Phonon focusing and phonon conduction in orthorhombic and tetragonal crystals in the boundary-scattering regime. II

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Striking differences (up to a factor of 100) are predicted in the intensity of phonons propagating ballistically along difFerent directions in certain orthorhombic and tetragonal crystals. The predicted results arise from phonon focusing due to elastic anisotropy, due to the fact that in elastically anisotropic crystals the phonon phase and group velocities are, in general, not collinear. Conditions for the existence of cuspidal edges in group-velocity surfaces are given in symmetry planes along all directions where the phase and group velocities are collinear. Approximate amplification factors have been calculated for phonons of each polarization along symmetry-plane collinear axes. An analytic expression is also given for the nonsymmetry collinear direction for the longitudinal and one of the transverse modes. Calculations have been performed for a number of crystals and demonstrate that the phonon-focusing property can cause difFerences in the phonon transport in the boundary-scattering regime by more than 80%.

I. INTRODUCTION

Thermal energy in dielectric solids is carried by phonons. At sufficiently low temperatures the phonons propagate ballistically so that in the absence of defect or impurity scattering the mean free path becomes limited by the linear dimensions of the sample.¹ A theory of the thermal conductivity applicable to this temperature range was first developed by Casimir.² Corrections to Casimir's theory have been derived for samples of finite length, ' for samples in which a fraction of the phonon are specularly reflected from the end surfaces,⁴ and for samples in which phonon focusing
is important.^{5,6} is important.

For superconducting metals in the temperature range $T/T_c \ll 1$, there are negligible normal-state electrons to carry heat' so that thermal transport is dominated by phonon-scattering processes. At the lowest temperatures where the electronic scattering of phonons can be insignificant, the phonon mean free path becomes limited by scattering from sample boundaries and crystal imperfections. For a sufficiently defect-free superconductor, i.e., $\Lambda_{ph} \sim l$, the thermal conductivity at $T/T_c \ll 1$ should be determined by the same factors as in a dielectric crystal. This is indicated in the most recent measurements on niolium' where at lowest temperatures $\Lambda_{ph} \sim l$, and the thermal conductivity was proportional to $T³$, characteristic of the Casimir result.

Recent heat-pulse measurements^{9,10} have shown striking differences in the intensity of phonons propagating ballistically in an elastically anisotropic crystal. These results were shown to arise from phonon focusing due to the fact that the phase and group velocities are not collinear except along

certain axes. It is only along these axes that the energy flow or ray vector is in the same direction as the wave vector. Because of elastic anisotropy the angular deviation between the phase and group velocities varies with the direction of the wave vector. Phonon focusing occurs when the direction of the group velocity varies more slowly than in an elastically isotropic solid. Furthermore, for certain ratios between the elastic constants, two or more wave vectors can give rise to the same group-velocity direction and the group-velocity surface is said to have cuspidal edges. Conditions for cuspidal edges have been derived by Musfor cuspidal edges have been derived by Mus-
grave,¹¹ Maris,¹² and McCurdy.¹³ Maris¹² has pointed out that the presence of cusps increases the phonon intensity, particularly along the edges where the direction of the group velocity varies slowly with wave vector. As a result the energy flow is enhanced about cuspidal or highly focused directions and significantly decreased along other directions.

Subsequent measurements of the thermal conductivity of silicon and calcium fluoride in the boundary- scattering regime demonstrated anisotropies ary-scattering regime demonstrated anisotropies
of up to 50% for silicon and 40% for calcium fluo-
ride.^{5,6} The predictions of Casimir's theory, ride. The predictions of Casimir's theory, generalized to allow for phonon focusing, gave quantitative agreement with experimental results. Similar anisotropies in the thermal conductivity have been predicted for sufficiently defect-free, have been predicted for sufficiently defect-free,
superconducting lead and niobium at $T/T_c \ll 1.^{14}$

Phonon-focusing effects have also been predicte
elastically anisotropic hexagonal crystals.¹³ in elastically anisotropic hexagonal crystals. Subsequent heat-pulse measurements in solid 4He by Narayanamurti and Dynes¹⁵ indicated a phonon intensity approximately 45° to the c axis, consisintensity approximately 45° to the *c* axis, consistent with predictions of a cuspidal edge.¹³ Calcu

18 6576

In this paper phonon-focusing effects are studied in orthorhombic and tetragonal crystals. Results derived for the hexagonal lattice¹³ (hereafter referred as paper I) are generalized to include all the symmetry planes of the orthorhombic, tetragonal, and cubic lattices. Conditions for phonon focusing, and for the existence of cuspidal edges about collinear axes, are given for wave vectors in symmetry planes. Approximate phonon amplification factors are calculated for phonons of each polarization along high-symmetry collinear axes. Calculations of phonon focusing are given for a number of crystals, and calculations of thermal conductivity are given for one orthorhombic, one tetragonal, and one cubic crystal. Strong phonon focusing is predicted to have a dramatic effect upon the phonon conductivity. For sufficiently defect-free solids, this should be observable in dielectrics at temperatures which are a small fraction of the Debye temperature, but for superconductors at temperatures which are a small fraction of the superconducting transition temperature.

II. THEORY

A. Calculation of phonon phase and group velocities

The solutions for the phonon phase velocities in the symmetry planes of the orthorhombic, tetragonal, cubic, and hexagonal elastic solids are well known.¹⁶⁻¹⁸ For any symmetry plane of these lattices the phonon phase velocities can be expressed in terms of generalized elastic constants $as¹⁹$

$$
s_1^2 = (a_1 \sin^2 \theta_k + a_2 \cos^2 \theta_k) / \rho \tag{1}
$$

and

$$
s_{0,2}^{2} = \frac{1}{2}\rho \{ (a_{3} \sin^{2} \theta_{k} + a_{4} \cos^{2} \theta_{k})
$$

$$
\pm |[(a_{5} \sin^{2} \theta_{k} - a_{6} \cos^{2} \theta_{k})^{2} + (2a_{7} \sin \theta_{k} \cos \theta_{k})^{2}]^{1/2} |.
$$
 (2)

The displacement vector \mathbf{u} , giving the direction of the deformation for wave vectors in symmetry planes, is given by 20

$$
\vec{u}_1 = (\vec{e} \times \vec{n})/[1 - (\vec{e} \cdot \vec{n})^2]^{1/2},
$$
\n
$$
\vec{u}_{0,2} = \vec{n} - \left(\frac{a_5 \sin^2 \theta_k + (2a_7 - a_6) \cos^2 \theta_k}{2a_7 \cos \theta_k} + \frac{[(a_5 \sin^2 \theta_k - a_6 \cos^2 \theta_k)^2 + (2a_7 \sin \theta_k \cos \theta_k)^2]^{1/2}}{2a_7 \cos \theta_k}\right) \vec{e}.
$$
\n(3)

In these equations, s is the phase velocity, ρ is the density, the a_i are second-order elastic constants or linear combinations of these constants, \overrightarrow{n} is a unit vector in the direction of the wave vector, and \vec{e} is a unit vector parallel to the $\vec{\eta}$ axis. The angle θ_b gives the angular direction of the wave vector in a symmetry plane measured with respect to the η axis. For any symmetry plane containing the z axis, the η axis is chosen parallel to the [001] direction, but for the (001) symmetry plane the η axis is chosen parallel to the [100] direction. Expressions for the generalized constants a_i for each of the symmetry planes of the orthorhombic, tetragonal, and cubic lattices are orthorhombic, tetragonal, and cubic lattices are
given in Table L^{21} Expressions for the hexagona lattice for symmetry planes containing the c axis are also included in this table. The subscripts 0, 1, 2 on the phase veLocity and the disp1acement vector refer to the different modes of propagation which will be designated as the fast, transvers T_1 , and slow modes, respectively.²² The sign T_1 , and slow modes, respectively.²² The sign preceding the radical in Eq. (2) is positive for the fast mode and negative for the slow mode, but is negative for the fast mode and positive for the slow mode in Eq. (4). Note that $2\rho s^2 = a_4 + |a_6|$ for the fast mode, but $a_4 - |a_6|$ for the slow mode when $\theta_{\rm k}$ = 0°, and that $2\rho s^2 = a_{\rm s} + |a_{\rm s}|$ for the fast mode, but $a_n - |a_n|$ for the slow mode when $\theta_b = 90^\circ$ so that the fast mode is always of higher velocity than the slow mode. A schematic diagram of ρs^2 for each of the different modes in an orthorhombic lattice is shown in Fig. 1. The μs^2 surfaces for a tetragonal crystal are shown in Fig. 2.

Conditions for elastic stability place restrictions on the constants a_i . In order for a solid to be elastically stable the determinant $|C_{\alpha\beta}|$ of the elastic matrix must be positive. This in turn requires
that the sequential principal minors be positive.²³ that the sequential principal minors be positive.²³ Furthermore, since an identical permutation of the rows and columns of the determinant $|C_{\alpha\beta}|$ can bring any principal minor to the top left corner, there are three equivalent sets of conditions for elastic stability in the orthorhombic lattice. These are given by inequalities (6). For the orthohombic lattice

$$
C_{11} > 0
$$
, $C_{22} > 0$, $C_{33} > 0$,
 $C_{44} > 0$, $C_{55} > 0$, $C_{66} > 0$, (5)

$$
C_{11}C_{22} > C_{12}^2
$$
 or $C_{11}C_{33} > C_{13}^2$ or $C_{22}C_{33} > C_{23}^2$, (6)

and

6578

$$
C_{33}(C_{11}C_{12} - C_{12}^2)^2 > C_{23}^2 C_{11} + C_{13}^2 C_{22} - 2 C_{12} C_{13} C_{23}.
$$
\n(7)

lm the tetragonal lattice there are only two equivalent sets of conditions for stability. These are inequalities (9). For the tetragonal lattice

$$
C_{33} > 0, \quad C_{44} > 0, \quad C_{66} > 0,
$$
 (8)

$$
C_{11} > |C_{12}| \text{ or } C_{11}C_{33} > C_{13}^2, \tag{9}
$$

and

$$
C_{33}(C_{11} + C_{12}) > 2C_{13}^2. \tag{10}
$$

Since C_{11} > $|C_{12}|$ it follows that C_{11} > $(C_{11} + C_{12})/2$ > 0 so that inequalities (9) and (10) can be written as

$$
C_{11}C_{33} > C_{33}(C_{11} + C_{12})/2 > C_{13}^2.
$$
 (11)

In a similar way, conditions for elastic stability in the hexagonal lattice can be expressed as

$$
C_{33} > 0, \quad C_{44} > 0 \tag{12}
$$

$$
\begin{array}{c}\n\circ \\
\circ \\
\circ\n\end{array}
$$

$$
C_{11}C_{33} > C_{33}(C_{11} + C_{12})/2 > C_{13}^2, \qquad (13)
$$

and for the cubic lattice as

$$
C_{11} > 0, \quad C_{44} > 0 \tag{14}
$$

and

$$
C_{11}^2 > C_{11}(C_{11} + C_{12})/2 > C_{12}^2.
$$
 (15)

In hexagonal crystals $C_{66} = (C_{11} - C_{12})/2$ so that inequality (12) can be written as

$$
C_{11}C_{33} > C_{33}(C_{11} - C_{66}) > C_{13}^2, \qquad (16)
$$

which requires $C_{11} > C_{66}$, whereas $C_{11} < C_{66}$ in one known tetragonal crystal, paratellurite.

The above conditions require $a_1 > 0$, $a_2 > 0$, a_3 > 0 , and $a_4 > 0$. Since it is physically more reason-
able, a_7 will be chosen positive.²⁴ Constants a_5 and able, a_{7} will be chosen positive. 24 Constants a_{5} and $a₆$ are greater than zero for all known materials with one recently discovered exception, paratellwith one recently discovered exception, paratel
urite, a tetragonal piezoelectric crystal.^{25,26} In this material at room temperature C_{66} > C_{11} , so that a_5 and a_6 are negative in the (001) symmetry plane. As a result the fast mode is quasitransverse and the slow mode quasilongitudinal in the (001) plane near the $[100]$ and $[010]$ directions. Furthermore, since $C_{66} > C_{11}$, $a_1 > (a_3 + a_5)/2$ for the (010) or (100) symmetry planes so that the

TABLE I. Values of the generalized elastic constants in symmetry planes of orthorhombic, tetragonal, hexagonal, and cubic crystals.

FIG. 1. ρs^2 surfaces of orthorhombic gallium in symmetry planes. In this material a_5 and $a_6 > 0$ for all three symmetry planes. Note particularly the interesting character of the phase velocity surface, for example, where ρs^2 equals C_{55} in the [001] direction. This surface is T_1 in the (100) plane but T_2 in the (010) plane.

phase velocity of the transverse T_1 mode exceeds the phase velocity of the fast mode along the [100] and $[010]$ axes.

