

## Temperature dependence of thermo-optical properties of fluoride glasses determined by thermal lens spectrometry

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In this work we report on the use of the thermal lens spectrometry to determine the absolute values of thermal diffusivity, thermal conductivity, and temperature coefficient of optical path-length change of several fluoride glasses. The results showed that fluoride glasses doped with minor quantities of Ga, In, and Zn exhibit thermal conductivities and thermal diffusivities roughly 20% larger than that of fluorozirconate (ZBLAN) glasses, whereas their temperature coefficients for the optical path-length change was found to be 50% smaller. This suggests that these fluoride glasses may be considered as promising candidates for high power laser applications. We have also demonstrated how this technique can be used for the complete thermo-optical properties characterization as a function of temperature. [S0163-1829(99)01342-9]

### INTRODUCTION

Fluoride glasses have been a subject of increasing interest mainly due to their high transparency at long wavelength, up to 10  $\mu\text{m}$ .<sup>1,2</sup> When doped with rare-earth ions these glasses present very low nonradiative decay rates as compared to the oxide glasses. These two features are essentially due to their low-field strength and weak chemical bonds.<sup>1</sup> However, this also implies in poor physical and chemical properties, namely high expansion coefficients, low values of both thermal conductivity ( $K$ ) and thermal diffusivity ( $D$ ) and high-temperature coefficient of the optical path-length change ( $ds/dT$ ).<sup>3-6</sup> These thermo-optical properties are among the most important characteristics determining the figures of merit of optical glasses. They essentially determine the glass servicing conditions such as thermal shock and thermal stress resistance,<sup>5</sup> thermal lens effect, and so on. The thermal diffusivity measures essentially the thermalization time of a given material and it is known to be strongly dependent upon the compositional and microstructural variables as well as processing conditions,<sup>7-10</sup> while  $ds/dT$  describes the thermally induced distortion of a laser beam after its passing through the sample.<sup>7</sup> Furthermore, it is also important to know the thermal properties in a wide temperature range, up to the glass transition temperature ( $T_g$ ), since they affect the fiber pulling, glass formation and devitrification processes.<sup>11</sup>

The thermal lens (TL) technique has proved to be a valuable method to study the thermo-optical properties of transparent materials.<sup>9,10,12-16</sup> It allows the determination of thermal diffusivity and thermal conductivity,<sup>9,10,15</sup> the temperature coefficient of optical path length,<sup>9,13</sup> optical absorption coefficient,<sup>16</sup> and fluorescence quantum efficiency.<sup>12,13</sup> Since this is a remote technique the measurement on a sample inside a furnace presents no extra difficulty, allowing therefore the measurements to be performed as a function of the temperature.

In the thermal lens effect, the propagation of a TEM<sub>00</sub>

Gaussian laser beam (either the excitation laser beam itself or a probe beam) is affected by the refractive index profile, or more generally, by a profile of the optical path length  $s$ . This results in beam spreading (when  $ds/dT < 0$ ) with a reduction in its on-axis intensity, or beam focusing (when  $ds/dT > 0$ ) with an increase in on-axis intensity.

There are several experimental configurations for the thermal lens spectrometry. The two-beam mode-mismatched experimental arrangement has shown to be the most sensitive one.<sup>17</sup> The theoretical model for the thermal lens effect in this configuration has been developed and an analytical expressions to treat the thermal lens effect quantitatively was obtained.<sup>9,18,19</sup> By measuring the beam on-axis intensity in the far field and using this theoretical model the thermo-optical properties of the sample can be obtained.

Considering the importance in determining the thermo-optical properties of fluoride glasses and the difficulties in measuring these properties using conventional calorimetry, a simple and accurate method to determine the temperature dependence of these properties is of utmost importance. In this work the two-beam mode-mismatched TL technique is used to determine the absolute value of thermal diffusivity, thermal conductivity, and the temperature coefficient of the optical path-length change of several fluoride glasses. For the ZBLAN glass doped with 0.2% mol CoF<sub>2</sub> we have measured the temperature behavior of the thermal diffusivity and  $ds/dT$  from 25 °C up to 315 °C. This range of temperature includes the temperature transformation of the glass ( $T_g$ ), which is around 298 °C.

