Critical-point dewetting

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Already within Landau theory with short-ranged substrate-adsorbate forces, complete wetting is not necessary near critical points. Preferential adsorption, but only partial wetting all the way to the critical point, and even critical-point dewetting are possible. Physical systems displaying such behavior include uniaxial magnets with triplet surface fields, and special choices of adsorbed liquid-vapor systems, binary mixtures, liquid crystals, and critical-end-point systems.

When two coexisting phases α and β (e.g., a liquid and a vapor) are adsorbed at a phase γ (e.g., a substrate), and γ preferentially adsorbs α , then *complete wetting* of the β - γ interface by α is expected close to a α - β critical point. A macroscopic layer of α then intrudes between β and γ . If partial wetting occurs (when there is a three-phase contact line) the system is expected to display a phase transition to complete wetting as the critical point is approached. These expectations have become common since Cahn's theory of critical-point wetting and the discovery of the wetting phase transition in theory^{1,2} and experiment.³ Up to date several reviews have dealt with this topic.⁴⁻⁹

It has been found recently that critical-point wetting need not always occur in systems with long-range forces (with power-law decay), in theory $10-13$ and experiment.¹ This is relevant for adsorbed fluids with van der Waals forces, for example. In systems with short-range forces (with exponential decay) between substrate and adsorwith exponential decay) between substrate and adsor-
bate, it is commonly believed that critical-point wetting is
necessary and ubiquitous. Landau theory, 1,15 mean-field necessary and ubiquitous. Landau theory, ^{1,15} mean-field and density-functional theories, and model calculations^{5,16} provide firm grounds for this belief.

However, as this paper would like to emphasize, already in the Landau theory with short-range forces criticalpoint wetting need not always occur. Examples are given where preferential adsorption takes place, but only partial wetting is obtained up to the critical point. Moreover, critical-point dewetting is possible: The system makes a phase transition from complete to partial wetting as the critical point is approached. These findings contradict Cahn's scaling argument¹ but are consistent with scaling theory. The paradox is resolved by noting that from scaling theory alone critical-point wetting cannot be predicted.

The physical relevance of the following examples is

probably limited because the choices of substrateadsorbate energies are special.

Consider the Landau surface free-energy functional^{1,6,15}

$$
\gamma[m(z)] = \int_0^\infty \left[\frac{c^2}{4} \left(\frac{dm}{dz} \right)^2 + f(m(z)) \right] dz + \gamma_s(m_1) , \qquad (1)
$$

of the order-parameter profile $m(z)$, for $z \ge 0$. The substrate is at $z = 0$. The surface density of m at the substrate is denoted by m_1 . For the bulk free-energy density the usual form

 $f(m(z)) = a_0 + a_2 m^2 + a_4 m^4 + \cdots$ (2)

is taken. For the substrate-adsorbate energy the form

$$
\gamma_s(m_1) = -h_1 m_1 - \frac{g}{2} m_1^2 - \frac{h_3}{3} m_1^3 \tag{3}
$$

is chosen. In addition to a surface field h_1 and a surfacecoupling enhancement g, a "triplet" surface field h_3 is added. This new addition is pertinent, e.g., to model a three-spin coupling (or external triplet field) at the free surface of a uniaxial ferromagnet.

From now on attention will be restricted mainly to the special case $h_1 = 0$. An analysis of the profiles $m(z)$, which minimize γ , then yields critical-point wetting for $g > 0$ (enhancement), critical-point dewetting for $g < 0$ (dehancement), and temperature-independent contact angles for $g = 0$.

In calculations I have taken $a_n = 0$ for $n > 4$, $a_4 = 1$, $a_2=2(T-T_c)$, and a_0 such that min[$f(m)$] =0. Denoting by γ_+ and γ_- the surface free energies corresponding to bulk + and - phases at $z = \infty$, respectively, and by γ_{+} the tension of a free $+$ – interface, one obtains at coexistence $(T \leq T_c)$, with $m_0^2 \equiv T_c - T$,

$$
\gamma_{-} - \gamma_{+} = \frac{4}{3} \, \text{cm}^3 \left\{ \frac{1}{2} \left(Q_+^2 - Q_-^2 \right) \phi^3 + \frac{3}{4} \left(Q_+ - Q_- \right) \phi + \frac{1}{2} \left[\left(\phi^2 Q_- + 1 \right)^{3/2} Q_-^{1/2} - \left(\phi^2 Q_+ + 1 \right)^{3/2} Q_+^{1/2} \right] \right\} \,,\tag{4}
$$

Here, $Q_{\pm} = (1 \pm h_3/c)^{-1}$, and $\phi = -g(2cm_0)^{-1}$. The contact angle of the wetting problem is found via $\cos\theta \equiv (\gamma_--\gamma_+)/\gamma_{+-}$ (5) In this calculation, the physical domain is restricted to $0 \le |h_3| < c$. For larger $|h_3|$ it is necessary to include a positive sixth-order term in $f(m)$.