From Eq. (4) it can be seen that if $a_e > 0$ the fast mode is quasilongitudinal and the slow mode quasitransverse²⁷ near η_{\perp} , but if a_{5} < 0 the fast mode is quasitransverse and the slow mode quasilongitudinal near this direction. Similarly, if $a_6 > 0$ the fast mode is quasilongitudinal and the slow mode

FIG. 2. ρs^2 surfaces of tetragonal indium in symmetry planes. In this material a_5 and $a_6 > 0$ for all three symmetry planes. Note in this case, because of the equivalence of the [100] and [010] axes, the phase-velocity modes in the (100) and (010) planes are the same in the [001] direction. The abscissa of the T_2 surface in the (001) plane along the [110] axis is $\frac{1}{2}(C_{11}- C_{12})$.

quasitransverse near the η axis, but if $a_6 < 0$ the fast mode is quasitransverse and the slow mode quasilongitudinal near this axis.

In symmetry planes the components of group velocity parallel and perpendicular to the η axis, respectively, can be determined using the relations²⁸

$$
v_{\parallel} = \frac{\partial s}{\partial (\cos \theta_k)}
$$
 and $v_{\perp} = \frac{\partial s}{\partial (\sin \theta_k)}$. (17)

The direction θ_n of the group velocity can then be determined by the relation

$$
\tan \theta_v = v_\perp / v_\parallel \,. \tag{18}
$$

For the T_1 mode this expression becomes

$$
\tan \theta_v = (a_1/a_2) \tan \theta_k
$$

or

$$
\cot \theta_v = (a_2/a_1) \cot \theta_k, \qquad (19)
$$

and for the fast and slow modes

$$
\tan \theta_v = (u/v) \tan \theta_k, \qquad (20)
$$

where

$$
u = a_3 \pm \frac{a_5^2 \tan^2 \theta_k + 2a_7^2 - a_5 a_6}{\left[(a_5 \tan^2 \theta_k - a_6)^2 + (2a_7 \tan \theta_k)^2 \right]^{1/2}}
$$
 (21)

$$
v = a_4 \pm \frac{(2a_7^2 - a_5a_6)\tan^2\theta_h + a_6^2}{\left[\left((a_5\tan^2\theta_h - a_6)^2 + (2a_7\tan\theta_h)^2\right]^{1/2}\right]},
$$
 (22)

with the "+" sign used for fast waves and the "-" sign for slow waves.

For directions nearly perpendicular to the η axis it is more convenient to use

$$
\cot \theta_v = (u'/v') \cot \theta_k, \qquad (23)
$$

where u' is u and v' is v, but with a_3 and a_4 interchanged, a_5 and a_6 interchanged, and with $\cot \theta_k$ replacing tan θ_k .

The angular deviation between the group and phase velocities can be written in the convenient $form^{29,30}$

$$
\tan(\theta_v - \theta_k) = \frac{1}{s} \frac{\partial s}{\partial \theta_k} = \frac{1}{2s^2} \frac{\partial s^2}{\partial \theta_k}.
$$
 (24)

These equations make it possible to calculate the angle between the phase and group velocities for each mode along all wave-vector directions in symmetry planes. In elastically anisotropic crystals the phonon phase and group velocities are collinear for only certain directions determined by the symmetry and the kind of anisotropy.

For certain ratios between the elastic constants it is possible to find values of θ_v for the slow mode which permit more than one corresponding value of θ_k . In these regions the values of θ_k can be double or triple valued and the group-velocity sur-

FIG. 3. Relation between the direction of the wave vector and the group-velocity vector in the (001) plane for orthohombic potassium pentaborate using the elastic constants of Cook and Jaffe. Angles are measured with respect to the [100] axis. Note the negative slope of the T_2 curve near θ_2 , indicating a cusp about that direction. Wave vectors in directions θ_2 , θ_3 , and θ_4 all give rise to group-velocity vectors in the θ_2 direction.

FIG. 4. Relation between the direction of the wave vector and the group-velocity vector in the (001) plane of gallium using the elastic constants of Lyall and Cochran. Angles are measured with respect to the [100] axis. Note the cuspidal edges in the T_2 mode about the [100] and [010] axes.

face is said to have cuspidal edges (see Figs. 3 and 4).

Cuspidal edges can occur not only when the wave vectors are confined to symmetry planes, but also for wave vectors on either side of a symmetry plane. In the orthorhombic lattice there are collinear directions, not contained in any symmetry plane, about which cuspidal edges can occur. Cuspidal edges occurring for wave vectors confined to symmetry planes are discussed in See. IID. Cuspidal edges occurring for wave vectors on either side of a symmetry plane are discussed in See. III.

B. Calculations of collinear and pure-mode axes

A collinear axis will be defined as one along which the phase velocity or wave vector and the corresponding group velocity or ray vector are collinear. It should be emphasized that $\omega_l v$ along these axes is the flow of energy in the same direction as the wave vector. Since collinearity requires $\theta_p = \theta_k$, Eq. (24) shows that collinear points in symmetry planes are points where $\partial s/\partial \theta_k$ is zero and thus, are points of tangency to the phase-velocity surface. A pure-mode axis, however, is one along which the displacement or polarization vector and the wave vector are parallel for a pure longitudinal wave or perpendicular for pure transverse waves. Since the three polarization vectors are mutually perpendicular for each value of the wave vector, a pure-mode axis is a direction along which a pure longitudinal and two pure transverse waves propagate. Pure-mode axes for a number of cry-
stal symmetries have been given by Brugger.³¹ A stal symmetries have been given by Brugger. Although pure modes propagate in general only for wave vectors parallel to the x , y , and z axes, directions which incidently are also collinear axes for all modes, pure transverse and pure longitudinal waves also propagate along all longitudinal (collinear) axes.

The solution for the collinear axes in symmetry planes can be obtained from Egs. (20) – (22) . It is clear that the transverse T_1 mode, although a pure transverse wave, has no collinear axes except for $\theta_b = 0^0$ and 90^0 unless $a_1 = a_2$, in which case this mode is collinear for all wave-vector directions in that symmetry plane. The solution for the collinear axes for the fast and slow modes in symmetry planes yields the values $\theta_b = 0^0$ and 90^0 required by symmetry, as well as a quadratic equation in $tan^2\theta_k$, whose roots are

$$
\tan^2\theta_k = (a_6 + a_7)/(a_5 + a_7)
$$

or

$$
\tan^2\theta_k=(a_6-a_7)/(a_5-a_7).
$$

The collinear axis θ_s for the slow mode which in

18

general is quasitransverse³² near θ_s is

 \overline{B}

$$
\tan \theta_s = [(a_6 + |a_7|)/(a_5 + |a_7|)]^{1/2}, \tag{25}
$$

and the collinear axis θ_t for the fast mode which is pure longitudinal at θ_t is

$$
\tan \theta_f = [(a_6 - |a_7|)/(a_5 - |a_7|)]^{1/2}.
$$
 (26)

Equation (26) thus gives the collinear axis for the longitudinal mode and the direction along which a pure longitudinal and two pure transverse waves propagate.

For nonsymmetry planes solutions for the collinear axes can be found using the defining relations

$$
s_x = ls = v_x = \frac{\partial s}{\partial l},
$$

\n
$$
s_y = ms = v_y = \frac{\partial s}{\partial m},
$$

\n
$$
s_z = ns = v_z = \frac{\partial s}{\partial n};
$$

\n(27)

thus the direction cosines of the collinear axes can be expressed as

$$
l=\frac{1}{s}\ \frac{\partial s}{\partial l}\ ,\ \ m=\frac{1}{s}\ \frac{\partial s}{\partial m}\ ,\ \ n=\frac{1}{s}\ \frac{\partial s}{\partial n}\ .
$$
 (28)

Brugger³¹ used a method due to Borgnis³³ to derive the relations for the collinear axes for the longitudinal mode. Using the notation in this paper, his results can be expressed as

$$
\frac{m}{l} = \left(\frac{a_{xx}^* b_{xx}^* - a_{xx}^* b_{yx}^* - b_{xy}^* b_{xx}^*}{a_{yx}^* b_{yx}^* - a_{yx}^* b_{xx}^* - a_{xy}^* b_{yx}^*}\right)^{1/2},
$$
\n(29)

$$
\frac{n}{l} = \left(\frac{a_{xy}^+ b_{xy}^- - a_{yz}^+ b_{xy}^- - a_{zx}^+ a_{xy}^-}{a_{yx}^+ b_{yz}^- - a_{yz}^+ b_{xz}^- - a_{xy}^+ b_{yz}^-}\right)^{1/2},
$$
\n(30)

where

$$
a_{xy}^* = (a_5 - a_7)_{xy} = C_{22} - 2C_{66} - C_{12},
$$

\n
$$
a_{xz}^* = (a_5 - a_7)_{xz} = C_{11} - 2C_{55} - C_{13},
$$

\n
$$
a_{yz}^* = (a_5 - a_7)_{yz} = C_{22} - 2C_{44} - C_{23},
$$

\n
$$
b_{xy}^* = (a_6 - a_7)_{xy} = C_{11} - 2C_{66} - C_{12},
$$

\n
$$
b_{xz}^* = (a_6 - a_7)_{xz} = C_{33} - 2C_{55} - C_{13},
$$

\n
$$
b_{yz}^* = (a_6 - a_7)_{yz} = C_{33} - 2C_{44} - C_{23}.
$$

\n(31)

The double-letter subscripts designate the planes in Table I where the values of a_5 , a_6 , and a_7 are given in terms of the second-order elastic constants. The angle ϕ_f of the collinear axis for the fast mode can be calculated from

$$
\tan \phi_f = m/l \tag{32}
$$

and the angle θ_f can be found by using

 $\tan\theta_f = l/n \cos\phi_f$. (33)

For one of the transverse modes, however, the

results for the collinear axis are equivalent to a change in the signs of some of the terms in Brugger's expression for the longitudinal mode. These results are

$$
\frac{m}{l} = \left(\frac{a_{xx}^* b_{xx}^* - a_{xx}^* b_{yx}^* - b_{xy}^* b_{xx}^*}{a_{xx}^* b_{xy}^* - a_{yx}^* b_{yx}^* - a_{xy}^* b_{yx}^*}\right)^{1/2}
$$
(34)

and

$$
\frac{n}{l} = \left(\frac{a_{xy}^+ b_{xy}^- - a_{yz}^+ b_{xy}^- - a_{xz}^+ a_{xy}^-}{a_{yx}^+ b_{yx}^+ - a_{yz}^+ b_{xz}^+ - a_{xy}^+ b_{yz}^+}\right)^{1/2},
$$
\n(35)

where

$$
a_{xz}^{+} = (a_{5} + a_{7})_{xz} = C_{11} + C_{13},
$$

\n
$$
a_{yz}^{+} = (a_{5} + a_{7})_{yz} = C_{22} + C_{23},
$$

\n
$$
b_{xz}^{+} = (a_{6} + a_{7})_{xz} = C_{33} + C_{13},
$$

\n
$$
b_{yz}^{+} = (a_{6} + a_{7})_{yz} = C_{33} + C_{23}.
$$
\n(36)

The angles ϕ_s and θ_s of the collinear axis for this transverse mode can be calculated from Eqs. (32) and (33) but with ϕ_s replacing ϕ_f , and θ_s replacing θ_f . Collinear axes for a number of orthorhombic materials are tabulated in Table II. The elastic constants of these materials listed in Table II are tabulated in Table XVI.

C. Approximate phonon-amplification factor for cusp-free velocity surfaces about collinear axes in symmetry planes

A cusp-free surface is one for which there is one and only one wave vector for each group-veloce ity direction.³⁴ Since an elastically anisotropic ority direction. Since an elastically anisotropic orthorhombic lattice has no transverse isotropy, exact analytic expressions cannot be obtained for the phonon-amplification factor as in the case of the hexagonal lattice. To find the cusp-free phonon-amplification factor for a nonhexagonal lattice consider first a collinear direction which is the intersection of two mutually orthogonal symmetry intersection of two mutually orthogonal symmetr
planes,³⁵ and consider all the group-velocity directions in a solid angle $\Delta\Omega_v$ subtended by a detector, all points of which are within a small angle $\Delta\theta$ from the collinear axis. Each phonon trajectory or group-velocity direction corresponds to a wave vector in a direction $\Delta\theta_k$ from the collinear axis which because of elastic anisotropy is different from $\Delta\theta_v$ both in angular distance from the collinear axis and in azimuthal angle from a reference symmetry plane. The phonon-amplification factor A is defined as the ratio of the solid angle $\Delta\Omega_k$ in wave-vector or k space to the corresponding solid angle $\Delta\Omega_v$ in group-velocity space. If there are no cuspidal edges in the group-velocity surface, then each group-velocity has only one corresponding value of wave vector, and the phonon-amplification factor (PAF} in the collinear

TABLE II. Collinear and pure-mode axes in nonsymmetry planes of orthorhombic crystals. The collinear axis for the longitudinal mode is also a pure-mode axis. Double-starred values were found by a numerical search method; other values were found analytically.

