

## SiO<sub>2</sub> precipitation in highly supersaturated oxygen-implanted single-crystal silicon

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An extended transmission-electron-microscopy investigation of oxygen-implanted silicon has been carried out and has given evidence for a new precipitation mechanism. This mechanism is related to SiO<sub>2</sub> precipitation of free oxygen involved in dense and hot collisional cascades and produces the largest precipitates in the region where oxygen concentration is still high but primary events originating the collisional cascades are no longer sufficient to guarantee the spatial covering of the silicon. This mechanism prevails at relatively low fluence, while at high fluence the conventional precipitation dominates; in the present experimental conditions (energy = 100 keV, target temperature ≈ 250 °C) the oxygen fluence separating these two behaviors is in the interval  $1 \times 10^{16} - 1 \times 10^{17} \text{ cm}^{-2}$ .

### I. INTRODUCTION

Despite the fact that silicon is one of the most studied substances and oxygen is its major contaminant, relatively little is known of the Si:O system, especially at high oxygen concentration ( $> 2 \times 10^{18} \text{ cm}^{-3}$ ) and temperature below 600 °C.

Single-crystal silicon is usually prepared by Czochralski (CZ) or float zone (FZ) techniques, with typical oxygen concentrations  $C$  of the order of  $10^{18} \text{ cm}^{-3}$  and  $10^{16} \text{ cm}^{-3}$ , respectively.<sup>1</sup> Oxygen in CZ silicon comes from SiO production at the Si(melt)-SiO<sub>2</sub> (crucible) interface and incorporation in the melt, and from preferential oxygen segregation in the crystal at the moving Si(crystal)-Si(liquid) interface.

Oxygen in silicon is known to be a covalently bonded interstitial; in this form (a two-dimensional rationalization is shown in Fig. 1) it is electrically inactive.

The diffusion of covalently bonded interstitial oxygen O<sub>i</sub> in the temperature interval 350–1250 °C is an activated process with diffusion coefficient  $D$  given by

$$D(T) = D_0 \exp(-E^*/k_B T), \quad (1)$$

where  $T$  is the absolute temperature,  $k_B$  is the Boltzmann constant,  $D_0 = 0.13 \text{ cm}^2/\text{s}$ , and  $E^* = 2.53 \text{ eV}$ .<sup>2</sup> Anomalous fast diffusing oxygen has hitherto been observed in two situations: in high fluence, ion-implanted silicon,<sup>3–6</sup> where it is believed to be in the form of molecular oxygen O<sub>2</sub> obtained after heat treatments at moderate temperature,<sup>7</sup> and in silicon exposed to atomic hydrogen, where

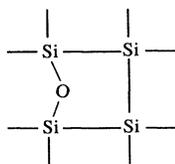


FIG. 1. Two-dimensional rationalization of covalently bonded interstitial oxygen in silicon.

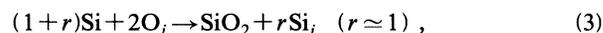
oxygen diffusivity is presumably related to OH groups.<sup>8</sup>

The solubility  $C^{\text{sol}}$  of oxygen in silicon can be described by the formula

$$C^{\text{sol}}(T) = C_0^{\text{sol}} \exp(-\Delta E/k_B T), \quad (2)$$

where  $C_0^{\text{sol}} = 9 \times 10^{22} \text{ cm}^{-3}$  and  $\Delta E = 1.52 \text{ eV}$ . Equation (2) is accurate within a factor of 2 in the range 800–1400 °C; all experimental data can be collected in an Arrhenius plot within two straight lines with slope 1.26 and 1.80 eV.<sup>2</sup>

Since oxygen concentration in CZ silicon generally exceeds the solid solubility up to almost the melting point, oxygen can separate as SiO<sub>2</sub> provided that the duration of the thermal process is long enough to allow the formation of SiO<sub>2</sub> precipitates. Since SiO<sub>2</sub> has a molar volume approximately twice that of silicon, inner silicon oxidation takes place with the injection of self-interstitials Si<sub>i</sub>,



provided that the crystal elastic energy associated with the stress generated by the SiO<sub>2</sub> precipitate exceeds the formation energy of the self-interstitial (Ref. 9, Ch. 3).

The electrical activity of oxygen is manifested by the formation of thermal donors, which are complexes involving four or more oxygen atoms formed after prolonged annealing at 500 °C with a rate faster than that permitted by standard oxygen diffusivity (though the formation-destruction kinetics are well characterized experimentally,<sup>10</sup> the microscopic structure of the thermal donor is, as discussed extensively by Bourret,<sup>11</sup> a problem not solved yet) and new thermal donors, which are oxygen complexes involving carbon formed after annealing at higher temperature;<sup>10</sup> oxygen is also suspected<sup>12</sup> to be responsible for the electron-hole pure generation phenomena discovered by Cerofolini and Polignano.<sup>13,14</sup>

There is a wide body of experimental knowledge of the structures formed after annealing of moderately supersaturated CZ silicon; as the annealing temperature  $T$  increases, the following complexes are known to be formed: vacancy-oxygen complexes (for  $T = 200 - 400$  °C), thermal

donors (around  $T=500^\circ\text{C}$ ), new thermal donors (for  $T=600\text{--}900^\circ\text{C}$ ), platelets (for  $T=950\text{--}1050^\circ\text{C}$ ), and eventually polyhedral SiO<sub>2</sub> precipitates (for  $T\gtrsim 1100^\circ\text{C}$ ).<sup>15,16</sup>

By far less known are the silicon-oxygen complexes formed in highly supersaturated silicon ( $C > 10^{19}\text{ cm}^{-3}$ ). A way to explore which metastable structures are formed in this concentration domain is to insert the wanted amount of oxygen in the silicon crystal at low temperature and to study the evolution of the system after isothermal heat treatments. The most practical way to insert amounts of oxygen producing local concentrations in the range  $10^{19}\text{--}10^{22}\text{ cm}^{-3}$  in the crystal is ion implantation at fluences  $\Phi$  in the range  $10^{15}\text{--}10^{18}\text{ cm}^{-2}$  at a temperature high enough to allow an appreciable reconstruction of the crystal, but not so high as to produce a large oxygen redistribution. A target temperature in the range  $100\text{--}500^\circ\text{C}$  satisfies both these conditions.

## II. EXPERIMENT

### A. Sample preparation

Oxygen was implanted into single-crystal silicon by an Eaton NV-4206 medium-current ion implanter at an energy  $E=100\text{ keV}$  and fluence in the range  $\Phi=1\times 10^{15}\text{--}1\times 10^{17}\text{ cm}^{-2}$ . The target was formed by CZ-grown,  $n$ -type,  $7\text{--}10\text{-}\Omega\text{ cm}$  resistivity, (100)-oriented, silicon slices of thickness  $525\text{ }\mu\text{m}$  and diameter  $10\text{ cm}$ . The silicon slices were tilted  $7^\circ$  or  $15^\circ$  with respect to the beam to minimize channeling effects. The typical current density was  $100\text{ }\mu\text{A}/\text{cm}^2$  with a rastered beam of area around  $1\text{ cm}^2$  covering the whole silicon area.

Unless otherwise stated, the data refer to samples obtained by implanting slices in poor thermal contact with the wafer holder. In this situation the temperature increased during the implantation, ranging from room temperature at  $\Phi=0$  to around  $150^\circ\text{C}$  at  $\Phi\approx 1\times 10^{15}\text{ cm}^{-2}$ , eventually reaching approximately  $250^\circ\text{C}$  for  $\Phi\gtrsim 2\times 10^{15}\text{ cm}^{-2}$ . This means that in all experiments with  $\Phi > 5\times 10^{15}\text{ cm}^{-2}$  most of the implantation was carried out in isothermal conditions at  $T\approx 250^\circ\text{C}$ . In a few cases, care was taken to improve the thermal contact (by means of a conductive glue) and the wafer temperature was kept very close to  $77\text{ K}$  by cooling the wafer holder with liquid nitrogen. Thermal cycles formed by isothermal steps were carried out in an inert atmosphere<sup>17</sup> in the temperature range  $450\text{--}1200^\circ\text{C}$ , for a typical duration (8 h) much longer than the time required to ramp-up or ramp-down the furnace.

### B. Analytical tools

The analyses of as-implanted and annealed samples were carried out by secondary-ion-mass spectrometry (SIMS) and transmission electron microscopy (TEM) in plan or cross-section views, in diffraction contrast or high-resolution (HREM) modes.

### 1. SIMS

The oxygen measurements were performed using a Cameca ims-4f ion microprobe equipped with cesium primary ion source. In order to avoid having to consider the artifacts produced by oxygen adsorption on the surface and by the knock-on effect, we limited our analysis to the depth region  $x=50\text{--}400\text{ nm}$  around the maximum of oxygen concentration.

### 2. TEM

The microscopic analysis was carried out in diffraction contrast, weak beam and HREM modes with a JEOL 2010 transmission electron microscope with a resolution limit of  $0.23\text{ nm}$ , thus allowing the silicon crystal lattice to be imaged along the  $\langle 110 \rangle$  direction. Observations were performed in plan view to give evidence for, and when possible to measure the density of, SiO<sub>2</sub> precipitates and lattice defects, and in the cross-section view to allow relevant thicknesses and depths to be determined.

