Effect of Electron Thermal Conductivity on Resonant Plasmonic Detection in Terahertz Hot-Electron Bolometers Based on Metal/Black-AsP/Graphene FETs

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We analyze the operation of terahertz (THz) bolometric detectors based on field-effect transistor (FET) structures with graphene channels (GCs) and black-phosphorus and black-arsenic gate barrier layers (BLs). Such GC FETs use two-dimensional electron gas (2DEG) heating by the incident THz radiation leading to the thermionic emission of hot electrons from the GC via the BL into the gate. Due to the excitation of plasmonic oscillations in the GC by THz signals, the GC FET detector response can be pronouncedly resonant, leading to elevated values of the detector responsivity. The lateral thermal conductivity of the 2DEG and its Peltier cooling can markedly affect the GC FET responsivity, in particular its spectral characteristics. These effects should be considered for the optimization of GC FET detectors.

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I. INTRODUCTION

The field-effect transistor (FET) structures with the graphene channel (GC) and the gate barrier layer (BL) made of the black phosphorus (bP), black arsenic (bAs), and the compounds of these materials $(bAs_{1-x}P_x)$ have shown promise for various device applications. This is because of the unique electron properties of GCs [1] and the bAs_{1-x}P_x layers [2,3] (predicted and demonstrated a long time ago [4,5]). Changing the As mole fraction *x* and the BL thickness W[6–8] allows one to achieve a desirable band alignment and the height of the barriers between GC and the gate, therefore controlling the thermionic activation energy. The latter opens up additional prospects for the FET optimization and use for novel devices, in particular photodetectors [9–21].

In this paper, we evaluate the hot-electron bolometric detectors of terahertz (THz) radiation based on such FET structures. We develop the device model of GC FET detectors with bP and bAs BLs by accounting for the following effects:

(1) the resonant plasmonic heating of the DEG in the GC by the impinging THz radiation input into the GC FET using an antenna;

(2) the electron energy relaxation in the GC associated with the electron-phonon interactions;

(3) the electron thermal conductance along the GC;

(4) the electron cooling due to the thermionic emission from the GC into the gate (the Peltier cooling).

As demonstrated, the role of the electron thermal conductivity can be crucial because it is fairly high (see, for example, [22,23]). Thermionic cooling can become essential at elevated gate bias voltages when the effective height of the energy barrier for electrons (holes) decreases. Our analysis confirms the controllability of the electron activation energy by doping and the gate bias voltage and predicts high values of the detector responsivity associated with the effective heating of the two-dimensional electron gas (2DEG) in the GC by the signal electric field produced by the impinging THz radiation, especially when the plasmonic oscillations are resonantly excited. These effects can influence the detector's performance and should be taken into account for its optimization.

II. DEVICE STRUCTURE

Figure 1 shows the GC FET structure cross-section and top view and its band diagram when the gate bias voltage $V_G \gtrsim 0$. For the definiteness, the materials for the BL and the metal gate, and the GC doping are chosen to provide the flat band in the BL at $V_G = 0$. This band diagram configuration corresponds to the Ohmic side contacts (the FET source and drain). In particular, we focus on the GC FETs with the bP and bAs BLs and Al and Ti gates (the Al/bP/GC and Ti/bAs/GC devices). The GC and the gate

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FIG. 1. (a) Cross-section and top view of the GC FET detector structure with the Al or Ti gate, $bAs_{1-x}P_x$ BL, and the GC on the h-BN substrate and (b) its band diagram under the applied dc bias and ac signal voltages $V_G + \delta V_{\omega} \exp(-i\omega t)$ between the gate the GC side contacts.

length (the spacing between the side contacts, their width, and the thickness of the BL are set to be 2*L*, *H*, and *W*, respectively, with 2*L*, $H \gg W$). We focus on the GC FETs with the GC doped by donors. We assume that the activation energy for the electrons in the GC $\Delta_C - \mu_D = \Delta_M >$ Δ_V , where Δ_C and Δ_V are the band offsets between the BL conduction and valence bands and the Dirac point in the GC, and Δ_M is the difference between the BL and the GC work functions. Here μ_D is the electron Fermi energy in the GC at $V_G = 0$, which is determined by the donor density Σ_D . The latter inequality implies that the thermionic electron gate current dominates over the hole current. The GC FET devices in which the above condition is not valid can be considered analogously.