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direction for an infinitesimal solid angle is

 $A = \Delta \Omega_b / \Delta \Omega_v$. (37)

The area of the group-velocity space for phonons arriving at the detector subtending an angle $\Delta\theta_n$ about the collinear axis is given by

$$
\Delta\Omega_v = \pi (\Delta\theta_v)^2 \,. \tag{38}
$$

In an orthorhombic material, for a circular groupvelocity space, the wave-vector space for a cuspfree surface is nearly elliptical and its area is $\Delta\Omega_k = \pi(\Delta\theta_k)_a(\Delta\theta_k)_b$. (39)

The subscripts a and b refer to mutually orthogon-The subscripts a and b refer to mutually ortho
al symmetry planes,³⁶ and ($\Delta\theta_k$)_a, ($\Delta\theta_k$)_b are the angles subtended by the quasiellipse's semimajor and semiminor axes, respectively. The width of the wave-vector space in a symmetry plane which corresponds to $\Delta\theta_n$ is given by

$$
(\Delta \theta_k)_a = (d\theta_k / d\theta_v)_a \Delta \theta_v \tag{40}
$$

 ${\bf 18}$

$$
(\Delta \theta_{\mathbf{k}})_b = (d\theta_{\mathbf{k}}/d\theta_{\mathbf{v}})_b \Delta \theta_{\mathbf{v}} . \qquad (41)
$$

When the arrival points of the phonons on the detector surface lie within a circle, the amplification factor can be written

$$
A(\theta_k, \phi_k) = \frac{\Delta \Omega_k}{\Delta \Omega_v} = \frac{\pi (d\theta_k/d\theta_v)_a \Delta \theta_v (d\theta_k/d\theta_v)_b \Delta \theta_v}{\pi (\Delta \theta_v)^2}
$$

which simplifies to

$$
A(\theta_{k}, \phi_{k}) = (d\theta_{k}/d\theta_{v})_{a} (d\theta_{k}/d\theta_{v})_{b}.
$$
 (42)

Numerically it is more convenient, however, to use a circular wave-vector space

$$
\Delta \Omega_{\mathbf{k}} = \pi (\Delta \theta_{\mathbf{k}})^2 \tag{43}
$$

and calculate the corresponding group-velocity space $\Delta\Omega_v$. This is far more efficient in computer time than trying to calculate the wave-vector space for a circular group-velocity space where a binary search technique would have to be used for each point on the boundary of the surface. Examples of some calculated group-velocity spaces are plotted in Figs. 5 and 6 for a 1° departure from the collinear axis and 2° increments in the azimuthal angle measured from a reference symmetry plane. As the figures indicate, most of these spaces are'nearly ellipses which subtend solid angles given by

$$
\Delta\Omega_v = \pi (\Delta\theta_v)_a (\Delta\theta_v)_b . \tag{44}
$$

For an infinitesimal detector the resulting expression for the PAF is independent of whether $\Delta\Omega$ or, conversely, $\Delta\Omega$ is chosen circular and, in fact, is really independent of the exact shape of the solid angle.

Selection of the appropriate phase-velocity surfaces in the mutually orthogonal symmetry planes is important. Figure 1 shows that the $T₁$ surface in the (100) symmetry plane meets the $T₂$ surface in the (010) symmetry plane along the $[001]$ direction where $\rho s^2 = C_{55}$. To determine the PAF in the [001] direction for the $\rho s^2 = C_{55}$ surface, one must multiply the $(d\theta_{k}/d\theta_{v})_{a}$ of the T_{2} mode in the (010) plane by the $(d\theta_{\mathbf{k}}/d\theta_{\nu})_b$ of the T_1 mode in the (100) plane.

The $[001]$ direction for the tetragonal and the $\langle 100 \rangle$ directions for the cubic lattice have two sets of orthogonal symmetry planes so that the PAF defined in the above manner for transverse waves does not have a unique value. In fact, since the transverse surfaces involved are neither circles nor ellipses (see Fig. 7), this condition is irrelevant. In this case, the area can be determined by numerical integration, which yields results that are in close agreement with those calculated from the averages of explicit expressions to be given in Table V.

FIG. 5. Group-velocity directions which correspond to a quarter-circle of wave vectors located one degree from the [100] axis in gallium. For the counterclockwise rotation of the wave vector, the L and T_1 vectors rotate counterclockwise. The $T₂$ vector rotates clockwise because of the cusp about the [100] axis in the (001) plane. The origin is the $[100]$ axis and the x and y axes are the (001) and (010) symmetry planes, respectively.

Along the η axis the derivative $d\theta_{\mathbf{k}}/d\theta_{\mathbf{v}}$ for the T_1 mode is given as follows:

$$
\left. \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_0 = 0} = \frac{a_2}{a_1} \,. \tag{45}
$$

For the other two modes it is

$$
\left. \frac{d\theta_{k}}{d\theta_{v}} \right|_{\theta_{k} = \theta_{v} = 0} = \frac{a_{4} \pm |a_{6}|}{a_{3} \pm (2a_{7}^{2} - a_{5}a_{6})/|a_{6}|}
$$
(46)

where the 4 ⁻ sign is used for the fast mode, the "-" sign for the slow mode, and the magnitude bars on a_6 for the case when $a_6 < 0$. In symmetry planes in directions perpendicular to the η axis the results are the same, but with a_1 and a_2 interchanged, a_3 and a_4 interchanged, and a_5 and a_6 interchanged.

Along the collinear axis θ_s , for the slow mode³⁷

FIG. 6. Group-velocity directions which correspond to ^a semicircle of wave vectors located 1' from the θ_0 and the θ_1 axis in the (001) plane of gallium. For wave vectors around θ_0 , the origin is the [100] axis and the x and y axes are the (001) and (010) symmetry planes, respectively. For wave vectors around θ_{1} , the origin is the $[010]$ axis and the x and y axes are the (001) and (100) symmetry planes, respectively. Both vectors rotate counterclockwise.

6584

$$
\frac{d\theta_{k}}{d\theta_{v}}\bigg|_{\theta_{k}=\theta_{v}=\theta_{s}} = \left(1 - \frac{4(a_{6}+|a_{7}|)(a_{5}+|a_{7}|)(a_{5}a_{6}-a_{7}^{2})}{|a_{7}|[(a_{5}+|a_{7}|)+(a_{6}+|a_{7}|)][\frac{1}{2}(a_{4}+a_{6})(a_{5}-a_{6})+(a_{4}-|a_{7}|)(a_{6}+|a_{7}|)]}\right)^{-1}
$$
(47)

and along the collinear axis θ_f , for the fast mode the same expression applies, but the signs preceding
each $|a_r|$ are interchanged.³⁸ This result can be rewritten as each $|a_{7}|$ are interchanged.³⁸ This result can be rewritten as

$$
\frac{d\theta_{\mathbf{a}}}{d\theta_{\mathbf{v}}} \bigg|_{\theta_{\mathbf{a}} = \theta_{\mathbf{b}} = \theta_{\mathbf{f}}} = \left(1 - \frac{4(|a_{\tau}| - a_{\mathbf{b}})(|a_{\tau}| - a_{\mathbf{b}})(a_{\tau}^2 - a_{\mathbf{a}}a_{\mathbf{b}})}{|a_{\tau}|[(|a_{\tau}| - a_{\mathbf{b}}) + (|a_{\tau}| - a_{\mathbf{b}})][\frac{1}{2}(a_{4} + a_{\mathbf{b}})(a_{\mathbf{a}} - a_{\mathbf{b}}) + (|a_{\tau}| + a_{\mathbf{a}})(|a_{\tau}| - a_{\mathbf{b}})]}\right)^{-1}.
$$
\n(48)

Explicit expressions for the approximate PAF for orthorhombic, tetragonal, and cubic lattices are given in Tables III-V. Expressions for some directions have. been omitted in the tetragonal and cubic tables since these are easily obtained from the orthorhombic and tetragonal expressions, respectively.

Consider now the phonon-amplification factor along the collinear axes in one symmetry plane only, for cusp-free group-velocity surfaces. Consider also a circular phonon detector, a distance D from a phonon source, centered about the collinear axis with its boundaries at an angle $\Delta\theta_n$ of approximately 1' from the collinear axis. The wave vectors which give rise to the phonons that strike the circular detector are found to lie in a solid angle which is almost elliptical (see Fig. 8). If a and b are the lengths of the semimajor and semiminor axes, respectively, of the quasiellipse surrounding the collinear direction, the PAF can be written

$$
A = \Delta \Omega_{\rm h} / \Delta \Omega_{\rm v} = \pi a b / \pi (D \Delta \theta_{\rm v})^2
$$

Furthermore, if the distance D from the phonon source to the detector is unity,

FIG. 7. Group-velocity directions which correspond to a quarter-circle of wave vectors located 1° from the f100] axis in cubic calcium fluoride. Note that the surfaces for the transverse modes are neither circles nor ellipses. Note also the cusp about the $(01\bar{1})$ plane in the $T₁$ mode where three different wave vectors give rise to the same group-velocity direction. For wave vectors rotated counterclockwise about the [100] axis, the group-velocity vectors all rotate counterclockwise. The origin is the $[100]$ axis and the x and y axes are the (001) and (010) symmetry planes, respectively.

$$
A = ab/(\Delta \theta_v)^2. \tag{49}
$$

When b lies in a symmetry plane which contains the [001] axis and the PAF along θ_2 is being considered, then

$$
b = \Delta \theta_{\mathbf{k}} = \Delta \theta_{\mathbf{v}} \left. \frac{d\theta_{\mathbf{k}}}{d\theta_{\mathbf{v}}} \right|_{\Theta_{\mathbf{p}} = \Theta_{\mathbf{k}} = \Theta_{2}}
$$
(50)

and the PAF becomes

$$
A = \frac{a}{\Delta \theta_v} \left. \frac{d\theta_k}{d\theta_v} \right|_{\theta_v = \theta_k = \theta_2}.
$$
 (51)

The $d\theta_{\nu}/d\theta_{\nu}$ factor was given in Eq. (47), but the factor $a/\Delta\theta_v$ is most easily determined numerically and is the same regardless of whether the solid angle, $\Delta\Omega_k$ or $\Delta\Omega_v$, is chosen circular. If a circular wave-vector space is chosen, the factor $a/\Delta\theta$. is the ratio of the radius of the wave-vector surface surrounding $\theta_k = \theta_s$ to a semiaxis of the quasiellipse (see Fig. 8) surrounding the collinear axis.

The PAF along the collinear axis θ_f can be found in an analogous manner.

D. Conditions for cuspidal edges in symmetry planes

A cuspidal edge exists for wave vectors in a symmetry plane if $d\theta_h/d\theta_v < 0$. As a result, more than one wave-vector direction in a symmetry plane can give a group-velocity vector along one given direction (see Figs. 3 and 4). Cuspidal edges are always absent in the transverse T_1 mode and in the fast mode. This property is stated as Theorem III and proved in the Appendix.