## III. EXPERIMENTAL RESULTS

In relation to the behavior of the implanted samples after annealing, it is convenient to describe separately the samples implanted in the “low-fluence” regime and in the “high-fluence” regime. It is anticipated that the behavior of SiO<sub>2</sub> precipitates in these two regimes is that sketched in Fig. 2. In this sketch two important depths are emphasized:  $x_{\text{max}}$ , the depth of maximum oxygen concentration, at which homogeneous precipitation takes place; and a depth  $x_{\ddagger}(\Phi)$ , at which “etherogeneous” precipitation takes place at fluence  $\Phi$ . With etherogeneous precipitation we mean a kind of heterogeneous precipitation on preferential sites produced temporarily during the implantation itself (the *hot clouds* of Sec. IV). With the low-fluence regime we denote the fluence domain for which homogeneous SiO<sub>2</sub> precipitates are unstable and disappear after suitable annealing; with the high-fluence regime we denote the opposite situation.

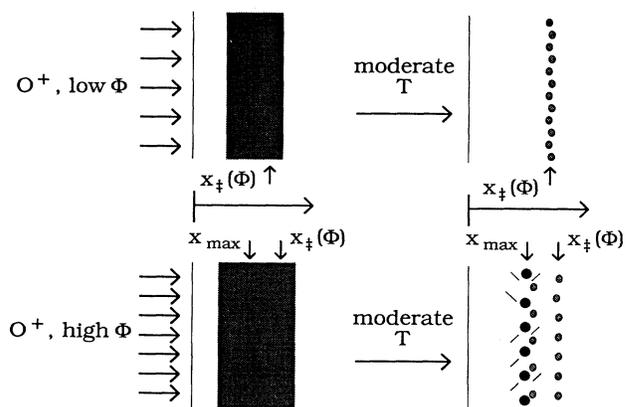


FIG. 2. Schematic behavior of SiO<sub>2</sub> precipitation in (a) low-fluence and (b) high-fluence samples.

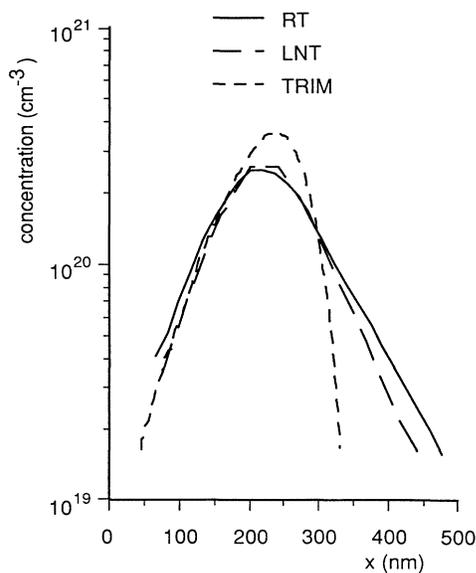


FIG. 3. Oxygen profiles in samples implanted at room temperature (RT) and liquid-nitrogen temperature (LNT) are compared with TRIM simulation. The LNT sample was stored at room temperature before SIMS analysis.

#### A. Low-fluence samples

The following considerations apply to samples implanted at floating temperature. For a comparison a sample was implanted at liquid-nitrogen temperature, with  $E=100$  keV and  $\Phi=5\times 10^{15}$  cm $^{-2}$ ; this implantation produced a continuous amorphous layer centered on a depth of 205 nm with a thickness of 160 nm.

##### 1. Oxygen profiles

Oxygen profiles of the samples implanted at  $\Phi=5\times 10^{15}$  cm $^{-2}$  at floating temperature and at liquid-nitrogen temperature are presented in Fig. 3 together with the expected profile [obtained by transport of ions in

matter (TRIM) simulation<sup>18</sup>] in an amorphous target. The oxygen profiles of samples implanted at lower fluence,  $1\times 10^{15}$  cm $^{-2}$  and  $2\times 10^{15}$  cm $^{-2}$ , were also determined and were found to scale linearly from that of the sample implanted at  $5\times 10^{15}$  cm $^{-2}$ .

##### 2. SiO<sub>2</sub> precipitates

We shall refer to oxygen-related complexes, produced either during the implantation itself or after subsequent annealing, as SiO<sub>2</sub> precipitates without pretending that the fully stoichiometric compound is actually synthesized. Figure 4 shows the in-depth evolution after annealing of the damaged region in the sample implanted at  $\Phi=5\times 10^{15}$  cm $^{-2}$ . From the comparison of the various photographs it is immediately realized that the damaged region is centered on the depth  $x_{\max}$  of maximum oxygen concentration ( $x\approx 220$  nm) with a thickness  $\Delta x\approx 230$  nm in the as-implanted sample, and is shifted to a depth  $x_{\dagger}\approx 290$  nm after annealing at  $T\geq 650$  °C. The width of the damaged region is reduced with the annealing temperature, eventually reaching the value  $\Delta x\approx 60$  nm after heating at 1200 °C.

The amount per unit area of SiO<sub>2</sub> precipitates was determined by plan-view analysis. For instance, Fig. 5 shows a plan view of the damaged region after annealing at 650 °C; the amount of SiO<sub>2</sub> precipitates contained in this sample is around  $3\times 10^{11}$  cm $^{-2}$ , the average diameter being  $(6\pm 1)$  nm, thus showing that practically all the contained oxygen is separated as SiO<sub>2</sub>.

##### 3. Silicon defects

Together with SiO<sub>2</sub> precipitates, other extended defects are also found, namely: {113} stacking faults (which are known to be produced during the implantation and to survive up to 750 °C), {100} defects, {111} stacking faults (observed after annealing at  $T\geq 750$  °C), and dislocations (produced after annealing at  $T\geq 750$  °C). The amounts of silicon atoms involved in {113}, {100}, and {111} extended defects are reported in Table I. This table is fully consistent with the interpretation for which {113} stack-

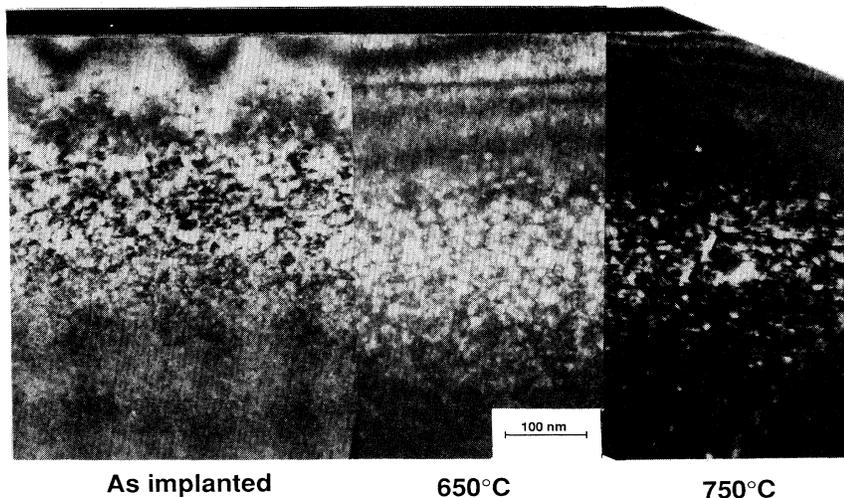


FIG. 4. Cross-section views of the implanted region in as-implanted and annealed samples;  $\Phi=5\times 10^{15}$  cm $^{-2}$ ,  $E=100$  keV.

TABLE I. Defect amount per unit area  $n_{\square}$  and average length  $L$  in specimens implanted at  $\Phi = 5 \times 10^{15} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$ , in the as-implanted condition and after heat treatments. The asterisk indicates an estimated error of 50%. The dagger indicates uncertainty due mainly to the presence of a strong strain field and defect overlapping.

		As-implanted	650 °C	750 °C
{113} stacking faults	$n_{\square} (\text{cm}^{-2})$	$4 \times 10^{12}$	$5 \times 10^{12}$	$\approx 10^{12*}$
	$L (\text{nm})$	5	10	8–10
{100} defects	$n_{\square} (\text{cm}^{-2})$	$\approx 10^{11\dagger}$	$6 \times 10^{11}$	$1 \times 10^{12}$
	$L (\text{nm})$	5	10	10–80
{111} stacking faults	$n_{\square} (\text{cm}^{-2})$			$1.5 \times 10^{10}$
	$L (\text{nm})$			10

ing faults evolve after annealing eventually forming {100} defects.<sup>19</sup>

### B. High-fluence samples

The characterization of high-fluence samples is much less quantitative, essentially due to SiO<sub>2</sub> precipitates and

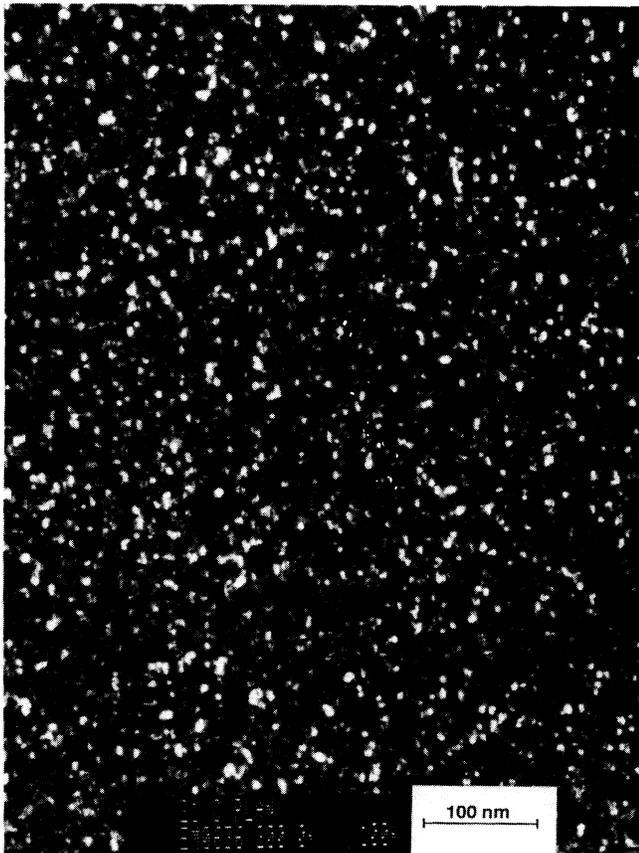


FIG. 5. Plan view of the implanted region in the sample implanted at  $\Phi = 5 \times 10^{15} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$  and annealed at 650 °C.

silicon extended defects which are so numerous as to make impossible their density calculation (see, for instance, Fig. 6). However, the following conclusions can be drawn.