The voltage between the GC side contacts and the highly conducting metal gate comprises, apart from the bias voltage V_G , the ac component $\delta V_{\omega} \exp(-i\omega t)$, where δV_{ω} and ω are the signal amplitude and the frequency. This is the signal generated in an antenna by incident THz radiation. The THz signal could excite the plasmonic oscillation modes with the symmetric spatial distribution of the ac potential in the GC.

III. 2DEG HEATING

The variation of the thermionic gate current, δj , associated with the incoming THz signal is given by

$$\delta j = j^{\max} \frac{\delta T}{T} \left(\frac{\Delta_C - \mu}{T} \right) \exp\left(-\frac{\Delta_C - \mu}{T} \right), \quad (1)$$

where j^{max} is the maximal value of the current density from the GC, which we estimate as $j^{\text{max}} = e\Sigma/\tau_{\perp}$ with Σ and τ_{\perp} being the 2DEG density in the GC and the escape time, respectively, of the electrons with the energy exceeding the barrier height. Both Σ and τ_{\perp} depend on doping and the gate bias voltage.

The quantity δj comprises the ac component $\delta j_{\omega} \exp(-i\omega t)$ and the rectified dc component $\langle \delta j_{\omega} \rangle$ (as well as the second and higher harmonics). The latter is the variation of the current density averaged over the period of the THz signal $2\pi/\omega$. According to Eq. (1), the rectified component can be presented as

$$\langle \delta j_{\omega} \rangle = j^{\max} \mathcal{F} \frac{\langle \delta T_{\omega} \rangle}{T},$$
 (2)

where

$$\mathcal{F} = \frac{\Delta_C - \mu}{T} \exp\left(-\frac{\Delta_C - \mu}{T}\right). \tag{3}$$

The dependence of the factor $\mathcal{F}(V_G)$ on the gate voltage is associated with the voltage dependence of the electron Fermi energy (see the following).

The variation of the local averaged 2DEG temperature, $\langle \delta T_{\omega} \rangle$ is governed by the following electron heat transport equation:

$$-h\frac{d^2\langle\delta T_{\omega}\rangle}{dx^2} + \frac{\langle\delta T_{\omega}\rangle}{\tau_{\varepsilon}} = Q_{\omega}^J - Q_{\omega}^B.$$
 (4)

Here $h \simeq v_W^2/2\nu$ is the electron thermal conductivity in the GC per electron (this corresponds to the Wiedemann-Franz relation), τ_{ε} is the electron energy relaxation time in the GC, $v_W \simeq 10^8$ cm/s is the characteristic electron velocity in GCs, and ν is the electron scattering frequency in the GC. The second term on the left-hand side of Eq. (4) is associated with the 2DEG energy transfer to the phonon system (in particular, to optical phonons), whereas the terms on the

right-hand site, Q_J and Q_B , are the Joule power received by the 2DEG in the GC and the power transferred by the electrons emitted from the 2DEG over the BL averaged over time (see, for example, [24]). The Joule contribution to the 2DEG heating is given by

$$Q_{\omega}^{J} = \frac{\text{Re}\sigma_{\omega}}{\Sigma} \langle |\delta E_{\omega}|^{2} \rangle.$$
 (5)

Here, accounting for the excitation of plasmonic oscillations in the gated 2DEG (see, for example, [25–35] and the references therein) by the THz signal received by an antenna, one can obtain for the ac potential in the GC

$$\delta\varphi_{\omega} = \delta V_{\omega} \frac{\cos(\gamma_{\omega} x/L)}{\cos(\gamma_{\omega})}.$$
(6)

Hence, for the square of the signal electric field amplitude we arrive at

$$\langle |\delta E_{\omega}|^{2} \rangle = \frac{1}{2} \left(\frac{\delta V_{\omega}}{L} \right)^{2} \left| \frac{\gamma_{\omega} \sin(\gamma_{\omega} x/L)}{\cos \gamma_{\omega}} \right|^{2}, \qquad (7)$$

where Re $\sigma_{\omega} = \sigma_0 v^2 / (v^2 + \omega^2)$, $\sigma_0 = e^2 \mu / \pi \hbar^2 v$ and v are the Drude dc conductivity and the electron scattering frequency in the 2DEG, $\gamma_{\omega} = \pi \sqrt{\omega(\omega + iv)} / 2\Omega_P$ and $\Omega_P = (\pi e/\hbar L) \sqrt{\mu W/\kappa}$ are the effective wavenumber and the plasmonic frequency (corresponding to the symmetric conditions at the contacts), respectively, with κ and W being the dielectric constant of the BL and its thickness. The quantity Q_{ω}^B , which characterizes the cooling of the 2DEG, is presented as

$$Q^{B}_{\omega} = \frac{\langle \delta j_{\omega} \rangle}{e\Sigma} \Delta_{C} = \frac{\mathcal{F} \Delta_{C}}{\tau_{\perp}} \frac{\langle \delta T_{\omega} \rangle}{T}.$$
 (8)