Conditions for cuspidal edges in the slow mode about the various collinear axes in symmetry planes are as follows:

about the η axis:

$$
a_7^2 > a_6(a_3 + a_5)/2 \quad \text{if} \quad a_6 > 0 \,, \tag{52}
$$

but

$$
a_{7}^{2} > |a_{6}|(a_{3} - a_{5})/2
$$
 if $a_{6} < 0$; (53)

about the η_{\perp} axis:

$$
a_{7}^{2} > a_{5}(a_{4} + a_{6})/2 \quad \text{if} \quad a_{5} > 0, \tag{54}
$$

but

$$
a_7^2 > |a_5|(a_4 - a_6)/2 \quad \text{if} \quad a_5 < 0; \tag{55}
$$

Axis	Surface	Amplification factor
[100]	$\rho S^2 = C_{cc}$	$\left(\frac{C_{66}}{C_{11}}\right)\left(\frac{C_{66}}{C_{22}-(C_{12}+C_{66})^2/(C_{11}-C_{66})}\right)$
[100]	$\rho S^2 = C_{55}$	$\left(\frac{C_{55}}{C_{44}}\right)\left(\frac{C_{55}}{C_{22}-(C_{42}+C_{55})^2/(C_{44}-C_{55})}\right)$
[100]	$\rho S^2 = C_{11}$	$\left(\frac{C_{11}}{C_{55}+(C_{19}+C_{55})^2/(C_{11}-C_{55})}\right)\left(\frac{C_{11}}{C_{66}+(C_{19}+C_{66})^2/(C_{11}-C_{66})}\right)$
[010]	$\rho S^2 = C_{\alpha\beta}$	$\left(\frac{C_{66}}{C_{ee}}\right)\left(\frac{C_{66}}{C_{11}-(C_{12}+C_{66})^2/(C_{22}-C_{66})}\right)$
[010]	$\rho S^2 = C_{14}$	$\left(\frac{C_{44}}{C_{\text{CF}}}\right)\left(\frac{C_{44}}{C_{\text{CP}} - (C_{22} + C_{44})^2/(C_{22} - C_{44})}\right)$
[010]	$\rho S^2 = C_{22}$	$\left(\frac{C_{22}}{C_{11}+(C_{22}+C_{11})^2/(C_{22}-C_{11})}\right)\left(\frac{C_{22}}{C_{22}+(C_{12}+C_{22})^2/(C_{22}-C_{22})}\right)$
[001]	$\rho S^2 = C_{55}$	$\left(\frac{C_{55}}{C_{55}}\right)\left(\frac{C_{55}}{C_{11}-(C_{12}+C_{55})^2/(C_{22}-C_{55})}\right)$
[001]	$\rho S^2 = C_{AA}$	$\left(\frac{C_{44}}{C_{22}}\right)\left(\frac{C_{44}}{C_{22}-(C_{22}+C_{44})^2/(C_{22}-C_{44})}\right)$
[001]	$\rho S^2 = C_{33}$	$\left(\frac{C_{33}}{C_{55}+(C_{12}+C_{55})^2/(C_{32}-C_{55})}\right)\left(\frac{C_{33}}{C_{44}+(C_{23}+C_{44})^2/(C_{33}-C_{44})}\right)$

TABLE III. Expressions for the phonon-amplification factor for orthorhombic lattices.

and about the θ , axis:

$$
4(a_6 + |a_7|)(a_5 + |a_7|)(a_5a_6 - a_7^2)
$$

> |a_7|[a_5 + |a_7|) + (a_6 + |a_7|)]
> $\left[\frac{1}{2}(a_4 + a_6)(a_5 - a_6) + (a_4 - |a_7|)(a_6 + |a_7|)\right]$. (56)

Inequalities (52) and (54) have previously been derived by $Musgrave¹¹$ by considering the inverse phase-velocity surface. Inequality (56) follows from Theorem II in the Appendix.

If a cuspidal edge occurs in the slow mode about the η axis, wave vectors at angle θ_0 can also give group-velocity vectors parallel to the η axis where θ_0 is defined by

$$
\tan^2\theta_0 = \frac{a_5a_6 - 2a_7^2}{a_5^2} \pm \frac{2a_3a_7}{a_5^2} \left(\frac{a_7^2 - a_5a_6}{a_3^2 - a_5^2}\right)^{1/2}, \quad (57)
$$

where the choice in sign must make $\tan^2\theta_0$ positive. Similarly, a cuspidal edge about η_{\perp} gives wave vectors at angle θ_1 with group-velocity vectors along η_{\perp} where $\cot^2\theta_1$ replaces $\tan^2\theta_0$, a_4 replaces a_{3} , and a_{5} is interchanged with a_{6} in Eq. (57).

If, however, a cuspidal edge occurs about the collinear axis θ_s , solving for the other values of θ_k giving $\theta_v = \theta_s$ results in a sixth-degree equation in $\tan \theta_k$. This equation is identical for the fast and slow modes and has no general algebraic solution unless $a_3 = a_4$ and $a_5 = a_6$ as, for example, in the

tetragonal lattice. In this case the $[100]$ and $[010]$ directions are equivalent and the collinear axis for the fast and slow modes is the $[110]$ direction. Because of the symmetry, the equation can be factorized into three quadratic equations:

$$
\tan^2 \theta_k - 2 \tan \theta_k + 1 = 0 \tag{58}
$$

and

$$
\tan^2 \theta_k - 2(a+b)\tan \theta_k + 1 = 0,
$$
\n(59)

where

$$
a \mp b = -\left(\frac{a_{7}^{2} - a_{5}^{2}}{a_{3}^{2} - a_{5}^{2}}\right) \pm \frac{a_{3}}{a_{5}} \frac{\left[(a_{7}^{2} - a_{5}^{2})(a_{7}^{2} - a_{3}^{2})\right]^{1/2}}{a_{3}^{2} - a_{5}^{2}},
$$
\n(60)

giving two pairs of reciprocal roots:

$$
\tan \theta_{3,4} = (a - b) \pm [(a - b)^2 - 1]^{1/2} \tag{61}
$$

or

$$
(a+b) \pm [(a+b)^2 - 1]^{1/2}. \tag{62}
$$

Of course, one pair of these roots will be an extraneous complex conjugate pair for whichever sign gives $(a + b) < 1$.

In general, however, the sixth-degree equation cannot be factored. Although one root, $tan \theta_{s}$, can be extracted, the resulting fifth-degree equation has no general algebraic solution and one of the

6586 G. G. WINTERNHEIMER AND A. K. MCCURDY

TABLE V. Expressions for the phonon-amplification factor for cubic lattices. As in the tetragonal case, when there are two values, their average yields a result which agrees within several percent with that obtained by numerical integration.

			Amplification factor
Axis	Surface	$\phi = 0$, 90° planes	$\phi = -45$, 45° planes
$\langle 100 \rangle$	$\rho S^2 = C_{44}$ (T ₁)		$\left(\frac{2C_{44}}{C_{44}-C_{42}}\right)^2$
$\langle 100 \rangle$	$\rho S^2 = C_{44}$ (T ₂)		$\left(\frac{C_{44}}{C_{11} - (C_{12} + C_{44})^2/(C_{11} - C_{44})}\right)^2 \left(\frac{C_{44}}{\frac{1}{2}(C_{11} + C_{12}) + C_{44} - (C_{12} + C_{44})^2/(C_{11} - C_{44})}\right)^2$
$\langle 100 \rangle$	$\rho S^2 = C_{11}$ (L)		$\left(\frac{C_{11}}{C_{44}+(C_{12}+C_{44})^2/(C_{11}-C_{44})}\right)^2 \qquad \left(\frac{C_{11}}{C_{44}+(C_{12}+C_{44})^2/(C_{11}-C_{44})}\right)^2$
$\langle 111 \rangle$	$\rho S^2 = \frac{1}{3}(C_{11} + 4C_{44} + 2C_{12})$ (<i>L</i>)		$\left(1+\frac{4wx}{(C_{12}+C_{11})yz}\right)^{-2}$
	$w = [C_{11} - C_{44} - (C_{12} + C_{44})][\frac{1}{2}(C_{11} + C_{12}) - (C_{12} + C_{44})]$, $x=\frac{1}{2}(C_{11}+C_{12})(C_{11}-C_{44})-(C_{12}+C_{44})^2$,		
	$y = \frac{1}{2}(C_{11} + C_{12}) + C_{11} - C_{14} - 2(C_{12} + C_{14})$,		
and			
	$z = C_{11}C_{44} + \frac{1}{2}C_{11}(C_{11} + C_{12}) - C_{44}^{2} - 2C_{44}(C_{12} + C_{44}) - (C_{12} + C_{44})^{2}$		

remaining roots must be obtained numerically. It is most convenient to numerically determine a root, tan θ_5 , corresponding to $\theta_v = \theta_s$ for the fast mode. The resulting quartic equation can be facmode. The resulting quartic equation can be fac-
tored using the method of Descartes or Ferrari,³⁹ giving a pair of positive real roots, tan θ_3 and $tan\theta_4$, respectively, and a pair of complex conjugate roots. Such a solution has been performed for a number of crystals and the results are listed in Tables VI-VIII.

 $\sim 10^7$

 (001) $2₁$

FIG. 8. Group-velocity directions which correspond to circles of wave vectors located 1° from the θ_2 and the θ_6 cusp-free collinear axes in the (001) plane of orthorhombic gallium. The larger ellipse surrounds θ_2 ; the smaller is around θ_6 . The y axis is an orthogonal nonsymmetry plane. Both rotations are counterclockwise.

E. Conditions for phonon focusing in symmetry planes about collinear, cusp-free axes

A symmetry plane is cusp free if $d\theta_{\nu}/d\theta_{\nu}>0$ and exhibits cusp-free phonon focusing if $d\theta_{\nu}/d\theta_{\nu} > 1$. Cusp-free phonon focusing thus occurs for wave vectors in a symmetry plane about a collinear axis if $(d\theta_k/d\theta_v)_{\theta_b=\theta_v} > 1.$

Conditions for cusp-free phonon focusing along η for each mode are as follows
fast mode: $a_6^2 > a_7^2$ if $a_6 >$

t mode:
$$
a_6^2 > a_7^2
$$
 if $a_6 > 0$, (63)

but
$$
a_5 a_6 > a_7^2
$$
 if $a_6 < 0$;\n
(64)
(65)

slow mode:
$$
a_7^2 > a_5 a_6
$$
 if $a_6 > 0$, (65)

but
$$
a_7^2 > a_6^2
$$
 if $a_6 < 0$; (66)

$$
T_1 \text{ mode:} \quad a_2 > a_1. \tag{67}
$$

Similarly, conditions for cusp-free focusing along η_1 are as follows:
fast mode: $a_5^2 > a_7^2$ if $a_5 > 0$,

$$
fast mode: \t a_5^2 > a_7^2 \t if \t a_5 > 0,
$$
\t(68)

but
$$
a_5 a_6 > a_7^2
$$
 if $a_5 < 0$; (69)

slow mode:
$$
a_7^2 > a_5 a_6
$$
 if $a_5 > 0$, (70)

but
$$
a_7^2 > a_5^2
$$
 if $a_5 < 0$; (71)

$$
T_1 \text{ mode: } a_1 > a_2 \tag{72}
$$

For cusp-free focusing of the fast mode along θ_f :

$$
a_7^2 > a_5 a_6,\tag{73}
$$

TABLE VI. Collinear axes and other directions associated with cusps in symmetry planes of orthorhombic crystals. The angles θ_i , which are defined as in Figs. 3 and 4, are measured in degrees. In the (010) and (100) planes, entries under θ_0 and θ_1 indicate cuspidal edges about directions parallel and perpendicular, respectively, to the [001] axis. In the (001) plane, entries under θ_0 and θ_1 indicate cuspidal edges about the [100] and [010] directions, respectively. In the (010) and (100) planes, entries under θ_3 and θ_4 indicate cuspidal edges about directions having an angle θ_2 with respect to the [001] axis. In the (001) plane, entries under θ_3 and θ_4 indicate cuspidal edges about directions having an angle θ_2 with respect to the [100] axis.

		(010) , (100) , and (001) planes, respectively				
Orthorhombic material	θ_0	θ_1	θ_2	θ_3	θ_{4}	θ_6
Sodium tartrate	\cdots	\ddotsc	48.32	7.51	85.80	62.15
		\cdots	46.77	.	.	\ddotsc
			43.44	\cdots	\cdots	.
Staurolite	\ddotsc	\cdots	35.66	.	\ddotsc	\cdots
	34.32	53.65	43.15		\cdots	55.30
	\ddotsc	\cdots	51.90		\cdots	.
Strontium sulphate	\ddotsc	\cdots	46.96	\ddotsc	\ddotsc	\ddotsc
		\ddotsc	46.80	14.99	78.83	56.65
	30.63	59.31	44.87	\ddotsc	\cdots	45.96
Sulfur	$\dddot{\bullet}$.	\ddotsc	48.02	27.79	71.47	58.29
	34.18	59.00	48.44		\cdots	35.90
	\ddotsc	\ddotsc	46.34	.	\cdots	58.30
Terpine monohydrate	.	.	47.00	20.49	74.90	57.80
		\ddotsc	49.65	25.71	77.00	68.94
	\cdots	\cdots	47.49		.	\ddotsc
Topaz	6.98	79.41	45.50		.	41.92
		\ddotsc	43.07	.	\cdots	$\bullet\bullet\bullet$
	19.50	76.07	42.79	\cdots	\cdots	58.88
Uranium (at 4.2 °K)	\cdots	75.30	55.72		\cdots	\ddotsc
	32.23	60.06	47.97		$\ddot{}$	37.44
	20.68	.	37.67		\cdots	\cdots
Zinc sulphate	33.89	55.77	44.67		.	45.96
heptahydrate	18.08	70.05	45.77			36.74
	\cdots	\cdots	46.15		\cdots	20.06

TABLE VI. (Continued)

and for the slow mode along θ_{α} :

$$
a_5 a_6 > a_7^2. \tag{74}
$$

Inequalities (73) and (74) follow from Theorems I and II, respectively, in the Appendix.