### THEORY

In the mode mismatched thermal lens measurement, the sample is illuminated by a TEM<sub>00</sub> Gaussian laser beam. As a result of the optical energy absorption, a local temperature rise is produced within the sample due to the nonradiative decay processes. The change of the refractive index with the

TABLE I. Comparisons of the fluoride glasses studied in this work (mol %).

Acronym	ZrF <sub>4</sub>	YF <sub>3</sub>	LaF <sub>2</sub>	AlF <sub>3</sub>	GaF <sub>2</sub>	InF <sub>3</sub>	CaF <sub>2</sub>	SrF <sub>2</sub>	BaF <sub>2</sub>	ZnF <sub>2</sub>	PbF <sub>2</sub>	NaF
ZBLAN	53		4.5	3.5					29			10
YABC		20		40			20		20			
PGIZCa					20	15	20			15	30	
ISZn					6	34		20	16	20		4
InSBZnGdN					2GdF <sub>3</sub>	40		20	16	20		2

temperature produces a lenslike element within the heated region. A weak probe beam propagating through this heated region will experience an optical path-length change, resulting in a variation of its intensity at the beam center in the far field. The resulting change of the center probe beam intensity due to the thermal lens can be expressed as<sup>9,18,19</sup>

$$I(t) = I(0) \left[ 1 - \frac{\theta}{2} \tan^{-1} \left( \frac{2m\nu}{[(1+2m)^2 + \nu^2] \frac{t_c}{2t} + 1 + 2m + \nu^2} \right) \right]^2, \quad (1)$$

where

$$m = \left( \frac{\omega_{1p}}{\omega_e} \right); \quad V = \frac{Z_1}{Z_c} \text{ when } Z_c \ll Z_2; \quad t_c = \frac{\omega_e^2}{4D}. \quad (2)$$

Here,  $t_c$  is the characteristic thermal lens time constant,  $\omega_e$  is the excitation laser beam radius at the sample,  $D = K/\rho C$  ( $\text{cm}^2 \text{s}^{-1}$ ) is the thermal diffusivity,  $\rho$  ( $\text{g cm}^{-3}$ ) is the density,  $C$  ( $\text{J g}^{-1} \text{K}^{-1}$ ) is the specific heat,  $Z_c$  is the confocal distance of the probe beam,  $Z_1$  is the distance between the probe beam waist and the sample,  $Z_2$  is the distance between the sample and the detector,  $\omega_{1p}$  is the probe beam radius at the sample, and  $I(0)$  is the value of  $I(t)$  when the transient time  $t$  or  $\theta$  is zero. The TL transient signal amplitude is proportional to its phase shift  $\theta$ , given by<sup>9</sup>

$$\theta = - \frac{PA_e L}{K\lambda_p} \frac{ds}{dT}, \quad (3)$$

where  $\theta$  is approximately the phase difference of the probe beam at  $r=0$  and  $r=(2^{1/2}\omega_e)$  induced by the thermal lens,  $P(W)$  is the excitation laser power,  $A_e(\text{cm}^{-1})$  is the absorption coefficient at the excitation beam wavelength,  $K(\text{W K}^{-1} \text{cm}^{-1})$  is the thermal conductivity,  $\lambda_p(\text{cm})$  is the probe beam wavelength,  $L(\text{cm})$  is the sample thickness and  $ds/dT(\text{K}^{-1})$  is the optical path-length change with temperature, which is given by<sup>9,20</sup>

$$\frac{ds}{dT} = \frac{(n-1)}{L} \left( \frac{dL}{dT} \right)_{T_o} + \left( \frac{dn}{dT} \right)_{T_o}, \quad (4)$$

where  $n$  and  $L$  are the sample's refractive index and length, respectively, at the initial temperature  $T_o$ . We note that the above expression for  $ds/dT$  is a normalized quantity taking

into account both thermal expansion and refractive index changes. According to Refs. 9 and 20  $ds/dT$  can be expressed as

$$\frac{ds}{dT} = (n-1)(1+\nu)\gamma + \frac{dn}{dT}, \quad (5)$$

where  $\gamma(\text{K}^{-1})$  is the linear thermal expansion coefficient,  $n$  is the refractive index, and  $\nu$  is Poisson's ratio. Since the first term in Eq. (4) is always positive, glasses with negative  $dn/dT$  are required to minimize  $ds/dT$ . So far all glasses with  $ds/dT$  are fluoride glasses or glasses containing fluorine. In order to analyze the magnitude of  $ds/dT$  it is convenient to express it as proportional to  $[\phi - \eta\beta]$ ,<sup>9</sup> where  $\phi$  and  $\beta$  are the temperature coefficients of the electronic polarizability and volume expansion, respectively, and  $\eta$  is a constant that depends on the glass refractive index and the Poisson ratio  $\nu$ . It can be seen that the values of  $\phi$  and  $\beta$  determine the absolute value of  $ds/dT$ .

