omega + \cosh \alpha \cos \gamma) \delta \beta_{\omega}}{(i\Omega + \cosh \alpha \cos \gamma)^2 + \sinh^2 \alpha \sin^2 \gamma}, \quad (D5)$$

$$\sqrt{h}\,\delta s_{\omega} = -\frac{\sinh\alpha(i\Omega\,\cos\gamma + \cosh\alpha)\,\delta\beta_{\omega}}{(i\Omega + \cosh\alpha\cos\gamma)^2 + \sinh^2\alpha\sin^2\gamma}, \quad (D6)$$

where  $\Omega = \omega \tau$ . Substituting  $\delta s$  and  $\delta \gamma$  into Eq. (30) gives the complex ac resistance  $R_{\omega} = V_{\omega}/J_a$ ,

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$$\frac{R_{\omega}}{R} = \frac{\sinh\alpha\cosh\alpha - \Omega^2 + i\Omega e^{\alpha}\cos\gamma}{\sinh^2\alpha + \cos^2\gamma - \Omega^2 + 2i\Omega\cosh\alpha\cos\gamma}.$$
 (D7)

Equation (D7) reduces to Eq. (40), using Eqs. (B5)-(B8).

# APPENDIX E: SEPARATION OF FAST AND SLOW VARIABLES

The time averages of

$$\langle \sin \gamma \rangle = \langle (\sin \psi \cos n \, \omega t + \cos \psi \sin n \, \omega t) \cos(q \sin \omega t) \rangle$$

+ 
$$(\cos\psi\cos n\omega t - \sin\psi\sin n\omega t)\sin(q\sin\omega t)\rangle$$
,

, .

$$\langle \cos \gamma \rangle = \langle (\cos \psi \cos n \, \omega t - \sin \psi \sin n \, \omega t) \cos(q \sin \omega t) \\ - (\sin \psi \cos n \, \omega t + \cos \psi \sin n \, \omega t) \sin(q \sin \omega t) \rangle,$$
(E2)

can be calculated, using the identities<sup>69</sup>

$$\cos(q\sin\omega t) = J_0(q) + 2\sum_{k=1}^{\infty} J_{2k}(q)\cos(2k\omega t),$$
 (E3)

$$\sin(q\sin\omega t) = 2\sum_{k=0}^{\infty} J_{2k+1}(q)\sin[(2k+1)\omega t],$$
 (E4)

where  $J_k(q)$  is the Bessel function. Averaging Eqs. (E1) and (E2) yields Eqs. (76) and (77) because only one resonant term with 2k=n or 2k+1=n in the sums (E3) and (E4) gives a nonzero dc contribution to  $\langle \sin \gamma \rangle$  and  $\langle \cos \gamma \rangle$ .

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