

## Nonuniversal behavior of finite quantum Hall systems as a result of weak macroscopic inhomogeneities

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We show that, at low temperatures, macroscopic inhomogeneities of the electron density in the interior of a finite sample cause a reduction in the measured conductivity peak heights  $\sigma_{xx}^{\max}$  compared to the universal values previously predicted for infinite homogeneous samples. This effect is expected to occur for the conductivity peaks measured in standard experimental geometries such as the Hall bar and the Corbino disk. At the lowest temperatures, the decrease in  $\sigma_{xx}^{\max}(T)$  is found to saturate at values proportional to the difference between the adjacent plateaus in  $\sigma_{xy}$ , with a prefactor that depends on the particular realization of disorder in the sample. We argue that this provides a possible explanation of the “nonuniversal scaling” of  $\sigma_{xx}^{\max}$  observed in a number of experiments. We also predict an enhancement of the “nonlocal” resistance due to the macroscopic inhomogeneities. We argue that, in the Hall bar with a sharp edge, the enhanced “nonlocal” resistance and the size corrections to the “local” resistance  $R_{xx}$  are directly related. Using this relation, we suggest a method by which the finite-size corrections may be eliminated from  $R_{xx}$  and  $R_{xy}$  in this case.

### I. INTRODUCTION

The fascinating property of the quantum Hall effect (QHE) that initially attracted such great attention to the phenomenon is the precise quantization of the Hall conductivity  $\sigma_{xy}$  at certain values of the magnetic field. Most theoretical research has focused on the properties of the electron system inside these quantized plateaus in  $\sigma_{xy}$ . The plateaus have been associated with the incompressibility of the two-dimensional (2D) electron gas, arising either from Landau quantization, at integer filling factors, or from electron-electron interactions, at fractional filling factors. The transition regions, where  $\sigma_{xy}$  crosses over between quantized values and the longitudinal conductivity  $\sigma_{xx}$  experiences maxima, have received less attention. The main factor, which inhibits progress in this direction, is the lack of reproducible experimental results on the interplateau regions, despite the impressive stock of data on the QHE that has been accumulated over the past decade. In addition to the fact that the general behavior of the QHE depends on the electron density, temperature, and disorder, samples cut from the same substrate and measured at the same temperature often reveal different dependences  $\sigma_{xy}(B)$  and  $\sigma_{xx}(B)$ . This annoying data dispersion is particularly apparent at low temperatures.<sup>1</sup> A certain success in obtaining reproducible data has been achieved only for the critical behavior of the width of interplateau regions at low temperatures.<sup>2</sup> However, as far as the heights or shapes of the peaks in  $\sigma_{xx}$  are concerned, the general impression is that too many factors are involved to allow any systematic conclusions.

On the other hand, there do exist a number of theoretical works which argue that certain universal behavior of the conductivity tensor must exist at low temperatures in the regions between well-pronounced pairs of plateaus (critical regime). Kucera and Streda<sup>3</sup> considered semiclassical single-electron transport in a partially filled Landau level for a simple model of a periodic long-range potential. They found that the maxi-

um value of  $\sigma_{xx}$  reached at half-integer filling factors does not depend on either the magnitude of the potential or the Landau level number  $N$  and is equal to  $e^2/2h$ . This result was later mapped onto the fractional regime by using two related approximations of the correlated electron state: the dirty boson<sup>4</sup> and the composite fermion approach.<sup>5</sup> A different sort of argument for both integer and fractional regime was presented in Refs. 6 and 7. Based on the rather general assumption that, at low temperatures, the electron system in a critical transition region can be represented by a random mixture of two quantum liquids with different quantized local Hall conductivities  $\sigma_2$  and  $\sigma_1$ , it was shown that  $\sigma_{xx}$  and  $\sigma_{xy}$  are connected by a universal relation. The peak height  $\sigma_{xx}^{\max}$  was found to be equal to one half of the difference between the Hall conductivities of the adjacent plateaus  $|\sigma_2 - \sigma_1|/2$ . For the integer peaks, this result yields the value  $e^2/2h$  obtained in Ref. 3. For the fractional regime, it matches the results of Refs. 4 and 5, after the latter are somewhat corrected to allow for the fact that the maxima of  $\sigma_{xx}(B)$  of the integer peaks do not map exactly onto the maxima of  $\sigma_{xx}(B)$  for the principal series.<sup>8</sup> We can also refer the reader to quantum Monte Carlo studies in Ref. 9, where the same value,  $0.5e^2/h$ , for the integer peaks was obtained in a simulation of single-electron scattering off short-range impurities. Thus, while different theoretical models agree on an expected universality of the conductivity peak heights and even on their values, experiment offers no evidence to support this prediction.

To make the situation even more confusing, a puzzling feature was observed in a number of experiments performed at very low temperatures (15–40 mK): the relative heights of most of the conductivity peaks obtained in the fractional regime were, indeed, found to scale approximately as  $|\sigma_2 - \sigma_1|$ , but with an absolute factor which differed from 1/2 and, moreover, varied from sample to sample.<sup>10</sup> Such a “universality within one sample,” while there is none between different samples, is hard to understand. This feature

was especially well seen in recent experiments performed in the Corbino geometry,<sup>11</sup> where scaling of the peak heights was observed simultaneously for the fractional and integer regimes, i.e., in quite different ranges of magnetic field. As a function of temperature, the height of each peak was found to pass through a maximum value. These maximum values differed for different peaks, being scattered below, though not very far from, the universal values predicted by theory. On the low temperature side of these maxima, therefore, with decreasing temperature the peak heights fell further below the universal values, as has also been earlier observed in low-mobility samples.<sup>1</sup> At the lowest temperatures (14 mK), however, different peaks in a given sample converged to the corresponding theoretical values multiplied by the same sample-dependent factor.

In this work, we suggest an explanation of the phenomenon of the “nonuniversal” scaling of the peak heights. Our explanation assumes that in the interior of the sample, there exist random inhomogeneities of the electron density with a very large correlation length  $R_c$ . While the origin of these inhomogeneities is unclear, we note that the existence of such fluctuations was also a necessary assumption in recent work,<sup>12</sup> which proposed an explanation for another experimental puzzle—the Resistivity Law, which is observed in some samples at higher temperatures. We can only speculate as to whether such fluctuations might result from imperfections in the doping process or from incomplete equilibration of the electron density on sample cool down, or from both. The fact that the experimental traces in the interplateau regions often change after the sample is reheated and cooled down again, indicates that that the latter mechanism may be important. By whatever means they might arise, we argue that even small fluctuations of the electron density become crucial at low enough temperatures, where the dependence of the conductivity tensor on the local value of the filling factor is almost singular. In particular, we show that, due to the finite size of the sample, the sample edge gives rise to a positive contribution to the Corbino resistance, which is proportional to  $1/(\sigma_2 - \sigma_1)$ . This contribution increases with decreasing temperature, due to the growing correlation radius of the random clusters, which are responsible for the current transfer. At sufficiently low temperatures, when the correlation radius exceeds the sample size, the edge contribution dominates the sample conductance. The heights of the observed peaks in  $\sigma_{xx}$  in a given sample are found to freeze at values that differ from the corresponding “universal” values in an infinite sample, by a random geometric factor that is the same for all peaks.

By making use of a current-voltage duality that exists in two-dimensional conductivity problems, we show how our results may also be applied to the Hall bar geometry. We find that macroscopic inhomogeneities have the same effect on the measured peaks in  $\rho_{xx}$  in this geometry as on the peaks in  $\sigma_{xx}$  for the Corbino disk. This is in agreement with the fact that sample-dependent scaling of the peak heights has been observed in both geometries.<sup>10,11</sup>

It has previously been realized that density inhomogeneities may distort conductivity measurements in the Hall bar geometry. In particular, for certain gated or mesa-etched systems, the boundary to a vacuum is believed to involve a rather gradual decrease in electron density. This creates a

strip along the edge with a quantized Hall conductivity and very low scattering, while the bulk of sample can be in a transition region with noticeable dissipation. Such a strip can trap a significant portion of the current, making the current distribution in the sample inhomogeneous and affecting the measured resistance  $R_{xx}$ . In the language of the edge-transport theory, this can be reformulated as poor equilibration between the edge states and the bulk. While this model has been successful in accounting for certain nonlocal resistance measurements, the presence of a smooth edge cannot explain the observed nonuniversal scaling of the conductivity peak heights. Therefore, since the random bulk inhomogeneities are crucial for this scaling, and since the effects of a smooth edge have been discussed before,<sup>13–15</sup> in this work we will focus only on the consequences of macroscopic bulk inhomogeneities. The results we present for the Hall bar, therefore, apply to samples with sharp edges (i.e., with the edge width less than magnetic length). For certain samples, some combination of the two models may be appropriate.

As well as giving rise to “nonuniversal scaling” of the peak heights at the lowest temperatures, we show that macroscopic inhomogeneities in the bulk also lead to an enhancement of the nonlocal resistance. In fact, by developing a general “boundary-strip” approach, which describes finite-size effects in a macroscopically inhomogeneous sample, we show that, for a sample with a sharp edge, both of these effects are directly related. Using this relation, we propose an experimental method by which the edge contribution in the observed resistivity may be separated from the bulk contribution, at least over the range of temperature for which the edge contribution is not too big (at intermediate  $T$ ).

The paper is organized as follows. In Sec. II, we discuss the role of macroscopic inhomogeneities in the transport properties of an infinite QHE system in different regimes of temperature. Finite-size effects on the low-temperature two-terminal resistance of an inhomogeneous Corbino disk are considered in Sec. III and in the Appendix. The boundary impedance matrix formalism, which provides a description of small edge contributions to the measured resistances in any sample geometry (Corbino disk, Hall bar, etc.), is developed in Sec. IV. The explicit form of the impedance matrix is evaluated for a macroscopically inhomogeneous sample with a sharp edge. The enhanced “nonlocal” resistance arising from the macroscopic inhomogeneities is studied in Sec. V, where it is also shown that this is directly related to the edge corrections in the measured “local” and Hall resistances. Section VI concludes the paper.

## II. INFINITE SAMPLE

We consider an infinite sample in the presence of macroscopic inhomogeneities of the electron density. The local value of the filling factor can be written as  $\nu(\mathbf{r}) = \bar{\nu} + \delta\nu(\mathbf{r})$ , where  $\bar{\nu}$  is the average filling factor, and  $\delta\nu(\mathbf{r})$  is a small fluctuating component with a magnitude  $\delta\nu_0 \ll \bar{\nu}$ . We assume that some impurity scattering occurs on scales much smaller than  $R_c$ , such that the local conductivity tensor exhibits the quantum Hall effect. Specifically, we will assume that at a critical value  $\nu_c$ , the Hall conductivity undergoes a sharp crossover between two quantized values,  $\sigma_1 = e^2\nu_1/h$ , and  $\sigma_2 = e^2\nu_2/h$ . Here,  $\nu_1$  and  $\nu_2$  are a

pair of adjacent values of  $\nu$  at which the electron system is incompressible,  $\nu_1 < \nu_c < \nu_2$ . The diagonal conductivity  $\sigma_{xx}(\nu)$  has a sharp peak in the crossover region, being very small everywhere else [Fig. 1(a)]. The width of the crossover region  $\delta\nu_T$  vanishes as  $T \rightarrow 0$ . We can consider this picture as simply following from numerous experimental data on the low-temperature quantum Hall effect in large samples.