We have performed time-resolved TL experiments in several fluoride glasses, using the two-beam mode-mismatched TL configuration. From the transient TL signal data fitting the parameters  $\theta$  and  $t_c$  are obtained from which the values of  $D$ ,  $K$ , and  $ds/dT$  are deduced.

## EXPERIMENT

The fluoride glasses are very transparent, presenting a very low absorption coefficient ( $A \sim 10^{-3} - 10^{-4} \text{ cm}^{-1}$ ) in the visible and an even lower coefficient in the mid infrared. Since the TL signal is proportional to  $A$ , the signal of undoped matrixes is very low. We have accordingly increased the absorption of these glasses by doping them with low concentrations of Cobalt fluoride,  $\text{CoF}_2$ , in order to improve the signal-to-noise ratio.

The starting materials used for the preparation of our glasses were fluorides (BDH and Strem products) and oxides as  $\text{In}_2\text{O}_3$ ,  $\text{ZnO}$ , and  $\text{Ga}_2\text{O}_3$  (MetalEurop). The ammonium bifluoride was used to transform oxides into fluorides. The mixtures were heated in a platinum crucible for melting and refining. Finally, the melt was poured into a brass mold preheated few degrees below  $T_g$  temperature to prepare samples 4-mm thick. All these operations were carried out in a glove box with controlled inert atmosphere whose relative moisture was kept below 10 ppm. Table I summarizes the glass compositions used in this work. They are fluoroindates (PGIZCa, ISZn, InSBZnGdN), fluoroaluminate (YABC), and fluorozirconates (ZBLAN). The  $\text{Co}^{2+}$  doped glasses presented a wide ( $\sim 130 \text{ nm}$ ) absorption band, centered at 550 nm with significant absorbance at 514.5 nm. The density of the samples were measured using the buoyancy method with  $\text{CCl}_4$  as the

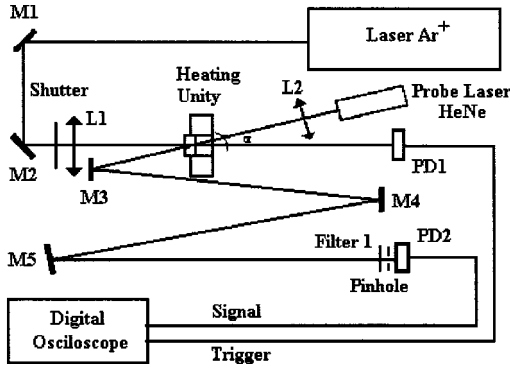


FIG. 1. A schematic diagram of the mode-mismatched thermal lens experimental apparatus, where  $M_1$ ,  $M_2$ ,  $M_3$ ,  $M_4$ , and  $M_5$  are mirrors,  $PD_1$  and  $PD_2$  are detectors, and  $L_1$  and  $L_2$  are lenses. Sample is placed inside the heating unity.

immersion liquid. The samples' specific heat were measured by using the thermal relaxation method.

The mode-mismatched thermal lens experimental setup is shown in Fig. 1. We have used an  $Ar^+$  laser as an excitation beam and a HeNe laser as the probe beam. The sample was positioned at the waist of the excitation laser beam, where the power density is maximum. The excitation beam was focused with a  $f_1=15$ -cm lens ( $L_1$ ), and the sample was positioned at its focal plane. The exposure of the sample to the excitation beam was controlled by means of a shutter. The probe laser beam was focused using a converging lens ( $L_2$ ) with focal length  $f_2=25$  cm at an angle  $\alpha < 1.5^\circ$  with respect to the excitation beam and centered to pass through the thermal lens to maximize the TL signal. The excitation beam was incident on a detector ( $PD_1$ ) and used as a trigger. The adjustable mirrors  $M_3$ ,  $M_4$ , and  $M_5$  were used to get a long optical length ( $\sim 2$  m) from the sample to an iris mounted before the detector ( $PD_2$ ). For the measurements at different temperatures, the sample was placed in an oven. The experiments were carried out in the temperature range between  $25^\circ C$  up to  $\sim 350^\circ C$ . Using the same TL experimental configuration we have also measured the optical absorption coefficients of our samples, by measuring the transmitted  $Ar^+$  laser light as a function of the incident power.