IV. RECTIFIED CURRENT

Assuming sufficiently low thermal resistance of the highly conducting side contacts, we set the following boundary conditions for Eq. (4):

$$\langle \delta T_{\omega} \rangle|_{x=\pm L} = 0, \qquad \langle \delta j_{\omega} \rangle|_{x=\pm L} = 0.$$
 (9)

Solving Eq. (4) with the boundary conditions given by Eq. (9) and invoking Eq. (2), we arrive at the following spatial distribution of the rectified current density:

$$-\mathcal{L}^{2}\frac{d^{2}\langle\delta j_{\omega}\rangle}{dx^{2}} + \langle\delta j_{\omega}\rangle = \frac{e\text{Re}\sigma_{\omega}}{2T}\frac{\tau_{\varepsilon}\mathcal{F}/\tau_{\perp}}{(1+\tau_{\varepsilon}\mathcal{F}\Delta_{C}/\tau_{\perp}T)} \times \left|\frac{\gamma_{\omega}\sin(\gamma_{\omega}x/L)}{\cos\gamma_{\omega}}\right|^{2}\left(\frac{\delta V_{\omega}}{L}\right)^{2},$$
(10)

where $\mathcal{L} = \sqrt{h\tau_{\varepsilon}/(1 + \tau_{\varepsilon}\mathcal{F}\Delta_C/\tau_{\perp}T)}$ is the "thermal" length. The spatial dependence in the right-hand side of Eq. (10) reflects the nonuniformity of the 2DEG heating associated with the nonuniform distribution of the ac plasmonic electric field along the GC.

The rectified current density $\langle \delta j_{\omega} \rangle$ is an oscillatory function of the signal frequency. It exhibits the resonant peaks at $\omega \simeq (2n-1)\Omega_P$, where $n = 1, 2, 3, \ldots$ is the index of the plasmonic resonance, provided that $\nu \ll \Omega_P$. The latter inequality is assumed in the following.

Considering the condition $\nu \ll \Omega_P$, Eq. (10) can be somewhat simplified and presented as

$$-\mathcal{L}^{2} \frac{d^{2} \langle \delta j_{\omega} \rangle}{dx^{2}} + \langle \delta j_{\omega} \rangle$$

$$\simeq \frac{2e\sigma_{0}}{T} \frac{\tau_{\varepsilon} \mathcal{F} / \tau_{\perp}}{(1 + \tau_{\varepsilon} \mathcal{F} \Delta_{C} / \tau_{\perp} T)} \left(\frac{\delta V_{\omega}}{L}\right)^{2}$$

$$\times \frac{\sin^{2}[\pi \omega / 2\Omega_{P})(x/L)]}{\sin^{2}(\pi \omega / 2\Omega_{P}) + (4\Omega_{P} / \pi \nu)^{2} \cos(\pi \omega / 2\Omega_{P})^{2}]}.$$
(11)

Introducing the parameter $\mathfrak{a} = \mathcal{L}/L$ and solving Eq. (10) with boundary conditions (9), we obtain

$$\langle \delta j_{\omega} \rangle = \frac{e\sigma_0}{T} \frac{\tau_{\varepsilon} \mathcal{F} / \tau_{\perp}}{(1 + \tau_{\varepsilon} \mathcal{F} \Delta_C / \tau_{\perp} T)} \left(\frac{\delta V_{\omega}}{L} \right)^2 \left\{ \frac{1 - \frac{\cos(\pi \,\omega \, x / \,\Omega_P L)}{1 + (\pi \, \varpi \, \omega / \,\Omega_P)^2} - \left[1 - \frac{\cos(\pi \,\omega / \,\Omega_P)}{1 + (\pi \, \varpi \, \omega / \,\Omega_P)^2} \right] \frac{\cosh(x/L\varpi)}{\cosh(1/\varpi)}}{\sin^2(\pi \, \omega / 2\Omega_P) + (4\Omega_P / \pi \, \nu)^2 \cos^2(\pi \, \omega / 2\Omega_P)} \right\}.$$
(12)

