# Quantum State Tomography for Kerr Parametric Oscillators

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Kerr parametric oscillators (KPOs) implemented in the circuit quantum electrodynamic architecture can operate as qubits. Their applications to quantum annealing and universal quantum computation have been studied intensively. For these applications, the readout of the state of KPOs is of practical importance. We develop a scheme of state tomography for KPOs with reflection measurement. Although it is known that the reflection coefficient depends on the state of the KPO, it is unclear whether tomography of a qubit encoded into a KPO can be performed in a practical way mitigating decoherence during the measurement, and how accurate it is. We show that the reflection coefficient has a one-to-one correspondence with a diagonal element of the density matrix of the qubit when a probe frequency is properly chosen and an additional single-photon drive is introduced. Thus, our scheme offers a novel way to read out the qubit along an axis of the Bloch sphere, and therefore the reflection measurement and single-qubit gates can constitute state tomography.

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### **I. INTRODUCTION**

In the early days of digital computers, classical parametric phase-locked oscillators [1,2] were utilized as classical bits. Their quantum counterparts, called Kerr parametric oscillators (KPOs) or Kerr-cat qubits [3–5], have recently been attracting much attention in terms of their applications to quantum information processing [6] and studies of quantum many-body systems [7,8]. A KPO can be implemented by a superconducting resonator with Kerr nonlinearity, driven by an oscillating pump field [6,9–11]. In a KPO, two coherent states with opposite phases can exist stably, and be used as qubit states.

An advantage of KPOs as qubits is rooted in a characteristic of their errors. The bit-flip error in a KPO is greatly suppressed because of the stability of the coherent states against photon loss. Thus, the phase-flip error is predominant over the bit-flip error in a KPO. This biased nature of errors enables us to perform quantum error corrections with less overhead compared to other qubits with unbiased errors [12,13]. Previous studies on applications of KPOs include theoretical studies of quantum annealing [5,14–21] and universal quantum computation [22–24], experimental demonstration of single-qubit operations [11], theoretical studies of qubit gate operations [25–29], and high error-correction performance by concatenating the *XZZX* surface code [13] with KPOs [30]. There are other subjects such as fast and accurate controls [31,32], spectroscopy [33,34], controls and dynamics not confined in qubit space [10,35], Boltzmann sampling [36], the effect of a strong pump field [37], the effect of decay and dephasing [24], quantum phase transitions [7,8,38], and quantum chaos [3,39,40].

In almost all of these applications, the readout of KPOs is essential. Quantum state tomography of a KPO using the transient power spectrum density (PSD) was demonstrated experimentally in Ref. [10]. In Ref. [11], authors extracted the state of a KPO by adiabatically transforming it to a Fock qubit and performing state tomography of the Fock qubit. They also proposed a quantum nondemolition measurement along the *z*-axis of the Bloch sphere using an additional readout resonator, where the *z*-axis is defined so that the stable coherent states are located on the axis.

In this paper we develop a scheme of quantum state tomography with reflection measurement which is widely and routinely used for circuit quantum electrodynamic

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systems. Our scheme does not require reading a small number of photons, in contrast to transient PSD, nor a readout resonator. Also, it does not use a transformation of a KPO to a Fock qubit caused by control of a pump field. Therefore, it is expected that our scheme can simplify the design of KPO systems and avoid decoherence during the adiabatic transformation of a KPO to a Fock qubit.

In Ref. [33] the reflection coefficient was obtained as a function of density-matrix elements of a KPO, and it was examined especially for a KPO in a stationary state. Since the reflection coefficient depends on the state of a KPO, it is expected that we can in principle estimate the density matrix of a qubit encoded into the KPO with reflection measurements. However, it is not obvious if tomography can be performed in a practical manner and how accurate it is. For example, it is nontrivial to decide which probe frequency should be chosen and what controls are needed. Because a KPO has effective phase decay rate proportional to the photon number stored in the KPO [24], the decoherence during the reflection measurement can degrade the efficiency of the tomography. This paper addresses all of these points.

This paper is organized as follows. In Sec. II we outline our method of state tomography. In Sec. III we explain how to extract the diagonal elements of the density matrix of a KPO with reflection measurement. In Sec. IV we examine the sensitivity of the reflection coefficient to density-matrix elements. Section V provides a summary and discussion. We present a way to obtain off-diagonal elements and examine the accuracy of the tomography in Appendix A.

# **II. METHOD OF TOMOGRAPHY**

The Hamiltonian of an isolated KPO can be written in a rotating frame at a frequency of  $\omega_p/2$  as [6]

$$\frac{H_{\rm KPO}}{\hbar} = -\frac{K}{2}\hat{a}^{\dagger 2}\hat{a}^2 + \frac{p}{2}\left(\hat{a}^{\dagger 2} + \hat{a}^2\right),\tag{1}$$

where K(> 0), p(> 0) and  $\omega_p$  are the nonlinearity parameter, pump amplitude, and angular frequency of the pump field, respectively. The highest and second highest eigenstates of the Hamiltonian (1) are given by

$$\begin{aligned} |\varphi_0\rangle &= N_+(|\alpha\rangle + |-\alpha\rangle),\\ |\varphi_1\rangle &= N_-(|\alpha\rangle - |-\alpha\rangle), \end{aligned} \tag{2}$$

where  $|\pm\alpha\rangle$  is a coherent state,  $\alpha = \sqrt{p/K}$ , and  $N_{\pm} = (2 \pm 2e^{-2\alpha^2})^{-1/2}$ . It can be verified that these states respectively become Fock states  $|0\rangle$  and  $|1\rangle$  as *p* goes to zero.  $|\varphi_0\rangle$  and  $|\varphi_1\rangle$  can be used as qubit states [22]. In this paper we consider the large-*p* regime where the two coherent states  $|\pm\alpha\rangle$  are orthogonal and therefore can be used as qubit states. We use these coherent states as qubit states. In this parameter regime, these coherent states are long-lived even



FIG. 1. Schematic of the effective potential  $\langle \alpha' | H_{\text{KPO}} | \alpha' \rangle$ , where  $\alpha'$  is real. The potential is tilted due to the drive amplitude  $\Omega$  as explained in Sec. III. The pink and green wave packets represent the two highest-energy eigenstates. During the ramp of the drive field,  $|\alpha\rangle$  and  $|-\alpha\rangle$  are adiabatically loaded to  $|\Psi_0\rangle$  and  $|\Psi_1\rangle$ , respectively.

with photon loss, and the highest and second highest eigenstates are approximately degenerate. The coherent states are located around the maxima of the effective potential with an inverted double-well structure (Fig. 1). With these coherent states, the density operator of the KPO at time  $\tau$ is given by

$$\rho(\tau) = \sum_{i,j=0}^{1} \rho_{ij}(\tau) |\tilde{i}\rangle \langle \tilde{j}|, \qquad (3)$$

where  $|\tilde{0}(\tilde{1})\rangle \equiv |\alpha(-\alpha)\rangle$ . In Eq. (3) we assume that leakage out of the qubit subspace is negligible. The condition for this assumption to be valid is reported in Ref. [25].