The critical behavior of the conductivity tensor has been studied well. The width of the crossover region vanishes as  $T \rightarrow 0$ , according to

$$\delta\nu_T \sim T^\kappa,$$

with an exponent  $\kappa$ , which has been argued to take the universal value  $3/7$ .<sup>16</sup> In the zero-temperature limit, the maximum value of the dissipative conductivity is thought to approach  $e^2/2h$  in the spin-split integer quantum Hall effect,<sup>6,7,9</sup> and  $(\sigma_2 - \sigma_1)/2$  for the fractional regime.<sup>6,7</sup> As explained in the Introduction, this prediction was deduced from the hypothesis that the correlated electron state in the vicinity of a QHE transition represents a random mixture of two incompressible liquids with localized quasiparticles on top. The correlation radius  $R_c^{\text{mic}}$  of this two-phase system was assumed to be larger than the magnetic length  $(\hbar c/eB)^{1/2}$ .

To avoid confusion, we emphasize that the correlation radius of the macroscopic density fluctuations  $R_c$ , which we consider in the present work, is assumed to be much larger than  $R_c^{\text{mic}}$ , which is thus considered as a microscopic length. The ‘‘local’’ conductivity tensor  $\hat{\sigma}(\mathbf{r})$  introduced above is defined at scales larger than  $R_c^{\text{mic}}$  (and, if effects of quantum interference are important, larger than the phase-breaking length), but smaller than  $R_c$ . For our purposes, the peak value of the local dissipative conductivity will not be important; we shall only assume that it is either of the order of or less than the difference in the quantized values of the Hall conductivity,  $\sigma_2 - \sigma_1$ . We believe that this assumption agrees with existing data on the quantum Hall effect in a strong magnetic field.

Let the magnetic field be tuned, so that the average filling factor  $\bar{\nu}$  is close to  $\nu_c$ . At sufficiently low temperatures, the crossover width  $\delta\nu_T$  becomes much less than the fluctuation magnitude  $\delta\nu_0$ , which is small but temperature independent. Hence, as temperature goes down, the conductivity distribution becomes strongly inhomogeneous. In most of the sample, as illustrated in Fig. 1(a,b), the Hall conductivity  $\sigma_{xy}$  is quantized at either  $\sigma_1$  or  $\sigma_2$ , and the diagonal conductivity  $\sigma_{xx}$  is very small. Only a narrow intermediate region, within the interval  $|\nu - \nu_c| \sim \delta\nu_T$ , has a noticeable  $\sigma_{xx}$ . This region is indicated by the gray color in Fig. 1(c)]. As long as  $\bar{\nu}$  stays within this interval, the ‘‘gray’’ region forms an infinite percolation cluster. The latter consists of strips of a small width  $w_T \sim R_c \delta\nu_T / \delta\nu_0$ , which join near saddle points (critical vertices). The characteristic size of a cluster cell, i.e., the distance between two vertices, follows from classical percolation theory,<sup>17</sup>

$$\xi_T \sim R_c (\delta\nu_0 / \delta\nu_T)^{4/3}. \quad (1)$$

We note that the true geometry of the percolating cluster includes also loops and bypasses on links between vertices not shown in Fig. 1(c).

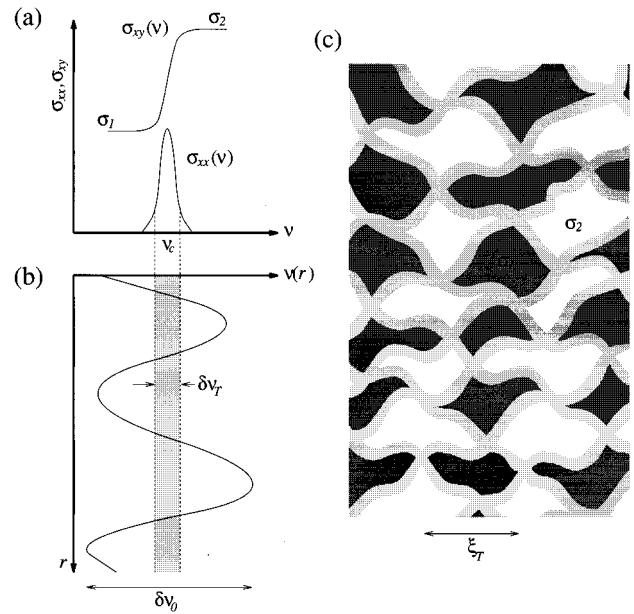


FIG. 1. (a) Local conductivity tensor components  $\sigma_{xx}$  and  $\sigma_{xy}$  versus the local filling factor  $\nu$ . (b) Macroscopic fluctuations of the local filling factor. (c) Conductivity tensor distribution in inhomogeneous system at low temperatures. Black and white regions correspond to quantized Hall regions with  $\sigma_{xy} = \sigma_1$  and  $\sigma_2$ , respectively, and  $\sigma_{xx} \approx 0$ . The gray color, which corresponds to the gray strip in (b), shows the intermediate (nonquantized) region.

The evaluation of the effective conductivity tensor  $\sigma^*$  requires an understanding of how the current density is distributed in such an inhomogeneous system. The current distribution is known to be quite different in the two limiting cases, which are reached as the relative values of the dimensionless parameters  $w_T/R_c$  and  $\sigma_{xx}^{\text{max}}/(\sigma_2 - \sigma_1)$  are varied.

When  $\sigma_{xx}^{\text{max}}$  is very small (how small will be determined below), the continuity conditions force the current to flow almost exactly along lines of constant  $\sigma_{xy}$ .<sup>18,15</sup> For an infinite random system, this means that the current is concentrated near the percolation threshold of the function  $\sigma_{xy}(\mathbf{r})$ , within a sparse percolation network inside the gray area shown in Fig. 1(c). The characteristic parameters of this new network—the width  $w$  and the length  $l$  of an elementary link of the cluster—are determined by the value of  $\sigma_{xx}$  at the percolation level in  $\nu$ . They can be estimated from the self-consistent condition that the current is able to cross the lines of constant  $\sigma_{xy}$ , in order to pass from one critical saddle point of the network to the next one, which has a slightly different value of  $\sigma_{xy}$ .<sup>17,12</sup> We give here the final expressions for both parameters,

$$w \sim w_T \left( \frac{\sigma_{xx}}{\sigma_2 - \sigma_1} \right)^{3/13} \left( \frac{R_c}{w_T} \right)^{10/13}, \quad l \sim R_c \left( \frac{(\sigma_2 - \sigma_1) R_c}{\sigma_{xx} w_T} \right)^{7/13}. \quad (2)$$

Here inequalities  $w \ll w_T$ ,  $l \gg \xi_T$  are implied. The net diagonal conductivity of the system  $\sigma_{xx}^*$  is determined by the geometry of an elementary link, as given by  $\sigma_{xx}^* \sim \sigma_{xx} l/w$  which yields, for the maximum value of  $\sigma_{xx}$ ,

$$\sigma_{xx}^* \text{max} \sim (\sigma_{xx}^{\text{max}})^{3/13} (\sigma_2 - \sigma_1)^{10/13} \left( \frac{\delta\nu_0}{\delta\nu_T} \right)^{10/13}. \quad (3)$$

Note that the effective conductivity decreases with increasing temperature, more or less as  $1/\delta\nu_T$ , unless the temperature dependence  $\sigma_{xx}^{\text{max}}(T)$  is very sharp.

The net Hall conductivity  $\sigma_{xy}^*$  does not depend on the geometry of the network and simply coincides, apart from small corrections, with the percolation threshold value  $\sigma_{xy}(\bar{\nu})$ . Hence,  $\sigma_{xy}^*$  crosses over from  $\sigma_1$  and  $\sigma_2$  within the same interval of  $\bar{\nu}$ , as does the local Hall conductivity,  $|\bar{\nu} - \nu_c| \sim \delta\nu_T$ .

This picture is correct provided that  $\sigma_{xx}$  is sufficiently small and the gray regions are not too narrow, such that the current can stay within these regions,  $w \ll w_T$ . The last condition can be written as  $T \gg T_{s1}$ , with  $T_{s1}$  given by the equation,

$$\delta\nu_T(T_{s1}) = \delta\nu_0 \left( \frac{\sigma_{xx}(T_{s1})}{\sigma_2 - \sigma_1} \right)^{3/10}. \quad (4)$$

The regime exists only if  $\sigma_{xx}$  is much less than  $\sigma_2 - \sigma_1$ , at temperatures at which the system can already be considered to be macroscopically homogeneous,  $\delta\nu_T(T) \sim \delta\nu_0$ .

As the temperature is reduced below  $T_{s1}$ , the current spills out into the quantum Hall regions. In the limit  $T \ll T_{s1}$ , which will be mostly considered in the rest of the paper, the currents flow predominately in the quantized Hall regions. The details of the gray areas become unimportant (except near the saddle points), and they may be replaced by sharp boundaries. This represents a particular example from a class of “black-and-white” systems, which was studied in Refs. 19, 6, and 7. Due to the continuity conditions and the absence of scattering in the bulk, the currents in the “black” and “white” phases cannot cross the phase boundary. Instead, the currents have to focus at vertices to pass between the two corners of the same color. The net conductivity tensor depends on the ratio of the average currents flowing in the two phases, which is controlled by  $\bar{\nu}$ . At  $\nu_c - \bar{\nu} \gg \delta\nu_T$ , all saddle points have values of  $\sigma_{xy}$  close to  $\sigma_1$ , which ensures good percolation in the “black” color, so that the white current is relatively small and  $\sigma_{xy}^* \approx \sigma_1$ . At  $\bar{\nu} - \nu_c \gg \delta\nu_T$ , we get good percolation in “white,” and  $\sigma_{xy}^* \approx \sigma_2$ . A crossover takes place within the interval  $\delta\nu_T$ , when both currents are comparable. Since the local diagonal conductivity is small in both quantized regions, the net conductivity  $\sigma_{xx}^*$  is also small when either of these phases percolates freely, and experiences maximum in the crossover region. In the limit of zero dissipation in each of the quantized Hall regions, the dependence of  $\sigma_{xx}^*$  vs  $\sigma_{xy}^*$  of the isotropic two-phase system is known to be a universal function—a semicircle,<sup>7</sup>

$$(\sigma_{xx}^*)^2 + \left( \sigma_{xy}^* - \frac{\sigma_1 + \sigma_2}{2} \right)^2 = \left( \frac{\sigma_1 - \sigma_2}{2} \right)^2. \quad (5)$$

In particular, the maximum value of the average conductivity is

$$\sigma_{xx}^* \text{max} = (\sigma_2 - \sigma_1)/2, \quad (6)$$

independent of the details of the “gray” areas.

To conclude, the long-range inhomogeneities in the infinite sample do not essentially alter the conductivity peak width. They cause the peak height in  $\sigma_{xx}^*$  to saturate at low temperatures at the universal value (6). If the microscopic conductivity tensor components  $\sigma_{xx}, \sigma_{xy}$ , as argued in Refs. 6 and 7, also satisfy the “semicircle” relation (5), then the presence of the macroscopic inhomogeneities has no effect in the low-temperature limit. In a finite sample, however, as we now proceed to show,  $\sigma_{xx}^*$  at  $T=0$  deviates drastically from the universal value, due to the inhomogeneities.