Integrating $\langle \delta j_{\omega} \rangle$, given by Eq. (12), over the GC plane, for the net rectified current $\langle \delta J_{\omega} \rangle = H \int_{-L}^{L} dx \langle \delta j_{\omega} \rangle$ at the plasmonic resonances, we arrive at the following expression:

$$\langle \delta J_{\omega} \rangle = \frac{2HLe\sigma_0}{T} \frac{\tau_{\varepsilon} \mathcal{F}/\tau_{\perp}}{(1 + \tau_{\varepsilon} \mathcal{F} \Delta_C/\tau_{\perp} T)} \left(\frac{\delta V_{\omega}}{L}\right)^2 \frac{\Pi_{\omega}(\mathfrak{x})}{\left[\sin^2(\pi \,\omega/2\Omega_P) + (4\Omega_P/\pi \nu)^2 \cos^2(\pi \,\omega/2\Omega_P)\right]}.$$
 (13)

Here

$$\Pi_{\omega} = 1 - \frac{\sin(\pi \,\omega/\Omega_P)}{(\pi \,\omega/\Omega_P)[1 + (\pi \,\varpi \,\omega/\Omega_P)^2]} - \left[1 - \frac{\cos(\pi \,\omega/\Omega_P)}{1 + (\pi \,\varpi \,\omega/\Omega_P)^2}\right] \operatorname{etanh}\left(\frac{1}{\varpi}\right). \quad (14)$$

The factor $\Pi_{\omega}(\mathbf{a})$ characterizes the effect of the electron thermal conductivity on the rectified current and the signal frequency dependence of the latter.

V. GC FET DETECTOR RESPONSIVITY

The current responsivity (in the units A/W) of the GC FET detector R_{ω} is proportional to the net rectified current $\overline{\langle \delta J_{\omega} \rangle}$, which is given by Eqs. (13) and (14), divided the incident THz radiation power P_{ω} collected by an antenna. Considering that the relation between the ac voltage generated at the side contacts δV_{ω} and the half-wavelength dipole antenna with the gain g = 2 the power P_{ω} [36] (see also [22] for details) is given by $\delta V_{\omega}^2 = 32P_{\omega}/gc$ with *c* and *g* being the speed of light in vacuum and the antenna gain (g = 1.64), we obtain the GC FET bolometric detector

TABLE I. Parameters of the GC FET structures under consideration [38–40].

Structure	$\Delta_M ({\rm meV})$	$\Delta_V (\text{meV})$	$\Delta_C (\mathrm{meV})$	$\mu_D ({\rm meV})$
Al/bP/GC	85	125	225	140
Ti/bAs/GC	70	90	190	120

responsivity $R_{\omega} = \overline{\langle \delta J_{\omega} \rangle} / P_{\omega}$

$$R_{\omega} = \overline{R} \frac{(\tau_{\varepsilon} \mathcal{F} \Delta_C / \tau_{\perp} T)}{(1 + \tau_{\varepsilon} \mathcal{F} \Delta_C / \tau_{\perp} T)} \frac{(v_W / L)}{[\overline{\nu} + \tilde{\nu} (\omega / \Omega_P)^2]} \times \frac{\Pi_{\omega}(\mathfrak{a})}{[\sin^2(\pi \omega / 2\Omega_P) + (4\Omega_P / \pi \nu)^2 \cos^2(\pi \omega / 2\Omega_P)]}.$$
(15)

Here

$$\overline{R} = \frac{32}{137\pi g} \frac{e}{\Delta_C} \frac{\mu_D}{\hbar} \frac{H}{v_W},$$
(16)

where we have taken into account that the fine structure parameter $\alpha = e^2/c\hbar \simeq 1/137$. To account for the effect of the 2DEG viscosity on the plasma oscillations damping



FIG. 2. Normalized responsivity R_{ω}/\overline{R} versus signal frequency $\omega/2\pi$ of the GC FETs (a)–(c) with the Al/bP/GC structure and the GC half-length (a) $L = 1 \ \mu m \ (\Omega_P/2\pi = 0.52 \text{ THz})$ and $\tilde{\nu} = 0.1 \text{ ps}^{-1}$, (b) $L = 1.5 \ \mu m \ (\Omega_P/2\pi = 0.35 \text{ THz})$ and $\tilde{\nu} = 0.1 \text{ ps}^{-1}$, (c) $L = 1 \ \mu m \ (\Omega_P/2\pi = 0.52 \text{ THz})$ and $\tilde{\nu} = 0.25 \text{ ps}^{-1}$, and (d) with Ti/bAs/GC structure and $L = 1 \ \mu m \ (\Omega_P/2\pi = 0.48 \text{ THz})$ and $\tilde{\nu} = 0.1 \text{ ps}^{-1}$.