F. Phonon-amplification factor for the orthorhombic lattice when cuspidal edges are present

The presence of a cuspidal edge increases the phonon-amplification factor because wave vectors in more than one direction contribute to groupvelocity vectors in a given direction. Consider a circular phonon detector centered about the [001] axis with its boundaries at an angle $\Delta \theta$, of approximately 1' from this axis. If ^a cusp exists along the [001] axis, there are additional wavevector spaces besides the one about the [001] axis which provide phonons that strike the detector. Orthorhombic uranium, for example, has a cusp about the [001]axis in the (100) plane, (see Table VI), so that two wave-vector spaces near $\theta_k = \theta_0$ $= 32.23^{\circ}$, one on each side of the [001] axis in the (100) plane, give rise to phonons that strike a phonon detector centered about the [001] axis. In orthorhombic topaz, for example, there are two cuspidal edges about the $[100]$ axis, one in the (001)

plane, the other in the (010) plane, (see Table VI). If a circular phonon detector is centered about the $[100]$ axis, wave vectors near the $[100]$ axis, the two θ_0 directions (one on each side of the [100] axis in the (001) plane), and the two θ , directions (one on each side of the $[100]$ axis in the (010) plane) give rise to transversely polarized phonons which strike the detector. The two cusps, however, occur on different velocity surfaces (see Fig. 1) so that each transverse velocity surface has contributions from only two wave-vector spaces in addition to the one about the $[100]$ axis. A similar situation exists about the $[010]$ axis. If a circular detector is centered about a θ_2 collinear axis about which there is a cusp, then wave-vector spaces surrounding θ_2 , θ_3 , and θ_4 give rise to phonons that strike the detector (see Fig. 3).

If the solid angle $\Delta\Omega_v$ subtended by the detector is circular, the wave-vector solid angles $\Delta\Omega_k$ surrounding the collinear axes or the θ_0 , θ_1 , θ_3 , and θ_4 directions are nearly elliptical. Let a and b be the lengths of the semimajor and semiminor axes, respectively, of the quasiellipse surrounding the collinear direction, and let a_i and b_i be the lengths of the semimajor and semiminor axes of a quasiellipse about either the θ_0 or θ_1 directions. Since there are three wave-vector spaces contributing

TABLE VII. Collinear axes and other directions associated with cusps in symmetry planes of tetragonal crystals. The angles θ_i which are defined as in Figs. 3 and 4, are measured in degrees. In the (010) and (110) planes, entries under θ_0 and θ_1 indicate cuspidal edges about directions parallel and perpendicular, respectively, to the [001] axis. In the (001) plane, entries under θ_0 and θ_1 indicate cuspidal edges about the [100] and [010] directions, respectively. In the (010) and (110) planes, entries under θ_3 and θ_4 indicate cuspidal edges about directions having an angle θ_2 with respect to the [001] axis. In the (001) plane, entries under θ_3 and θ_4 indicate cuspidal edges about directions having an angle θ_2 with respect to the [100] axis.

phonons which strike the detector, (the distance D from the source of phonons to the detector is assumed to be unity), the PAF can be written as

$$
A = \frac{\sum \Delta \Omega_k}{\Delta \Omega_v} = \frac{\pi a b + 2\pi a_i b_i}{\pi (D \Delta \theta_v)^2} = \frac{a b + 2a_i b_i}{(\Delta \theta_v)^2}.
$$
 (75)

$$
a = \Delta \theta_k \Big|_{\theta_k = 0} = \Delta \theta_v \Big| \frac{d\theta_k}{d\theta_v} \Big|_{\theta_k = \theta_v = 0} = \Delta \theta_v \Big| \frac{a_2}{a_1} \Big|, \tag{76}
$$

$$
b = \Delta \theta_k \Big|_{\theta_k = 0} = \Delta \theta_v \Big| \frac{d\theta_k}{d\theta_v} \Big|_{\theta_k = \theta_v = 0} = \Delta \theta_v \Big| \frac{a_4 - |a_6|}{a_3 - (2a_7^2 - a_5 a_6) / |a_6|} \Big|,
$$

For example, if the PAF along the $[001]$ axis in uranium is considered, then additional contributing wave-vector spaces surround θ_0 in the (100) plane. Since a is evaluated for the T_1 portion, and b for the T_2 portion of the surface $\rho s^2 = C_{44}$ (see Fig. 1),

		(010) and (110) planes, respectively				
Cubic material	θ_0	θ_1	θ_{2}	θ_3	θ_4	$\theta_{\scriptscriptstyle\mathcal{B}}$
Calcium fluoride	$\dddot{\bullet}$		45.00	19.22	70.78	45.00
	.	.	46.52	26.76	68.31	54.74
Diamond	\cdots	\cdots	45.00	\cdots	\cdots	45.00
	.	.	43.85	\cdots	.	54.74
Lead (at 0° K)	39.16	50.84	45.00	\cdots	.	45.00
	33.12	55.07	43.10	\cdots	\cdots	54.74
Lithium fluoride	23.86	66.14	45.00	.	\cdots	45.00
	18.73	75.81	43.09	\cdots	\cdots	54.74
Magnesium oxide	21.03	68.97	45.00	.	\cdots	45.00
(at $4.2 \text{ }^{\circ} \text{K}$)	15.50	82.41	43.28	\cdots	\cdots	54.74
Niobium (at $4.2 \text{ }^{\circ} \text{K}$)	.	.	45.00	13.96	76.04	45.00
		.	46.07	19.19	73.80	54.74
Silicon	23.65	66.35	45.00	.	.	45.00
	18.15	76.58	43.32	.	\cdots	54.74
Sodium fluoride		.	45.00	24.09	65.91	45.00
	\cdots	\cdots	46.59	33.82	62.17	54.74

TABLE VIII. Collinear axes and other directions associated with cusps in symmetry planes of cubic crystals. The entries are as described in Table VII.

$$
b_i = b_0 = \Delta \theta_k \Big|_{\theta_k = \theta_0} = \Delta \theta_v \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_0 \theta \theta_v = 0}
$$

$$
\frac{d\theta_{\mathbf{k}}}{d\theta_{\mathbf{v}}} \bigg|_{\theta_{\mathbf{k}} = \theta_{0}, \theta_{\mathbf{v}} = 0} = \frac{2a_{4}a_{7} \left[(a_{7}^{2} - a_{5}a_{6})/(a_{3}^{2} - a_{5}^{2}) \right]^{1/2} - \left[(2a_{7}^{2} - a_{5}a_{6})\tan^{2}\theta_{0} + a_{6}^{2} \right]}{(2\tan^{2}\theta_{0})(1 + \tan^{2}\theta_{0})(a_{3}^{2} - a_{5}^{2})}
$$
\n
$$
(79)
$$

where $\tan^2\theta_0$ is given by Eq. (57).

Note that a in Eq. (76) is evaluated in the (010) plane, but that b and b_0 in Eqs. (77) and (79), respectively, are evaluated in the (100) plane. Since the cusp occurs about the $[001]$ axis in the (100) plane, the value of $(ab)/(\Delta \theta_p)^2$ can be found by taking the magnitude of the expression for the PAF given in Table III for the $\rho s^2 = C_{44}$ surface along the [001] axis. The factor $a_0/\Delta\theta_v$ is most easily determined numerically and is the same if either solid angle, $\Delta\Omega_k$ or $\Delta\Omega_v$, is chosen circular. If a circular wave-vector space is chosen, then the factor $a_0/\Delta\theta_v$ is the ratio of the radius of the wave-vector surface surrounding $\theta_k = \theta_0$ to a semiaxis of the quasiellipse surrounding the collinear axis.

For a cusp about the [100] axis, for example in the (010) plane, the results are similar. Evaluating a for the T_1 portion, and b for the T_2 portion of the surface $\rho s^2 = C_{55}$ (see Fig. 1) yields results (76)-(79), but with $\cot^2\theta_1$ replacing $\tan^2\theta_0$, a_3 interchanged with a_4 , and a_5 interchanged with a_{6} . Note again that a is evaluated in the (001) plane, but b and b_1 are evaluated in the (010) plane. Again, $(ab)/(\Delta\theta_v)^2$ can be found using the magnitude of the PAF given in Table III for the $\rho s^2 = C_{55}$ surface along the $[100]$ axis.

For a cusp about the $[100]$ axis in the (001) plane, a and b are evaluated for the $\rho s^2 = C_{66}$ surface giving results (76)-(79), but with a_1 and a_2 interchanged. In this case a is evaluated for the (010) plane, but b and b_1 are evaluated in the (001)

 (78)

plane. A cusp about $[010]$ in either the (100) plane or the (001) plane can be treated in a similar manner.

Since the collinear axis θ_2 is in general not at the intersection of orthogonal symmetry planes, the determination of the PAF is slightly different for a cusp about this axis. When a given θ_2 axis lies in only one symmetry plane, the quasielliptical wave-vector spaces around θ_3 and θ_4 are neither equal nor located at equal angular distances from θ_{2} .

The PAF for this case can be written, using the form of Eq. (75) , as

$$
A = \frac{\sum \Delta \Omega_k}{\Delta \Omega_v} = \frac{\pi a b + \pi a_3 b_3 + \pi a_4 b_4}{\pi (D \Delta \theta_v)^2} = \frac{a b + a_3 b_3 + a_4 b_4}{(\Delta \theta_v)^2},
$$
\n(80)

w'here

$$
b = \Delta \theta_k \Big|_{\theta_k = \theta_2} = \Delta \theta_v \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_v = \theta_2},
$$
\n(81)

which can be evaluated from Eq. (47),

$$
b_3 = \Delta \theta_k \Big|_{\theta_k = \theta_3} = \Delta \theta_v \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_3, \theta_v = \theta_2}, \tag{82}
$$

$$
b_4 = \Delta \theta_k \Big|_{\theta_k = \theta_4} = \Delta \theta_v \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_4, \ \theta_v = \theta_2}.
$$
 (83)

When these values are substituted into Eq. (80), the PAF becomes

$$
A = \frac{a_3}{\Delta \theta_v} \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_{3}}, \ \theta_v = \theta_2 \frac{d_4}{\Delta \theta_v} \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_{4}}, \ \theta_v = \theta_2
$$

$$
+ \frac{a}{\Delta \theta_v} \left| \frac{d\theta_k}{d\theta_v} \right|_{\theta_k = \theta_v = \theta_2} . \tag{84}
$$

The coefficient factors $a/\Delta\theta_v$, $a_3/\Delta\theta_v$, and $a_4/\Delta\theta_v$ can be determined numerically as before. Although the derivatives in Eqs. (82) and (83) can be represented by long expressions, they too are most easily calculated numerically.

For noncollinear directions, it is more convenient to use numerical integration to count the number of group-velocity vectors falling within a small solid angle using a fine angular mesh and a uniform angular density of k vectors. This has been done for some orthorhombie, tetragonal, and cubic crystals. The highest and lowest phonon intensities obtained along with their directions are listed in Tables IX and X. Phonon intensities obtained by the above method near collinear directions are given in Tables XI-XIII. More accurate calculations of phonon intensities using the dimensions of ellipses and circles are given in Table XIV.

In the $[001]$ direction tetragonal and cubic materials have two sets of mutually orthogonal symmetry planes. For a circular phonon detector and group-velocity space centered on the [001] direction, the corresponding wave-vector space must have four-fold symmetry and thus can not be a quasiellipse. Conversely, the group-velocity space corresponding to a circular wave-vector space is not quasielliptic. The vector spaces for cubic calcium fluoride in Fig. 7 clearly illustrate this and even indicate the presence of a cusp. Numerical integration may be used to determine the area of the surface when such a cusp is present.

 \cdot When a cusp exists about the [110] direction in tetragonal and cubic materials, circular wave vector spaces centered about the $[110]$ direction, the θ , directions in the (110) plane, or the θ , and θ_4 directions in the (001) plane can be expected to give rise to quasielliptic group-velocity surfaces about the $[110]$ direction. Calculation of the areas of the two group-velocity spaces which correspond to wave vectors about θ_3 and θ_4 is shortened by the fact that these areas are equal and located at equal angular distances from θ_{2} .

In cubic crystals no cusp is expected about the $\langle 111 \rangle$ directions because collinear axes exist in these directions only for the L mode. For a circular wave-vector space centered about the [111] direction the corresponding group-velocity space has three-fold symmetry. However, for 1 angular deviations about the $\langle 111 \rangle$ directions the resulting group-velocity space is very nearly circular and thus its approximate area ean be easily calculated.