## RESULTS AND DISCUSSION

Figure 2 shows a typical TL signal for the ZBLAN with 0.2% mol of  $CoF_2$ . The experimental data fitting to Eq. (1) yielded  $\theta=0.3010 \pm 0.0005$  and  $t_c=0.55 \pm 0.01$  ms. Using Eq. (2) for  $t_c$  we obtained  $D=(2.5 \pm 0.1) \times 10^{-3} \text{ cm}^2/\text{s}$ , for the thermal diffusivity. The same procedure was carried out with all the other fluoride samples, and the resulting values for thermal diffusivity are summarized in Table II. In particular, for the case of the ZBLAN glasses, we have performed the measurements with four samples with different concentrations of  $CoF_2$ , namely, 0.1, 0.2, 0.3, and 0.38 mol %. The results obtained for their thermal diffusivities in this concentration range is practically constant and equal to  $D=(2.6 \pm 0.1) \times 10^{-3} \text{ cm}^2/\text{s}$ , as shown in Table II. From this value of  $D$ , and the measured values of  $\rho$  and  $C$  also shown in Table II, the thermal conductivity for these samples was calculated as  $K=(7.6 \pm 0.1) \times 10^{-3} \text{ W/cm K}$ . For the other

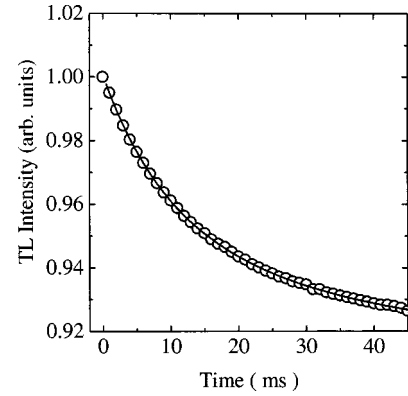


FIG. 2. Transient TL signal at room temperature for the 0.2%  $CoF_2$  ZBLAN sample. The line indicates the curve fitting using Eq. (1) of the text.

fluoride samples the thermal conductivity values are summarized in Table II.

In this way, we could perform a complete thermal properties characterization of the fluoride glass samples using the thermal lens technique. In particular, we note from Table II that the introduction of Ga, In, and Zn fluorides in the base composition of the fluoride glasses results in an improvement of the thermal properties of these glasses, without affecting the good optical properties of these materials. The thermal diffusivity and thermal conductivity of the first three glasses in Table II are roughly between 25 and 35% higher than those of ZBLAN. For laser applications, this represents a considerable gain in terms of heat dissipation, especially for the case of high power applications.

We have next used the above values of the thermal conductivity of these samples, together with the corresponding measured values for their optical-absorption coefficients and  $\theta$ , to calculate  $ds/dT$ . The results are summarized in Table II. All fluoride glasses studied presented positive  $\theta$ , which [cf Eq. (1)] indicates negative  $ds/dT$  values. The reason for this is that fluoride glasses are known to present very large thermal expansion coefficient  $\beta$ , which combined with the small values of  $\phi$  for the fluoride ions, results in negative  $dn/dT$  and  $ds/dT$ .<sup>21-23</sup> It can be seen from Table II that for the first three samples, containing the Ga, In, and Zn fluorides,  $ds/dT$  is roughly 50% smaller as compared to the ZBLAN sample values. That is, the addition of these fluorides to the base composition not only improves their thermal properties but also makes the optical path within these materials less susceptible to temperature changes. Considering that  $ds/dT$  is proportional to  $[\phi - \eta\beta]$ , the observed decrease in the value of  $ds/dT$  for the samples 1, 2, and 3 can be associated with a better combination of the two parameters  $\phi$  and  $\beta$  minimizing the values of  $ds/dT$  for these samples as compared to the ZBLAN glasses. The observed decrease of  $ds/dT$  for these samples is quite interesting. It indicates that these glasses should exhibit lower thermal distortions, at the same time that it suggests that further modification in the samples composition may lead to an improvement in lowering the  $ds/dT$  values for these samples.