FIG. 3. Same as for Fig. 2(a), but for weak electron thermal transport (in the limit x = 0).

in Eq. (15), we set [37] $v = \overline{v} + \tilde{v} (\omega/\Omega_P)^2$, where \overline{v} and \tilde{v} are related to the electron interaction with impurities and acoustic phonons and the electron viscosity of the 2DEG in the GC, respectively.

For $\mu_D = 120 - 140$ meV and H = 10 - 20 μ m, Eq. (16) yields $\overline{R} \simeq (450-900)$ A/W.

VI. SPECTRAL CHARACTERISTICS

In the following we calculate the room-temperature GC FET detector responsivity as a function of the signal frequency for different plasmonic and collision frequencies and bias voltages using Eqs. (15) and (16) and invoking Eq. (14). As examples, we consider the GC FETs with the band parameters listed in Table I. Other parameters are indicated in the figure captures. The chosen values of the plasmonic frequency correspond to $W \simeq (10-20)$ nm.

Figure 2 shows the spectral dependences of the normalized responsivity of the GC FET bolometric detectors with the Al/bP/GC and Ti/bAs/GC structures calculated for different values of the frequencies $\bar{\nu}$ and $\tilde{\nu}$ (and, hence, different electron thermal lengths) and different GC lengths at T = 25 meV and $V_G \simeq 0$. The latter implies that $\mathcal{F} \simeq \mathcal{F}_0 = (\Delta_M/T) \exp(-\Delta_M/T)$). The structural parameter ranges are discussed in Appendix A.

The frequency dependences of the responsivity demonstrated in Figs. 2 and 3 exhibit the pronounced peaks at the frequencies close to the plasmonic resonant frequencies $\omega = (2n - 1)\Omega_P$. As follows from the comparison of Figs. 2(a) and 2(c), an increase in the electron viscosity markedly smears the higher plasmonic resonances.

One can see from Fig. 2 that the responsivity R_{ω} can be markedly smaller than its characteristic value \overline{R} , even at the resonant maxima (about one order of magnitude smaller as follows, for example, from Eq. (17) and the consequent estimate).

VII. ROLE OF ELECTRON THERMAL CONDUCTIVITY

An increase in the collision frequency $\overline{\nu}$ leads, as might be expected, to a smearing of the resonant peaks. However, the average values of the responsivity show a moderate increase with increasing $\overline{\nu}$. This can be interpreted by a smaller electron thermal conductivity h in the GCs with a larger $\overline{\nu}$. As a result, increasing collision frequency $\overline{\nu}$ gives rise to a smaller Joule power but a weaker transfer of the 2DEG heat to the side contacts. The comparison of Figs. 2(a) and 2(b) indicates that in the devices with a longer GC, the peaks corresponding to higher resonances can be much more pronounced. This is because an increase in L leads to a weakening of the electron thermal transfer (the parameter æ $\propto L^{-1}$).

To confirm the significance of the electron thermal transfer in the GC FETs under consideration, we calculated the frequency dependences of the responsivity disregarding the electron thermal conductivity, i.e., neglecting the electron heat transfer to the side contacts. Figure 3 shows the responsivity of the GC FET with the parameters used for Figs. 2(a) and 2(c) calculated for the hypothetical case when the electron thermal conductivity is insignificant. One can see that in the case of $\alpha \rightarrow 0$, the resonant peaks are higher and their smearing is weaker. Thus, the electron thermal transfer along the GC to the side contacts pronouncedly affects the responsivity spectral characteristics. The comparison of the plots in Figs. 3(a) and 3(b) indicates that the electron viscosity naturally weakens the plasmonic resonances.