The purpose of the quantum state tomography is to obtain  $\rho_{ij}(\tau)$ . The scheme of the tomography consists of a single-qubit gate and subsequent measurement which determines the diagonal elements  $\rho_{ii}(\tau)$ . For example, the off-diagonal elements  $\rho_{01}(\tau)$  and  $\rho_{10}(\tau)$  can be measured with  $R_x(\pi/2)$  and  $R_y(\pi/2)$  gates followed by the measurement for diagonal elements. This is because  $R_x(\pi/2)$  and  $R_y(\pi/2)$  gates change the coefficient of the term  $|\tilde{0}\rangle \langle \tilde{0}|$  from  $\rho_{00}(\tau)$  to  $1/2 - \text{Im}[\rho_{01}(\tau)]$  and  $1/2 - \text{Re}[\rho_{01}(\tau)]$ , respectively, as explained in Appendix A.

#### III. EXTRACTION OF $\rho_{ii}$

Our scheme to extract  $\rho_{ii}(\tau)$  can be divided into two processes: ramping of a single-photon-drive field and subsequent reflection measurement. Hereafter, we refer to the single-photon-drive field as the drive field. The role of the drive field is to make the reflection coefficient dependent on  $\rho_{ii}(\tau)$  (see Appendix B). At time  $t = \tau$ , we start to ramp a drive field resonant to the KPO, while *p* and *K* are fixed. All the parameters are kept constant for  $t > \tau + t_{ramp}$ , where  $t_{ramp}$  is the ramping time. The reflection measurement is started at  $t = \tau + t_{ramp} + t_{delay}$ , where  $t_{delay}$  is the delay time. We assume that the duration of these processes is sufficiently smaller than the typical time that the bit-flip occurs so that the bit-flip is negligible. The role of the delay time is explained later.

# A. Ramping of drive field

As the drive field gradually increases, the energy eigenstates  $|\tilde{0}\rangle$  and  $|\tilde{1}\rangle$  change to  $|\psi_0\rangle$  and  $|\psi_1\rangle$ , respectively, as illustrated in Fig. 1. Here,  $|\Psi_0\rangle$  and  $|\Psi_1\rangle$  are the highest and second highest eigenstates of  $H_{\text{KPO}}(\tau + t_{\text{ramp}})$ , where

$$\frac{H_{\rm KPO}(t)}{\hbar} = -\frac{K}{2}\hat{a}^{\dagger 2}\hat{a}^2 + \frac{p}{2}\left(\hat{a}^{\dagger 2} + \hat{a}^2\right) + \Omega(t)(\hat{a}^{\dagger} + \hat{a}),\tag{4}$$

and  $\Omega$  is the drive amplitude. We set  $t_{\text{ramp}}$  long enough to suppress undesired nonadiabatic transitions in the state of the KPO.

Then the diagonal elements of the density operator changes from  $\rho_{ii} |\tilde{i}\rangle \langle \tilde{i} |$  to  $\rho_{ii} |\psi_i\rangle \langle \psi_i |$ . The off-diagonal elements in Eq. (3) are suppressed much faster than bit-flip. The effective phase decay rate increases linearly in  $|\alpha|^2$  and is explicitly written as  $2\kappa_{tot} |\alpha|^2$  [24], where  $\kappa_{tot}$  is the total photon loss rate defined by  $\kappa_{tot} = \kappa_{ex} + \kappa_{int}$  with the external and internal decay rates,  $\kappa_{ex}$  and  $\kappa_{int}$ . On the other hand, the bit-flip rate is suppressed exponentially in  $|\alpha|^2$  [41,42]. The off-diagonal elements vanish when the delay time  $t_{delay}$ is long enough. As a result, the density operator  $\rho(t)$  for  $t \ge \tau + t_{ramp} + t_{delay}$  is approximated by

$$\rho' = \rho_{00}(\tau) |\psi_0\rangle \langle \psi_0| + \rho_{11}(\tau) |\psi_1\rangle \langle \psi_1|.$$
 (5)

In this manner, our method takes advantage of the biased nature of errors of the KPO: the typical time that the phaseflip occurs is much shorter than the typical time of the bitflip.

In order to demonstrate the time evolution of a KPO discussed above, we numerically solve the master equation in the Lindbladian form expressed as

$$\frac{d\rho(t)}{dt} = -\frac{i}{\hbar} \left[ H_{\text{KPO}}(t), \rho(t) \right] + \frac{\kappa_{\text{tot}}}{2} \mathcal{D}[\hat{a}]\rho(t), \quad (6)$$

where the Lindbladian superoperator term is defined by  $\mathcal{D}[\hat{O}]\rho = 2\hat{O}\rho\hat{O}^{\dagger} - \hat{O}^{\dagger}\hat{O}\rho - \rho\hat{O}^{\dagger}\hat{O}$ . In the numerical simulation, we set  $\tau = 0$  and  $\rho(0) = (\sqrt{0.2} |\tilde{0}\rangle + \sqrt{0.8} |\tilde{1}\rangle)(\sqrt{0.2} \langle \tilde{0}| + \sqrt{0.8} \langle \tilde{1}|)$ . The time dependence of the drive amplitude is given by

$$\Omega(t) = \frac{\Omega_0}{2} \left[ 1 - \cos\left(\frac{\pi t}{t_{\text{ramp}}}\right) \right]$$
(7)

for  $0 \le t \le t_{\text{ramp}}$ , so that  $\Omega$  is gradually increased. The time dependence of  $\Omega$  in Eq. (7) was chosen so that  $\Omega$  and  $d\Omega/dt$  are continuous to avoid unwanted nonadiabatic transitions.

We consider the fidelity between  $\rho(t)$  and  $\rho'$  in Eq. (5) defined by  $\mathcal{F}[\rho(t), \rho']$ , where  $\mathcal{F}[\rho, \rho'] = (\text{Tr}[\sqrt{\sqrt{\rho}\rho'\sqrt{\rho}}])^2$ . Figure 2(a) shows the infidelity defined by  $1 - \mathcal{F}[\rho(t), \rho']$ . The infidelity tends to decrease as t



FIG. 2. (a) Infidelity on logarithmic scale,  $1 - \mathcal{F}[\rho(t), \rho']$ , as a function of *t*. Amplitude of diagonal (b) and off-diagonal elements (c) of the density matrix as a function of *t*. The blue and red curves in (b) and the black curve in (c) represent  $|\langle \psi_0 | \rho(t) | \psi_0 \rangle|, |\langle \psi_1 | \rho(t) | \psi_1 \rangle|$ , and  $|\langle \psi_{0(1)} | \rho(t) | \psi_{1(0)} \rangle|$ , respectively. The parameters used are p/K = 9.0,  $t_{\text{ramp}} = 20/K$ ,  $\Omega_0/K = 0.1$ ,  $\kappa_{\text{ex}}/K = 0.01$ , and  $\kappa_{\text{in}}/\kappa_{\text{ex}} = 0.5$ .

increases, and is lower than  $10^{-3}$  for  $t \ge 10/K$ . Figures 2(b) and 2(c) respectively represent the diagonal and offdiagonal elements of the density matrix as a function of t. The diagonal elements are almost unchanged for 0 < t < 400/K, while the off-diagonal elements vanish rapidly. These results indicate that  $\rho'$  approximates  $\rho(t)$  well for a considerably long period of time.