#### 1. Oxygen profiles

The oxygen profiles in as-implanted samples do not show large deviations from that observed at low fluence up to  $\Phi = 1 \times 10^{17} \text{ cm}^{-2}$ , thus showing that phenomena such as swelling, change of stopping power, sputtering, etc., though existing, are not very important yet.

#### 2. SiO<sub>2</sub> precipitates

Two bands of SiO<sub>2</sub> precipitates are formed; after final annealing at 1000 °C they are sharply centered on the depths  $x_{\text{max}} = 220 \text{ nm}$  and  $x_{\dagger} = 320 \text{ nm}$ , respectively (Fig. 7).

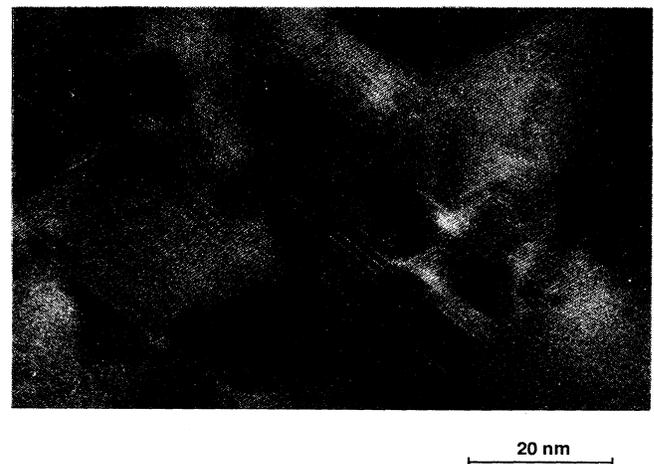


FIG. 6. High-resolution picture showing overlapping {111} stacking faults formed in the region of homogeneous precipitation after final annealing at 800 °C ( $\Phi = 1 \times 10^{17} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$ ).

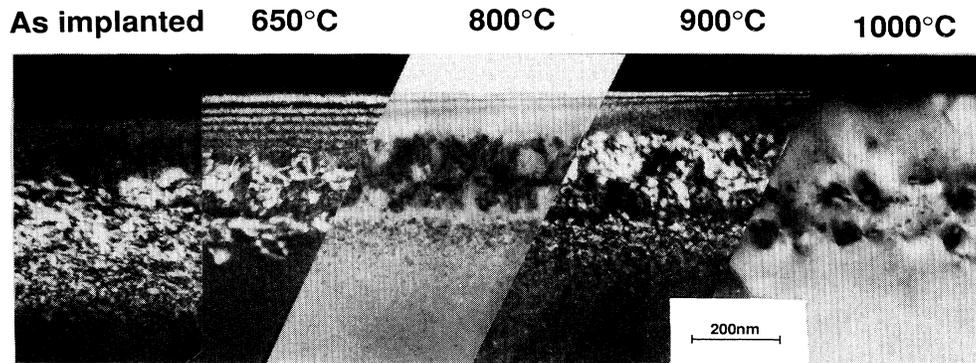


FIG. 7. Cross-section views of the implanted region in as-implanted and annealed samples;  $\Phi = 1 \times 10^{17} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$ .

### 3. Silicon defects

In samples annealed first at 650°C and henceforth at higher temperature in the range 800–1000°C, the same defects and defect evolution observed in low-fluence samples are observed. However, the {111} defects are formed already at 650°C; the amount of these defects is maximum after annealing at 800°C (Fig. 6). The increase of amount and length of {111} stacking faults up to 800°C suggests that SiO<sub>2</sub> precipitation is not completed up to this temperature. The decrease of the amount of {111} stacking faults at 900°C suggests that the growth of precipitates takes place mainly through their coalescence rather than by further precipitation.

### C. The border

Since even in low-fluence samples the oxygen concentration largely exceeds the solid solubility, precipitation is expected to occur even in this case. As discussed later, however, the nucleation mechanism produces very small precipitates which are dissolved after annealing unless they are so close as to coalesce and form larger precipitates. In our experimental conditions (energy, current density, and target temperature) the threshold fluence  $\Phi_T$ , dividing the behaviors sketched in Fig. 2 is in the interval  $10^{16}$ – $10^{17} \text{ cm}^{-2}$ .

## IV. FOUNDING THE MODEL

The development of the theory requires a brief summary of the concept of hot cloud, as stems from Refs. 20 and 21. We define *hot cloud* as the final, thermal stage of the collisional cascade. A collisional cascade, formed by binary collisions in an energy regime for which collisions take place with a mean free path of the order of the interatomic distance, becomes dense when it involves approximately  $N_* \approx 10^4$  atoms. From this stage on one can speak in terms of cascade temperature which decays asymptotically with time as  $(t_0 + t)^{-3/2}$  [because the cascade size increases in the quenching regime as  $(t_0 + t)^{1/2}$ ],  $t_0$  being a characteristic time ( $t_0 \approx 10^{-11} \text{ s}$ ) related to the minimum time required to render dense the cascade.<sup>22</sup>

Most of the radiation damage is described in terms of maximum temperature  $T_*$  of the hot cloud. In turn, the maximum temperature is determined by the energy released in elastic collisions inside the smallest dense collisional cascade of diameter  $d_*$  (where  $n_{\text{Si}} \pi d_*^3 / 6 = N_*$  and  $n_{\text{Si}}$  is the silicon atomic density,  $n_{\text{Si}} = 5 \times 10^{22} \text{ cm}^{-3}$ ). This picture is applied to the formation of SiO<sub>2</sub> by assuming that precipitation is possible when the hot-cloud temperature  $T_*$  exceeds a critical temperature  $T_{\ddagger}$ .

The problem of calculating the maximum hot-cloud temperature is attacked as follows. Assume, temporarily, that the energy  $\epsilon$  of the projectile originating the cascade is so high that on an average the projectile stops outside the minimum hot cloud, i.e., its range  $R(\epsilon)$  is appreciably higher than the cascade diameter  $d_*$ . Therefore, only a few projectiles have a fate allowing them to impart all the energy they lose in elastic collisions to the hot cloud; only when the projectile stops in the minimum volume  $V_*$  of the hot cloud itself [ $V_* = \frac{4}{3} \pi (d_*/2)^3$ ] does all the projectile energy imparted to the crystal in elastic collisions (the electronic energy loss not being responsible for heating the collisional cascade<sup>20,21</sup>) contribute to heating the collisional cascade itself. This means that only a fraction of projectiles with kinetic energy greater than  $\epsilon$  are useful to form dense collisional cascades with the required temperature.

Let  $\eta_{\text{Si}}(\epsilon)$  be this fraction for silicon recoils and  $\eta_{\text{O}}(\epsilon)$  the fraction of oxygen projectiles stopping in the volume  $V_*$ ; these quantities can be estimated by direct TRIM simulations at different energies (Fig. 8). The “effective hot-cloud yield”  $y(x, \epsilon)$  (i.e., the yield of collisional cascades where all the energy lost in elastic collisions is imparted to the hot cloud of minimum size) is then given by<sup>23</sup>

$$y(x, \epsilon) = \eta_{\text{O}}(\epsilon) \chi(x, \epsilon) + \eta_{\text{Si}}(\epsilon) Y(x, \epsilon),$$

where  $\chi(x, \epsilon)$  is the projectile concentration per unit fluence at depth  $x$  with energy  $\epsilon$  and  $Y(x, \epsilon)$  is the total recoil concentration per unit fluence. Figure 9 shows graphs  $y(x, \epsilon)$  versus depth  $x$ , with the energy  $\epsilon$  as parameter.

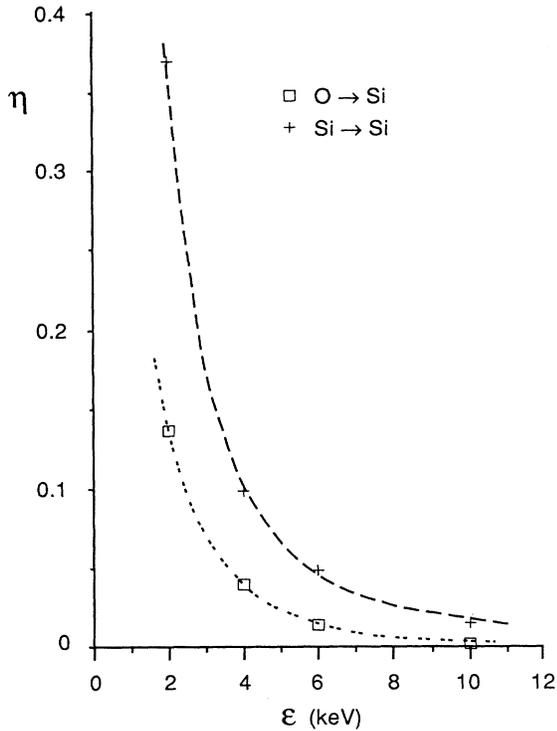


FIG. 8. Probability that silicon or oxygen stop inside the minimum-size hot cloud they produce as a function of projectile energy.