### III. FINITE-SIZE EFFECTS IN THE CORBINO GEOMETRY

To study finite-size effects, we have to resort to a realistic experimental setup, which means that we have to specify the geometry of the sample and the attachment of the contacts. Experiments are performed on the Hall bar, in the van der Pauw method, and on the Corbino disk. Our initial choice will be the Corbino disk, on which recent experiments in Ref. 11 have been performed. In Sec. III, we show how to transfer our results to the Hall bar using the current-voltage duality. We will not discuss the van der Pauw geometry explicitly in this work.

#### A. Contact resistance

A Corbino disk cut from an inhomogeneous sample is shown schematically in Fig. 2(a). The two-terminal resistance between the metal probes attached at the inner and outer circular edges is measured. We consider an ideal contact without any tunnel barriers or dielectric layers between metal and sample, the metal boundary having a constant potential. We assume, first, that the correlation radius of the “gray” cluster  $\xi_T$  is much less than all sample dimensions,  $r_1, r_2$  and  $W \equiv r_2 - r_1$ . In the limit  $\xi_T/W \rightarrow 0$ , the sample can be considered to be homogeneous with the conductivity tensor  $\hat{\sigma}^*$ . The two-terminal resistance is then given by

$$R_0 = \frac{A_0}{\sigma_{xx}^*}, \quad A_0 = \frac{1}{2\pi} \ln \frac{r_2}{r_1}, \quad (7)$$

where  $A_0$  is the geometric aspect ratio, which for  $W \ll r_1, r_2$  is close to  $A_0 \approx W/2\pi r$ . A finite value of  $\xi_T/W$ , as we now demonstrate, leads to an increase in the two-terminal resistance above this value (7), due to an effective contact contribution.

The simplest way to estimate this correction is by monitoring the Joule heat dissipated in the sample. At low temperatures,  $T \ll T_{s1}$ , as already discussed, the currents flow in the (black or white) quantized Hall regions. Since scattering in the bulk is negligible, the currents cannot cross the phase boundaries and, in order to pass through the sample, must focus at vertices formed by adjacent corners of different phases. All the energy dissipation in the system occurs in “hot spots” at the vertices. The vertices are of two kinds: 4-vertices in the sample interior, formed by alternating “black” and “white” corners, and 3-vertices at the boundary, “black-white-metal.” The above resistance (7) corresponds to dissipation at internal vertices, as given by

$$Q_{\text{int}} = I^2 R_0. \quad (8)$$

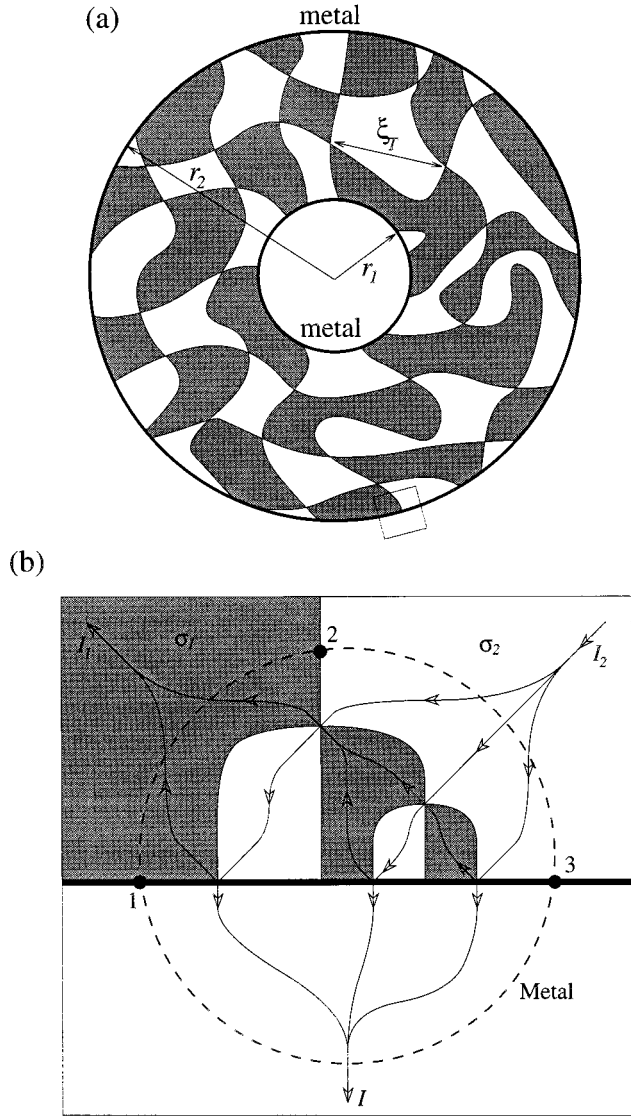


FIG. 2. (a) Conductivity distribution in an inhomogeneous Corbino disk. Black and white are quantized regions as in Fig. 1(c), the intermediate gray region is not shown. (b) Complex “fork vertex” from the small square in (a) shown in magnified view. The arrows schematically show currents passing between different regions by focusing at simple vertices.

Since the metal contact boundary is at a constant potential, the current lines have to focus at 3-vertices, in order to enter the (e.g., inner) contact. This causes additional dissipation at the edge given by

$$Q_{\text{edg}}^{(1)} = \sum_{\alpha} I_{\alpha}^2 R_{\alpha},$$

where  $I_{\alpha}$  is the current passing to the metal at the 3-vertex  $\alpha$ , and  $R_{\alpha}$  is the effective resistance of the vertex.

It turns out that focusing of the current lines occurs only at those of the 3-vertices at which the Hall conductivity  $\sigma_{xy}$  increases from  $\sigma_1$  to  $\sigma_2$  to the right when looking into the sample from the metal (we call these “active” vertices).

For the remaining half of the vertices,  $I_{\alpha} = 0$ . As shown in the Appendix, the resistance of an active 3-vertex is always given by

$$R_{\alpha} = R_3 \equiv \frac{1}{2(\sigma_2 - \sigma_1)}, \quad (9)$$

independent of the microscopic details of the vertex core. In particular, the result remains valid if the phase boundary branches when approaching the metal forming a forklike structure, as illustrated in Fig. 2(b) in magnified view. Branching, though not shown in Fig. 2(a), does occur in a random percolation cluster on scales smaller than  $\xi_T$ . Only the fork vertices, with white as the rightmost color, are active.

For a uniform pattern of white/black regions, the current entering the contact  $I$  will be shared approximately equally between the  $\pi r_1 / \xi_T$  vertices at the edge, so that

$$Q_{\text{edg}}^{(1)} \sim I^2 R_3 \frac{\xi_T}{\pi r_1}. \quad (10)$$

The total two-terminal resistance  $R_{\text{tot}}$  can be found from the total Joule heat,

$$Q_{\text{tot}} = I^2 R_{\text{tot}} = Q_{\text{edg}}^{(1)} + Q_{\text{edg}}^{(2)} + Q_{\text{int}}.$$

Using Eqs. (7)–(10), we find

$$R_{\text{tot}} = \frac{A_0}{\sigma_{xx}^*} + \left( \frac{1}{r_1} + \frac{1}{r_2} \right) \frac{\xi_T}{2\pi(\sigma_2 - \sigma_1)}. \quad (11)$$

The second term in this expression is, of course, an estimate. In the next section, we rederive Eq. (11) rigorously for a simple model of a periodic chessboard two-phase distribution, with  $\xi_T$  replaced by the square size.

Thus, at the maximum of  $\sigma_{xx}^*(\bar{\nu})$ , the relative correction to the peak resistance arising from the edges is of the order of  $\xi_T/W$ . (We assumed here that  $r_1$  is not much less than  $r_2$ , and used the fact that, at the lowest temperatures,  $\sigma_{xx}^{*\text{max}} \sim \sigma_2 - \sigma_1$ .) The experimentally measured value of the diagonal conductivity  $\sigma_{xx}^{\text{exp}}$  defined by<sup>11</sup>

$$\sigma_{xx}^{\text{exp}} = A_0 / R_{\text{tot}}$$

is now lower than the “bulk” conductivity  $\sigma_{xx}^*$  by the same relative amount. This negative correction increases as temperature is lowered, since  $\xi_T$  becomes larger [Eq. (1)]. We believe that the decrease in  $\sigma_{xx}^{\text{exp}}$  that we predict from these considerations provides a possible explanation for the observations of Rokhinson *et al.*<sup>11</sup>

Note that the correction to  $\sigma_{xx}^{\text{exp}}$  may be different for different conductivity peaks, since the width  $\delta\nu_T$  and, hence, the correlation length  $\xi_T$ , may vary from peak to peak. This accounts for the dispersion of traces  $\sigma_{xx}^{\text{max}}(T)$  observed for different peaks in the integer regime, see data for two samples by Rokhinson *et al.*,<sup>11</sup> which we reproduced here in Fig. 3. At the lowest temperatures, however, as one can see from the figure, all the traces converge and tend to collapse onto one curve. The corresponding low-temperature value can be written as  $\sigma_{xx}^{\text{max}} = k e^2 / 2h$ , where the coefficient  $k$  is almost the same for different peaks, but is sample dependent<sup>11</sup> [compare Figs. 3(a) and 3(b)]. As found in the

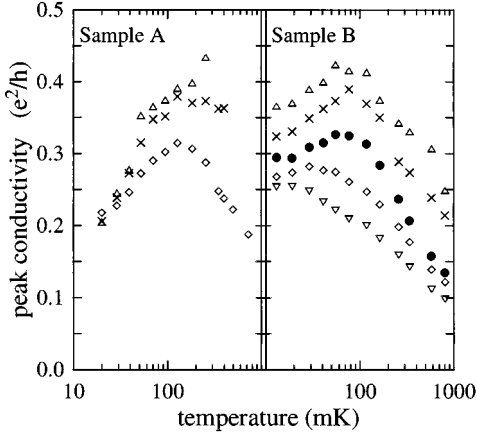


FIG. 3. The temperature dependence of peak values of  $\sigma_{xx}$  for different transitions between adjacent IQHE states obtained by Rokhinson *et al.* in Ref. 11. Different symbols correspond to transitions: 5–6 ( $\nabla$ ), 6–7 ( $\diamond$ ), 7–8 ( $\bullet$ ), 10–11 ( $\times$ ), 13–14 ( $\triangle$ ). Some transitions are omitted by authors of Ref. 11 for sake of clarity. The geometric aspect ratios of the samples are  $A=0.21$  (sample A) and  $A=0.32$  (sample B).

quoted work, the well-pronounced peaks in the fractional regime have the height  $k(\sigma_2 - \sigma_1)/2$ , with approximately the same  $k$  as do the peaks obtained on the same sample in the integer regime. This agrees with earlier data on the fractional quantum Hall effect mostly obtained in the Hall bar geometry,<sup>10</sup> which show that, at the lowest temperatures, most of the peak heights are proportional to the difference in adjacent plateaus in  $\sigma_{xy}$ , with a prefactor that fluctuates from sample to sample. To understand the origin of the curious “universality within one sample,” let us consider the lowest temperatures.