#### **B.** Reflection measurement

We consider reflection measurement of the KPO subjected to a fixed pump and drive fields at  $t = \tau + t_{ramp} + t_{delay}$  [Fig. 3(a)]. A microwave with frequency of  $\omega_{in}$  is injected from a transmission line (TL) attached to the KPO.

A recent study [33] finds that the reflection coefficient is given by

$$\Gamma = 1 + \sum_{mn} \xi_{mn} \tag{8}$$

with

$$\xi_{mn} = \frac{\kappa_{\text{ex}} X_{mn} \sum_{k} \left( X_{kn}^{*} \rho_{km}^{(F)}[0] - \rho_{nk}^{(F)}[0] X_{mk}^{*} \right)}{i \Delta_{nm} + \kappa_{\text{tot}} X_{nn} X_{mm}^{*} - \frac{\kappa_{\text{tot}}}{2} \left( Y_{nn} + Y_{mm} \right)}, \quad (9)$$

where  $\Delta_{nm} = \omega_{in} - \omega_p/2 - \omega_n + \omega_m$ . In Eq. (9),  $X_{mn} = \langle \psi_m | \hat{a} | \psi_n \rangle$  and  $Y_{mn} = \langle \psi_m | \hat{a}^{\dagger} \hat{a} | \psi_n \rangle$ .  $\rho_{mn}^{(F)}[0]$  is the Fourier



FIG. 3. (a) Schematic of reflection measurement. A microwave with frequency of  $\omega_{in}$  is injected from a transmission line (TL) attached to the KPO. The reflected microwave is measured. (b) Schematic of the effective potential tilted due to the drive amplitude  $\Omega$ . The straight arrows indicate transitions  $|\psi_0\rangle \rightarrow |\psi_2\rangle$  and  $|\psi_1\rangle \rightarrow |\psi_3\rangle$  caused by the input field. Here,  $\Delta\omega_{nm}$  is the energy difference between  $|\psi_n\rangle$  and  $|\psi_m\rangle$  defined by  $\Delta\omega_{nm} = \omega_n - \omega_m$ , where  $\omega_m$  is the eigenenergy of  $|\psi_m\rangle$ . The oscillating curve with an arrow indicates the input field with frequency  $\omega_{in}$ . (c) Wigner function, W(x + iy), of the four highest energy levels for p/K = 9 and  $\Omega/K = 0.1$ .

component of  $\langle \psi_m | \rho | \psi_n \rangle$  at a frequency of 0 in the rotating frame. Thus, the information of the density operator is embedded in the reflection coefficient. In Eq. (8),  $\xi_{mn}$ can be interpreted as the contribution from the transition  $|\psi_m\rangle \rightarrow |\psi_n\rangle$  to the reflection coefficient. When the input field is resonant with this transition, that is,  $\omega_{in} - \omega_p/2 = \omega_n - \omega_m$ , the amplitude of  $\xi_{mn}$  becomes large because its denominator becomes small. Thus, the resonant transitions dominate the reflection coefficient over the other nonresonant transitions.

We assume that the reflection measurement is performed after the off-diagonal elements of the density matrix vanish, and that bit-flip does not occur during the measurement. If the input field is sufficiently weak, the change in  $\rho_{mn}^{(F)}[0]$  from that given by Eq. (5) is negligible. Therefore, we have approximately

$$\rho_{mn}^{(F)}[0] = \rho_{00}(\tau)\delta_{m0}\delta_{n0} + (1 - \rho_{00}(\tau))\delta_{m1}\delta_{n1}, \quad (10)$$

where we used  $\rho_{11}(\tau) = 1 - \rho_{00}(\tau)$ . Straightforward substitution of Eqs. (9) and (10) into Eq. (8) shows a linear relationship between  $\Gamma$  and  $\rho_{00}(\tau)$ . This linear relationship suggests that measurement of  $\Gamma$  allows  $\rho_{00}(\tau)$  to be extracted. Hereafter, we write the reflection coefficient as  $\Gamma[\rho_{00}(\tau)]$  to clearly express that it depends on  $\rho_{00}(\tau)$ .

In this paper we mainly consider the case where the offdiagonal elements  $\rho_{mn(\neq m)}^{(F)}[0]$  are zero during the reflection measurement for simplicity. However, the effect of the offdiagonal elements is actually negligible when the pump amplitude is sufficiently large, as shown in Appendix C. Therefore,  $\tau_{delay}$  can be set to zero in such a parameter regime.

# IV. SENSITIVITY OF REFLECTION COEFFICIENT

Accurate extraction of  $\rho_{00}(\tau)$  requires sufficient sensitivity of the reflection coefficient to  $\rho_{00}(\tau)$ . In this section we consider  $|\Gamma(1) - \Gamma(0)|$  as a measure of the sensitivity and show that high sensitivity is obtained with experimentally feasible parameters. Hereafter, we call  $|\Gamma(1) - \Gamma(0)|$ sensitivity.

#### A. Analytic formula in large-pump limit

We derive an asymptotic formula for the sensitivity in the large-pump limit. As an example, we consider the case where the input field is resonant with the transition  $|\psi_0\rangle \rightarrow |\psi_2\rangle$  and off-resonant with the other transitions [Fig. 3(b)]. Then the reflection coefficient is approximately given by  $\Gamma = 1 + \xi_{02}$ . When *p* is sufficiently large, there is a regime of  $\Omega$ , where the highest levels are well approximated by  $D(\pm \alpha) |m\rangle$  [10] with the displacement operator  $D(\alpha) = \exp(\alpha \hat{a}^{\dagger} - \alpha^* \hat{a})$  (see Appendix D). The Wigner function of the four highest energy levels is exhibited in Fig. 3(c). The Wigner function is defined by  $W(z) = 2\text{Tr}[D(z)\rho D(-z)P]/\pi$  with z = x + iy with the parity operator  $P = \exp(i\pi \hat{a}^{\dagger} \hat{a})$ . The use of  $|\psi_{0(2)}\rangle =$  $D(\alpha) |0(1)\rangle$  and Eq. (9) leads to

$$|\Gamma(1) - \Gamma(0)| = \frac{2\kappa_{\text{ex}}}{\kappa_{\text{tot}}}.$$
(11)

The same result can be obtained for the input field resonant with the transition  $|\psi_1\rangle \rightarrow |\psi_3\rangle$ . The above discussion suggests that the sensitivity approaches 2, which is the maximum value of the sensitivity, when the pump amplitude becomes strong and  $\kappa_{\text{int}} \ll \kappa_{\text{ex}}$ . This large sensitivity of the reflection coefficient to  $\rho_{00}(\tau)$  is useful for extraction of  $\rho_{00}(\tau)$ .

### **B.** Numerical results

The reflection coefficients for  $\rho_{00}(\tau) = 0$  and 1 are compared in Fig. 4. The reflection coefficient clearly changes with the value of  $\rho_{00}$ . In particular, the difference between



FIG. 4. Real part (a),(b) and imaginary part (c),(d) of the reflection coefficient  $\Gamma$  as function of  $\omega_{in}$  and p for  $\rho_{00} = 0$  and 1. The parameters used are  $\Omega/K = 0.5$ ,  $\kappa_{ex}/K = 0.01$ ,  $\kappa_{in}/\kappa_{ex} = 0.5$ .