VIII. COMMENTS

An increase in the gate voltage V_G results in the rise of R_{ω} associated with a larger \mathcal{F} factor in some range of larger voltages (see Appendices A and B). Considering Eq. (3) and accounting for Eq. (B3), for not too large V_G , we obtain

$$\mathcal{F} \simeq \frac{\Delta_M - \mu_0 e V_G / (\mu_0 + \mu_D)}{T} \times \exp\left[-\frac{\Delta_M - \mu_0 e V_G / (\mu_0 + \mu_D)}{T}\right].$$
(17)

Here $\mu_0 = (\hbar^2 v_W^2 \kappa)/8e^2 W$ (see Appendices A and B). As follows from Eq. (17), the sensitivity of the factor \mathcal{F} to the gate voltage V_G is weakened by a relatively small parameter $\mu_0/(\mu_0 + \mu_D)$.

In the expression for the signal current density given by Eq. (2), we disregarded the rectified component associated with the modulation of the activation energy by the plasmonic oscillations potential. The thermionic current density as a function of the net voltage drop is determined by the following factor:

$$\frac{\mu_0}{(\mu_0 + \mu_D)} \frac{e(V_G + \delta\varphi_\omega)}{T}$$

where $\delta \varphi_{\omega}$ is given by Eq. (6). At low gate voltage, the pertinent ac current density component is equal to

$$\begin{split} \langle \delta \tilde{j}_{\omega} \rangle &\simeq \frac{j^{\max}}{2} \exp\left(-\frac{\Delta_M}{T}\right) \left(\frac{\mu_0}{\mu_0 + \mu_D}\right)^2 \frac{\langle \delta \varphi_{\omega}^2 \rangle}{T^2} \\ &\simeq \frac{j^{\max}}{4} \exp\left(-\frac{\Delta_M}{T}\right) \left(\frac{\mu_0}{\mu_0 + \mu_D}\right)^2 \left|\frac{\cos(\gamma_{\omega} x/L)}{\cos \gamma_{\omega}}\right|^2 \\ &\qquad \times \frac{(\delta V_{\omega})^2}{T^2}. \end{split}$$
(18)

Comparing the thermionic rectified current density given by Eq. (2) and the consequent formulas with $\langle \delta \tilde{j}_{\omega} \rangle$, described by Eq. (18), at the pronounced plasmonic resonances ($\Omega_P \gg \nu$), we obtain

$$\frac{\langle \delta j_{\omega} \rangle}{\langle \delta \tilde{j}_{\omega} \rangle} \simeq \left(\frac{\kappa}{\pi}\right) \frac{\tau_{\varepsilon} \nu \Delta_M}{e^2 W \Sigma} \left(\frac{\mu_0 + \mu_D}{\mu_0}\right)^2 \\ \simeq 8(\tau_{\varepsilon} \nu) \left(\frac{\mu_0 + \mu_D}{\mu_D}\right)^2 \left(\frac{\Delta_M}{\mu_0}\right) \simeq 8(\tau_{\varepsilon} \nu) \left(\frac{\Delta_M}{\mu_0}\right).$$
(19)

Since the factors $\tau_{\varepsilon}\nu$ and Δ_M/μ_0 in the right-hand side of Eq. (19) are much larger than unity, $\langle \delta j_{\omega} \rangle / \langle \delta \tilde{j}_{\omega} \rangle \gg 1$.

Apart from the detector responsivity R_{ω} we analyzed previously, the responsivity, R_{ω}^{area} , normalized by the detector area 2*lH* can be used. For R_{ω}^{area} one can obtain $R_{\omega}^{area} = R_{\omega}(S_{\omega}/2LH)$, where $S_{\omega} = \lambda_{\omega}^2 g/4\pi$ is the antenna aperture [36] and $\lambda_{\omega} 2\pi c/\omega$ is the wavelength of the incident radiation in vacuum. This implies that $R_{\omega}^{area} \gg R_{\omega}$, at least in the THz range, and $R_{\omega}^{area} \propto R_{\omega}/\omega^2$, hence R_{ω}^{area} and R_{ω} exhibit fairly different spectral characteristics.