G. Effect of phonon focusing on phonon conduction

In the orthorhombic lattice the phase velocities along the x , y , and z axes are in general different so that the thermal conductivity can be expected to be anisotropic at all temperatures. In the boundary-scattering regime, where ballistic phonon propagation occurs, phonon focusing can be responsible for anisotropic heat conduction even when the phonon phase velocities along the x , y , and z axes are equal. In fact, focusing will always be present whenever a solid is elastically anisotropic. and occurs even in cubic crystals.

TABLE IX. Calculated maximum and minimum phonon intensities in orthorhombic materials. The directions at which the extrema occur are given by the spherical polar angles θ and ϕ in degrees. The angle θ is measured with respect to the [001] axis and the angle ϕ is measured in the (001) plane with respect to the [1001 axis. For an elastically isotropic solid the corresponding intensities are unity. Calculations were performed using a 1° mesh in θ and ϕ , the number of wave vectors at each point weighted to give a uniform density. Because of this mesh, a much larger number of different wave vector directions fell within a 1° deviation from the [001l axis than for any other axis making any azimuthal variation in intensity about the [001] axis clearly observable. This is indicated in the table.

The anisotropy in the thermal conductivity of cubic crystals was first reported by McCurdy, Maris, and Elbaum⁵ on measurements made in silicon and calcium fluoride. Anisotropies of up to 50% for silicon and 40% for calcium fluoride were observed and shown to be the direct result of phonon focusing arising from elastic anisotropy.

Phonon focusing and conductivity calculations have also been made by McCurdy for elasticall
anisotropic hexagonal crystals.¹³ For materia anisotropic hexagonal crystals.¹³ For material having large elastic anisotropies differences in phonon intensity (up to factors of several hundred) were predicted for various crystallographic directions. Calculations of the thermal conductivity demonstrated that the phonon-focusing property could cause differences in the phonon conductivity in the ballistic regime by as much as 300%.

Winternheimer and McCurdy¹⁴ have predicted that the phonon-focusing property will cause anisotropic heat conduction even in cubic superconductors providing the temperature is a small fraction of the superconducting transition temperature, and the phonon mean-free path approaches sample dimensions, (i.e., $\Lambda_{\rm ph} \sim l$).

Calculations have been made for a number of

	Highest phonon		Direction	Lowest phonon		Direction
Tetragonal material	intensity	θ	φ	intensity	θ	φ
Ammonium dihydrogen phosphate	31.30L	$88 -$	0 ₀	0.00	90	0 ⁰
Indium (at $4.2 \text{ }^{\circ} \text{K}$)	11.34	74	12	0.00	24	45
Nickel sulphate hexahydrate	13.93	46	42	0.00	0 ₀	0 ⁰
Paratellurite	64.32	00	30	0.00	90	0 ₀
Potassium dihydrogen phosphate	10.00L	90	0 ₀	0.00	90	0 ⁰
Rutile	28.50	00	04	0.00	90	45
White tin (at $4.2 \text{ }^{\circ} \text{K}$)	10.47	56	20	0.00	22	00
Zirconium silicate	14.61	46	0 ₀	0.00	90	00
Cubic material						
Calcium fluoride	9.49	88	38	0.00	90	00
Lead (at $0^{\circ}K$)	32.65	28	00	0.00	46	45
Lithium fluoride	46.61	00	38	0.00	54	45
Magnesium oxide (at $4.2 \text{ }^{\circ} \text{K}$)	51.62	00	44	0.00	54	45
Niobium (at $4.2 \text{ }^{\circ} \text{K}$)	12.24	64	30	0.00	72	16
Silicon	34.65	04	04	0.00	54	45
Sodium fluoride	14.06	48	26	0.00	54	45

TABLE X. Calculated maximum and minimum phonon intensities in tetragonal and cubic materials. The corresponding intensities for an elastically isotropic solid are unity. : 'The angles ' θ and ϕ are defined in Table IX. Calculations were performed using the same mesh as described in Table IX. The suffix L refers to the longitudinal mode.

orthorhombic and tetragonal crystals, and, as expected, anisotropic phonon conductivity was predicted in those crystals which were elastically anisotropic. The direction of high thermal conductivity always coincided with the direction in which the PAP was high. To illustrate the effects of focusing, calculations were performed to determine the phonon-conduction-enhancement factor A_{κ} defined as

$$
A_{\kappa} = \kappa_{\nu}/\kappa_{s} \,, \tag{85}
$$

where κ_n is the thermal conductivity calculated by correctly including effects of phonon focusing and K_s is the thermal conductivity calculated using phase-velocity vectors instead of group-velocity vectors for each mode. Calculations of κ_s thus disregard the angular deviation between the groupvelocity vectors and their corresponding wave vectors for elastically anisotropic solids. Values of κ_s depend on the crystallographic direction of the heat-flow axis and will be largest in those

directions having the largest inverse-square phase velocity averaged over the three modes.

Samples used in the calculation of κ_n and κ_s were assumed to have circular cross-sections with a thermal length of 3 cm and a diameter D of 0.3 cm. Calculations of the thermal conductivity κ .: end-corrected mean free path, Λ_{corr} ; and thermal-conduction-enhancement factors A_{κ} are given in Table XV for several crystallographic directions. For elastically isotropic solids the thermalconductivity-enhancement factor A_{κ} is unity, and the end-corrected mean free path $\Lambda_{\rm corr}$ is 0.926D. Note that higher values of thermal conductivity coincide with higher values of A_{κ} . Tables VI-XV show that the highest values of thermal conductivity are found along directions about which cuspidal edges exist. The above results should be applicable (for dielectric solids) at temperatures which are a small fraction of the Debye temperature. For the superconductors, however, these results should not apply until the temperature becomes a

TABLE XI. Approximate phonon-amplification factor $A(\theta_v,\phi_v)$ in some orthorhombic crystals near collinear directions. The PAF values given are those calculated at the nearest even integer number of degrees to the collinear axes. The PAF was calculated as the ratio of the number of group-velocity vectors to the number of wave vectors for a solid angle of 4 square degrees. Four wave vectors were used in each $2^{\circ} \times 2^{\circ}$ box and each box was weighted to give a uniform density of wave vectors over all space. Entries for θ and ϕ are in degrees.

(θ_v, ϕ_v)		Aragonite	Barium sulphate	Benzophenone	Ga (at $4.2 \text{ }^{\circ} \text{K}$)	Strontium sulphate	Topaz	U (at $4.2 \text{ }^{\circ} \text{K}$)
(0, 0)	L	0.00	2.00	0.00	4.00	2.00	1.00	0.00
	Slow T	0.00	0.00	0.00	1.00	0.00	1.00	4.00
	FastT	3.00	1.00	1.00	1.00	1.00	0.00	0.00
$(\theta_6, 0)$	L	0.51	\cdots	0.00	\cdots	\ddotsc	1.51	\cdots
	SlowT	1.38	\cdots	2.95	\cdots	\cdots	1.03	\ddotsc
	Fast T	0.68	.	1.31	\cdots	\ddotsc	0.90	\ddotsc
	θ_{6}	28.62	\ddotsc	32.01	\cdots		41.92	\ddotsc
$(\theta_2, 0)$	L	0.43	1.09	0.00	1.10	1.10	1.54	0.00
	Slow T	13.51	0.59	4.60	2.92	0.65	0.99	0.50
	Fast T	0.51	0.00	0.51	0.00	0.00	0.45	1.64
	θ_2	36.18	47.42	40.11	48.27	46.96	45.50	55.72
(90, 0)	L	9.99	1.00	4.00	1.00	1.00	0.00	0.00
	Slow T	0.00	13.95	0.00	5.00	6.00	14.91	3.96
	FastT	1.00	2.00	12.00	2.00	$2.00\,$	3.00	0.00
$(90, \phi_6)$	L	\cdots	3.00	4.50	2.00	2.00	1.50	\cdots
	SlowT	\ddotsc	1.50	0.00	0.00	0.00	0.50	\cdots
	Fast T	\ddotsc	0.00	0.50	0.00	0.00	1.00	\cdots
	ϕ_6	\ddotsc	49.36	40.44	39.69	45.96	58.88	\ldots
$(90, \phi_2)$	L	1.00	3.00	4.50	2.00	1.50	1.50	0.00
	SlowT	4.48	2.50	0.00	0.00	0.50	0.50	0.50
	Fast T	0.00	0.00	0.50	0.00	0.00	1.00	2.43
	ϕ_{2}	51.54	44.44	45.63	46.16	44.87	42.79	37.67
(90, 90)	L	0.00	2.00	2.00	0.00	1.00	1.00	0.00
	SlowT	23.80	0.00	1.00	1.00	1.00	1.00	17.29
	FastT	4.00	5.00	7.00	1.00	1.00	17.00	0.00
$(\theta_2, 90)$	L	0.98	0.52	0.84	0.56	1.06	0.46	6.12
	Slow T .	3.49	1.52	3.00	1.03	4.66	1.51	0.00
	Fast T	0.00	0.00	0.00	0.00	2.49	9.66	0.97
	θ_2	44.66	46.76	41.46	49.72	46.80	43.07	47.97
$(\theta_6, 90)$	L	1.00	0.50	\ddotsc	\cdots	0.50	\cdots	6.13
	Slow T	3.20	7.06	.	\ddotsc	8.15	\cdots	0.58
	Fast T	0.00	0.00	\ddotsc	\ddotsc	2.03	\ddotsc	1.91
	θ_6	47.80	50.96	.	\ddotsc	56.65	\ddotsc	37.44
$(\theta_{\text{ns}}, \phi_{\text{ns}})$ ^a	L	1.00	1.25	.	1.50	1.25	\ddotsc	\ldots
	$\theta_{\rm ns}$	48.55	57.80	.	62.57	58.31	\cdots	\ddotsc
	ϕ _{ns}	85.18	28.47	.	35.83	33.84	\ddotsc	\cdots
$(\theta_\text{ns},\phi_\text{ns})$	Slow T	.	.	.	0.97	2.20	3.30	\ddotsc
	$\theta_{\rm ns}$	\ddotsc	\ddotsc	.	16.73	36.98	48.47	\cdots
	ϕ ns	\ddotsc	\ddotsc	.	31.81	31.35	67.16	\cdots
$(\theta_{\text{ns}}, \phi_{\text{ns}})$	Fast T	\cdots	3.26	.	12.08	10.19	0.50	0.00
	$\theta_{\rm ns}$	\ddotsc	46.06		47.25	45.83	42.74	50.18
	ϕ _{ns}	\ddotsc	47.14	\ddotsc	43.42	44.47	56.84	41.13

 $\theta_{\texttt{ns}}, \phi_{\texttt{ns}}$ are the nonsymmetry collinear axes.

(θ_v, ϕ_v)		In (at $4.2 \text{ }^{\circ} \text{K}$)	Nickel sulphate hexahydrate	$TeO2$ ^a	KDP ^b	Rutile	White tin (at $4.2 \text{ }^{\circ} \text{K}$)	Zirconium silicate
(0, 0)	L	1.00	1.00	4.00	4.00	1.00	1.00	4.00
	SlowT	1.00	4.00	0.00	0.00	18.00	4.00	0.00
	FastT	0.00	0.00	0.00	0.00	1.00	0.00	0.00
$(\theta_6, 0)$	L	1.49	0.49	\cdots	2.00	\ddotsc	.	3.00
	Slow T	0.00	0.00	\cdots	0.00	\cdots	.	0.00
	Fast T	2.13	0.00	\cdots	4.92	.	.	1.13
	θ_6	48.98	37.49	\cdots	39.92	\cdots	\cdots	57.22
$(\theta_2, 0)$	L	1.46	0.00	0.00	0.97	0.00	1.09	1.06
	SlowT	0.00	0.00	0.00	0.00	1.59	0.58	0.00
	Fast T	1.44	0.00	1.74	4.57	0.80	0.00	14.61
	θ_2	44.66	43.78	52.07	44.12	50.83	47.30	46.57
(90, 0)	L	1.00	0.00	0.00	10.00	0.00	1.00	5.00
	SlowT	1.83	2.00	1.99	0.00	11.90	3.00	0.00
	Fast T	2.00	0.00	0.00	0.00	0.00	1.00	0.00
(90, 45)	L	2.00	13.49	35.99	0.00	6.00	2.00	0.00
	SlowT	9.07	0.00	0.00	2.00	0.00	0.00	1.99
	Fast T	5.49	0.00	0.00	0.00	1.00	1.00	0.00
$(\theta_6, 45)$	L	.	1.50	1.75	\ddotsc	3.75	1.50	.
	SlowT	\cdots	0.00	0.00	\cdots	0.00	0.00	.
	FastT	.	1.18	2.06	\cdots	1.08	2.26	.
	θ_6	\ldots	24.04	39.83	\cdots	62.02	50.26	\ddotsc
$(\theta_2, 45)$	L	1.33	0.84	1.92	0.27	1.32	1.53	0.58
	SlowT	0.00	0.00	0.00	2.36	0.00	0.00	1.08
	Fast T	0.00	5.82	2.70	1.81	3.93	8.21	0.39
	θ_2	43.39	39.11	43.56	47.58	46.54	45.49	50.17

TABLE XII. Approximate phonon-amplification factor in some tetragonal crystals. The entries are as described in Table XI.