### B. Low-temperature limit

Since the characteristic correlation radius  $\xi_T$  grows as the temperature is reduced, it will eventually become of the same order as the distance between the contacts  $W$  at some temperature  $T \sim T_{s2}$ . At this point, the edge contribution to the resistance in Eq. (11) is as large as the bulk contribution. When temperature is decreased further,  $T \ll T_{s2}$ , a strong inequality  $\xi_T \gg W$  is met for any peak, so that no critical 4-vertices [shown in Fig. 2(a) for higher temperatures] fall within the sample. The current is transported directly from contact to contact by one or more pairs of “white” and “black” clusters connecting the contacts. Black and white clusters of the size  $W$  can exist simultaneously, while  $\bar{\nu}$  is in the interval  $|\bar{\nu} - \nu_c| \leq \delta\nu_w$ , where  $\delta\nu_w$  is determined from the equation

$$W \sim R_c \left( \frac{\delta\nu_0}{\delta\nu_w} \right)^{4/3}. \quad (12)$$

Outside of this interval, percolation between contacts can exist only in one phase, either in the white or in the black. The resistance in this case is equal to that of a homogeneous Corbino sample with no scattering inside, that is,  $R_{\text{tot}} = \infty$ , and  $\sigma_{xx}^{\text{exp}} = 0$ . Hence,  $\delta\nu_w$  in Eq. (12) represents the observed peak width.

Notice that  $\delta\nu_w$  does not depend on temperature and is much larger than the value for the infinite sample  $\delta\nu_T$ . Since no 4-vertices are now found in the sample, the finite value of  $\delta\nu_T$  is no longer relevant. All temperature dependence has now disappeared from the problem and all the peaks  $\sigma_{xx}^{\text{exp}}(\bar{\nu})$  must become identical. We suggest that this explains why the experimental traces  $\sigma_{xx}^{\text{exp}}(T)$  in integer regime converge at low temperatures.<sup>11</sup> Recall that it was the differing values of  $\delta\nu_T$  that caused the contact contributions to the total resistance to vary for different peaks at  $T \gg T_{s2}$ .

This saturation of the peak width, which we predict at low temperatures is similar to the well-known saturation effect, which is expected to occur in small samples when the coherence length  $\xi_c$  becomes comparable to the sample size.<sup>21</sup> The observable difference between the two mechanisms is in the size dependence,  $\delta\nu_w \propto W^{-\kappa}$ : we predict the classical index  $\kappa = 3/4$  instead of the  $3/7$ , which is thought to be appropriate for the quantum problem.<sup>20,21</sup>

We now discuss the height and possible shape of the peak. As we shall show below, in the zero-temperature limit, the two-terminal conductance  $1/R_{\text{tot}}$  can take only quantized values

$$1/R_{\text{tot}} = M(\sigma_2 - \sigma_1), \quad (13)$$

where  $M$  is an integer (including zero) that depends on the specific realization of the disorder. As the average filling fraction is varied, the value of the integer  $M$  may change, and the peak in  $\sigma_{xx}^{\text{exp}}(\bar{\nu})$  can display an unusual steplike dependence on filling fraction, as illustrated schematically in Figs. 4(c) and 4(d). Although the shape of these peaks (number and position of the steps) depends on the specific realization of disorder, this shape is the same, with the peak height expressed in units of  $\sigma_2 - \sigma_1$ , for all peaks in a given sample.

Let us fix the average filling factor  $\bar{\nu}$  somewhere within the peak width  $\delta\nu_w$ , e.g., at the point  $\bar{\nu} = \nu_c$ . We have to distinguish two major cases depending on the random configuration of a sample. Either both black and white percolate in the radial direction, or both black and white percolate in the azimuthal direction, as illustrated in Figs. 4(a) and 4(b). Together with the case in which only one phase percolates in both directions, which we determined above as being outside of the peak width, this exhausts all topological possibilities. In the case of azimuthal percolation, Fig. 4(b), the current can barely pass between contacts, since it is not allowed to cross the phase boundary. Hence, peaks are missing,  $R_{\text{tot}} = \infty$ . More precisely,  $\sigma_{xx}^{\text{exp}}$  is as small as the average of  $\sigma_{xx}$  in the quantized regions, and therefore rapidly vanishes as  $T \rightarrow 0$ . Such behavior is observed in experiment,<sup>25</sup> but it is usually attributed to a “bad sample” or “bad contacts” and, consequently, does not reach publication. In some sense, it is correct to say this in our model as well; however, both “bad” and “good” samples belong to the same statistical ensemble with a quite small amplitude of inhomogeneities. In the case shown in Fig. 4(a), when the contacts are connected by one black and by one white region, the resistance is finite and equal to the doubled resistance of the 3-vertex  $R_{\text{tot}} = 2R_3 = 1/(\sigma_2 - \sigma_1)$ , see Eq. (9) for the 3-vertex resistance.

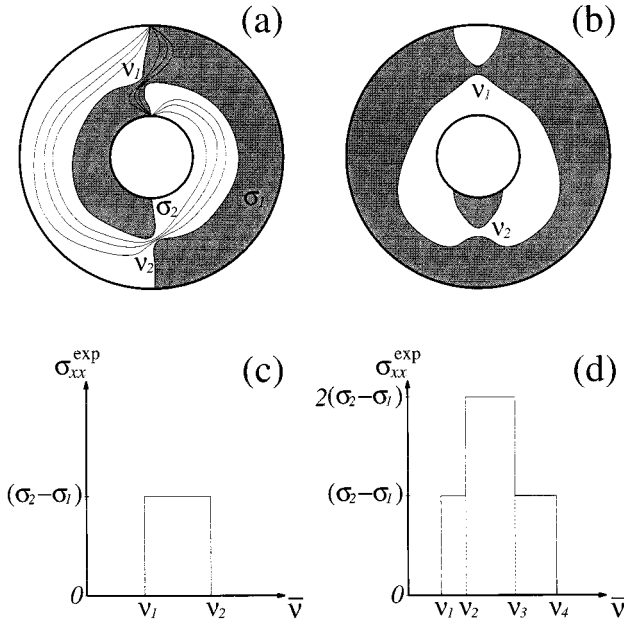


FIG. 4. Two basic configurations of the conductivity distribution in the Corbino disk in the saturation regime ( $T \ll T_{s2}$ ) shown at  $\nu_1 < \bar{\nu} < \nu_2$ , where  $\nu_1$  and  $\nu_2$  are filling factors of the two saddle points. (a) Configuration with a finite two-terminal resistance. Thin lines are the lines of equal potential. (b) Configuration with infinite two-terminal resistance. No current passing between contacts. (c) Predicted observed diagonal conductance  $\sigma_{xx}^{\text{exp}}$  vs average filling factor for configuration (a). (d) Analogous dependence for a configuration controlled by four saddle points.

We can easily obtain the shape of the peak in  $\sigma_{xx}^{\text{exp}}$  for the configuration in Fig. 4(a). Let  $\nu_1$  and  $\nu_2$  be the filling factors at the two saddle points that control the current transfer,  $\nu_2 - \nu_1 \sim \delta\nu_w$ . When  $\bar{\nu}$  is shifted down and crosses the level of the lower saddle-point  $\nu_1$ , the corresponding black bridge becomes white, and percolation in black quits, so that the resistance  $R_{\text{tot}}$  becomes infinite. This transition occurs abruptly in  $\bar{\nu}$  (more precisely, within a small interval  $\sim \delta\nu_T$ ). Similarly, for  $\bar{\nu} > \nu_2$ , the white region percolates, and the system is on a quantized Hall plateau corresponding to  $\nu_2$ . The resulting “peak” in  $\sigma_{xx}^{\text{exp}}$  represents a box of a width  $\nu_2 - \nu_1$ , Fig. 4(c). The latter is of the order of  $\delta\nu_w$  and fluctuates from sample to sample by 100%.

There may, of course, be more than one pair of black and white regions connecting the contacts (and, hence, more saddle points which switch). Since all of the 3-vertices at the same edge are connected in parallel, the inverse resistance is given by Eq. (13), where  $M$  is the number of pairs of connecting regions. In the degenerate case shown in Fig. 4(b),  $M=0$ . Thus, the total conductance of the sample is an integer multiple of  $\sigma_2 - \sigma_1$ . The number of “quanta”  $M$  depends on the value of  $\bar{\nu}$ . A typical shape of the peak for  $M_{\text{max}}=2$  is shown in Fig. 4(d). Each step in  $\sigma_{xx}^{\text{exp}}$  results from the switch of some saddle point from a black to a white bridge. Note that the resistance (13) does not demonstrate regular scaling with the aspect ratio of the sample, since  $M$  is just a random integer varying from sample to sample. The probability distribution for different  $M$  does, however, depend on the shape of the sample. For

instance, if  $r_2 - r_1 \sim r_1$ , the most probable values are  $M=0,1$ , or 2. In a very narrow ring,  $W \ll r$ , the most probable values are close to  $M=C/A_0 \gg 1$ , where  $C$  is some numerical factor. In the latter case, the resistance will seem to scale properly with the sample dimensions, as if the sample was homogeneous, except for the wrong numerical factor. The quantization of  $R_{\text{tot}}$  will be difficult to see.

Our prediction of the *longitudinal* resistance quantization allows a comparison of our theory with the experiments of Ref. 11. Although neither of the two samples shown in Fig. 3 reveals the saturation of the peak heights, which we expect to occur at low enough temperature, still, we can see that the heights of all peaks become close to each other at the lowest temperature studied,  $T=14$  mK. Hence, we assume that saturation occurs not very far below this temperature and use the values of  $\sigma_{xx}^{\text{exp}}$  obtained at 14 K as good approximations to the zero-temperature values. Taking account of the aspect ratios quoted in the caption to Fig. 3, for both samples we obtain  $R_{\text{tot}} = A_0 / \sigma_{xx}^{\text{exp}} \approx h/e^2$  within an accuracy of 10% [we averaged  $\sigma_{xx}^{\text{exp}}(T=0)$  over five values for different peaks in sample B]. This corresponds to  $M=1$  in Eq. (13), which is consistent with our prediction. Thus, at least for these data, the “fluctuation” of  $\sigma_{xx}^{\text{exp}}$  between samples is simply correlated with the different aspect ratios,  $A_0$ , which were used to calculate  $\sigma_{xx}^{\text{exp}} = A_0 / R_{\text{tot}}$ .

#### IV. BOUNDARY-STRIP FORMALISM

So far, we have considered the simplest geometry of the Corbino disk. Although this method can directly produce the value of  $\sigma_{xx}$  for a homogeneous system, it also has some obvious disadvantages. First, it does not allow one to measure the Hall conductivity. Second, it leaves no hope of separating  $\sigma_{xx}^{\text{exp}}$  into the contributions arising from the bulk and those arising from the edge. Both disadvantages stem from the fact that only one independent experimental parameter (the two-terminal resistance) is obtained in this method. To permit a larger number of independent measurements, one must consider another geometry, such as the Hall bar. As we will show in this section, macroscopic inhomogeneities in a finite-sized Hall bar lead to a similar decrease of the observed peak heights in  $\rho_{xx}^{\text{exp}}$ , as for the observed peak heights of  $\sigma_{xx}^{\text{exp}}$  in the Corbino disk geometry. In Sec. V, we will suggest a method by which this edge effect may be compensated in the Hall bar geometry, at least, over the temperature range for which this contribution is small. At the lowest temperatures,  $T \ll T_{s2}$ , as clearly follows from analysis in Sec. III, all information on the bulk properties is lost beyond recovery.