 $\Gamma(1)$  and  $\Gamma(0)$  is large for  $\omega_{in} - \omega_p/2 = \Delta \omega_{20}$  and  $\Delta \omega_{31}$  corresponding to the transitions  $|\psi_0\rangle \rightarrow |\psi_2\rangle$  and  $|\psi_1\rangle \rightarrow |\psi_3\rangle$ , where  $\Delta \omega_{nm} = \omega_n - \omega_m$ . Therefore, these values of  $\omega_{in}$  are suitable for extraction of  $\rho_{00}$ .

Figure 5 shows the reflection coefficient in a complex plane for varying  $\omega_{in}$  (a,b) and fixed  $\omega_{in}$  (c,d). The numerical results are consistent with the linearity and sensitivity to  $\rho_{00}$  proven analytically. Because there is a one-to-one correspondence between  $\rho_{00}$  and  $\Gamma$ ,  $\rho_{00}$  can be determined from  $\Gamma$ .

Figure 6 shows the sensitivity as a function of  $\omega_{in}$  for different values of  $\kappa_{ex}$  and p. There are high peaks of the sensitivity at  $\omega_{in}$  corresponding to the transitions  $|\psi_0\rangle \rightarrow$  $|\psi_2\rangle$  and  $|\psi_1\rangle \rightarrow |\psi_3\rangle$ . There is also a small peak corresponding to the transition  $|\psi_1\rangle \rightarrow |\psi_4\rangle$  when  $\kappa_{ex}$  and p are small. This peak is buried in a higher adjacent peak when  $\kappa_{ex}$  becomes large as each peak becomes broader.

The sensitivity depends on the pump amplitude. Figure 7 shows the dependence of the sensitivity on the pump amplitude p. The frequency of the input field is set to  $\omega_{in} - \omega_p/2 = \Delta \omega_{20}$  or  $\Delta \omega_{31}$ . The sensitivity increases with p toward the asymptotic value in Eq. (11). This is because the relevant energy eigenstates are approximated well by  $D(\pm \alpha) |m\rangle$  when p becomes large, as numerically confirmed in Appendix D. The sensitivity corresponding to the transition  $|\psi_0\rangle \rightarrow |\psi_2\rangle$  is higher than that for  $|\psi_1\rangle \rightarrow |\psi_3\rangle$ . We attribute this to the fact that  $|\psi_2\rangle$  is approximated well by  $D(\alpha) |1\rangle$  while  $|\psi_3\rangle$  deviates from  $D(-\alpha) |1\rangle$  especially when p is small, as numerically demonstrated in Appendix D. Because the energy of  $|\psi_3\rangle$  is lower than that





FIG. 5. Reflection coefficient in a complex plane for varying  $\omega_{in}$  (a),(b) and fixed  $\omega_{in}$  (c),(d). For panels (a),(c) and (b),(d),  $d\omega$  is defined by  $d\omega = \omega_{in} - \omega_p/2 - \Delta\omega_{20}$  and  $d\omega = \omega_{in} - \omega_p/2 - \Delta\omega_{31}$ , respectively. The values of  $\rho_{00}$  and  $d\omega$  used are written in (a),(b) and (c),(d), respectively. In (c),(d), the black circle, square, triangle, inverted triangle, and diamond, are for  $\rho_{00} = 0.0, 0.25, 0.5, 0.75, and 1.0$ , respectively. The parameters used are  $\Omega/K = 0.5, p/K = 9.0, \kappa_{ex}/K = 0.01, and \kappa_{in}/\kappa_{ex} = 0.5$ .

of  $|\psi_2\rangle$ ,  $|\psi_3\rangle$  is more loosely trapped than  $|\psi_2\rangle$  in one of the potential wells of the inverted double-well potential.

The sensitivity depends also on the drive amplitude. Figure 8 shows the sensitivity as a function of  $\Omega$ . The sensitivity corresponding to the transition  $|\psi_1\rangle \rightarrow |\psi_3\rangle$ decreases for the large- $\Omega$  regime, while the sensitivity corresponding to the transition  $|\psi_0\rangle \rightarrow |\psi_2\rangle$  increases monotonically in the range of  $\Omega$  used. The decrease of the sensitivity is due to the deviation of  $|\psi_3\rangle$  from  $D(-\alpha)|1\rangle$ , which is discussed in Appendix D. Because  $|\psi_3\rangle$  is more loosely trapped than  $|\psi_2\rangle$ , the state vector of  $|\psi_3\rangle$  is sensitive to  $\Omega$  compared to  $|\psi_2\rangle$ . When  $\Omega$  increases beyond 0.7K, the order of energy levels is changed. For example, the energy level approximated by  $D(-\alpha) |0\rangle$  becomes lower than the level approximated by  $D(\alpha) |1\rangle$ . We do not consider such regime of  $\Omega$  for simplicity. When the input field is resonant to different transitions, the formula for the reflection coefficient in Eq. (8) becomes less valid due to interference between the transitions [33]. We do not consider such parameter regimes in this paper.

So far, we have explained the method to obtain the diagonal elements of the density matrix,  $\rho_{00}(\tau)$  and  $\rho_{11}(\tau)$ . In Appendix A, we explain the method to obtain the offdiagonal elements,  $\rho_{01}(\tau)$  and  $\rho_{10}(\tau)$ , and examine the accuracy of the tomography.



FIG. 6. Sensitivity as a function of  $\omega_{in}$  for p/K = 4.0 (a) and p/K = 9.0 (b). Black, blue, and red curves are for  $\kappa_{ex}/K = 0.33$ , 0.1, and 0.01. We also vary  $\kappa_{int}$  so that  $\kappa_{int}/\kappa_{ex} = 0.5$ . Black dashed lines represent the energy differences between relevant levels. We set  $\Omega/K = 0.5$ .

#### V. SUMMARY AND DISCUSSION

We have developed a scheme of quantum state tomography for KPOs with reflection measurement. A drive field is used to realize the one-to-one correspondence between the reflection coefficient and the diagonal elements of the density matrix. We have examined the sensitivity of the reflection coefficient to the density matrix for various system parameters. In addition, we have examined the accuracy of the tomography by numerically simulating the gate operations. Our scheme does not use readout of a small number of photons in contrast to transient PSD. Moreover, it does not require a transformation of a KPO to a Fock qubit nor an additional resonator. This measurement along *z*-axis can be used also for readouts of KPOs in quantum annealing.

The proposed scheme utilizes the direct coupling of a KPO to a TL. However, the external coupling to the TL degrades the fidelity of gate operations because of the effective phase decay rate increasing with  $\kappa_{tot}$  (see Appendix A for the accuracy of the tomography under the effect of the effective phase decay). Therefore,  $\kappa_{ex}$ should be sufficiently small, although a part of the reflected



FIG. 7. The sensitivity as a function of p for  $\Omega/K = 0.1$  (a) and 0.5 (b). The red and blue curves are for  $\omega_{in} - \omega_p/2 = \Delta \omega_{20}$  and  $\Delta \omega_{31}$ , respectively. The insets show the same things but with a wider range of p. The red and blue curves are overlapping in the inset of (a). The parameters used are  $\kappa_{ex}/K = 0.01$  and  $\kappa_{in}/\kappa_{ex} = 0.5$ . The asymptotic value of the sensitivity in Eq. (11) is approximately 1.33, and is represented by dashed lines in the insets.

field  $\xi_{mn}$  in Eq. (9) containing the information of the KPO becomes weak as it is proportional to  $\kappa_{ex}$ . The weakness of the signal can be compensated by the data



FIG. 8. The sensitivity as a function of  $\Omega$  for p/K = 4.0. The red and blue curves are for  $\omega_{\rm in} - \omega_p/2 = \Delta \omega_{20}$  and  $\Delta \omega_{31}$ , respectively. The parameters used are  $\kappa_{\rm ex}/K = 0.01$  and  $\kappa_{\rm in}/\kappa_{\rm ex} = 0.5$ .

accumulation time of the reflection measurement and the number of measurements.