 $\overline{\text{TeO}_2}$, paratellurit

KDP, potassium dihydrogen phosphate.

TABLE XIII. Approximate phonon-amplification factor in some cubic crystals, The entries are as described in Table XI.

(θ_v, ϕ_v)		$_{\rm{CaF_2}}$	P _b (at 0 ^o K)	LiF	MgO $(at 4.2 \gamma K)$	Nb (at $4.2 \text{ }^{\circ} \text{K}$)	Si	NaF
(0, 0)	L	4.00	0.00	0.00	1.00	4.00	1.00	4.00
	$S \sim T$	0.00	0.00	15.00	42.55	0.00	6.00	0.00
	FastT	0.00	1.00	9.00	19.00	0.00	11.00	0.00
(45, 0)	L	0.50	2.43	1.96	1.96	0.50	1.96	0.50
	SlowT	0.00	0.00	0.50	0.50	0.00	0.50	0.00
	FastT	3.88	1.59	10.67	16.09	3.27	14.69	4.64
$(\theta_{\beta}, 45)$	L	0.25	2.49	2.24	2.24	0.50	2.24	0.25
	SlowT	3.16	0.00	1.76	3.23	2.40	1.76	4.93
	FastT	0.00	0.00	0.00	0.00	0.98	0.00	0.00
	$\theta_{\rm g}$	54.74	54.74	54.74	54.74	54.74	54.74	54.74
$(\theta_2, 45)$	L	0.52	2.41	1.97	2.02	0.52	2.44	0.52
	SlowT	5.43	0.50	1.56	1.50	2.45	1.26	6.66
	FastT	0.30	0.00	0.00	0.00	0.23	0.00	1.95
	θ_2	46.52	43.10	43.09	43.28	46.07	43.32	46.59

TABLE XIV. More accurate phonon-amplification factors, $A(\theta_v, \phi_v)$, along selected col-Finear axes for orthorhombic, tetragonal, and cubic materials whose elastic constants were determined at or below 4.2 'K. %hen the group-velocity spaces generated by the circular wavevector spaces were quasielliptical, the PAF values given were calculated from their dimensions. The values marked with a dagger indicate that three wave-vector spaces gave rise to groupvelocity vectors near the collinear axis. The value 0.1322 under calcium fluoride was not found by this method; it was obtained by numerical integration and agreed to within 1.3% of the value obtained when using Table V.

(θ_v, ϕ_v)		Ga	U	In	$_{\rm{CaF_2}}$	MgO	Si	
(0, 0)	L	2.92	.	0.506	3.22	0.279	0.272	
	Slow T	0.531	.	\ddots	\ddotsc	.	\cdots	
	FastT	0.731	.	\cdots	0.1322	.	\dots	
$(\theta_6, 0)$	L	\ddotsc	\cdots	0.96	0.782	1.39	1.42	
$(\theta_2, 0)$	SlowT	\ddotsc	0.359	0.0613	\cdots		\cdots	
	FastT	0.605	وووه	\ddotsc	3.10 [†]		.	
(90, 0)	L	0.559	\cdots	0.42	.	.	\cdots	
	SlowT	0.772	.	\ddotsc	.	\ddotsc		
	Fast T	5.27 [†]	.	.	.	\cdots		
$(90, \phi_6)$	L	2.09	\cdots	2.09	.	\cdots	\ddotsc	
$(90, \phi_2)$	SlowT	0.262	0.272	0.190	.	\ddotsc	\ddotsc	
	Fast T	\ldots	.	\ddotsc	\ddotsc	\ddotsc	\ddotsc	
(90, 90)	L	0.452	
	SlowT	0.430	\cdots		.	.	\ddotsc	
	Fast T	2.86†	\cdots	.	\cdots	.	\ddotsc	
$(\theta_2, 90)$	Slow T	\ldots	0.203	\cdots	\cdots	.	\ddotsc	
	Fast T	0.826	\ddotsc	.	.	.	\cdots	
$(\theta_6, 90)$	L	\cdots	5.8	\ddotsc	\cdots	\cdots	\ddotsc	
$(\theta_6, 45)$	L	.	\cdots	\ddotsc	0.445	2.12	2.16	
$(\theta_2, 45)$	Slow T		.	0.051	\cdots	0.441	0.311	
	FastT		\ddotsc	\cdots	\cdots	\cdots	\cdots	
(90, 45)	L	\cdots	.	2.09	0.78	1.39	1.423	
	Slow T		.	0.19	0.32	0.267	0.228	
	FastT	\cdots	\cdots	15.0	\cdots	\cdots	\cdots	

TABLE XV. Thermal conductivity, end-corrected mean free path, and thermal-conductionenhancement factor for selected crystals at very low temperatures. Calculations were performed for samples in the form of circular cross-section rods with a thermal length of ten rod diameters. Symbols are defined in the text. The elastic constants used are those given in Table XVI.

TABLE XVI. (Continued)

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small fraction of the superconducting transition temperature.

III. DISCUSSIDN

In the hexagonal. lattice, because of transverse isotropy, all wave vectors occur in symmetry planes. As a result, general statements¹³ concerning cuspidal edges (Sec. IID) and phonon focusing (Sec. IIE and Appendix) are valid for all wavevector directions in the lattice. In orthorhombic, tetragonal, and cubic lattices, however, such general statements are valid only when the wave vectors are confined to the symmetry planes of the lattice. Note also that since $a₇ > 0$, a collinear axis θ , always exists for the slow mode in each of the symmetry planes. A number of solids do not have a collinear axis θ_f for the fast mode (see Tables VI-VIII) because focusing (defocusing) in the symmetry plane of the wave vectors does not occur both parallel and perpendicular to the η axis. It is also evident, that for wave vectors confined to a given symmetry plane, focusing (defocusing) of the T_1 mode in this plane about the η axis must result in defocusing (focusing) of this mode, for

this plane, about η .

In orthorhombic lattices cusps about θ , in the (001) plane are very rare, occuring in only one material in Table VI, i.e., in potassium pentaborate. Cusps about θ_2 are more common in the other two symmetry planes. In the (100) plane they occur in 3 of the 22 materials listed, and in the (010) plane they occur in 9 of the 22. Eight of the orthorhombic materials, however, have cusps about both the [100] and [010] directions in the (001) plane.

In tetragonal materials, however, cusps about θ_2 in the (001) plane are far more frequent than they are in orthorhombic materials. They occur in nearly half the tetragonal materials in Table VII. Further consideration reveals that cusps about θ_2 are almost evenly distributed among the (010), (110) , and (001) planes. Cusps about the $\lceil 001 \rceil$ axis are rather rare and exist in only two of the tetragonal materials of Table VII because only indium and indium bismuth, show a θ_0 value in the (010) or the (110) planes. Indium, indiumbismuth, and rutile are the only tetragonal materials listed which have a cusp about the [100] direction in the

TABLE XVI. (Continued)

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(010) plane. Notice that of the tetragonal materials listed only indium bismuth has a cusp about the [110] direction in the (110) plane. Cusps about the $[100]$ and $[010]$ axes in the (001) plane, however, are quite common, occurring in six of the ten materials listed.

Cusps in the group-velocity surface of the T_1 mode are always absent for wave vectors in symmetry planes (see Theorem III). Cuspidal edges in the T_1 group-velocity surface, however, can exist for wave vectors in orthogonally intersecting, nonsymmetry planes. As a result, considerable care must be exercised before a group-velocity surface is given a cusp-free designation. Consider, for example, the phase-velocity surface of orthorhombic gallium in Fig. 1. Note that the $T₂$ portion of the ρs^2 surface in the (001) plane meets the T, portion in the (010) plane at the [100] axis, and the T_1 portion in the (100) plane at the [010] axis. Because a cusp exists about the $[100]$ axis in the (001) plane (see Table VI), symmetry considerations require that group velocities in the (010) plane can also be generated by wave vectors

on either side of the (010) plane. These group velocities form a second (inner) locus in the (010) plane and form part of the cuspidal configuration which extends from the [100] axis toward the [001] direction on both sides of the (010) plane. A similar situation occurs about the [010] axis where, because of the cuspidal edge in the (001) plane about the $\lceil 010 \rceil$ axis, the cuspidal configuration extendsfromthe [010] axis toward the [001] direction on both sides of the (100) plane. In tetragonal indium, there is, in addition, a cuspidal edge about the [100] axis in the (010) plane, and about the [010] axis in the (100) plane (see Table VI), so that a cuspidal configuration extends from the $\lceil 100 \rceil$ axis to the $\lceil 010 \rceil$ axis on both sides of the (001) plane. Similarly, in cubic calcium fluroride, the cuspidal edge shown in Fig. 7 around the $[100]$ axis is part of the cuspidal configuration about the \lceil 011] axis in the (100) plane which extends from the $\lceil 011 \rceil$ axis toward the $\lceil 100 \rceil$ direction.

Note that the presence of cuspidal edges can give rise to a large phonon-amplification factor. The amount of enhancement is related to the width of the cusp (the narrower the cusp the higher the phonon intensity). The highest phonon intensities in Tables IX and X occur where the direction of the group velocity varies on the average most slowly with wave-vector direction within the 2° mesh used in the computer calculations. For some of the materials listed in Tables IX and X this occurs in the vicinity of a cusp (see Tables VI-VIII), but for others where conditions for a cusp are nearly satisfied.

A cusp in a symmetry plane about a principal axis may not give a high phonon intensity within a 1 deviation from that axis if the group-velocity direction varies quite rapidly with wave-vector direction in the other symmetry plane. Gallium, for example, has a cusp about the [010] axis in the (001) plane (see Table VI), but in the (100) plane near the [010] direction calculations show that the group-velocity direction varies more than twice as rapidly as the wave-vector direction. It should not be surprising, therefore, that the resulting phonon intensity along the [010] axis is only unity.

However, high phonon intensities can exist in the absence of a cusp if the group-velocity direction varies slowly with wave-vector direction in. both symmetry planes. Orthorhombic aragonite gives a good example of this (see Tables VI and XL) There is no cusp about its [010] axis, but near this axis the group-velocity directions for both transverse modes varies slowly with wavevector direction in both the (001) and (100) planes. The result is a phonon intensity along the $\lceil 010 \rceil$ axis of 23.8 for the slow transverse mode and 4.0 for the fast transverse mode. High intensities can also occur in the longitudinal mode when the group-velocity direction varies slowly with wave vector. An excellent example is paratellurite in the (001) plane, where conditions for a cuspidal edge about θ = 45° in the fast mode are more favorable than in any other known material.

Note that the orthorhombic lattice can not have double cusps along its principal axes generated by wave vectors confined to symmetry planes. This is evident from Fig. 1 which shows that for a given surface, a $T₂$ portion in one symmetry plane always meets a T_1 portion in the adjoining symmetry plane, However, double cusps can exist along the [001] axis in tetragonal and cubic crystals even when wave vectors are confined to symmetry planes. In fact, indium has a cusp along the [001] direction in all symmetry planes which contain the [001] direction. This is possible because, as is shown in Fig. 2, all $T₂$ portions on symmetry planes can meet at a common point along the [001] axis in tetragonal and cubic crystals. Figure 2 also indicates that double cusps can not exist along the [100], [110], and [010] directions in a tetragonal

crystal (when wave vectors are confined to symmetry planes) because, for a given surface along these directions, all $T₂$ portions in symmetry planes meet T_1 portions.

Materials for which the ratios of the elastic constants are similar have similar anisotropies and focusing properties. Cubic materials, for example, with similar anisotropies have many similar PAP values (see Table XIII). Table VIII shows that calcium fluoride, niobium, and sodium fluoride (which shall be designated Set A) all have cusps about the $\langle 110 \rangle$ directions and near the $\langle 111 \rangle$ directions, while lead, lithium fluoride, magnesium oxide, and silicon (designated as Set B) all have cusps about the $\langle 100 \rangle$ and $\langle 110 \rangle$ directions. As a result energy flow is enhanced along the (100) and $\langle 110 \rangle$ directions in Set B, but along the $\langle 111 \rangle$ and (110) directions in Set A. Thus for Set B the thermal conductivity is larger along the $\langle 100 \rangle$ and $\langle 110 \rangle$ directions than along the $\langle 111 \rangle$ directions and for Set A higher along the $\langle 111 \rangle$ and $\langle 110 \rangle$ di-
rections than along the $\langle 110 \rangle$ directions.^{12, 14} rections than along the $\langle 110 \rangle$ directions.^{12, 14}

Furthermore, calculations of A_{κ} show that the effects of focusing can actually reverse the anisotropy one obtains by neglecting the angular deviation between the phase and group velocities. For example, magnesium oxide would have a thermal conductivity κ_s of 0.0234 in the $\langle 100 \rangle$ directions and 0.0244 in the $\langle 111 \rangle$ directions if focusing were neglected, but when focusing effects are considered the correct thermal conductivity κ_p is 0.0340 in the $\langle 100 \rangle$ directions and 0.0231 in the $\langle 111 \rangle$ directions. Similarly, for rutile, $\kappa_{\rm s}$ is 0.0303 and0. 0381 for the [001] and [110] directions, respectively, but the correct thermal condducitivity κ_v is 0.0436 and 0.0316, respectively, for these same directions.