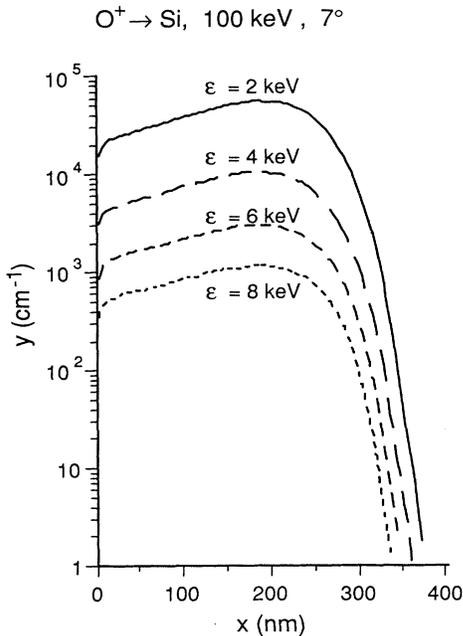


FIG. 9. Effective hot-cloud yield as a function of depth with energy as a parameter.

The function  $y(x, \epsilon)$  allows us to define the yield of formation of SiO<sub>2</sub> precipitates,

$$y_{\dagger}(x) = \eta_{\text{O}}(\epsilon_{\dagger})\chi(x, \epsilon_{\dagger}) + \eta_{\text{Si}}(\epsilon_{\dagger})Y(x, \epsilon_{\dagger}),$$

where  $\epsilon_{\dagger}$  is the minimum energy producing a hot cloud with maximum local temperature  $T_{\dagger}$  high enough to allow for SiO<sub>2</sub> precipitation. The concentration per unit fluence of projectiles at rest,  $\chi(x, \epsilon=0)$ , will henceforth be denoted by the symbol  $\chi_0(x)$ .

#### A. Formation kinetics of SiO<sub>2</sub> precipitates

Once the yield  $y_{\dagger}(x)$  is known, the amount of SiO<sub>2</sub> complexes as a function of the fluence is determined as follows. The change of oxygen concentration  $dC_p(x)$  due to oxygen separation as SiO<sub>2</sub> produced by effective hot clouds in the elementary implantation step of fluence  $d\Phi$  is given by

$$dC_p(x) = V_* [C(x) - C_p(x)] y_{\dagger}(x) d\Phi, \quad (4)$$

where  $C(x) - C_p(x) = \chi_0(x)\Phi - C_p(x)$  is the concentration of available oxygen involved in effective hot clouds.

Defining  $\Phi_{\dagger}(x) = 1/V_* y_{\dagger}(x)$  and setting the initial condition  $C_p = 0$  when  $\Phi = 0$ , the solution of Eq. (4) is

$$C_p(x) = \chi_0(x)\Phi_{\dagger}(x) \times \left\{ \frac{\Phi}{\Phi_{\dagger}(x)} - \left[ 1 - \exp \left( -\frac{\Phi}{\Phi_{\dagger}(x)} \right) \right] \right\}, \quad (5)$$

which exhibits the following asymptotic behaviors:

$$C_p(x) \simeq \chi_0(x)\Phi^2/2\Phi_{\dagger}(x) \quad \text{for } \Phi \lesssim \Phi_{\dagger}(x)$$

and

$$C_p(x) \simeq \chi_0(x)[\Phi - \Phi_{\dagger}(x)] \quad \text{for } \Phi \gg \Phi_{\dagger}(x).$$

#### B. Nucleation mechanism

By the addition of a convenient hypothesis, explaining the fate of precipitates involved in new hot clouds, the model can be extended to predict the average density  $n_p(x)$  and size  $d_p(x)$  of the produced SiO<sub>2</sub> precipitates. The hypothesis we assume is that an *effective hot cloud investing an already formed precipitate does not destroy it, but rather produces another precipitate with the available oxygen*. This hypothesis can be restated by saying that *inside a hot cloud, homogeneous precipitation prevails on heterogeneous precipitation on preexisting precipitates* (a possible explanation of this quite-extravagant assumption will be given in the last statement of the Appendix). In this hypothesis the density of precipitates is given by

$$n_p(x) = y_{\dagger}(x)\Phi, \quad (6)$$

so that, for any given energy  $\epsilon_{\dagger}$ , the density distribution of precipitates copies the profile  $y_{\dagger}(x)$ . In the region where effective hot clouds produce SiO<sub>2</sub> precipitates, their diameter is given by

$$d_p(x) = 2 \left( \frac{3}{4\pi} \frac{N_O(x)}{n_O} \right)^{1/3}, \quad (7)$$

where  $N_O(x)$  is the number of oxygen atoms in the precipitate and  $n_O$  is close to the atomic density of oxygen in  $\text{SiO}_2$  ( $n_O = 4.4 \times 10^{22} \text{ cm}^{-3}$ ). In turn,  $N_O(x)$  can be calculated as a piecewise function of  $x$ , by distinguishing regions where effective hot clouds are, on the mean, spatially superimposed, from regions where hot clouds do not cover completely the space. The probability of spatial superimposition of hot clouds can be either of the order of unity or negligible in relation to the fact that the amount of effective hot clouds generated per unit volume,  $y_{\dagger}(x)\Phi$ , exceeds or does not exceed the critical value  $n_* = n_{\text{Si}}/N_*$ , which guarantees the full covering of the region of interest. The critical depth  $x_{\dagger}$ , where spatial superimposition is no longer complete, is given by the condition

$$y_{\dagger}(x)\Phi = n_*, \quad (8)$$

which, considered as an equation for  $x$ , may have (see Fig. 9) no solution (for  $\Phi < n_*/y_{\dagger\text{max}}$ ), one solution [for  $\Phi > n_*/y_{\dagger}(0)$ ], or two solutions [for  $n_*/y_{\dagger\text{max}} \leq \Phi \leq n_*/y_{\dagger}(0)$ ]. In the second case we denote the solution of Eq. (8) as  $x_{\dagger} = x_{\dagger}(\Phi)$ . The number of oxygen atoms in each precipitate is therefore given by

$$N_O(x) = \begin{cases} \chi_0(x)/y_{\dagger}(x) & \text{for } x < x_{\dagger}(\Phi) \\ \chi_0(x)\Phi N_*/n_{\text{Si}} & \text{for } x \geq x_{\dagger}(\Phi) \end{cases}. \quad (9)$$

Due to the relatively flat behavior of  $\chi_0(x)$  at  $x = x_{\dagger}(\Phi)$ ,  $N_O(x)$  and  $d_p(x)$  have maxima centered on  $x_{\dagger}(\Phi)$ .

## V. VALIDATING THE MODEL

The predictions of the model about depth location of precipitates and threshold fluence for precipitate coalescence are considered in this section.

### A. Density and size of $\text{SiO}_2$ precipitates

The model hitherto developed speaks about nucleation phenomena during the implantation. It is, however, expected that an annealing process after the implantation will result in growth of large precipitates and dissolution of small precipitates. Since the largest precipitates are located at  $x_{\dagger}(\Phi)$  rather than at  $x_{\text{max}}$ , our model can be tested versus the current mode of nucleation by annealing an as-implanted sample.

Figure 10 shows a TEM cross section of a sample implanted at  $\Phi = 5 \times 10^{15} \text{ cm}^{-2}$  and annealed at  $T = 1200^\circ\text{C}$ . The inspection of this photograph shows that the  $\text{SiO}_2$  precipitates are located at  $x = (290 \pm 30) \text{ nm}$ ; this depth is reproduced by assuming an energy  $\epsilon_{\dagger} = 5_{-2.5}^{+1.5} \text{ keV}$ . In turn, the knowledge of  $\epsilon_{\dagger}$  allows us to calculate from Eq. (6) the average density  $n_p(x)$  and from Eqs. (7) and (9) the diameter  $d_p(x)$  of the so-produced  $\text{SiO}_2$  precipitates (Figs. 11 and 12, respectively).

Figure 13 shows a TEM cross section of a sample implanted at  $\Phi = 1 \times 10^{17} \text{ cm}^{-2}$  and annealed at  $1000^\circ\text{C}$ ; the

picture shows that the energy  $\epsilon_{\dagger}$  which allows for the precipitation region at 290 nm in the sample implanted at  $5 \times 10^{15} \text{ cm}^{-2}$  gives  $x_{\dagger}(\Phi) = 320 \text{ nm}$  at  $1 \times 10^{17} \text{ cm}^{-2}$ , thus accounting for the precipitation region centered on depth of  $(325 \pm 25) \text{ nm}$ .