For $g > 0$, one obtains complete wetting for $h_3 > 0$ (or "drying" for $h_3 < 0$) provided $|h_3| \geq (\sqrt{3}/2)c$, and a first-order phase transition from partial to complete wetting when approaching the critical point for $|h_3|$ $\langle \sqrt{3}/2 \rangle_c$. In this latter case, the phase boundary between partial and complete wetting in the critical region ($T \approx T_c$) is described by (expressing $\cos\theta = \pm 1$),

$$
h_{3}g^{3}
$$
 $\sim (T_c - T_W)^{3/2}$, (6)

where T_W is the wetting (or drying) transition temperature. For $g \le 0$ one finds new behaviors. For $g = 0$, the wetting problem is independent of temperature and $\cos\theta$ depends only on h_3 . The wetting phase boundary then reads (dashed lines in Fig. 1)

$$
|h_3| = (\sqrt{3}/2)c \tag{7}
$$

For $g < 0$, partial wetting is found for all temperatures $T \leq T_c$ if $|h_3| \leq (\sqrt{3}/2)c$. For larger $|h_3|$ a phase transition from complete to partial wetting occurs as T_c is approached. The phase boundary represents critical-point dewetting and is shown in Fig. 1. It satisfies, for $|h_3| \gtrsim (\sqrt{3}/2)c$,

$$
|h_3| - (\sqrt{3}/2)c - (-g)(T_c - T_W)^{-1/2}.
$$
 (8)

For the contact angle near criticality $(T = T_c)$, one finds

$$
\cos\theta \sim h_3(-g)^{-3}(T_c-T)^{3/2} \tag{9}
$$

which implies the remarkably fast approach

$$
\gamma_{-}-\gamma_{+}\!\sim\!(T_c-T)^3,
$$

FIG. 1. Critical-point dewetting and dedrying phase boundaries (solid lines) in the plane of triplet field h_3 and temperature T, separating complete wetting (CW) from partial wetting (PW) at $h_3 > 0$, and complete drying (CD) from partial drying (PD) at $h_3 < 0$. The phase transitions are of first order.

whereas

$$
\gamma_{+} \sim (T_c - T)^{3/2}
$$

In the previous example, a triplet field h_3 has been assumed. In the Landau theory with $h_3 = 0$ previous studies have shown that critical-point wetting is unavoidable in general.¹⁵ However, even there exceptions can be constructed: systems with preferential adsorption but only partial wetting for all $T \leq T_c$.

The first example deals with systems without intrinsic order-parameter inversion symmetry $(m \leftrightarrow -m)$, such as liquid-vapor systems, binary mixtures, liquid crystals, etc. Let η denote a generalized density (particle density or concentration. . .). In the Landau theory for critical phenomena one assumes an expansion of the bulk free-energy density in powers of the order parameter $x \equiv \eta - \eta_c$ of the form

$$
|h_3| = (\sqrt{3}/2)c
$$
 (7) $f(p,T,x) = a_0 + a_1x + a_2x^2 + a_3x^3 + a_4x^4 + \cdots$ (10)

Here, p and T denote, e.g., pressure and temperature. At the critical point $(p_c, T_c): a_k = 0, k = 1, \ldots, 3$, and $a_4 > 0$. The bulk phase boundary is a curve in the (p, T) plane

$$
a_k(p,T) = a_k(x_0^2), \ k = 1, \ldots, 3 \tag{11}
$$

parametrized by a variable x_0^2 $(x_0^2 - T_c - T$ or $p_c - p)$. There is no *a priori* reason why $a_1(x_0^2)$ and $a_3(x_0^2)$ should vanish, unless there is a physical symmetry as in the case of a uniaxial ferromagnet in zero field $h(p \leftrightarrow h)$. However, the order parameter can always be redefined to obtain a symmetric f up to the fourth-order terms. Physically this redefinition transforms an asymmetric coexistence curve into a symmetric one in the (x, T) plane.

Consider now a Landau theory as given by Eq. (1) with $f(x(z))$ of the general form of Eq. (10) and the special choice

$$
\gamma_s(x_1) = -\frac{g}{2} x_1^2. \tag{12}
$$

For concreteness, consider a one-parameter family of functions f_a of the form

$$
f_a(x) = (x - x_0)^2 (x + ax_0)^2 , \qquad (13)
$$

with $\alpha \ge 1$, to describe the coexistence region (x_0^2) $=T_c - T \ge 0$). The coexistence curve is asymmetric for $\alpha \neq 1$. Alternatively, one can symmetrize the model and work with

$$
f_{sym}(y) = (y^2 - y_0^2)^2 , \qquad (14)
$$

with $y_0 = [(1 + \alpha)/2]x_0$. This brings f back to the form of Eq. (2) but transforms γ_s to

$$
\gamma_s(y_1) = \frac{a-1}{a+1} g y_0 y_1 - \frac{g}{2} y_1^2 , \qquad (15)
$$

corresponding to the presence of a temperature-dependent surface field h_1 . The presence of h_1 induces preferential adsorption and, therefore, the wetting problem is well posed. One obtains