For the remainder of this paper, we will, therefore, focus on the regime of small edge corrections. In this limit, it is possible to develop a theory in which the edge effects can be accounted for by a “boundary strip.” Within this formalism, the Corbino disk and Hall bar are thought of as homogeneous samples with an infinitesimally thin layer attached at their boundaries to account for the edge effects. This boundary strip is characterized by an impedance matrix, which linearly relates the currents in the strip to the potential gradients at the boundary. Effectively, the presence of this strip changes the boundary conditions on the sample. Such an

approach is valid provided (i) the region along the edge responsible for the edge effects is narrow and (ii) the edges are homogeneous along their length. The first condition is necessary since, otherwise, one has to take into account, in addition to the gradients, second and higher derivatives of the electric potential to describe the boundary impedance. The boundary-strip formalism may be used to calculate the corrections arising from macroscopic inhomogeneities to the conductance of samples, of any geometry, in the regime in which these corrections are small. In the following, we will recover the result derived above (11) that, in the Corbino disk geometry, there is a decrease in the peak heights  $\sigma_{xx}^{\text{exp}}$  compared to a homogeneous sample. Within the boundary-strip formalism, this decrease in conductivity is viewed as arising from additional drops in potential that occur across the boundary strips at the inner and outer contacts. We will further show that, in the Hall bar geometry, the presence of the boundary strips causes additional currents to be trapped at the edges of the samples, and leads to a similar decrease in the observed values of the peak heights of  $\rho_{xx}^{\text{exp}}$ , as compared to a homogeneous sample.

In physical devices, there are two main types of edge effects that are important for transport. First, the finite-size effects due to the macroscopic inhomogeneities of the interior of the sample, as discussed above. This type of inhomogeneity, if present, is equally important for the Hall bar and the Corbino disk. Second, smooth-edge effects caused by a gradual change in the electron density when approaching the sample edge. One should expect the latter effect to be much stronger in the Hall bar geometry in which electron density at the edge is zero. In principle, the boundary-strip formalism is rather general and can be used to account for both types of inhomogeneities. For the macroscopic inhomogeneities, both of the conditions outlined in the previous paragraph are satisfied if the correlation radius  $\xi_T$  is much less than the sample width and, in the Hall bar, the distance between the voltage probes. Both conditions would also be satisfied for a Hall bar with a smooth edge if the voltage probes were small enough as not to affect the edge properties. In real devices, however, the probes are macroscopically large and interrupt the edge strip. Within the model of nonlocal resistance proposed by McEuen *et al.*, based on the edge-state formalism, the contacts have a strong effect on the current distribution, since they force equilibration between different edge channels.<sup>15</sup> Such a model is a clear example of a case in which the edge is not homogeneous along its length, and for which the boundary-strip formalism does not apply. We will, therefore, focus only on cases for which the edge of the Hall bar represents a sharp cut in the inhomogeneous sample, i.e., the characteristic width of the edge region is less than the magnetic length. The boundary properties are then independent of whether the edge is to vacuum (Hall bar) or to metal (Corbino disk). Below we will show how the conductance properties of such an edge can be related to the parameters of the two-phase model. First, we will derive the properties of the boundary strip for a periodic array of the two regions, and then we will discuss how these are modified for a random distribution.

As we have seen in Sec. III, the corners formed at each edge by alternating phases create an effective strip with properties distinct from that of the interior of the sample.

While discussing the Corbino disk, the boundary strip has been characterized by a single parameter, the contact resistance. This is defined as the ratio of the voltage drop across the strip  $V$  to the current  $j_{\perp}L$  crossing the strip, under the condition that the electric field component along the edge  $E_{\parallel}$  is zero. In general, quite different boundary conditions may be applied. For instance, in the standard Hall bar measurement,  $j_{\perp}=0$ ,  $E_{\parallel}\neq 0$ . We need to develop a quantitative description for the boundary strip, which does not depend on specific boundary conditions and which, therefore, applies to all geometries. We consider four variables:  $V, j_{\perp}, E_{\parallel}$ , and the additional current  $I$  flowing along the edge in the boundary strip. The four parameters are related by a boundary impedance matrix  $\hat{\Sigma}$ , as given by

$$\begin{pmatrix} I \\ j_{\perp} \end{pmatrix} = \hat{\Sigma} \begin{pmatrix} E_{\parallel} \\ V \end{pmatrix}, \quad (14)$$

which is analogous to the conductivity tensor in the bulk. Due to the low symmetry of the boundary strip, all four components of  $\hat{\Sigma}$  are *a priori* independent. The whole inhomogeneous sample can be thought of as consisting of a homogeneous interior, with the conductivity tensor of the infinite system  $\hat{\sigma}^*$  and with the same dimensions as the original sample, and an infinitesimally thin boundary strip described by the impedance matrix  $\hat{\Sigma}$ .

We will now determine the boundary impedance matrix for a simplified model: a periodic two-phase system in which black and white are regularly distributed as in a chessboard, and all vertices have identical scattering properties. Since, for a thin boundary strip, the sample shape is not important, we choose to study a convenient geometry, in which the sample is a long rectangle with rows of vertices aligned parallel to its sides. Let the width of the sample be  $W=Nd$ , where  $d$  is the lattice constant, and  $N$  is an integer. A section of a long sample is shown in Fig. 5(a). Although we are ultimately interested in the case of large  $N$ , the periodicity of the problem enables us to use a system with a small number of vertex rows [in Fig. 5(a),  $N=3$ ]. Our objective is to replace this system by an equivalent homogeneous sample with thin boundary strips attached, Fig. 5(b). The system is characterized by the electric field  $\mathbf{E}^{\infty}$  and the current density  $\mathbf{j}^{\infty}$  in the interior, and the four variables  $V, E_{\parallel}, I, j_{\perp}$  describing the boundary strip. The positive directions for the potential drop  $V$  and for the other three variables are shown by arrows in Fig. 5(b). All of these currents and fields are assumed to be uniform, representing one particular case which is sufficient to evaluate matrix (14). We will consider the field  $\mathbf{E}^{\infty}$  and the current density  $\mathbf{j}^{\infty}$  to be given as boundary conditions. Even though these two vectors are related by the conductivity tensor of the infinite system  $\hat{\sigma}^*$ , in what follows, we are not going to use this relation, and will treat  $\mathbf{E}^{\infty}$  and  $\mathbf{j}^{\infty}$  as independent variables.

The criteria for the equivalence of the two systems are as follows. (i) The field  $\mathbf{E}_{\infty}$  and the current density  $\mathbf{j}_{\infty}$  in the sample must be the same as the average electric field and the average current density, which would be in the original sample if the latter was infinite; that is, the properties of the interior are independent of the presence of the boundaries. (ii) The standard continuity conditions  $j_{\perp}=j_y^{\infty}, E_{\parallel}=E_x^{\infty}$  must be satisfied. (iii) The total current along the sample



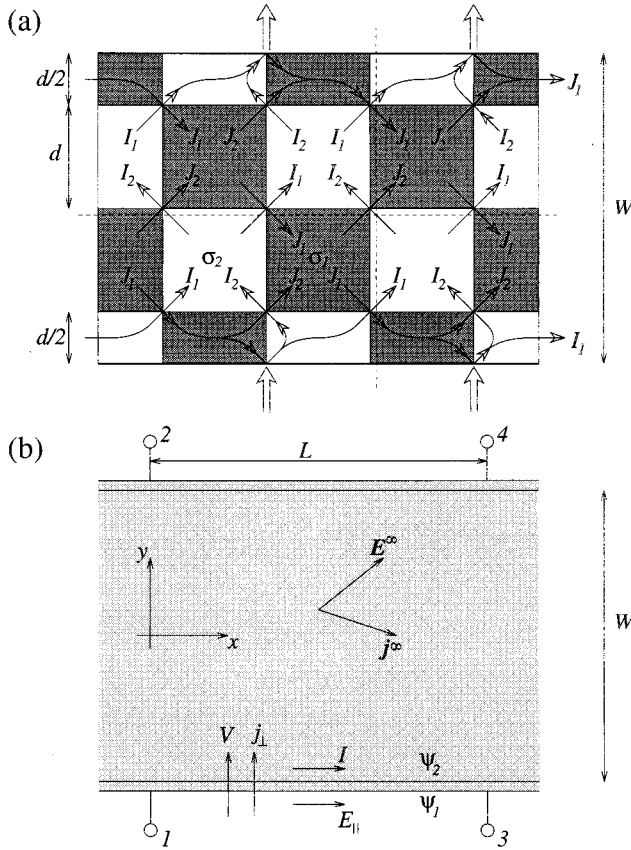


FIG. 5. Diagram illustrating the boundary impedance matrix formalism. (a) Chessboard model of the two-phase distribution in a long rectangular sample. The arrows schematically show currents passing from one (white or black) region to another by focusing at vertices. Wide arrows show currents flowing from (to) metallic contacts. (b) Equivalent sample formed by infinitely thin boundary strips attached to a homogeneous interior of the same width as that of the sample in (a).

$$I_{\text{tot}} = 2I + Wj_x^{\infty} \quad (15)$$

and the total potential drop across the sample

$$V_{\text{tot}} = 2V + WE_y^{\infty} \quad (16)$$

must be the same as the corresponding quantities in the original system.

To apply these rules, consider the current-field distribution in the original system, Fig. 5(a). As shown in Refs. 6 and 7, each 4-vertex is characterized by the white-to-white current  $I_i$  and the black-to-black current  $J_i$ . Each arrow in Fig. 5(a) denotes a set of current lines. When passing through the white or black square, the current spread all over the square, then focuses at a corner where it can pass to another square. We remind the reader that current lines cannot cross the boundaries between quantized regions, so that the specific distribution of these lines inside any square is irrelevant. Each side of a square is at constant potential. The potential drop between the two sides forming a white (or black) corner is given by

$$U_i = \frac{I_i}{\sigma_2} \quad \left( V_i = \frac{J_i}{\sigma_1} \right), \quad (17)$$

where  $I_i$  ( $J_i$ ) is the total current focusing at the corner. Since the system is periodic, and average fields and currents are taken to be uniform, the set of local currents  $I_i, J_i$  must also be periodic. The pair of currents at a vertex takes either of two values,  $I_1, J_1$ , for odd vertices, and  $I_2, J_2$ , for even vertices. The current crosses a sample boundary by focusing at 3-vertices, as shown in Fig. 5(a) for the case  $\sigma_2 > \sigma_1$ . This occurs at every other 3-vertex, since current lines can focus only if  $\sigma_{xy}$  experiences a steplike increase to the right when looking from the edge into the sample (see the Appendix). The splitting of arrows schematically shows the splitting of the sets of current lines. A diagram similar to Fig. 5(a) can be drawn for the equipotential lines, except the notations  $I_i$  and  $J_i$  must be replaced everywhere by  $U_i$  and  $V_i$ , respectively.