Finally, to further demonstrate the usefulness of the TL technique for the complete thermo-optical characterization of glass samples, we have performed some measurements of the thermal properties as a function of temperature. These mea-

TABLE II. Optical absorption coefficient  $\Theta/P$ , thermal diffusivity, thermal conductivity, and  $ds/dT$  of the fluoride glasses determined at room temperature.

Samples	$L$ (cm)	$A_e$ ( $\text{cm}^{-1}$ )	$\Theta/P$ ( $\text{W}^{-1}$ )	$D$ ( $10^{-3} \text{ cm}^2/\text{s}$ )	$\rho$ ( $\text{g cm}^{-3}$ )	$C$ J/g K	$K$ ( $10^{-3} \text{ W/K cm}$ )	$ds/dT$ ( $10^{-6} \text{ K}^{-1}$ )
PGIZCa 0.2 CoF <sub>2</sub>	$0.366 \pm 0.001$	$0.90 \pm 0.04$	$1.200 \pm 0.002$	$2.9 \pm 0.1$	$5.359 \pm 0.004$	$0.67 \pm 0.03$	$10.4 \pm 0.9$	$-2.4 \pm 0.3$
IsZn 0.2 CoF <sub>2</sub>	$0.324 \pm 0.001$	$1.0 \pm 0.1$	$0.700 \pm 0.001$	$3.1 \pm 0.1$	$4.761 \pm 0.004$	$0.67 \pm 0.03$	$9.9 \pm 0.8$	$-1.3 \pm 0.2$
InSBZnGdN 0.3 CoF <sub>2</sub>	$0.272 \pm 0.001$	$0.80 \pm 0.02$	$0.700 \pm 0.001$	$3.2 \pm 0.1$	$4.753 \pm 0.004$	$0.67 \pm 0.03$	$10.2 \pm 0.8$	$-2.1 \pm 0.2$
YABC 0.38 CoF <sub>2</sub>	$0.212 \pm 0.001$	$1.80 \pm 0.03$	$1.500 \pm 0.002$	$3.3 \pm 0.1$	$3.704 \pm 0.004$	$0.67 \pm 0.03$	$8.2 \pm 0.7$	$-2.0 \pm 0.2$
ZBLAN 0.1 CoF <sub>2</sub>	$0.31 \pm 0.001$	$0.40 \pm 0.05$	$1.500 \pm 0.003$	$2.6 \pm 0.1$	$4.445 \pm 0.004$	$0.67 \pm 0.03$	$7.7 \pm 0.7$	$-5.9 \pm 1.3$
ZBLAN 0.2 CoF <sub>2</sub>	$0.349 \pm 0.001$	$0.70 \pm 0.01$	$3.100 \pm 0.004$	$2.5 \pm 0.1$	$4.445 \pm 0.004$	$0.67 \pm 0.03$	$7.4 \pm 0.7$	$-6.0 \pm 0.6$
ZBLAN 0.3 CoF <sub>2</sub>	$0.322 \pm 0.001$	$1.50 \pm 0.02$	$6.000 \pm 0.001$	$2.5 \pm 0.1$	$4.445 \pm 0.004$	$0.67 \pm 0.03$	$7.4 \pm 0.7$	$-5.8 \pm 0.6$
ZBLAN 0.38 CoF <sub>2</sub>	$0.268 \pm 0.001$	$2.20 \pm 0.10$	$7.400 \pm 0.001$	$2.7 \pm 0.1$	$4.445 \pm 0.004$	$0.67 \pm 0.03$	$8.0 \pm 0.7$	$-6.4 \pm 0.9$