The pure dephasing, if it exists, can degrade the efficiency of the measurement. The degradation is rooted not only in the enhanced relaxation of a KPO but also in the large nominal internal decay rate which brings the KPO to an undercoupling regime. The effect of the pure dephasing on the reflection coefficient is examined in Appendix E.

Although our scheme requires only three types of gate operations  $[I, R_x(\pi/2), \text{ and } R_y(\pi/2)]$  to extract the density-matrix elements, other gate operations can be additionally used to further increase the accuracy of the tomography. Then numerical optimization techniques such as those used in Ref. [10] will be useful to find an estimated density matrix which well reproduces measurement results.

Continuous homodyne and heterodyne measurements along the *z*-axis by reading the leaked field from a KPO were theoretically studied [42,43] and experimentally demonstrated [34]. These measurements are continuous in the sense that the leaked field is kept measured while a pump field is on. Homodyne and heterodyne measurement could alternatively be used for extraction of diagonal elements of the density matrix if the timing of the detection is controlled.

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# APPENDIX A: OFF-DIAGONAL ELEMENTS AND ACCURACY OF TOMOGRAPHY

The off-diagonal elements of the density matrix,  $\rho_{01}(\tau)$ and  $\rho_{10}(\tau)$ , can be measured with  $R_x(\pi/2)$  and  $R_y(\pi/2)$ gates, followed by the measurement for diagonal elements. The gate operations transform  $\rho(\tau)$  in Eq. (3) as

$$R_{x}(\pi/2)\rho(\tau)R_{x}(\pi/2)^{\dagger} = \frac{1}{2} \begin{pmatrix} 1 - 2\mathrm{Im}[\rho_{01}] & i\rho_{00} + \rho_{10} + \rho_{01} - i\rho_{11} \\ -i\rho_{00} + \rho_{10} + \rho_{01} + i\rho_{11} & 1 + 2\mathrm{Im}[\rho_{01}] \end{pmatrix},$$
(A1)

$$R_{y}(\pi/2)\rho(\tau)R_{y}(\pi/2)^{\dagger} = \frac{1}{2} \begin{pmatrix} 1 - 2\operatorname{Re}[\rho_{01}] & \rho_{00} + \rho_{10} - \rho_{01} - \rho_{11} \\ \rho_{00} - \rho_{10} + \rho_{01} - \rho_{11} & 1 + 2\operatorname{Re}[\rho_{01}] \end{pmatrix},$$
(A2)

where  $\rho_{ij}$  abbreviates  $\rho_{ij}(\tau)$ , and  $R_x(\theta)$  and  $R_y(\theta)$  are defined by

$$R_{x}(\theta) = \begin{pmatrix} \cos(\theta/2) & -i\sin(\theta/2) \\ -i\sin(\theta/2) & \cos(\theta/2) \end{pmatrix},$$
  

$$R_{y}(\theta) = \begin{pmatrix} \cos(\theta/2) & -\sin(\theta/2) \\ -\sin(\theta/2) & \cos(\theta/2) \end{pmatrix}.$$
(A3)

As seen from Eqs. (A1) and (A2), the measurement for diagonal elements of the density matrix after the gate operations allows us to extract  $\rho_{01}(\tau)$  and  $\rho_{10}(\tau)$ . We henceforth set  $\tau$  to zero for simplicity of notation.

The  $R_x$  gate for a KPO can be implemented by temporally controlling the detuning [23], which is the difference between the resonance frequency of the KPO and half the frequency of the pump field. The role of the detuning is to lift the degeneracy between the two highest levels and to imprint the different dynamical phase to each level which gives rise to the  $R_x$  gate. The Hamiltonian of the KPO with detuning  $\Delta$  is written as

$$\frac{H_{\rm KPO}(t)}{\hbar} = \Delta(t)\hat{a}^{\dagger}\hat{a} - \frac{K}{2}\hat{a}^{\dagger 2}\hat{a}^{2} + \frac{p}{2}\left(\hat{a}^{\dagger 2} + \hat{a}^{2}\right).$$
 (A4)

The time dependence of the detuning is chosen as

$$\Delta(t) = \Delta_0 \sin^2 \frac{\pi t}{T_x},\tag{A5}$$

for  $0 \le t \le T_x$ . The value of  $\Delta_0$  is chosen so that the gate fidelity is maximized for given  $T_x$ , p, K, and  $\theta$  in the case without decoherence. For example,  $\Delta_0 = -6.938K$  is used to obtain a gate fidelity of 0.997 for  $T_x = 2.5/K$ , p/K = 9, and  $\theta = \pi/2$  in the case without decoherence. Thus, we have  $\rho(T_x) \simeq R_x(\pi/2)\rho(0)R_x(\pi/2)^{\dagger}$ . By using  $\rho(T_x) =$  $R_x(\pi/2)\rho(0)R_x(\pi/2)^{\dagger}$  and Eq. (A1), we obtain  $\rho_{00}(T_x) =$  $1/2 - \text{Im}[\rho_{01}(0)]$  and  $\rho_{11}(T_x) = 1/2 + \text{Im}[\rho_{01}(0)]$ . Therefore, we can obtain Im[ $\rho_{01}(0)$ ] by measuring the diagonal elements of  $\rho(T_x)$  with the method introduced in Sec. III.

Because  $R_y(\theta) = R_x(-\pi/2)R_z(\theta)R_x(\pi/2)$ , we can use two  $R_x$  gates and an  $R_z$  gate to realize an  $R_y(\theta)$  gate. It is known that the  $R_z$  gate of a KPO can be implemented by a pulsed drive field [23]. The Hamiltonian is given by Eq. (4). The time dependence of  $\Omega$  for an  $R_z(\theta)$  gate is given by

$$\Omega(t) = \frac{\pi\theta}{8T_z\sqrt{p/K}}\sin\left(\frac{\pi(t-T_x)}{T_z}\right)$$
(A6)

for  $T_x \le t \le T_x + T_z$ , where  $T_x$  and  $T_z$  are the duration of an  $R_x$  gate and an  $R_z$  gate, respectively. Assuming  $\rho(2T_x + T_z) = R_y(\pi/2)\rho(0)R_y(\pi/2)^{\dagger}$ , we obtain  $\rho_{00}(2T_x + T_z) =$  $1/2 - \operatorname{Re}[\rho_{01}(0)]$  and  $\rho_{11}(2T_x + T_z) = 1/2 + \operatorname{Re}[\rho_{01}(0)]$ . Therefore, we can obtain  $\operatorname{Re}[\rho_{01}(0)]$  by measuring the diagonal elements of the density matrix after these gate operations.