The components of the average current density in an infinite sample can be obtained as an average of the corresponding local currents over vertices of the two types, as given by

$$j_x^{\infty} = \frac{I_1 - I_2 + J_1 + J_2}{2d}, \quad (18)$$

$$j_y^{\infty} = \frac{I_1 + I_2 - J_1 + J_2}{2d}. \quad (19)$$

Analogously, for the electric field components, we have

$$E_x^{\infty} = \frac{1}{2d} \left( -\frac{I_1 + I_2}{\sigma_2} + \frac{J_1 - J_2}{\sigma_1} \right), \quad (20)$$

$$E_y^{\infty} = \frac{1}{2d} \left( \frac{I_1 - I_2}{\sigma_2} + \frac{J_1 + J_2}{\sigma_1} \right), \quad (21)$$

where we used Eqs. (17). The total current along the sample  $I_{\text{tot}}$  can be evaluated by adding the local currents crossing the vertical dashed line shown in Fig. 5(a). The result can be written as

$$I_{\text{tot}} = Ndj_x^{\infty} + 2I, \quad (22)$$

$$I = \frac{1}{4}(I_1 + I_2 + J_1 - J_2), \quad (23)$$

where  $j_x^{\infty}$  is given by Eq. (18). The total potential drop across the sample works out to be

$$V_{\text{tot}} = NdE_y^{\infty} + 2V, \quad (24)$$

$$V = \frac{1}{4} \left( \frac{I_1 + I_2}{\sigma_2} + \frac{J_1 - J_2}{\sigma_1} \right), \quad (25)$$

where  $E_y^{\infty}$  is given by Eq. (21). As we can see from condition (iii) [Eqs. (15), (16)], the parameters  $I$  and  $V$  introduced in Eqs. (23) and (25) represent, by definition, the effective current in the strip and the effective voltage drop at the strip, respectively. Notice that the right-hand sides of Eqs. (23), (25) depend only on  $I_1 + I_2$  and  $J_1 - J_2$ . Using the system of Eqs. (19), (20), we can express these two linear combinations in terms of components  $j_y^{\infty}, E_x^{\infty}$ . On the other hand, from condition (ii), we have  $j_y^{\infty} = j_{\perp}$  and  $E_x^{\infty} = E_{\parallel}$ . As a result, we arrive at two equations relating  $I$  and  $V$  to  $j_{\perp}$  and  $E_{\parallel}$ . This can be written in the form (14), with matrix  $\hat{\Sigma}$  given by

$$\hat{\Sigma} = \begin{pmatrix} -\frac{d}{4}(\sigma_2 - \sigma_1) & \frac{1}{2}(\sigma_2 + \sigma_1) \\ -\frac{1}{2}(\sigma_2 + \sigma_1) & \frac{1}{d}(\sigma_2 - \sigma_1) \end{pmatrix}. \quad (26)$$

Note that during this derivation we did not make any particular assumptions about the conductivity tensor in the bulk  $\hat{\sigma}^*$ , since we did not specify components of  $\mathbf{j}^\infty$  and  $\mathbf{E}^\infty$ .

Let us discuss possible modifications of our result for the case in which the two-phase system is random with a correlation radius  $\xi_T$ , Eq. (1). Obviously, the Hall components  $\Sigma_{12}$  and  $\Sigma_{21}$  in Eq. (26) will not change, since they simply reflect the fact that black-and-white phases, in the vicinity of the interplateau crossover, share the edge equally. Then, the diagonal components  $\Sigma_{11}$ ,  $\Sigma_{22}$  have to be proportional to  $\sigma_2 - \sigma_1$ , since they originate from the dissipative resistance of three vertices, Eq. (9). The lattice period  $d$  in the two components  $\Sigma_{11}$ ,  $\Sigma_{22}$  has to be replaced by some average lengths,  $d_1$  and  $d_2$ , respectively, both of the order of  $\xi_T$ . One might expect *a priori* that  $d_1$  and  $d_2$  could differ by a numerical factor, since directions along and across the edge are not equivalent. However, as we show below, both lengths are exactly equal,  $d_1 = d_2 = d$ .

We will employ a duality that exists between the current and field distributions in 2D conductors.<sup>22</sup> Let us imagine that the system in Fig. 5(a) (with many rows of vertices) is randomized, i.e., squares are distorted and vertices are not identical. The currents  $I_i, J_i$  and the voltage drops  $U_i, V_i$  at corners are no longer periodic. Although the system is fully characterized by the discrete set of currents and voltages at the vertices, it will be convenient for now to consider the local current density distribution  $\mathbf{j}(\mathbf{r})$  and the local electric field  $\mathbf{E}(\mathbf{r})$ . Both functions satisfy the continuity conditions that the number of current or potential lines entering and leaving a given (black or white) square are equal. Suppose that we have found the contact impedance matrix in this system which, as explained above, has a form

$$\hat{\Sigma} = \begin{pmatrix} -\frac{d_1}{4}(\sigma_2 - \sigma_1) & \frac{1}{2}(\sigma_2 + \sigma_1) \\ -\frac{1}{2}(\sigma_2 + \sigma_1) & \frac{1}{d_2}(\sigma_2 - \sigma_1) \end{pmatrix}. \quad (27)$$

Let us now map our system onto a primed system with the same geometry of the phase distribution and with the current density and electric field,

$$\mathbf{E}'(\mathbf{r}) = [\hat{z} \times \mathbf{j}(\mathbf{r})], \quad \mathbf{j}'(\mathbf{r}) = [\hat{z} \times \mathbf{E}(\mathbf{r})]. \quad (28)$$

The steady-state conditions,  $\nabla \cdot \mathbf{j}' = 0, \nabla \times \mathbf{E}' = 0$ , are obviously satisfied in the system, if they are satisfied in the original system,  $\nabla \cdot \mathbf{j} = 0, \nabla \times \mathbf{E} = 0$ . As follows from Eqs. (28), the quantized Hall conductivities in the black and white are

$$\sigma'_k = -\rho_k \equiv -1/\sigma_k, \quad k=1,2. \quad (29)$$

The average components  $I, V, j_\perp, E_\parallel$  characterizing the boundary strip are transformed in the same way as the components of the local current and electric field in Eqs. (28), that is

$$\begin{aligned} V' &= I, & E'_\parallel &= -j_\perp, \\ I' &= -V, & j'_\perp &= E_\parallel. \end{aligned} \quad (30)$$

Since the geometry of the phase distribution in the primed system does not differ from the original one, the variables  $I', j'_\perp$  should be related to  $E'_\parallel, V'$  via the same impedance matrix  $\hat{\Sigma}$  given in Eq. (27), except  $\sigma_k$  should now be replaced by  $\sigma'_k$ . Using Eqs. (29), (30), we arrive at the relation

$$\begin{pmatrix} E_\parallel \\ V \end{pmatrix} = \hat{P} \begin{pmatrix} I \\ j_\perp \end{pmatrix}, \quad \hat{P} = \begin{pmatrix} \frac{1}{d_2}(\rho_1 - \rho_2) & -\frac{1}{2}(\rho_1 + \rho_2) \\ \frac{1}{2}(\rho_1 + \rho_2) & -\frac{d_1}{4}(\rho_1 - \rho_2) \end{pmatrix}. \quad (31)$$

Comparing Eqs. (14) and (31), we see that  $\hat{P} = \hat{\Sigma}^{-1}$ . As one can easily check, this is only consistent with Eq. (27) if  $d_1 = d_2$ , which proves our assertion that  $d_1 = d_2 = d$  even for a random system.

Thus, the presence of the edge is equivalent to a fictitious homogeneous anisotropic strip of width  $d/2 \sim \xi_T$ , with the local resistivity tensor components,

$$\rho_{yx}^b = -\rho_{xy}^b = (\rho_1 + \rho_2)/2, \quad (32)$$

$$\rho_{xx}^b = -\rho_{yy}^b = (\rho_1 - \rho_2)/2. \quad (33)$$

The unusual fact that the dissipative resistivity in the direction perpendicular to the strip is negative deserves comment. A real physical strip (or a layer if in 3D) with well-defined geometric boundaries cannot have a negative net diagonal resistivity in any direction, since this would contradict the second law of thermodynamics. However, this is not the case here: the effective contact strip in our discussion has no real geometric boundary that could be drawn, for instance, inside of the sample in Fig. 4(a). The strip describes small corrections to the net conducting properties of the sample which, as a whole, has a positive dissipation.

We can now reobtain the contact resistance in the Corbino geometry, say, that from the inner contact  $\Delta R_1$ . Putting  $E_\parallel = 0$ , from Eqs. (14), (26), we have

$$\Delta R_1 = \frac{V}{j_\perp 2\pi r_1} = \frac{d}{2\pi r_1(\sigma_2 - \sigma_1)}, \quad (34)$$

which coincides with the corresponding term in  $R_{\text{tot}}$ , Eq. (11), if one puts  $d = \xi_T$ .

Consider now the standard Hall bar measurement in which the current flows parallel to the edges,  $j_\perp = j_y^\infty = 0$ . Relation (31) taken with  $d_1 = d_2 = d$  yields

$$E_\parallel = \frac{2\rho_{xx}^b}{d} I, \quad V = \rho_{yx}^b I, \quad (35)$$

where  $\rho_{xx}^b$  and  $\rho_{yx}^b$  are given by Eqs. (33) and (32). The electric field in the interior is homogeneous and given by

$$E_x^\infty = E_\parallel = \rho_{xx}^* j_x^\infty, \quad E_y^\infty = \rho_{yx}^* j_x^\infty. \quad (36)$$

where  $\hat{\rho}^* = (\hat{\sigma}^*)^{-1}$  is the resistivity tensor of an infinite sample. Expressions for the experimentally measured components of the resistivity tensor  $\rho_{xx}^{\text{exp}} = WE_\parallel / I_{\text{tot}}$ ,

$\rho_{yx}^{\text{exp}} = V_{\text{tot}}/I_{\text{tot}}$  can easily be obtained from Eqs. (15), (16), (35), and (36). The result has a form

$$\frac{1}{\rho_{xx}^{\text{exp}}} = \frac{I_{\text{tot}}}{WE_{\parallel}} = \frac{1}{\rho_{xx}^*} + \frac{d}{W\rho_{xx}^b}, \quad (37)$$

$$\rho_{yx}^{\text{exp}} = \frac{V_{\text{tot}}}{I_{\text{tot}}} = \rho_{yx}^* - \frac{d\rho_{xx}^*}{W\rho_{xx}^b}(\rho_{yx}^b - \rho_{yx}^*). \quad (38)$$

The last expression was expanded in terms of the small parameter  $d/W$ .

Thus, the presence of the edge leads to a negative correction in the measured  $\rho_{xx}^{\text{exp}}$ , as it did for  $\sigma_{xx}^{\text{exp}}$  in the Corbino geometry. Moreover, if  $\rho_1 - \rho_2 \ll \rho_1$ , the relative magnitudes of both corrections are the same provided that the Corbino disk is narrow and has the same ratio  $d/W$  as the Hall bar. As we have seen above, this fact is related to the current-field duality. Physically, the negative correction to  $\sigma_{xx}^{\text{exp}}$  in the Corbino measurement results from an additional voltage drop at the edge, and the negative correction to  $\rho_{xx}^{\text{exp}}$  in a Hall bar measurement results from an additional current trapped at the edge. Our conclusion agrees with the experimental observation that the peak heights tend to decrease at low temperatures in both geometries.<sup>11,1</sup> The correction to the measured Hall conductivity changes sign in the middle of the crossover region, where  $\rho_{yx} = (\rho_1 + \rho_2)/2$ . As a result, the characteristic width of the transition for both functions  $\rho_{yx}^{\text{exp}}(\bar{v})$  and  $\rho_{xx}^{\text{exp}}(\bar{v})$  is somewhat increased by a relative factor of  $d/W$ .