measurements were carried out with the ZBLAN sample with 0.2% CoF<sub>2</sub>. The sample was positioned inside an oven and the temperature was varied from 25 °C up to 320 °C. This upper limit for the temperature excursion was essentially dictated by the glass transition temperature  $T_g$  of this material. The glass transition temperature was independently measured using a differential thermal analyzer (DTA), and the value found for  $T_g$  was 298 °C. The results of our DTA measurements for the ZBLAN doped with 0.2% CoF<sub>2</sub> are shown in Fig. 3. In Figs. 4 and 5 we show the resulting temperature dependence of the thermal lens signal parameter  $\theta$  and thermal diffusivity of the ZBLAN sample as obtained from the TL measurements, respectively. As before, the values of these parameters were obtained from the transient TL signal data fitting to Eq. (1). We note from Figs. 4 and 5 that both parameters exhibit a marked change around  $T_g$ . The parameter  $\theta$  exhibits a sharp jump around  $T_g$ , whereas the thermal diffusivity, after remaining practically constant up to 280 °C, it passes through a sharp minimum at  $T_g$ . The overall decrease of the thermal diffusivity in the temperature range close to  $T_g$  is of a factor of 12. On the other hand, from

differential scanning calorimetry measurements on ZBLAN glasses,<sup>11</sup> it has been shown that the specific heat of these glasses exhibits a sharp increase of about 1.6 close to  $T_g$ . Assuming that this is actually the case, and noting that the thermal conductivity is related to  $D$  and  $C$  by  $K = \rho CD$ , we conclude that at the glass transition temperature the thermal conductivity should decrease by a factor of 8.

To get further insight into the observed temperature dependence of  $\theta$  we address ourselves to its definition. As given by Eq. (3),  $\theta$  is essentially a measure of the probe beam phase shift between  $r=0$  and  $r=\sqrt{2}\omega_e$  induced by the thermal lens. Writing the thermal conductivity  $K$  in terms of the thermal diffusivity, namely,  $K = \rho CD$ , Eq. (3) can be rewritten as

$$\theta = \left( \frac{PA_e L}{D \lambda_p} \right) \left( - \frac{1}{\rho C} \frac{ds}{dT} \right). \quad (6)$$

The first term on the right-hand side of Eq. (6) is essentially the energy deposited by the pumping beam within a probe beam characteristic volume consisting of a cylinder of unit

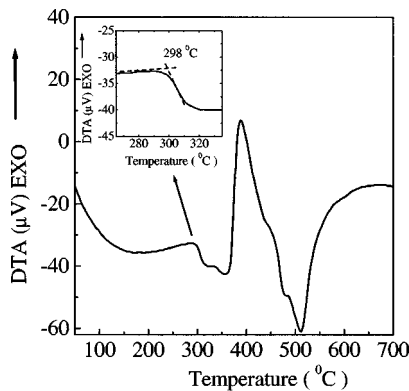


FIG. 3. Differential thermal analyzer (DTA) curve of the 0.2% mol of CoF<sub>2</sub> doped ZBLAN glass.

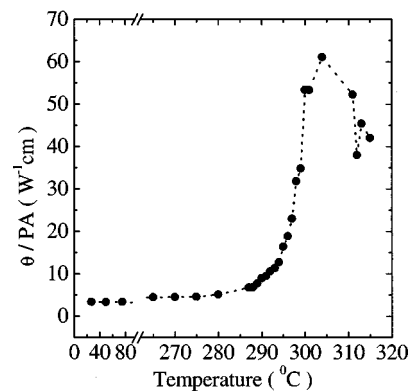


FIG. 4. Temperature dependence of the normalized thermal lens phase shift of the 0.2% mol of CoF<sub>2</sub> doped ZBLAN glass.

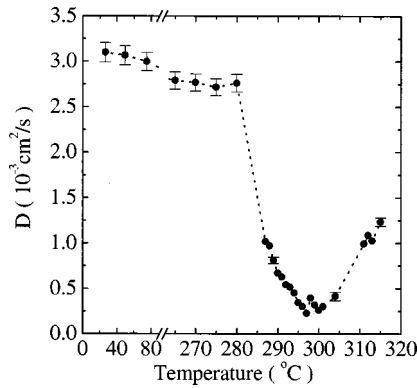


FIG. 5. Temperature dependence of the thermal diffusivity of the 0.2% mol of  $\text{CoF}_2$  doped ZBLAN glass.