We simulate the evolution of the system during gate operations and the ramp of the drive field and the free evolution for  $t_{delay}$ , by numerically integrating the master equation taking into account the effect of  $\kappa_{ex}$ . The diagonal elements of the density matrix at  $t_f \equiv T_g + t_{ramp} + t_{delay}$ are used to reconstruct  $\rho(\tau = 0)$ , where  $T_g$  is the duration of gate operations. Because no gate operation is required,  $T_g$  is zero for extraction of the diagonal elements of  $\rho(0)$ . We set  $t_{delay} = 0.4/\kappa_{ex}$  so that  $t_{delay}$  is inversely proportional to  $\kappa_{ex}$  because vanishing of the off-diagonal elements takes longer time for smaller total photon loss rate. We assume that the diagonal elements of the density matrix at  $t = t_f$  can be extracted exactly with the reflection measurement. The effect of the imperfection of the extraction of the diagonal elements is discussed later.

As an example, we consider six different reference states,  $\rho_i = |j\rangle\langle j|$ , at t = 0 where j denotes  $\{x\pm, y\pm, z\pm\}$ ;  $|x\pm\rangle = C_{x\pm}(|\tilde{0}\rangle \pm |\tilde{1}\rangle), |y\pm\rangle = C_{y\pm}(|\tilde{0}\rangle \pm i|\tilde{1}\rangle) \text{ and } |z+\rangle$  $(-)\rangle = |\tilde{0}(\tilde{1})\rangle$ ; and  $C_i$  is a normalization factor. The fidelity of the tomography is defined by  $\mathcal{F}[\rho_i, \rho'_i]$ , where  $\rho'_i$  is the reconstructed density operator. Figure 9 shows the fidelity averaged over the reference states as a function of  $\kappa_{ex}$ . In order to decrease numerical simulation time, we assume that the diagonal elements of the density matrix at  $t = t_f$  are well approximated by those at  $t = T_g$ . This assumption is valid when the fidelity of the gate operations is high because the change in the diagonal elements during the ramping of the drive field and the free evolution after the ramping is negligible, as exemplified in Fig. 2(b). The results obtained with this approximation are almost the same as that without the approximation. It is seen that the fidelity increases with the decrease in  $\kappa_{ex}$  because of the mitigation of unwanted effects of the decoherence.

Figure 10 exhibits the Wigner function of reference states  $\rho_{x+}$ ,  $\rho_{y+}$  and their reconstructed states. The approximation used for the solid curve in Fig. 9 is not used for this result and henceforth. The Wigner function of the reconstructed states are approximately the same as those of the reference states for  $\kappa_{ex}/K = 10^{-3}$ . On the other hand, the central fringe, which is the interference between the two



FIG. 9. The fidelity of the tomography as a function of  $\kappa_{ex}$  (crosses). The solid curve is obtained with the approximation that the diagonal elements of the density matrix at  $t = t_f$  are the same as those at  $t = T_g$ . The fidelity is averaged over the six different reference states. The parameters used are p/K = 9.0,  $T_x = 2.5/K$ ,  $T_z = 1/K$ , and  $\kappa_{int} = \kappa_{ex}/2$ .

stable coherent states and manifests the coherence of the KPO, becomes vague due to the decoherence during the gate operations for  $\kappa_{\text{ex}}/K = 10^{-2}$ .

We examine the sensitivity of the tomography to errors in diagonal elements of the density matrix. We assume that the measured value of the diagonal element corresponding to  $|\tilde{0}\rangle\langle\tilde{0}|$  is given by  $\cos^2[(\theta_{\text{true}} + \Delta\theta)/2]$ , while the true value is given by  $\cos^2(\theta_{\text{true}}/2)$ . Here,  $\Delta\theta$  characterizes the degree of the error. The error influences not only the diagonal elements of the reconstructed density matrix  $\rho'$  but also its off-diagonal elements because the reflection measurement is used for both of them. We define  $\rho'_{11}$  by  $\rho'_{11} = 1 - \rho'_{00}$  to satisfy  $\text{Tr}[\rho'] = 1$ . Because a density matrix should be positive semidefinite, we multiply the off-diagonal elements of  $\rho'$  by  $\eta(< 1)$  if  $\rho'$  is not positive semidefinite, where  $\eta$  is the maximum value that makes  $\rho'$  positive semidefinite. Figure 11 shows the fidelity averaged over the six different reference states as a function of  $\Delta \theta$ . A monotonic decrease is observed as  $|\Delta \theta|$  increases in the parameter regime studied. The average fidelity is higher than 0.94 for  $-0.1 < \Delta \theta / \pi < 0.1$  for the parameters used.

# APPENDIX B: REFLECTION COEFFICIENT WITHOUT A DRIVE FIELD

In this paper a drive field is used to make the reflection coefficient dependent on the diagonal elements of the density matrix  $\rho_{mm}(\tau)$ . In this section, we prove that the reflection coefficient is independent of  $\rho_{mm}(\tau)$  without the drive field.



FIG. 10. Wigner function of the reference states  $\rho_{x+,y+}$  (a),(d) and their reconstructed states  $\rho'_{x+,y+}$  for  $\kappa_{ex} = 10^{-3}$  (b),(e) and  $10^{-2}$  (c),(f). The other parameters used are the same as in Fig. 9.

Without the drive field, the Hamiltonian of the KPO is written as Eq. (1), and its eigenstates  $|\psi_m\rangle$  have even or odd parity because the Hamiltonian is parity preserving.



FIG. 11. Fidelity of the tomography as a function of  $\Delta\theta$  for  $\kappa_{\rm ex}/K = 10^{-3}$ . The fidelity is averaged over the six different reference states. The other parameters used are the same as in Fig. 9.

The density operator  $\rho(t)$  for  $t \ge \tau + t_{ramp} + t_{delay}$  can be approximated by

$$\begin{aligned} \rho' &= \rho_{00}(\tau) |\tilde{0}\rangle \langle \tilde{0}| + \rho_{11}(\tau) |\tilde{1}\rangle \langle \tilde{1}| \\ &= \frac{1}{2} |\psi_0\rangle \langle \psi_0| + \frac{\rho_{00} - \rho_{11}}{2} |\psi_0\rangle \langle \psi_1| \\ &+ \frac{\rho_{00} - \rho_{11}}{2} |\psi_1\rangle \langle \psi_0| + \frac{1}{2} |\psi_1\rangle \langle \psi_1|, \end{aligned} \tag{B1}$$

with  $|\psi_{0,1}\rangle = (|\tilde{0}\rangle \pm |\tilde{1}\rangle)/\sqrt{2}$ . It is seen from Eq. (B1) that the information of  $\rho_{00}$  is embedded in  $\rho_{10}^{(F)}[0]$  and  $\rho_{01}^{(F)}[0]$ . Therefore, the reflection coefficient  $\Gamma$  should depend on  $\rho_{10}^{(F)}[0]$  or  $\rho_{01}^{(F)}[0]$  for extraction of  $\rho_{00}$ . However,  $\Gamma$  is independent of  $\rho_{10}^{(F)}[0]$  and  $\rho_{01}^{(F)}[0]$  because, as seen in Eqs. (8) and (9), they appear in the reflection coefficient as a product with  $X_{ij} = \langle \psi_i | \hat{a} | \psi_j \rangle = 0$ , where *i* and *j* have the same parity. Note that  $X_{ij}$  is zero when  $|\psi_i\rangle$  and  $|\psi_j\rangle$  have the same parity.