When calculating the impedance matrix above, we considered the particular case in which the average current density and electric field in the interior of the equivalent sample shown in Fig. 5(b) are homogeneous. In the following section, we will discuss “nonlocal” resistance measurements for which this is not the case. We now discuss the applicability of the boundary-strip approach for an inhomogeneous electric field. Suppose that the electric field in the interior of the equivalent sample  $\mathbf{E}^{\infty}(\mathbf{r})$  varies with some characteristic length  $l_E$ , where  $l_E \gg d$ . Then the four parameters of the boundary strip entering matrix relation (14) will also depend on the coordinate along the edge  $x$ . Let us express the current density in the homogeneous interior in terms of the pseudoscalar  $\psi(\mathbf{r})$ , as given by

$$\mathbf{j}(\mathbf{r}) = [\hat{\mathbf{z}} \times \nabla \psi(\mathbf{r})], \quad (39)$$

which is always possible since  $\nabla \cdot \mathbf{j} = 0$ . Analogously, the electric field can be written in terms of the electric potential as  $\mathbf{E}^{\infty}(\mathbf{r}) = -\nabla \phi(\mathbf{r})$ . At the boundary strip,  $\psi$  experiences a step from  $\psi_1$  to  $\psi_2$ . The current inside the strip  $I$  and the current crossing the strip  $j_{\perp}$  are given by

$$I = \psi_1 - \psi_2, \quad j_{\perp} = \frac{1}{2} \left( \frac{d\psi_1}{dx} + \frac{d\psi_2}{dx} \right). \quad (40)$$

Analogously,  $V$  and  $E_{\parallel}$  are given by

$$V = \phi_1 - \phi_2, \quad E_{\parallel} = -\frac{1}{2} \left( \frac{d\phi_1}{dx} + \frac{d\phi_2}{dx} \right), \quad (41)$$

where  $\phi_1$  and  $\phi_2$  are the potentials at the outer and inner sides of the strip, respectively. Thus, the current across the

strip is defined as the average of the currents crossing the inner and the outer sides of the strip. Since the current along the strip  $I$  depends, in the general case, on the coordinate  $x$ , the two currents may be different. Similarly,  $E_{\parallel}$  is the average of the parallel components of the electric field at the two sides of the strip. Such a choice of the definitions of  $E_{\parallel}$  and  $j_{\perp}$  ensures that all parameters entering the relation (14) are expressed via first derivatives of functions  $\psi$  or  $\phi$ :  $I$  and  $V$  are discrete derivatives (differences) in  $y$ , and  $j_{\perp}$  and  $E_{\parallel}$  are continuous derivatives in  $x$ . As a result, the matrix relation (14) represents the correct description of the conducting properties of the edge to first order in the small parameter  $d/l_E$ . To increase the accuracy to second order, one would have to write a matrix relation, which also includes second derivatives of  $\psi$  and  $\phi$ , such as  $d\psi_1/dx - d\psi_2/dx$ ,  $d^2\psi_1/dx^2 + d^2\psi_2/dx^2$ , etc. In this and the following sections, we restrict ourselves to first-order effects in  $d/l_E$ . We note that the aforementioned equivalence between the effective boundary strip and a homogeneous strip with a resistivity tensor  $\hat{\rho}^b$  is also only correct to first-order in this parameter.

## V. COMPENSATING THE FINITE-SIZE EFFECT: “NONLOCAL” RESISTANCE

The objective of a standard QHE transport experiment performed on a large sample is to extract the bulk conductivity tensor  $\hat{\sigma}^*$  characterizing an infinite system. As we have argued above, at low temperatures comparable to  $T_{s2}$ , finite-size effects become noticeable. It would be very useful to devise a method by which these edge contributions could be separated from the measured resistances. In this section, we show how this may be achieved in systems for which the boundary-strip formalism of Sec. IV applies: that is, for samples with a sharp edge and for which the edge effects are not too large.

As shown in the previous section, at temperatures which are not too low, the edge effect can be described by a matrix  $\hat{\Sigma}$  (or  $\hat{P} = \hat{\Sigma}^{-1}$ ) which, for the two-phase model with a sharp edge, contains a single unknown parameter—the average length  $d \sim \xi_T$ . In order to determine this parameter, one additional measurement beyond the standard measurements of  $R_{xx}$  and  $R_{xy}$  in the Hall bar geometry is required. In what follows, we suggest a way in which  $d$  may be extracted from a measurement of the enhanced “nonlocal” resistance.<sup>13,23</sup>

Unlike the standard Hall bar measurement, for which the current passes along the sample, in a “nonlocal” measurement, the current is forced to cross the sample between probes 1 and 2 on opposite long sides of the sample, Fig. 5(b). The “nonlocal” resistance is determined from the potential difference between a second pair of probes 3 and 4,  $R_{\text{nlloc}} = V_{34}/I_{12}$ . In a homogeneous sample, as follows from standard electrostatic considerations,  $R_{\text{nlloc}}$  should decay with the distance between the current and voltage probes,  $L$ , as given by the series

$$R_{\text{nlloc}} = \rho_{xx}^* (C_1 e^{-\pi L/W} + C_2 e^{-3\pi L/W} + \dots), \quad (42)$$

where  $C_1 \sim C_2 \sim 1$  are numerical coefficients determined by the shape of the contacts. At  $L \gtrsim W$ , the resistance is dominated by the first exponential in this series. As found in Ref.

23, the experimental value of  $R_{\text{nlloc}}$  observed at low temperatures is much larger than that predicted by Eq. (42). This effect clearly indicates the existence of currents localized near the edge, in addition to the current passing in the interior of the sample.

The most common explanation for the enhanced “nonlocal” effect invokes the presence of a smooth edge to the sample, at which the electron density vanishes slowly. This would lead to the appearance of one or more quantized Hall strip(s) at the edge, within which the scattering can be very small, even when the bulk of the sample is in the region of the peak in  $\rho_{xx}$ . The low-dissipative strip can trap a noticeable portion of the current in the sample.<sup>6</sup> In the edge-state transport language, this can be formulated as a poor equilibration between different edge channels: those at the edge of the sample and those in the bulk.<sup>13,24</sup> It is also possible for an enhanced “nonlocal” effect to arise, even when the edge is abrupt, as a result of the random macroscopic inhomogeneities, which we have discussed in previous sections. As we have seen above, the effective boundary-strip traps an additional current  $I$  along the edge, which causes a decrease in the observed  $R_{xx}$ . As we will show in this section, the same edge current causes an enhanced “nonlocal” effect, which can be thought of as an effective increase in the sample width.

We present a simple quantitative theory, which allows one to relate the corrections in  $R_{xx}$  to the enhancement in  $R_{\text{nlloc}}$ . Since our derivation is based on the phenomenological boundary-strip description, this approach is rather general and can be used for a class of the edge models. Moreover, although the edge properties are described by the four components of the matrix  $\hat{\rho}^b$ , which are expected to depend on a specific edge model, the relation between the corrections in  $R_{xx}$  and the enhancement in  $R_{\text{nlloc}}$  turns out to be universal in the sense that it does not include any of these components. The edge corrections to the measured Hall resistance  $R_{yx}$  can be found from the nonlocal effect in the same manner. In this case, however, one has to know the component  $\rho_{yx}^b$  of the boundary-strip matrix.

We begin by deriving the current and potential distributions for a nonlocal measurement on the effective sample shown in Fig. 5(b). To do so, it is convenient to express the current density in terms of a pseudoscalar  $\psi(\mathbf{r})$ , as defined by Eq. (39). Correspondingly, the currents inside and across the strip are given by Eq. (40). The distribution  $\psi(\mathbf{r})$  in the interior of the sample satisfies the Laplace equation

$$\nabla^2 \psi = 0, \quad (43)$$

which follows from the conditions  $\nabla \times \mathbf{E} = 0$ ,  $\rho_{xx}^* \neq 0$ . In addition, the parallel component of the electric field in the interior  $E_x$  and the electric field in the strip  $E_{\parallel}$  must match, as given by

$$\begin{aligned} E_x(y = -W/2) = E_{\parallel}, \quad E_x = \rho_{xx}^* j_x - \rho_{yx}^* j_y, \\ E_{\parallel} = \rho_{xx}^b 2I/d - \rho_{yx}^b j_{\perp}, \end{aligned} \quad (44)$$

where the matrix  $\hat{\rho}^b$  is defined in Eqs. (32), (33). Using Eqs. (39), (40), the last condition can be written as

$$\frac{2}{d} \rho_{xx}^b (\psi_1 - \psi_2) - \frac{\rho_{yx}^b}{2} \frac{d\psi_1}{dx} + \left( \rho_{yx}^* - \frac{\rho_{yx}^b}{2} \right) \frac{\partial \psi_2}{\partial x} + \rho_{xx}^* \frac{\partial \psi_2}{\partial y} = 0, \quad (45)$$

where all partial derivatives are evaluated at the lower edge in Fig. 5(b),  $y = -W/2$ . The matching condition for the upper edge is analogous.

The solution of Eqs. (43), (45) depends on  $\psi_1(x)$ , i.e., on the conditions on the outer boundary of the sample, which are set in the experiment. Let us assume that, in the “nonlocal” resistance measurements, the current  $I_{12}$  enters and leaves the sample at small contacts 1 and 2, which are positioned at  $x=0$ , Fig. 5(a). Then we have  $\psi_1 = I_{12}/2$  at  $x > 0$  and  $\psi_1 = -I_{12}/2$  at  $x < 0$ , with a step at  $x=0$ . We will restrict ourselves to finding  $\psi(\mathbf{r})$  far from the current probes,  $x \gg W$ . In the limit  $x \rightarrow \infty$ , all currents vanish so that  $\psi_2 \rightarrow \psi_1$ . We will look for an asymptotic solution of Eqs. (43), (45) in the form

$$\psi(\mathbf{r}) = I_{12}/2 + C \cos(ky) e^{-kx}, \quad (46)$$

which is symmetric about  $y=0$  and satisfies Eq. (43). Substituting this ansatz and  $d\psi_1/dx=0$  into (45), we obtain the following equation for the decrement  $k$ ,

$$\tan\left(\frac{kW}{2}\right) = \frac{2\rho_{xx}^b}{kd\rho_{xx}^*} + \frac{\rho_{yx}^* - \rho_{yx}^b/2}{\rho_{xx}^*}. \quad (47)$$

We have to choose the smallest solution of this last equation, which tends to  $\pi/W$  as  $d/W \rightarrow 0$ . To first order in  $d/W$ , we obtain

$$k = \frac{\pi}{W_{\text{eff}}}, \quad W_{\text{eff}} = W + d \frac{\rho_{xx}^*}{\rho_{xx}^b}. \quad (48)$$

Clearly, the voltage between probes 3, 4 decays with the distance  $L$  in the same exponential way as the current density, such that  $R_{\text{nlloc}} \propto \exp(-\pi L/W_{\text{eff}})$ . Thus, as far as nonlocal resistance measurements are concerned, macroscopic inhomogeneities make the sample effectively wider. In the region of the peak in  $\rho_{xx}^*(\bar{v})$ , where  $\rho_{xx}^* \sim \rho_{xx}^b$ , the effective width increases by of order the correlation radius  $\xi_T$ .