area and length equal to the probe beam wavelength  $\lambda_p$ . The second term, namely,  $-(\rho C)^{-1} ds/dT$ , henceforth denoted by  $-ds/dQ$ , is a sample's characteristic response function telling us how the optical path changes with the heat deposited per unit volume. That is, it is a measure of the thermal lens distortion induced within a given material by a pumping beam. From the point of view of glass laser design, it may appear that this quantity is indeed the one we should be looking at when investigating the laser beam profiles and distortions within the active medium under high power operation conditions. Using our data for the 0.2%  $\text{CoF}_2$  doped ZBLAN glass we have plotted in Fig. 6  $-ds/dQ$  as a function of temperature. It follows from Fig. 6 that up to 250 °C,  $-ds/dQ$  remained roughly constant. Between 250 and 280 °C it increased with increasing temperature. As the temperature crosses the glass transition temperature, between 280 and 300 °C,  $-ds/dQ$  passes through a minimum to finally exhibit a sharp jump above 300 °C. This behavior of  $-ds/dQ$  is closely related to that of the DTA measurements as follows. Between 200 and 280 °C, the DTA measurements tell us that the sample tends to lose heat so that  $-ds/dQ$  should increase with increasing temperature. In the temperature range between 280 and 300 °C, the DTA data tell us that the sample tends to retain heat so that one expects  $-ds/dQ$  to decrease with increasing temperature. Finally, the sudden rise above  $T_g$  is basically attributed to the larger increase in the thermal expansion coefficient, and consequently of the optical path, which is observed in a glass transition.

### CONCLUSION

In this paper we have demonstrated the usefulness of the thermal lens spectrometry to determine the thermal diffusivity, thermal conductivity, and the temperature coefficient of optical path-length change of fluoride glasses. The results showed that glasses containing Ga, In, and Zn exhibited improved thermo-optical properties as compared to the ZBLAN formulation. Especially in the case of high power laser applications, the thermal parameters play an essential role. For these applications one requires glasses with high thermal conductivity in order to effectively dissipate the heat gener-

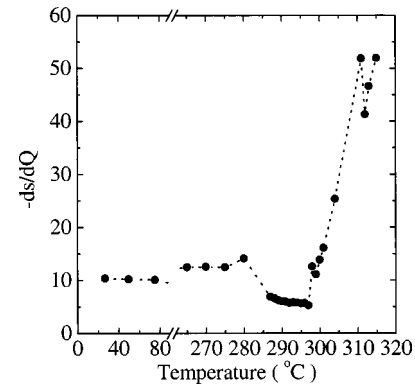


FIG. 6. Characteristic optical path changes with deposited heat ( $-ds/dQ$ ) as a function of temperature for the 0.2% mol of  $\text{CoF}_2$  doped ZBLAN glass.

ated within the laser action region, at the same time that a small temperature coefficient of optical path length is also desired for smaller thermally induced laser beam distortions.

It is well known that fluoride glasses do not have thermo-optical properties suitable for high power laser applications. Our results indicate that fluoroindate and fluoroaluminat glasses, which have very good optical properties, exhibit thermal conductivity and thermal diffusivity roughly 18 and 23%, respectively, greater than those of ZBLAN, while the temperature coefficient of optical path length was about 50% smaller. This better combination of the thermo-optical properties indicates that these glasses are promising candidates for laser applications. Finally, we have also demonstrated the ability of the thermal lens spectrometry to perform the thermo-optical characterization of glasses as a function of temperature. This was demonstrated for the case of the ZBLAN doped with 0.2%  $\text{CoF}_2$ . Two interesting aspects emerged from these measurements. First, it was shown that the thermal diffusivity exhibits a sharp minimum at 298 °C which coincides with the  $T_g$  value measured by DTA. Second, using the data for the thermal diffusivity and the probe beam phase shift, we calculated the rate of change of the optical path with respect to the heat absorbed. It was shown that this parameter not only reflects the characteristic dependence of the refractive index and thermal expansion coefficient with temperature, but is also closely related to the behavior of the DTA measurements.

This application of the thermal lens spectrometry completely evaluates the thermo-optical properties of fluoride glasses, including their temperature dependence. We believe that the sensitiveness together with its simplicity and its remote character may render this technique as a valuable tool for the complete characterization of the thermo-optical properties of a wide range of transparent materials, especially as a function of temperature.

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