Using Eqs. (14) and (18), we find that R_{ω} reaches a maximum at $V_G = V_G^{\text{max}} = (\Delta_M - T)(\mu_0 + \mu_D)/e\mu_0$. Setting, for example, $\Delta_M = 85$ meV, $\mu_D = 140$ meV, and $\mu_0 = (14-21)$ meV, we obtain $V_G^{\text{max}} \simeq (460-660)$ meV. However, it is impractical to use such large gate voltages because this can lead to very high dc density [given by Eq. (B4)], at which the spatial distribution of the steady-state temperature of the 2DEG can be substantially nonuniform, particularly, when the current-crowding effect might become crucial. Moreover, at the voltages in question, the electron tunneling between the GC and the gate can enable an elevated tunneling current (see Appendix C). Although the tunneling current does not markedly affect the bolometric response (due to its weak dependence on the 2DEG effective temperature), it together with the elevated thermionic current can substantially decrease the GC FET detector dark-current limited detectivity D^* .

In contrast, at relatively low voltages, the dark current, which, according to Eq. (B4), is proportional to V_G , the GC FET detector dark-current limited detectivity $D^* \propto 1/\sqrt{V_G}$ can be large. This implies that the maximal GC FET detector detectivity can be achieved at small V_G when the dark current density \overline{j} is fairly small, being primarily limited not by the dark current but by the Johnson-Nyquist noise (see, for example, [41]).

The speed of the GC FET detectors is determined by the electron characteristic times τ_{ε} and τ_{\perp} associated with the transfer of the 2DEG energy to phonons and the cooling due to the thermionic emission. The 2DEG cooling at the side contacts can also affect the characteristic time of the speed of GC FET detector operation t_{θ} . Assuming the device parameters using above, we obtain the estimate $t_{\text{theta}} \sim 20$ ps. It is worth noting that an increase in t_{theta} is usually beneficial for an increase in the detector responsivity. To study the dynamics GC FET photodetectors one need to modify (generalize) the device model accordingly. However, this is beyond the aim of this work.

IX. CONCLUSIONS

We have analyzed the GC FET bolometric THz detectors with the Al/bP/GC and Ti/bAs/GC. The operation of such devices is enabled by the heating of the 2DEG in the GC by the THz radiation resulting in an increase in the thermionic current from the GC via the bP or bAs BLs into a metal gate. We have demonstrated that the electron thermal conductivity and the Peltier cooling of the 2DEG in the GC can markedly influence the GC energy balance pronouncedly affecting the value and the spectral characteristics of the GC FET detectors, which should be accounted for in the device optimization.

The data that support the findings of this study are available within the article.

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APPENDIX A: DEVICE PARAMETERS

We assume that the electron energy relaxation time τ_{e} at room temperature is determined primarily by the GC optical phonons [42-46] and the interface optical phonons [14,47]. The analysis of these references, considering that the time of the spontaneous optical phonon emission in GC $\tau_0 \lesssim 1$ ps and accounting for the smallness of the optical phonon number at room temperature, leads to the estimate $\tau_{\varepsilon} \simeq 10$ –20 ps. The escape of an electron with an energy exceeding Δ_C from 2DEG into the gate via the BL is possible after its scattering on acoustic phonons and impurities with a substantial variation of the electron momenta (with the electron turning almost perpendicular to the GC plane). Assuming that the electron momentum relaxation time associated with the acoustic phonon scattering at room temperature $\tau_{ac} \sim 1$ ps [48–50], one can conclude that $\tau_{\perp} > \tau_{ac}$ or even $\tau_{\perp} \gg \tau_{ac}$. Considering this, in our estimates and calculations in the following, we set $\tau_{\perp} \sim 10$ ps.

The voltage factor $(\tau_{\varepsilon}\mathcal{F}/\tau_{\perp})/[1 + (\tau_{\varepsilon}\mathcal{F}\Delta_C/\tau_{\perp}T)]$ in Eqs. (9)–(12) depends on the bias voltage V_G , which affects the electron Fermi energy μ . At moderate bias voltages, the \mathcal{F} versus V_G is given by Eq. (3) with $\mu \simeq \mu_D + \mu_0 eV_G/(\mu_0 + \mu_D)$, where $\mu_0 = (\hbar^2 v_W^2 \kappa)/8e^2 W$ with $v_W \simeq 10^8$ cm/s being the characteristic electron velocity in GCs. If $\kappa = 4 - 6$ and W = 10 nm, one obtains $\mu_0 \simeq (14-21)$ meV. At low bias voltages $\mathcal{F} \simeq \mathcal{F}_0 = (\Delta_M/T) \exp(-\Delta_M/T)$. Considering the GC FET Al/bP/ GC structures with $\mu_D = 140$ meV and the Ti/bAs/GC structures with $\mu_D = 120$ meV, for room temperature we obtain $\mathcal{F}_0 \simeq 0.113$ and $\mathcal{F}_0 \simeq 0.170$, respectively.