# APPENDIX C: EFFECT OF OFF-DIAGONAL ELEMENTS OF THE DENSITY MATRIX

As explained in the main text, there is a one-to-one correspondence between  $\rho_{00}$  and the reflection coefficient  $\Gamma$ when off-diagonal elements of the density matrix are vanishing. In order to realize the one-to-one correspondence, we set the delay time long enough so that the off-diagonal elements vanish in the main text. However, as shown in this appendix, the effect of the off-diagonal elements on the reflection coefficient is negligible when the pump amplitude is sufficiently large. Therefore, the delay time can be set to zero in such a parameter regime.

In order to examine the effect of the off-diagonal elements, we numerically calculate  $\Gamma$  for the following two states with and without off-diagonal elements:

$$\rho = [(|\tilde{0}\rangle + |\tilde{1}\rangle)(\langle \tilde{0}| + \langle \tilde{1}|\rangle]/2,$$
  

$$\rho' = [|\tilde{0}\rangle \langle \tilde{0}| + |\tilde{1}\rangle \langle \tilde{1}|]/2.$$
(C1)

Figures 12(a) and 12(b) show the amplitude of the reflection coefficient for  $\omega_{in} - \omega_p/2 = \Delta \omega_{20}$  and  $\Delta \omega_{31}$ , respectively. The difference between the reflection coefficients for  $\rho$  and  $\rho'$  becomes small when the pump amplitude p increases. This implies that the effect of the off-diagonal elements becomes negligible for the large-p regime.

The insensitivity of  $\Gamma$  to the off-diagonal elements comes from the fact that  $X_{12}$  and  $X_{03}$  become small in the large-*p* regime, as shown in Fig. 12(c). The offdiagonal elements  $\rho_{10}^{(F)}[0]$  and  $\rho_{01}^{(F)}[0]$  appear in the form of  $X_{12}^*\rho_{10}^{(F)}[0]$  and  $X_{03}^*\rho_{01}^{(F)}[0]$  in the reflection coefficient in Eq. (8). Therefore, the effect of the off-diagonal elements becomes negligible when  $X_{12}$  and  $X_{03}$  are sufficiently small.



FIG. 12. The *p* dependence of the amplitude of  $\Gamma$  corresponding to  $\rho$  (red) and  $\rho'$  (blue) for  $\omega_{\rm in} - \omega_p/2 = \Delta \omega_{20}$  (a) and  $\Delta \omega_{31}$  (b). The *p* dependence of  $|X_{12}|$  (green curve) and  $|X_{03}|$  (orange curve). The parameters used are  $\Omega/K = 0.5$ ,  $\kappa_{\rm ex}/K = 0.01$ , and  $\kappa_{\rm in}/\kappa_{\rm ex} = 0.5$ .

The decrease in  $|X_{12}|$  and  $|X_{03}|$  in the large-*p* regime is explained as follows. As *p* increases, the four highest eigenstates of Hamiltonian (4) can be approximated as  $|\psi_{0(2)}\rangle = D(\alpha) |0(1)\rangle$  and  $|\psi_{1(3)}\rangle = D(-\alpha) |0(1)\rangle$ . Then we have

$$X_{12} = X_{03} = e^{-2|\alpha|^2} (1 - 2|\alpha|^2),$$
 (C2)

where  $\alpha = \sqrt{p/K}$ . From Eq. (C2), it is seen that  $|X_{12}|$  and  $|X_{03}|$  become small when p is sufficiently large.

# APPENDIX D: ENERGY EIGENSTATES AND THEIR ASYMPTOTIC FORM

As mentioned in the main text, the eigenstates of  $H_{\text{KPO}}$  in Eq. (4) can be approximated by  $D(\pm \alpha) |m\rangle$ . Here, we quantitatively examine the validity of the approximation.

Figure 13 shows the overlap,  $|\langle \psi_i | \psi_i' \rangle|^2$ , between relevant energy eigenstates  $|\psi_i\rangle$  and their approximated one  $|\psi_i'\rangle = D(\pm \alpha) |m\rangle$  as a function of p [Figs. 13(a) and 13(b)] and also as a function of  $\Omega$  [Figs. 13(c) and 13(d)]. It is seen that the approximation becomes more valid when p increases, as seen in Figs. 13(a) and 13(b).

The validity of the approximation can be degraded as  $\Omega$  increases. The overlap for  $|\psi_{0,1}\rangle$  is high for the small- $\Omega$  regime as seen in Fig. 13(c). However, the overlap decreases as  $\Omega$  becomes large. We consider that this is due to the distortion of the potential under the strong drive field. The overlap for  $|\psi_{2,3}\rangle$  is low in the small- $\Omega$  regime, as seen in Fig. 13(d). This is because that these states are loosely trapped by the double-well potential and their Winger function is distributed among both the wells when



FIG. 13. Overlap between energy eigenstates and their approximations  $D(\pm \alpha) | m \rangle$  is shown as a function of p (a),(b) and  $\Omega$  (c),(d). The parameters used are  $\kappa_{\rm ex}/K = 0.01$ ,  $\kappa_{\rm in}/\kappa_{\rm ex} = 0.5$ ,  $\Omega/K = 0.5$  (a),(b), and p/K = 4.0 (c),(d).

 $\Omega$  is small. On the other hand, as  $\Omega$  is increased,  $|\psi_{2,3}\rangle$  is trapped in either of the wells, and therefore the overlap increases. However, because  $|\psi_3\rangle$  is confined loosely in the well, the overlap starts to drop due to the distortion of the potential when the drive field is further strengthened.

# **APPENDIX E: PURE DEPHASING**

We consider the case where there is pure dephasing with the rate of  $\gamma$ . The pure dephasing enhances the relaxation of the diagonal elements of the density matrix, and increases the population of excited states out of the qubit subspace.

To examine the effect of the pure dephasing on the density matrix, we numerically solve the master equation

$$\frac{d\rho(t)}{dt} = -\frac{i}{\hbar} \left[ H(t), \rho(t) \right] + \frac{\kappa_{\text{tot}}}{2} \mathcal{D}[\hat{a}]\rho(t) + \gamma \mathcal{D}[\hat{a}^{\dagger}\hat{a}]\rho(t),$$
(E1)

with

$$H(t) = -\frac{K}{2}\hat{a}^{\dagger 2}\hat{a}^{2} + \frac{p}{2}\left(\hat{a}^{2} + \hat{a}^{\dagger 2}\right) + \Omega(t)(\hat{a}^{\dagger} + \hat{a}),$$

where  $\Omega(t)$  is given by Eq. (7). In the numerical simulation, the initial state is set to  $\rho(0) = (\sqrt{0.2} |\tilde{0}\rangle + \sqrt{0.8} |\tilde{1}\rangle)(\sqrt{0.2} \langle \tilde{0}| + \sqrt{0.8} \langle \tilde{1}|).$ 

The population of the first five levels defined by  $\langle \psi_i | \rho(t) | \psi_i \rangle$  is exhibited in Fig. 14. The change in the population is much faster than in the case without pure dephasing shown in Fig. 2(b). The energy levels out of the qubit subspace are also populated due to the relaxation caused by the pure dephasing. It is also seen that the larger  $\gamma$  is, the larger the change in the populations is.