The energy  $\epsilon_{\dagger}$  so determined is of the same order as the amorphization energy in silicon,<sup>20,21</sup> i.e.,  $\epsilon_{\dagger}$  is an energy able to displace permanently silicon atoms from their lattice positions. Since the energy required to break Si-O bonds is much larger, it is expected that these hot clouds are unable to destroy preexisting precipitates, therefore

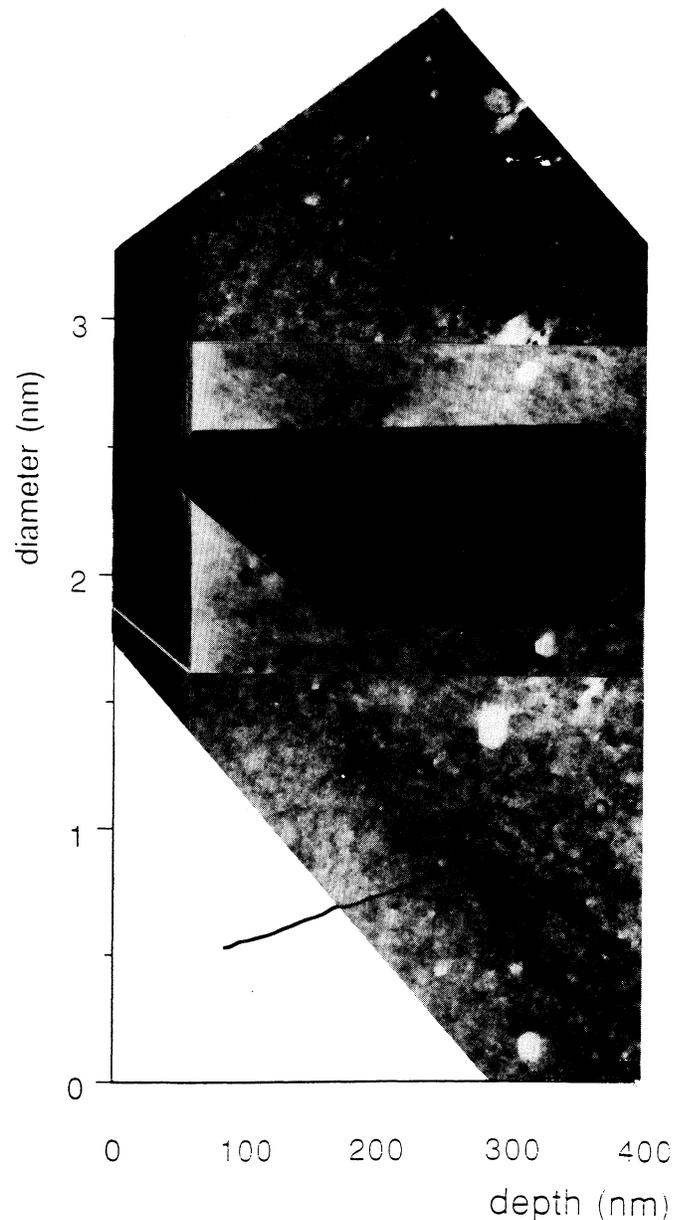


FIG. 10. Cross-section view of precipitates remaining after annealing at  $1200^\circ\text{C}$  of the sample implanted at  $5 \times 10^{15} \text{ cm}^{-2}$ , superimposed on the calculated diameter profile of precipitates produced in as-implanted conditions.

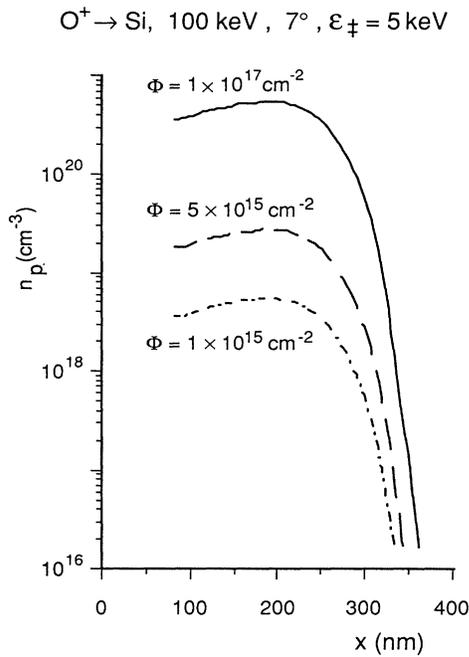


FIG. 11. Concentration of precipitates vs depth taking fluence as parameter.

upholding *a posteriori* the hypothesis that SiO<sub>2</sub> precipitates are not destroyed when invested by a hot cloud.

**B. The threshold fluence**

Figure 7 also shows the existence of a second precipitation region centered on  $x_{max}$  not present in the sample

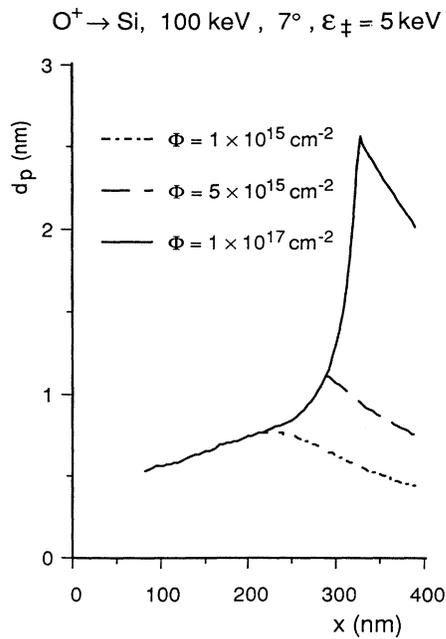


FIG. 12. Diameter of precipitates vs depth taking fluence as parameter.

implanted at  $\Phi = 5 \times 10^{15} \text{ cm}^{-2}$ . The problem of predicting the lowest value of fluence at which homogeneous precipitation prevails on heterogeneous precipitation is not of easy solution and can be attacked on statistical grounds.<sup>24</sup>

Consider, for any  $\Phi$ , the diameter  $d_p[x_{‡}(\Phi)]$  of precipitates formed at  $x = x_{‡}(\Phi)$  and define for a sake of compactness  $d_0(\Phi) = d_p[x_{‡}(\Phi)]$ ; while the diameter of these precipitates increases with  $\Phi$ , their concentration  $n_*$  is a constant. Precipitates formed at  $x_{max}$  are much smaller and closer to one another; two of them may be considered to form a *connected cluster* when they are separated by a distance smaller than  $d_{Si}$  (where  $d_{Si}$  is the silicon diameter,  $d_{Si} = 0.234 \text{ nm}$ ); they will be considered to form an *adjacent set* when they are separated by a distance between  $d_{Si}$  and  $2d_{Si}$ .

Consider now a covering of the region around  $x_{max}$ , obtained by sampling cubes each of edge  $d_0(\Phi)$ , and the volume occupied by a set of  $k$  adjacent precipitates. It is not unrealistic to assume that homogeneous precipitation

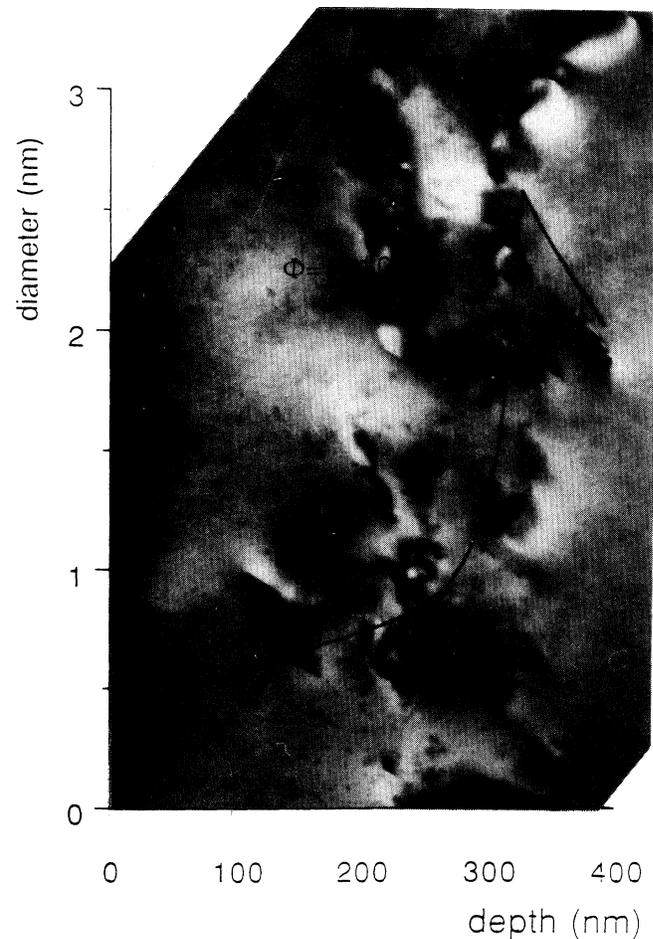


FIG. 13. Cross-section view of precipitates remaining after annealing at 1000°C of the sample implanted at  $1 \times 10^{17} \text{ cm}^{-2}$ , superimposed on the calculated diameter profile of precipitates produced in as-implanted conditions.

prevails when the density  $n_k$  of sampling cubes containing sets with  $k$  adjacent precipitates with total volume higher than  $\pi d_0(\Phi)^3/6$  exceeds  $n_*$ . Indeed, in the early stages of annealing small precipitates are dissolved and the oxygen they release is captured either by precipitates at  $x_{\dagger}$  [with a total cross section around  $\pi(d_0/2)^2 n_* \Delta_*$ , where  $\Delta_*$  is the thickness of the region where precipitates are dispersed] or by adjacent sets with  $k$  precipitates at  $x_{\max}$  [with a total cross section around  $\pi(d_k/2)^2 n_k \Delta_{\max}$ , where  $\Delta_{\max}$  is the thickness of the region where precipitates are dispersed], since the capture of oxygen atoms by adjacent sets transforms them in connected clusters with the same size. The condition for thermodynamic stability of these precipitates is therefore that their diameter  $d_k$  exceeds  $d_0$  and the condition for their prevalence is that their collection efficiency is higher than that at  $x_{\dagger}$ , i.e.,  $\pi(d_k/2)^2 n_k \Delta_{\max} > \pi(d_0/2)^2 n_* \Delta_*$ . Combining these conditions one has  $n_k \gtrsim n_*$ , provided that  $\Delta_{\max} \simeq \Delta_*$ .