Finally, note that phonon focusing, a general property of elastically anisotropic crystals, also occurs in crystal lattices of still lower symmetry. Strong focusing is predicted to have a dramatic effect upon the phonon conductivity at very low temperatures provided the phonon mean free path can approach sample dimensions.

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IV. APPENDIX

Since group-velocity vectors in a symmetry plane can be generated by wave vectors on either

side of that symmetry plane, the following three theorems assume that the wave vectors, and thus their corresponding group-velocity vectors are restricted to the symmetry planes of the crystal lattice.

Theorem I. If a collinear axis θ_t in a symmetry plane exists, any focusing (defocusing) occurring about θ , in the fast mode must be accompanied by defocusing (focusing) of the fast mode about both η and η_{\perp} axes, and conversely.

For focusing (defocusing) of the fast mode about θ _f,

$$
|a_{7}|[(|a_{7}|-a_{5})+(|a_{7}|-a_{6})]
$$

$$
\times [\frac{1}{2}(a_{4}+a_{6})(a_{6}-a_{5})+(|a_{7}|+a_{4})(|a_{7}|-a_{6})] > 0.
$$

Proof: From Figs. 3 and 4, based upon Eqs. (20)-(22), it is self-evident that for a θ_f to exist, and for focusing (defocusing) to occur about θ_f , that the values of θ_v versus θ_k must intersect the line θ_v $=\theta_{\nu}$ at $\theta_{\nu}=\theta_{\nu}$. Since η and η_{ν} are the only other collinear axes for the fast mode, focusing (defocusing) about θ_t must thus be accompanied by defocusing (focusing) about both η and η_+ , and conversely.

For a θ_f to exist, Eq. (26) requires

$$
(|a_7| - a_6)(|a_7| - a_5) > 0.
$$
 (A1)

Furthermore, for a θ_f to exist, and for defocusing to occur about η and η_{\perp} , inequality (A1) and Sec. II E require

$$
(|a_7| - a_6)(|a_7| - a_5)(a_7^2 - a_5a_6) > 0,
$$
 (A2)

but for focusing about these same two directions requires

$$
(|a_7|-a_6|(|a_7|-a_5|)(a_7^2-a_5a_6)<0.
$$
 (A3)

Because of Eq. (48) and inequalities (A2) and (A3), respectively, both focusing (defocusing) about θ , require

$$
\begin{aligned} \left| a_{7} \left| \left[\left(\left| a_{7} \right| - a_{5} \right) + \left(\left| a_{7} \right| - a_{6} \right) \right] \right| \\ \times \left[\frac{1}{2} (a_{4} + a_{6}) (a_{6} - a_{5}) + \left(\left| a_{7} \right| + a_{4}) (\left| a_{7} \right| - a_{6}) \right] \right| > 0 \,. \end{aligned} \tag{A4}
$$

Theorem II. If a collinear axis θ_s in a symmetry plane exists, any focusing or cuspidal edge occuring in the slow mode about θ_s must be accompanied by defocusing of the slow mode about both η and η_1 . Similarly, any defocusing of the slow mode about θ_s must be accompanied by focusing at both η and η_1 , or a cuspidal edge about either η or η_1 or both axes. The converse of the two previous statement is also true.

For a cuspidal edge, or focusing (defocusing) of the slow mode about θ_s

$$
\begin{aligned} \left| a_{7} \left| \left[(a_{5} + |a_{7}|) + (a_{6} + |a_{7}|) \right] \right| &\times \left[\frac{1}{2} (a_{4} + a_{6}) (a_{5} - a_{6}) + (a_{4} - |a_{7}|) (a_{6} + |a_{7}|) \right] > 0 \,. \end{aligned}
$$

Proof: From Figs. 3 and 4, based upon Eqs. (20)-(22), it is self-evident that for a θ_s to exist, and for a cuspidal edge or focusing (defocusing) to occur about θ_s , that the values of θ_{ν} versus θ_{ν} mus intersect the line $\theta_v = \theta_k$ at $\theta_k = \theta_s$. Since η and η_{\perp} are the only other collinear axes for the slow mode, a cuspidal edge or focusing about θ_s must be accompanied by defocusing about both η and η_{\perp} , and conversely. Similarly, defocusing of the slow mode about θ , must be accompanied by focusing of the slow mode about both η and η_1 , or a cuspidal edge about either η or η_i or both axes, depending upon the strength of the inequality a_7^2 $a_{\rm s}a_{\rm s}$. Conversely, focusing of the slow mode about both η and η_1 , or a cuspidal edge about either η or η_1 or both axes, must be accompanied by defocusing of the slow mode about $\theta_{\rm s}$.

For a θ_s to exist, Eq. (25) requires

$$
(a_5 + |a_7|)(a_6 + |a_7|) > 0.
$$
 (A5)

Also, for a cuspidal edge about θ_s or for focusing about θ_s , defocusing must occur about both η and η_{\perp} . Together with inequality (A5) this requires

$$
(a_5 + |a_7|)(a_6 + |a_7|)(a_5a_6 - a_7^2) > 0, \qquad (A6)
$$

but for focusing about these same two directions requires

$$
(a_5 + |a_7|)(a_6 + |a_7|)(a_5a_6 - a_7^2) < 0.
$$
 (A7)

Because of Eq. (47) and inequalities (A6) and (A7), respectively, both focusing (and defocusing) about θ , require

$$
\begin{aligned} \left| a_{7} \left| \left[\left(a_{5} + \left| a_{7} \right| \right) + \left(a_{6} + \left| a_{7} \right| \right) \right] \right| \\ &\times \left[\frac{1}{2} (a_{4} + a_{6}) (a_{5} - a_{6}) + (a_{4} - \left| a_{7} \right|) (a_{6} + \left| a_{7} \right|) \right] > 0. \end{aligned} \right.
$$
\n(A8)

Theorem III. Cuspidal edges in the transverse $T₁$ mode, and the fast mode about any collinear point in a symmetry plane, are always absent in an elastically stable solid.

Proof: For the T_1 mode in any symmetry plane

$$
\frac{d\theta_{k}}{d\theta_{v}} = \frac{a_{2} \sec^{2} \theta_{v}}{a_{1} \sec^{2} \theta_{k}} \tag{A9}
$$

Since $a_1 > 0$, $a_2 > 0$ therefore, $d\theta_{\mu}/d\theta_{\nu} > 0$ for all values of θ_{ν} , and a cuspidal edge is impossible. For the fast mode a cuspidal edge about the η axis requires

$$
\frac{a_4 + |a_6|}{a_3 + (2a_7^2 - a_5a_6)/|a_6|} < 0
$$

Since $a_4 + |a_6| > 0$, this requires

or

$$
a_3 + (2a_7^2 - a_5a_6)/|a_6| < 0
$$

$$
2a_7^2 < a_5 a_6 - a_3 \mid a_6 \mid \tag{A10}
$$

If $a_6 > 0$, then a cuspidal edge requires $2a_7^2$ $a_6(a_5 - a_3)$ which is impossible since $a_6 > 0$ and $(a_5 - a_8)$ < 0 for all symmetry planes. If a_6 < 0, then a cuspidal edge requires $2a_7^2 < a_6(a_5 + a_3)$ which again is impossible since $(a_5 + a_3) > 0$ and $a_6 < 0$.

For a cuspidal edge about the η_{\perp} axis the proof is similar but with a_3 replacing a_4 , and with a_5 and a_6 interchanged. Results for a_5 , $a_6 > 0$ and for the T_1 mode were previously proved by Musgrave,¹¹ T_1 mode were previously proved by Musgrave,¹¹ by considering the inverse phase-velocity surface.

For a cuspidal edge to exist about θ_{f} , Eq. (48) and inequalities (A2) and (A4) require

$$
4(|a_{7}|-a_{6})(|a_{7}|-a_{5})(a_{7}^{2}-a_{5}a_{6})
$$

> |a_{7}|[(|a_{7}|-a_{5})+(|a_{7}|-a_{6})]
×[$\frac{1}{2}$ (a_{4}+a_{6})(a_{6}-a_{5})+(|a_{7}|+a_{4})(|a_{7}|-a_{6})].
(A11)

Since a cuspidal edge about θ_f requires defocusing about both η and η_{\perp} , inequality (A1) and Sec. II E require

$$
(|a_7| - a_5) + (|a_7| - a_6) > 0
$$
 (A12)

and because of inequality (A4) requires

$$
\frac{1}{2} (a_4 + a_6)(a_6 - a_5) + (|a_7| + a_4)(|a_7| - a_6) > 0.
$$
 (A13)

Inequality (A13) reduces to the following conditions for each of the symmetry planes of the orthorhombic lattice. For the (010) plane:

$$
(C_{13} + 2C_{55})^2 - C_{11}C_{33} > 0 \quad \text{if} \quad a_7 > 0 \,, \tag{A14}
$$

but

$$
C_{13}^2 - C_{11}C_{33} > 0 \quad \text{if} \quad a_7 < 0 \tag{A15}
$$

the (100) plane:

$$
(C_{23} + 2C_{44})^2 - C_{22}C_{33} > 0 \quad \text{if} \quad a_7 > 0 \,, \tag{A16}
$$

but

$$
C_{23}^2 - C_{22}C_{33} > 0 \quad \text{if} \quad a_7 < 0 \tag{A17}
$$

the (001) plane:

$$
(C_{12} + 2C_{60})^2 - C_{11}C_{22} > 0 \quad \text{if} \quad a_7 > 0 , \tag{A18}
$$

but

$$
C_{12}^2 - C_{11}C_{22} > 0 \quad \text{if} \quad a_7 < 0 \tag{A19}
$$

and for the (110) plane of the tetragonal lattice to

$$
(C_{13} + 2C_{44})^2 - C_{33} \left[\frac{1}{2} (C_{11} + C_{12}) + C_{66} \right] > 0 \quad \text{if} \quad a_7 > 0 \tag{A20}
$$

but

$$
C_{13}^2 - C_{33} \left[\frac{1}{2} (C_{11} + C_{12}) + C_{66} \right] > 0 \quad \text{if} \quad a_7 < 0 \,. \tag{A21}
$$

Inequalities (A15), (A17) and (A19) violate conditions (6) , and $(A21)$ violates condition (11) for elastic stability. Inequalities (A14), (A16), (A18) and (6) give the necessary but not sufficient conditions on a_7 for a cusp about θ_f in the orthorhombic lattice. For the (010) plane:

$$
C_{13} + C_{55} > (C_{11}C_{33} - C_{13}^2)/4C_{55} > 0
$$
 (A22)

the (100) plane:

$$
C_{23} + C_{44} > (C_{22}C_{33} - C_{23}^2)/4C_{44} > 0, \qquad (A23)
$$

and the (001) plane:

$$
C_{12} + C_{66} > (C_{11}C_{22} - C_{12}^2)/4C_{66} > 0.
$$
 (A24)

Similarly, inequalities (A20) and (11) give the necessary but not sufficient conditions on a_r for a cusp about θ_f in the (110) plane of the tetragonal lattice:

$$
C_{13} + C_{44} > \left\{ C_{33} \left[\frac{1}{2} \left(C_{11} + C_{12} \right) + C_{66} \right] - C_{13}^2 \right\} / 4C_{44} > 0.
$$
\n(A25)

Necessary but not sufficient conditions on $a₇$ for a cusp about θ_t for the other symmetry planes of tetragonal, hexagonal and cubic lattices are easily obtained from inequalities (A22)- (A25).

Since $a_7 > 0$, a cusp, if one exists about θ_f , will most likely occur when $a_7 \gg |a_5|$, $a_7 \gg |a_6|$. For finite a_{7} , the most extreme case consistent with elastic stability occurs when $a_5 = a_6 = 0$, for which inequality (A11) reduces to $2a_7 > a_7 + a_4$. Inequality (A26) is impossible to satisfy since $a_4 > a_7$ when $a_5 = a_6 = 0$ for all symmetry planes in an elastically stable solid.

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