Notice that the formula (37) for the measured diagonal resistivity can now be rewritten as

$$\rho_{xx}^* = \rho_{xx}^{\text{exp}} \frac{W_{\text{eff}}}{W}, \quad (49)$$

which means that effect of inhomogeneities on the “local” resistance can be thought of as the same increase in the sample width:  $R_{xx} = \rho_{xx}^{\text{exp}} L/W = \rho_{xx}^* L/W_{\text{eff}}$ . This immediately gives a simple method by which the edge contribution to  $\hat{\rho}^{\text{exp}}$  can be eliminated to first order in  $d/W$ . First one must measure the “nonlocal” resistance  $R_{\text{nlloc}}$  with two pairs of voltage probes situated at different distances  $L_1, L_2$  (larger than  $W$ ) from the current probes. The effective width can be calculated as

$$W_{\text{eff}} = \pi(L_2 - L_1) \ln^{-1} \left[ \frac{R_{\text{nlloc}}(L_1)}{R_{\text{nlloc}}(L_2)} \right]. \quad (50)$$

Combined with a knowledge of the geometric sample width  $W$ , this can then be substituted in Eq. (49) to obtain  $\rho_{xx}^*$ . (Since precise measurements of the geometric width of the sample  $W$  may present some difficulties in experiment, one may determine it in the same way as  $W_{\text{eff}}$ , but at  $B=0$  when weak inhomogeneities are not important.) Using the same method, we can extract the bulk value of the Hall resistivity  $\rho_{yx}^*$  from observed Hall resistance  $R_{yx} = \rho_{yx}^{\text{exp}}$ . From Eqs. (48), (38), we get

$$\rho_{yx}^* = \rho_{yx}^{\text{exp}} + (\rho_{yx}^{\text{exp}} - \rho_{yx}^b) \left( \frac{W_{\text{eff}}}{W} - 1 \right). \quad (51)$$

It is worth emphasizing that when deriving expressions (49)–(51), we did not use any particular values for the components of the boundary-strip matrix  $\hat{\rho}^b$ . This means that the method of compensating the edge effect that we have just suggested is rather general and is not restricted to the black-and-white regime,  $T \ll T_{s1}$ , studied in Secs. III and IV. For instance, the method can be applied just as well at higher temperatures,  $T \gtrsim T_{s1}$ , when a significant part of the current is carried by the intermediate “gray” region in Fig. 1(c). This seems to be the case in experimental data shown in Fig. 3 at high temperatures when  $\sigma_{xx}^{\text{exp}}$  decreases with increasing  $T$ . Relation (49) used to compensate the edge effect in the diagonal resistivity is quite universal in the sense that it does not depend on any components of the boundary-strip matrix. In order to exclude the edge effect from the Hall resistivity using Eq. (51), one has to know the specific value of  $\rho_{yx}^b$ . We note, however, that the value  $\rho_{yx}^b = (\rho_1 + \rho_2)/2$  is more general than its derivation based on the black-and-white model that we gave in Sec. IV. It merely reflects the symmetry of the local Hall resistivity distribution  $\rho_{yx}(\mathbf{r})$  with respect to  $(\rho_1 + \rho_2)/2$ , which is conserved as long as the sample is effectively very inhomogeneous, i.e.,  $\delta\nu_T \ll \delta\nu_0$ .

We emphasize again that this method applies only to first order in  $d/W$ . It yields a partial compensation of the edge effect at  $T \gtrsim T_{s2}$ , and is useless at  $T \ll T_{s2}$  when all measured parameters have already saturated in temperature.

Our conclusions are easy to test experimentally. If the underlying model is appropriate in a particular sample, the application of this method should produce a wide range in the temperature dependence of  $\sigma_{xx}^{\text{max}}(T)$  within which the diagrams  $\sigma_{xx}$  vs  $\sigma_{xy}$  are close to the “universal semicircle.” In other words, by compensating the edge effects, the maxima in temperature like those shown in Fig. 3 can be broadened and brought much closer to  $0.5e^2/h$ . At the lowest temperatures, when the finite-size effects dominate the transport properties (the “saturation” regime), the method eventually breaks down and no universality can be retrieved. In fact, such a behavior close to the universal prediction was already observed, without any special methods, in the integer regime in the temperature ranges  $T = (0.5 - 2)$  K [Ref. 1(a)], and  $T = (2 - 4)$  K (Ref. 25). In these low-mobility samples, the high-temperature decrease of the peak heights starts late when the size effects are already small.

## VI. CONCLUSIONS

We have shown that low-temperature measurements of the quantum Hall effect in inter-plateau regions are very sen-

sitive to even weak macroscopic density inhomogeneities in the sample. The inhomogeneities may result in strong finite-size effects even in samples which, from a conventional point of view, are very large. This may be a reason why the predicted universal behavior of the transition regions in an infinite macroscopically homogeneous system is so hard to observe experimentally. Within our model of macroscopic inhomogeneities, we were able to account for both the decrease of the conductivity peak heights at low temperatures and the curious “nonuniversal” scaling of the peak heights revealed in some samples. In the low-temperature limit, the experimentally observed peaks in  $\sigma_{xx}$  in the Corbino geometry are shown to saturate at values proportional to the differences between adjacent plateaus in  $\sigma_{xy}$ . (Analogously, the peaks in  $\rho_{xx}$  observed in the Hall bar should be proportional to differences in  $\rho_{xy}$ .) The proportionality factor depends on the specific realization of disorder and fluctuates strongly between samples. The model also predicts unusual peak shapes, which show quantized plateaus in the *longitudinal* conductivity. The experimental peak heights obtained in Ref. 11 at the lowest temperatures are consistent with this quantization.

Finally, we also showed that for a Hall bar with a sharp edge, there exist simple relations between the enhanced non-local resistance and the size corrections in  $R_{xx}$  and  $R_{xy}$  when these corrections are small. These relations can be used to separate the edge effects from the bulk tensor components  $\rho_{xx}^*$  and  $\rho_{xy}^*$ .

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## APPENDIX: EFFECTIVE RESISTANCE OF A FORK VERTEX

In this appendix, we calculate the effective resistance  $R_3$  of a fork vertex, a relatively simple example of which is shown in Fig. 2(b). The current distribution in the vertex is shown by the arrows that denote beams of current lines. The beams split and focus at “simple” 3-vertices and 4-vertices, which form the fork vertex. (Recall that, since the longitudinal conductivity is assumed to be vanishingly small in black and white regions, the current lines cannot cross the border between phases or the metal boundary other than at these simple vertices.) The effective resistance  $R_3$  can be found from the net Joule heat  $Q = R_3 I^2$ , where  $I$  is the net current entering the metal contact. Although the problem would appear quite complex, it turns out that the dissipated heat does not depend on the specific structure of the vertex. We will now show this from very general arguments.

Let us draw an imaginary circle [the dashed line in Fig.

2(b)] enclosing all of the structure of the vertex. Consider the total currents  $I_1$ ,  $I_2$ , and  $I$  crossing this circle in the black, white, and metallic areas, respectively. From the current continuity condition,  $I=I_2-I_1$ , and from the condition that electric potentials at points 1, 3 of the metal boundary must be equal,  $I_1/\sigma_1=I_2/\sigma_2$ , we find

$$I_1 = \frac{\sigma_1}{\sigma_2 - \sigma_1} I, \quad I_2 = \frac{\sigma_2}{\sigma_2 - \sigma_1} I, \quad (\text{A1})$$

that is, only one of the three currents is an independent quantity.

The total Joule heat inside of the circle is determined by the general expression

$$Q = \int \mathbf{E}(\mathbf{r}) \mathbf{j}(\mathbf{r}) d^2 r, \quad (\text{A2})$$

where  $\mathbf{E}(\mathbf{r})$  and  $\mathbf{j}(\mathbf{r})$  are the local electric field and the local current density, respectively, at point  $\mathbf{r}$  inside of the circle. Since  $\nabla \cdot \mathbf{j} = 0, \nabla \times \mathbf{E} = 0$ , we can express  $\mathbf{j}$  in terms of the pseudoscalar  $\psi$ , and  $\mathbf{E}$  in terms of the electric potential  $\phi$ , as given by

$$\mathbf{j}(\mathbf{r}) = [\hat{z} \times \nabla \psi(\mathbf{r})], \quad \mathbf{E}(\mathbf{r}) = -\nabla \phi(\mathbf{r}). \quad (\text{A3})$$

In this notation, the three currents  $I, I_1, I_2$  can be written as

$$I = \psi_1 - \psi_3, \quad I_1 = \psi_2 - \psi_1, \quad I_2 = \psi_2 - \psi_3. \quad (\text{A4})$$

Substituting Eqs. (A3) into (A2), changing order in the mixed product, and integrating by parts, we get

$$Q = - \int \psi (\nabla \phi \cdot d\mathbf{l}), \quad (\text{A5})$$

where the integral is taken along the closed circle in Fig. 2(b). The circle can be broken into three segments: 3-2, 2-1, and 1-3. Within each of the segments, we have  $\nabla \phi = (1/\sigma_i) \nabla \psi$ , where the Hall conductivity  $\sigma_i$  is equal to  $\sigma_2, \sigma_1$ , and  $\infty$  (metal), respectively. Integration within separate segments yields

$$Q = - \frac{1}{2\sigma_2} (\psi_2^2 - \psi_3^2) - \frac{1}{2\sigma_1} (\psi_1^2 - \psi_2^2). \quad (\text{A6})$$

Using Eqs. (A1) and (A4), we obtain, finally,

$$Q = \frac{I^2}{2(\sigma_2 - \sigma_1)} \equiv R_3 I^2, \quad (\text{A7})$$

which yields the formula (9) quoted in the main text.

Note, that if the colors in Fig. 2(b) are interchanged, which corresponds to interchanging  $\sigma_2$  and  $\sigma_1$  in Eq. (A7), the Joule heat will be negative (recall that we assume  $\sigma_2 > \sigma_1$  everywhere in the paper). Since this would contradict the second law of thermodynamics, for such a vertex, all currents must be zero. Hence, only the vertices for which the rightmost color, as shown in Fig. 2(b), is white, can be ‘‘active’’ (can participate in the current transfer).

To illustrate our result (9), consider the simplest (without branching) example of a 3-vertex presented by a corner of a rectangular homogeneous conductor with the Hall conductivity  $\sigma_2$ . Two metallic probes are attached at the bottom and at the top of the rectangle, the sample on the left and on the right bordering to vacuum,  $\sigma_1 = 0$ . If  $\sigma_2 > 0$ , the current will leave and enter metallic probes focusing at the lower left and the upper right corners of the sample, which represent the active 3-vertices. The two-terminal resistance of such a sample is equal, as is easy to see, to the inverse Hall conductivity  $1/\sigma_2$ . This amounts to the effective resistance  $R_3 = 1/2\sigma_2$  per each active 3-vertex, in agreement with Eq. (9).

As is easy to check, the same rule of selection of active vertices applies if the metal in Fig. 2(b) is replaced by a vacuum, as is appropriate for a Hall bar with an abrupt edge (Sec. IV). In contrast to the edge-to-metal discussed above, we now have zero current out of the edge,  $I = 0$ , and a non-zero voltage difference  $V = \phi_3 - \phi_1$ . The expression for the Joule heat  $Q$  can be obtained in almost the same manner as Eq. (A5), except it is now convenient to use, instead of Eq. (A9), an equivalent formula

$$Q = \int \phi (\nabla \psi \cdot d\mathbf{l}). \quad (\text{A8})$$

The final answer has the form

$$Q = \frac{V^2}{2(\sigma_1^{-1} - \sigma_2^{-1})}, \quad (\text{A9})$$

which has the same sign as the right-hand side of Eq. (A7).

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