The minimum value  $\bar{k}$  of  $k$  satisfying the above conditions is that for which homogeneous precipitation prevails on the etherogeneous one. The value of  $\bar{k}$  must satisfy the conditions

$$\left[ \frac{d_0}{d_p(x_{\max}) + 2d_{\text{Si}}} \right]^3 \leq \bar{k} < \left[ \frac{d_0}{d_p(x_{\max}) + d_{\text{Si}}} \right]^3,$$

while the concentration  $n_k$  can be calculated by assuming that precipitates are distributed spatially according to the Poisson statistics. In this case,  $n_k$  is obtained dividing the probability of having  $k$  precipitates in the volume,

$$P_k = (m^k/k!) \exp(-m)$$

[where  $m$  is the average number of precipitates in the sampling cubes,  $m = y_{\dagger}(x_{\max})\Phi d_0(\Phi)^3$ ] by the sampling volume  $d_0^3$ .<sup>24</sup> The condition  $P_k(\Phi)/d_0(\Phi)^3 \geq n_*$  is an equation in  $\Phi$ , whose solution,  $\Phi_t = (1.6-2.5) \times 10^{16}$  cm<sup>-2</sup>, is in agreement with the experimental data (see Sec. III C).

## VI. DISCUSSION

While at relatively low temperature (say, below 600 °C) oxygen forms mainly complexes with vacancies,<sup>15</sup> at temperatures high enough to allow for appreciable oxygen diffusion, precipitation becomes possible and SiO<sub>2</sub> becomes the prevailing structure.<sup>16</sup> Since the oxidation number of oxygen does not vary during precipitate growth, the precipitation of SiO<sub>2</sub> in silicon can be regarded as diffusion limited. The standard description of diffusion-limited growth of precipitates, essentially due to Ham,<sup>25</sup> requires the knowledge of the initial radius and density of precipitates. In turn, information on these quantities is usually obtained from the Volmer and Weber theory of nucleation.<sup>26</sup>

In this theory, the free-energy difference  $\Delta F(d_p)$  of a precipitate of diameter  $d_p$  with respect to the solution has two contributions: one negative and increasing as  $d_p^3$ , and the other positive and increasing as  $d_p^2$ . Since  $\Delta F(d_p) \propto d_p^2$  for small  $d_p$  and  $\Delta F(d_p) \propto d_p^3$  for large  $d_p$ , surface effects will prevail for small precipitates while volume effects will prevail for big precipitates. There is

therefore a critical diameter  $d_{\text{pc}}$  separating these regions. The theory of nucleation specifies the number of precipitates with diameter  $d_{\text{pc}}$  as

$$n_{\text{pc}} = n_s \exp[-\Delta F(d_{\text{pc}})/k_B T], \quad (10)$$

where  $n_s$  is a concentration related to the density of nucleation sites.

The usual way to produce a theory of precipitate growth is to assume that at time  $t=0$  the density of precipitates is given by the density of nuclei with critical radius. The combination of Ham's theory of precipitate growth and the Volmer and Weber theory of nucleation can be inserted in standard simulation codes for impurity diffusion. A version of SUPREM III,<sup>27</sup> modified to describe in the above framework precipitation phenomena in supersaturated silicon, was demonstrated to give an accurate description of boron concentration in supersaturated Si:B.<sup>28</sup> Its application to the highly supersaturated Si:O system, however, does not describe precipitation at  $x_{\dagger}$ .

In the model developed here, this precipitation is ascribed to an initial condition different from that predicted by the Volmer and Weber theory of nucleation. While in the Volmer and Weber theory the formation of nuclei is, according to Eq. (10), driven by the heat reservoir temperature, in our model the initial condition results from the interaction of an intrinsically thermal phenomenon (the hot cloud), substantially uncoupled with the heat reservoir.

Since the thermal stage of the collisional cascade is intrinsic to the stopping mechanism of implanted ions, it may reasonably be concluded that *in all samples implanted at a fluence high enough to produce a supersaturated solution, nuclei are formed with a distribution differing appreciably from that predicted by the standard theory of nucleation.* This conclusion is especially important because in most situations supersaturation is obtained by high-fluence implantation. Of course, since the effective temperatures required to form the precipitate may be different for different impurities, the hot-cloud distribution and temperatures may vary from one projectile to another, and consequently the as-implanted distribution of precipitates is expected to differ from one situation to another.

The second observation concerns the method used for determining under which conditions homogeneous precipitation prevails on etherogeneous precipitation. Though the proposed model seems to work only for ion implantation, it can also be extended to understand under which conditions homogeneous precipitation prevails on heterogeneous precipitation in a supersaturated solution. Indeed, in this case a comparison is established between preexisting heterogeneous precipitates (whose average diameter  $d_0$  and density  $n_0$  are supposed to be known) and the distribution of homogeneous precipitates with critical diameter  $d_{\text{pc}}$  and density  $n_{\text{pc}}$ , both depending on temperature and concentration. The condition of prevalence of homogeneous precipitation is therefore obtained by sampling the space with cubes with edge  $d_0$  and searching the temperature  $T$  allowing for a distribution whose density of adjacent sets with diameter greater than  $d_0$  exceeds  $n_0$ .

## VII. CONCLUSIONS

An experimental and theoretical study of the Si:O system obtained by high-fluence oxygen implantation has been carried out. This study has given evidence for SiO<sub>2</sub> precipitation produced during oxygen implantation by dense and hot collisional cascades.

A theoretical, quantitative description has been proposed, in the light of a model of nucleation produced in the thermal stage of collisional cascades. This model predicts the dependence on depth of density and size of precipitates separated during implantation; the maximum of precipitate size is centered on a depth where oxygen concentration is still high but primary events originating the collisional cascades are no longer sufficient to guarantee the spatial covering of the silicon. Theoretical predictions agree with experimental TEM data.

### ACKNOWLEDGMENTS

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### APPENDIX: EXPECTED REACTIONS OF OXYGEN WITH POINT DEFECTS

Oxygen is expected to react easily with both vacancies and self-interstitials. Though there is no general consensus on structural, thermodynamic, and kinetic properties of both these defects (Ref. 9, Ch. 2), the following considerations are sufficiently robust to be independent of the exact value of formation energy and entropy and activation energy and entropy for migration. It is an additional fundamental stipulation, however, that two kinds of self-interstitials exist: the purely  $T_d$  self-interstitial, which is assumed to be formed at relatively low temperature (say, below 700 K), and the dumbbell self-interstitial, which is assumed to be formed at higher temperature.

For most of the forthcoming qualitative considerations we make the following assumptions:

(i) Enthalpy differences are calculated from bond energies.

(ii) The following values of bond energies are assumed:  $E(\text{Si—Si})=2.4$  eV (reported values range in the interval 2.2–2.6 eV),  $E(\text{Si—O})=3.8$  eV, and  $E(\text{O=O})=5.2$  eV.<sup>29</sup>

(iii) All corrections to these bond energies due to lattice relaxation, bond distortion, etc. are ignored unless the enthalpy difference between two configurations is more than 1 eV (which is the estimated uncertainty of our considerations).

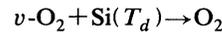
(iv) When the electronic energies of two different configurations are approximately the same (i.e., when their difference is less than 1 eV), the most stable configuration will be decided on manifestly evident criteria of minimum stress.

These assumptions are sufficient to have information on the stability and reactivity of most of the considered configurations.

## 1. Vacancy-oxygen reactions

The vacancy ( $v$ ) is a preferred site to trap oxygen by formation of oxygen bridges on the deformed Si-Si bonds of the vacancy (Fig. 14). For *covalently bonded oxygen* the stability of both the simply decorated vacancy,  $v\text{-O}$  [evidence for which was given by Watkins and Corbett in 1961 (Ref. 30)], and the doubly decorated one,  $v\text{-O}_2$  [which is formed after annealing at temperature higher than 300°C (Ref. 31)], are guaranteed by the relief of stress associated with the undecorated vacancy. That the oxidated vacancy has a lower stress than both the undecorated vacancy and the two  $\text{O}_i$  is immediately realized by comparing the Si-Si distance between next-nearest neighbors, 0.383 nm, with the Si-O-Si length for a linear arrangement, 0.366 nm, the covalent Si-Si distance being 0.234 nm. The doubly decorated vacancy is more stable than the singly decorated vacancy; the very fact that the distance between oxygen-bridged silicon atoms is almost exactly forced to the lattice distance stresses the other Si-Si bond in the vacancy; this is the presumable reason why the  $v\text{-O}$  complex is paramagnetically active.<sup>30</sup>

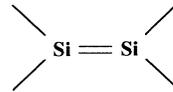
The fully oxidated vacancy  $v\text{-O}_2$  is unstable in the presence of  $T_d$  silicon interstitials, because though the reaction (Fig. 15)



has an approximately null enthalpy difference,  $\Delta H \approx 4E(\text{Si—O}) - 4E(\text{Si—Si}) - E(\text{O=O}) = 0.4$  eV, the stress associated with interstitial  $\text{O}_2$  (maximum size  $\approx 0.24$  nm) is, however, expected to be much smaller than that associated with  $T_d$  silicon (diameter = 0.234 nm) and  $v\text{-O}_2$ .

## 2. Self-interstitial-oxygen reactions

Several self-interstitial configurations seem possible; among them we quote the pure  $T_d$  self-interstitial, which is expected to be a fast diffuser,<sup>32</sup> and the dumbbell self-interstitial<sup>33</sup>



which might be the species relatively immobile up to 10<sup>3</sup>

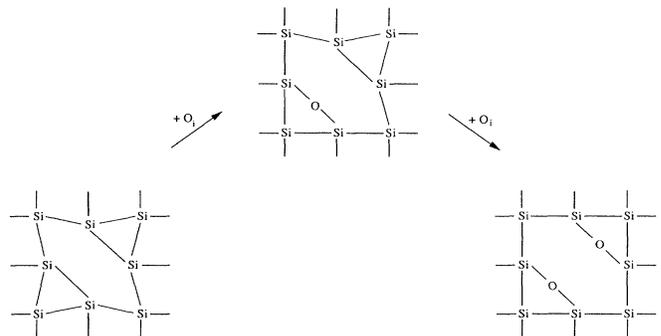


FIG. 14. The formation of oxygen-vacancy complexes by consecutive reactions with oxygen. The progressive loss of lattice distortion is emphasized.