7298 J. O. INDEKEU

$$
\cos \theta = -3 \frac{\alpha - 1}{\alpha + 1} \phi^2 + \frac{1}{2} \left[\left(1 + \phi^2 + 2 \frac{\alpha - 1}{\alpha + 1} \phi \right)^{3/2} - \left(1 + \phi^2 - 2 \frac{\alpha - 1}{\alpha + 1} \phi \right)^{3/2} \right],
$$
\n(16)

where $\phi = -g(2cy_0)^{-1}$. In the case $g > 0$ (enhancement) where $\psi = -g(2cy_0)$. In the case $g > 0$ (emhancement)
one finds critical-point wetting by the phase with $y = -y_0$ (since $h_1 < 0$). The wetting phase boundary in the (g, T) plane close to criticality takes the form

$$
g \sim (T_c - T_W)^{1/2} \tag{17}
$$

For $g < 0$ (dehancement) novel behavior occurs. The contact angle then satisfies $0 < \cos \theta < 1$ for all $T \le T_c$, signifying persistent partial wetting by the phase with $y = y_0$. In particular, as $T \rightarrow T_c^-$,

$$
\cos\theta \to \frac{1}{2} \left[\frac{\alpha - 1}{\alpha + 1} \right] \left[3 - \left[\frac{\alpha - 1}{\alpha + 1} \right]^2 \right] . \tag{18}
$$

In closing this example it is worthwhile pointing out how the discussion is translated in the liquid-crystal language. The Landau-de Gennes theory for the nematic-isotropic transition features a quadrupolar orderparameter tensor Q which reduces to a scalar q in the case of a uniaxial bulk nematic phase which homeotropicall aligns at a substrate. ' The bulk free-energy density $f(q)$ then takes the form of Eq. (10) with $a_k = a_k(h, T)$, for $k = 0, \ldots, 3$. Here, an external magnetic field h is included. Because $a_1(0,T) = 0$ but $a_3(0,T) \neq 0$ the isotropic-nematic transition is necessarily of first order in zero field. In the (h, T) plane the phase boundary terminates at a critical point at (h_c, T_c) . There a "paranematic" and a nematic phase become identical, at $q = q_c$. Once more, there is no a priori reason why the function f should have a symmetric expansion in $x \equiv q - q_c$ in the vicinity of the critical point. [If one assumes a_3 in $f(q)$ to be a constant, independent of h and T, a symmetric expansion results. I In the theory where f is not symmetric in x (up to fourth order) and where γ_s is taken of the form

$$
\gamma_s(q_1) = -h_1 q_1 - \frac{g}{2} q_1^2 \tag{19}
$$

one obtains preferential adsorption but only partial wetting for all $T \leq T_c$, provided $g < 0$ and

$$
h_1 + g q_c = 0 \tag{20}
$$

The second example features a system at a critical end point near a tricritical point.¹⁸ In this case

$$
f(x) = (x + x_0)^4 (x - x_0)^2 , \qquad (21)
$$

representing a critical phase at $x = -x_0$ coexisting with a noncritical phase at $x = x_0$. The tricritical temperature is T_{tc} and $x_0^2 = T_{tc} - T$. Furthermore, consider the choice

$$
\gamma_s(x_1) = -\frac{g}{2}x_1^2 \tag{22}
$$

Although no surface fields are present there is preferential adsorption because f is now intrinsically asymmetric with respect to interchange of x_0 and $-x_0$, reflecting the physical distinction between the bulk phases.

In this model one finds $\gamma_{+} = \frac{4}{3} c x_0^4$ and, for $g < 0$, partial wetting by the critical phase is obtained all the way to the tricritical point. In fact, as $T \rightarrow T_{tc}^-$,

$$
\cos\theta \to -\frac{3}{8} \quad . \tag{23}
$$

All the examples presented so far have the following features in common. The substrate-adsorbate energy $\gamma_s(x_1)$ has a minimum at (or near) the critical value of the bulk order parameter $x = 0$. In any case, as $T \rightarrow T_c$, the minimum moves to $x_1 = 0$ at least as fast as
 $x_0 \sim (T_c - T)^{1/2}$. Secondly, γ_s or the bulk function f should have some asymmetry in the order parameter in order to guarantee preferential adsorption. '

Scaling theory^{5,15} predicts that the cosine of the contact angle is a scaling function of the form

$$
\cos\theta = X(h_1 t^{-\Delta_1}, g t^{-\phi_1}, h_3 t^{-\Delta_3}) \tag{24}
$$

where $t = (T_c - T)/T_c \ll 1$. Many physical scenarios are compatible with this relationship. One checks that the behaviors outlined in this paper can be cast in this form and the corresponding values of Δ_1 , ϕ_1 , or Δ_3 can be easily read off. Cahn's argument¹ goes further by assuming that, e.g.,

$$
\cos\theta \sim h_1 t^{-\Delta_1} \tag{25}
$$

in the entire partial-wetting regime. From this would necessarily follow critical-point wetting (given $\Delta_1 > 0$). However, Eq. (25) presents only one possibility compatible with scaling theory, and is in fact contradicted by most of the present examples.

A subject of further research will be the effect of longrange forces on persistent partial wetting and criticalpoint dewetting.

This research was supported by the National Fund for Scientific Research in Belgium.

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 36

CRITICAL-POINT DEWETTING 7299

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