This result implies that the reflection measurement should be performed before the KPO relaxes to its stationary state. The reflection coefficient can be derived for the



FIG. 14. Time dependence of the population of relevant five levels,  $\langle \psi_i | \rho(t) | \psi_i \rangle$  for  $\gamma/K = 10^{-4}$  (a) and  $10^{-3}$  (b). The red, blue, green, light blue, and orange curves are for i = 0, 1, 2, 3, and 4, respectively. The black solid and red dashed curves in (c) represent the off-diagonal element  $\langle \psi_0 | \rho(t) | \psi_1 \rangle$  for  $\gamma/K = 10^{-4}$  and  $10^{-3}$ , respectively. The parameters used are p/K = 9.0,  $\Omega_0/K = 0.1$ ,  $t_{\text{ramp}} = 20/K$ ,  $\kappa_{\text{ex}}/K = 10^{-2}$  and  $\kappa_{\text{in}}/\kappa_{\text{ex}} = 0.5$ .

case with pure dephasing in the same manner as in Ref. [33]. The reflection coefficient can be written as Eq. (8) with

$$\xi_{mn} = \frac{\kappa_{\text{ex}} X_{mn} \sum_{k} \left( X_{kn}^{*} \rho_{km}^{(F)}[0] - \rho_{nk}^{(F)}[0] X_{mk}^{*} \right)}{i \Delta_{nm} + \kappa_{\text{tot}} X_{nn} X_{mm}^{*} - \frac{\kappa_{\text{tot}}}{2} \left( Y_{nn} + Y_{mm} \right) + L}, \quad (E2)$$

where  $L = 2\gamma Y_{nn}Y_{mm}^* - \gamma (Z_{nn} + Z_{mm})$  and  $Z_{mm} = \langle \psi_m | (\hat{a}^{\dagger} \hat{a})^2 | \psi_m \rangle$ . We assume that the reflection measurement is performed for  $20/K \le t \le 220/K$  and the time-averaged reflection coefficient  $\bar{\Gamma}$  is obtained. This duration of the measurement is approximately 3 µs for  $K/2\pi = 10$  MHz, which is experimentally feasible [34]. The initial state is set to  $\rho(0) = (\sqrt{\rho_{00}(0)} | \tilde{0} \rangle + \sqrt{1 - \rho_{00}(0)} | \tilde{1} \rangle)(\sqrt{\rho_{00}(0)} \langle \tilde{0} | + \sqrt{1 - \rho_{00}(0)} \langle \tilde{1} |)$ . Figure 15 shows  $\bar{\Gamma}$  as a function of  $\rho_{00}(0)$ . It is seen that  $\bar{\Gamma}$  monotonically changes with  $\rho_{00}(0)$ . Therefore, we can extract  $\rho_{00}(0)$  from  $\bar{\Gamma}$ .

When the input field is resonant to a transition  $|\psi_m\rangle \rightarrow |\psi_n\rangle$  and off-resonant to other transitions, the reflection coefficient can be written as  $\Gamma = 1 + \xi_{mn}$ . On the other hand, the reflection coefficient of a linear resonator is written as

$$\Gamma_r = 1 + \frac{\kappa_{\text{ex}}^{(r)}}{i\Delta_r - (\kappa_{\text{ex}}^{(r)} + \kappa_{\text{int}}^{(r)})/2},$$
(E3)



FIG. 15. The relationship between the time-averaged reflection coefficient  $\overline{\Gamma}$  and the diagonal element at the initial time  $\rho_{00}(0)$  for  $\gamma/K = 10^{-4}$  (a) and  $10^{-3}$  (b). The parameters used are p/K = 9.0,  $\Omega_0/K = 0.1$ ,  $t_{\text{ramp}} = 20/K$ ,  $\kappa_{\text{ex}}/K = 10^{-2}$ , and  $\kappa_{\text{in}}/\kappa_{\text{ex}} = 0.5$ .

with the external decay rate  $\kappa_{\text{ex}}^{(r)}$ , internal decay rate  $\kappa_{\text{int}}^{(r)}$ , and detuning  $\Delta_r = \omega_{\text{in}} - \omega_0$  where  $\omega_0$  is the angular resonance frequency of the resonator. Comparing  $\Gamma = 1 + \xi_{mn}$ with Eq. (E3), the nominal external and internal decay rates for the KPO [33] can be defined as

$$\begin{split} \tilde{\kappa}_{ex}^{(mn)} &= \kappa_{ex} X_{mn} \sum_{k} \left( X_{kn}^{*} \rho_{km}^{(F)}[0] - \rho_{nk}^{(F)}[0] X_{mk}^{*} \right), \\ \tilde{\kappa}_{int}^{(mn)} &= -2\kappa_{tot} X_{nn} X_{mm}^{*} + \kappa_{tot} \left( Y_{nn} + Y_{mm} \right) \\ &- 4\gamma Y_{nn} Y_{mm}^{*} + 2\gamma \left( Z_{nn} + Z_{mm} \right) \\ &- \kappa_{ex} X_{mn} \sum_{k} \left( X_{kn}^{*} \rho_{km}^{(F)}[0] - \rho_{nk}^{(F)}[0] X_{mk}^{*} \right). \end{split}$$
(F4)

Figure 16(a) shows the nominal internal and external decay rates as a function of  $\alpha$ . The frequency of the input field is set to that corresponding to the transition from  $|\psi_0\rangle$  to  $|\psi_2\rangle$ . The nominal internal decay rate is much higher than the nominal external decay rate for  $\gamma/K = 10^{-3}$ , that is, the KPO is in the undercoupling regime. Therefore, the reflection coefficient is insensitive to the frequency of the input field compared to the case without the pure dephasing.



FIG. 16. Nominal internal and external decay rates (a) and the real part of the reflection coefficient for  $\rho_{00} = 1$  (b) as functions of  $\alpha (= \sqrt{p/K})$ . The blue and red curves represent the nominal internal and external decay rates for  $\gamma/K = 10^{-3}$ , respectively, in (a). In (a), the blue dashed curve is the nominal internal for  $\gamma/K = 0$ . The other parameters are p/K = 9.0,  $\Omega/K = 0.1$ ,  $\omega_{in} - \omega_p/2 = \Delta \omega_{20}$ ,  $\kappa_{ex}/K = 10^{-2}$ , and  $\kappa_{in}/\kappa_{ex} = 0.5$ .

As seen in Fig. 16(a), the difference between the nominal internal and external decay rates becomes small at  $\alpha \sim 2.3$ . At this point, the sensitivity of the reflection coefficient to  $\rho_{00}$  becomes large compared to other points, as indicated by Re[ $\Gamma(1)$ ] in Fig. 16(b). (Note that  $\Gamma(0) \simeq 1$  in the range of  $\alpha$  used for this figure.) This result implies that there is a suitable point of  $\alpha$  for the measurement of a KPO along the *z*-axis.

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