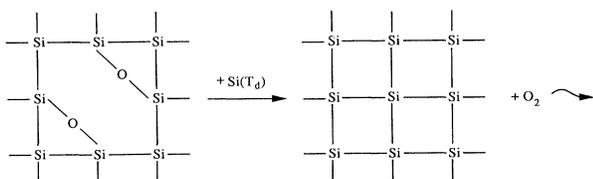


FIG. 15. Formation of molecular oxygen by reaction of a doubly decorated vacancy with a  $T_d$  self-interstitial.

K.<sup>34</sup> Information on the relative stabilities of  $T_d$  and dumbbell self-interstitials cannot be obtained with the above elementary considerations because the electronic configuration of each dumbbell silicon is given by three  $sp^2$  hybrid orbitals lying in the same plane and one  $p$  orbital perpendicular to it, while the  $T_d$  self-interstitial has presumably a  $3s^2 3p^2$  outer electronic configuration.

Though silicon has a very poor tendency to form  $\pi$  double bonds,<sup>29</sup> the existence of the dumbbell self-interstitial is strongly supported by the recent discovery of disilenic compounds and their chemistry.<sup>35</sup> Though disilene itself  $H_2Si=SiH_2$  is unstable, provided that the  $Si=Si$  double bond is protected by the replacement of hydrogen with a suitably large radical  $R$ , compounds  $R_2Si=SiR_2$  stable up to 170 °C can be isolated. The availability of these compounds has allowed the silicon double bond to be studied.

The  $Si=Si$  double bond has a length of 0.214–0.216 nm and an energy of 2.3–2.5 eV. Comparing these values with the length and energy of the simple bond, 0.234 nm and 2.2–2.6 eV, respectively, the relative stability of the double bond is confirmed. In spite of its relative stability, the  $Si-Si$   $\pi$  bond is rather reactive, the activation energy required to open it being a fraction of an eV.

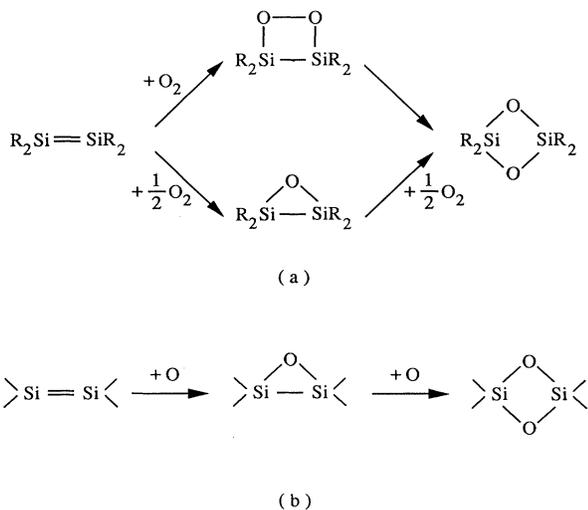


FIG. 16. The formation of cyclodisiloxanes (a) by oxidation of disilenes, and (b) by oxidation of a dumbbell self-interstitial.

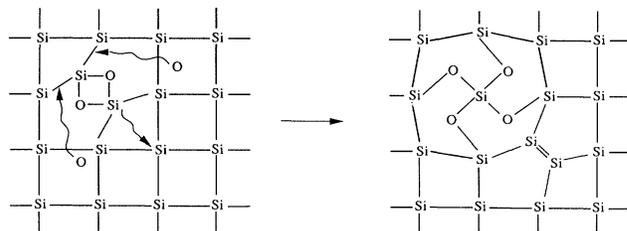


FIG. 17. Formation of a coherent precipitate by oxidation of a cyclodisiloxane ring and injection of a dumbbell self-interstitial.

Disilenic compounds are known to react with oxygen according to the scheme of Fig. 16(a) to eventually form cyclodisiloxanes, so that it is highly plausible that the dumbbell self-interstitial reacts readily with molecular or covalently bonded interstitial oxygen to form cyclodisiloxane, as shown in Fig. 16(b).

#### A model for $SiO_2$ precipitation

The dumbbell self-interstitial is a preferential site for oxygen precipitation if one stipulates that the highly strained heterocycle of Fig. 16(b) (with angle  $Si-O-Si=86^\circ-98^\circ$  and  $Si-Si$  distance of 0.231–0.245 nm) reacts further with atomic or molecular oxygen to form a  $SiO_4$  complex (where silicon coordination is the same as in silica) with the injection of a self-interstitial (Fig. 17). This injection restores the initial condition on the contour of the  $SiO_4$  complex so that the process can continue up to the formation of a  $SiO_2$  precipitate.

It is interesting to remark that this mechanism does not inject net self-interstitials until the  $SiO_4$  complex remains coherent with the matrix; this mechanism will terminate when the energy excess accumulated in this complex exceeds the formation energy of a self-interstitial. At this point reaction (3) will be activated and the precipitate will lose its coherence with the crystal.

According to this mechanism,  $SiO_2$  precipitation is characterized by three phases.

(i) *An induction phase*, where the number of self-interstitials remains constant so that the reaction proceeds smoothly via the mechanism sketched in Fig. 17.

(ii) *An early autocatalytic growth phase*, in which the number of self-interstitials, which are the seeds for oxygen separation as  $SiO_2$ , increases as the reaction proceeds but remains so small that they can remain localized at the growing  $Si-SiO_2$  interface.

(iii) *A final autocatalytic growth phase*, in which the number of self-interstitials (which increases with precipitate volume, i.e., with the third power  $R^3$  of precipitate radius  $R$ ) exceeds the number of available sites at the  $Si-SiO_2$  interface (which increases with  $R^2$ ).

The precipitate radius  $\bar{R}$  separating the early autocatalytic phase from the final autocatalytic phase is given by

$\bar{R} \approx 3\lambda/r$ , where  $r$  is the number of self-interstitials injected per newly formed SiO<sub>2</sub> molecule and  $\lambda$  is the thickness of the interface layer in which the self-interstitials are arranged.

Two situations can be hypothesized. At temperature so low as to forbid self-interstitial diffusion, precipitation can continue ( $R$  increases) only if the width  $\lambda$  of the interface region increases correspondingly; this low-temperature precipitation leads to precipitates surrounded by an interstitial-rich atmosphere. At higher temperature, self-interstitials will, however, diffuse and organize in defects of extrinsic type (e.g., {111} stacking faults) which react further with oxygen to form a platelike silicon-oxygen complex.

This overall process is expected to proceed only at temperatures sufficiently high to allow the dumbbell configuration of the self-interstitial. Interestingly

enough, internal gettering processes (in which the precipitates are formed by prolonged annealing at moderate temperature) are usually carried out in the temperature range 700–800 °C (Ref. 9, Ch. 9).

At last, we observe that the idea that dumbbell self-interstitials are preferential sites for the formation of SiO<sub>2</sub> precipitates is consistent with the assumption that precipitation in a hot cloud does not take place heterogeneously on a preexisting precipitate, but rather on preexisting clusters of dumbbell self-interstitials, possibly formed when a few native  $T_d$  self-interstitials are invested by a hot cloud and hence brought to the configuration stable at high temperature. Though this SiO<sub>2</sub> precipitation takes place heterogeneously on preexisting sites, it mimics homogeneous precipitation because small clusters of self-interstitials are not directly accessible to electron microscopy.

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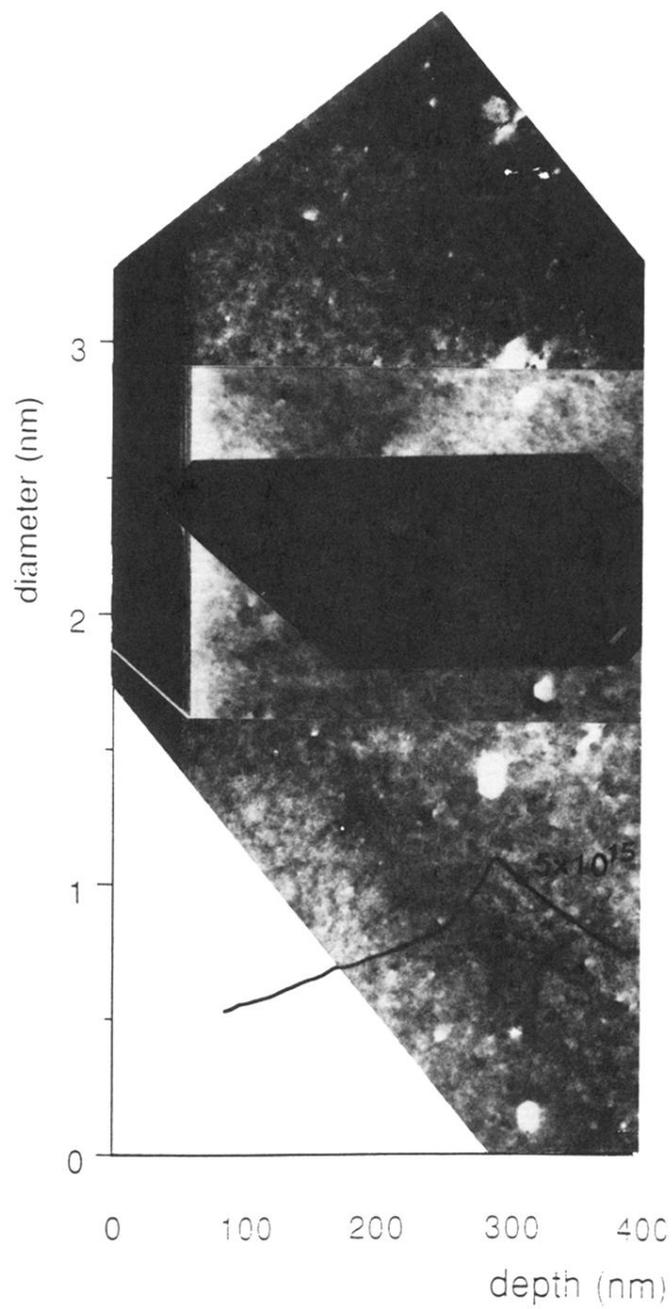


FIG. 10. Cross-section view of precipitates remaining after annealing at 1200°C of the sample implanted at  $5 \times 10^{15} \text{ cm}^{-2}$ , superimposed on the calculated diameter profile of precipitates produced in as-implanted conditions.

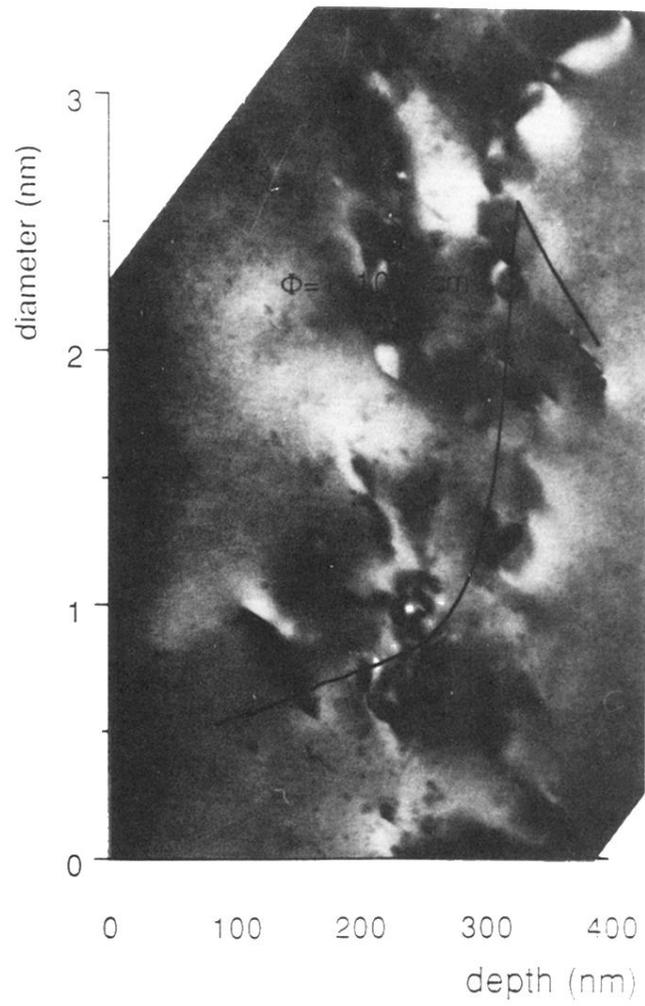


FIG. 13. Cross-section view of precipitates remaining after annealing at  $1000^\circ\text{C}$  of the sample implanted at  $1 \times 10^{17} \text{ cm}^{-2}$ , superimposed on the calculated diameter profile of precipitates produced in as-implanted conditions.

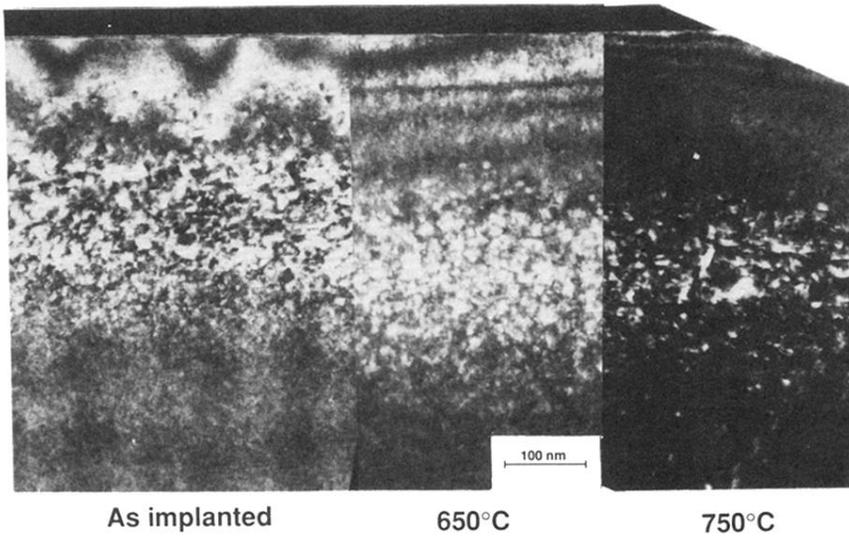


FIG. 4. Cross-section views of the implanted region in as-implanted and annealed samples;  $\Phi = 5 \times 10^{15} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$ .

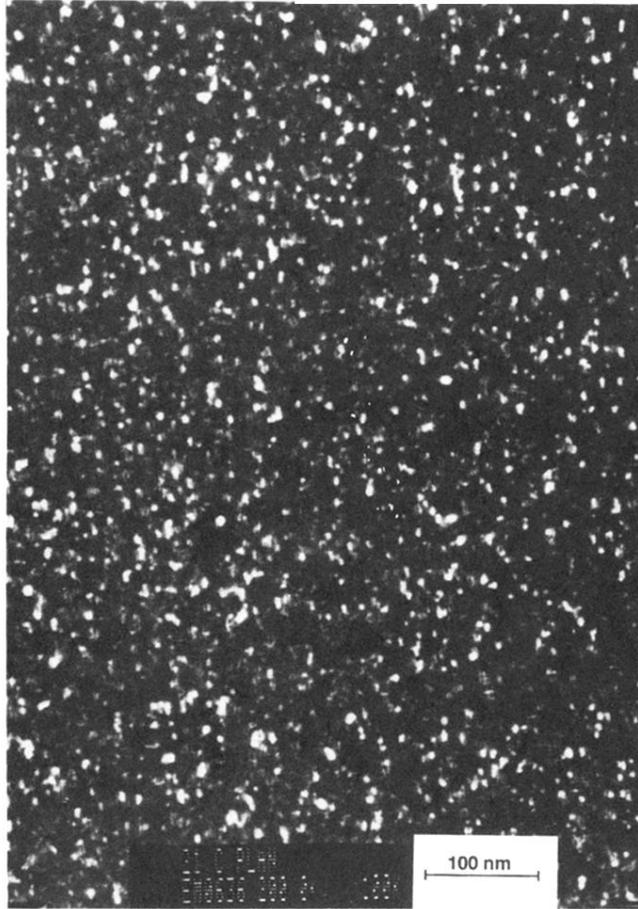
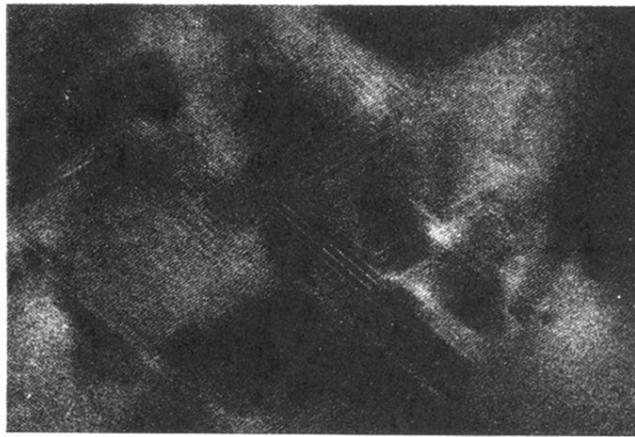


FIG. 5. Plan view of the implanted region in the sample implanted at  $\Phi = 5 \times 10^{15} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$  and annealed at  $650^\circ\text{C}$ .



20 nm

FIG. 6. High-resolution picture showing overlapping {111} stacking faults formed in the region of homogeneous precipitation after final annealing at 800°C ( $\Phi = 1 \times 10^{17} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$ ).

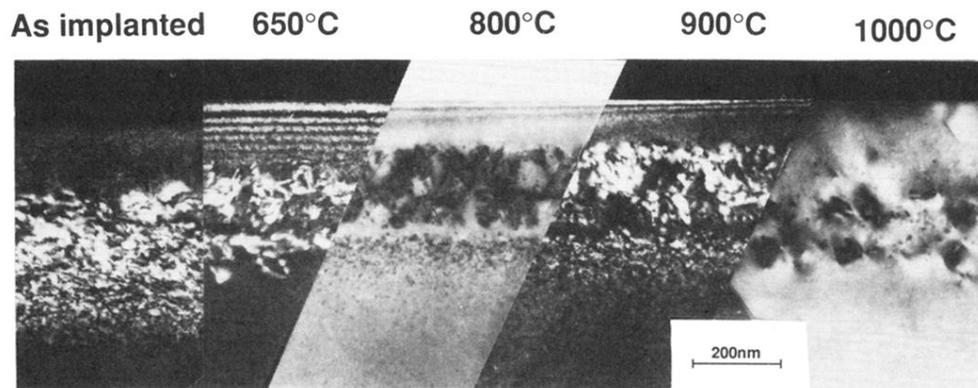


FIG. 7. Cross-section views of the implanted region in as-implanted and annealed samples;  $\Phi = 1 \times 10^{17} \text{ cm}^{-2}$ ,  $E = 100 \text{ keV}$ .