We estimate the electron thermal conductivity as $h \simeq v_W^2/2\nu$. For $\nu = (1-2)$ ps⁻¹, the latter yields $h \simeq (2.5-5.0) \times 10^3$ cm²/s. These values are smaller than the record electron thermal conductivity, which can be extracted from the experimental papers [22,23] for the 2DEG in the suspended GCs with the electron densities $\Sigma \gtrsim 10^{13}$ cm⁻¹. The lower values assumed by us can be justified by the presence of the gate layer and the substrate surrounding the GC in the devices under consideration. Thus, the thermal length (at a small V_G)

$$\mathcal{L}_0 \simeq \sqrt{\frac{v_W^2 \tau_\varepsilon}{2\nu (1 + \tau_\varepsilon \mathcal{F}_0 \Delta_C / \tau_\perp T)}}$$
(A1)

depends on the quality of the GC and the interfaces between the GS and the surrounding layers (via the dependence on ν) and on the contribution of the surface optical phonons to the electron energy relaxation time (via the dependence on τ_{ε}). This implies that the value of \mathcal{L}_0 can vary in a wide range. For definiteness, we fix τ_{ε} and τ_{\perp} , calculating the GC FET detector characteristics for different ν .

Setting $\tau_{\varepsilon} \simeq 10 \text{ ps}$, $\tau_{\perp} = 10 \text{ ps}$, $\mathcal{F}_0 = 0.113 - 0.170$, and $\nu = (0.5 - 2.5) \text{ ps}^{-1}$, we find $\mathcal{L}_0 \simeq (0.9 - 2.2) \text{ }\mu\text{m}$.

The quantity $\tilde{\nu} \simeq \xi_{\text{visc}} q_P^2 \simeq \xi_{\text{visc}} (\pi/2L)^2 (\omega/\Omega_P)^2$, where $\xi_{\text{visc}} \simeq (250-1000) \text{ cm}^2/\text{s}$ [37] is the electron viscosity coefficient and $q_P = (\pi \omega/2L\Omega_P)$ is the wavenumber of the plasma mode in the GC FET under consideration. For the above values of ξ_{visc} and $L = 1 \, \mu\text{m}$, one obtains $\tilde{\nu} \simeq (0.06-0.25) \, \text{ps}^{-1}$.

APPENDIX B: FERMI ENERGY VS GATE VOLTAGE

When the electron plasma in the GC is degenerate ($\mu \gg T$) μ is governed by the following equation:

$$\mu = \hbar v_W \sqrt{\pi \Sigma_D + \frac{\kappa \overline{\Phi}}{4eW}},\tag{B1}$$

where the term proportional to $\overline{\Phi} = (\Delta_C - \Delta_M - \mu + eV_G)/e$ corresponds to the electron density electrically induced in the GC (its dependence on μ reflects the quantum capacitance effect [51–53]). Under the condition of the BL flat band $\overline{\Phi} = \Delta_C - \Delta_M - \mu_D = 0$ at $V_G = 0$, hence $\mu = \mu_D$, and $\Sigma_D = \Sigma_D^{=} = (\Delta_C - \Delta_M)^2 / \pi \hbar^2 v_W^2$. Considering this, we arrive at

$$\mu = \sqrt{\mu_D^2 + \mu_0 (eV_G + \mu_D - \mu)}$$
(B2)

with $\mu_0 = (\kappa \hbar^2 v_W^2 / 8e^2 W)$.

For moderate and high gate voltages Eq. (B2) yields

$$\mu \simeq \mu_D + \frac{\mu_0}{(\mu_D + \mu_0)} eV_G, \ \mu \simeq \sqrt{\mu_D^2 + 2\mu_0 eV_G}, \ \ (B3)$$

respectively.

In particular, using Eqs. (2) and (B3), for the dc currentvoltage characteristics in the most actual range of moderate gate voltages, we obtain

$$\overline{j} \simeq j^{\max} \exp\left(-\frac{\Delta_M}{T_0}\right) \exp\left[\frac{\mu_0}{(\mu_D + \mu_0)} \frac{eV_G}{T_0}\right] \times \left[1 - \exp\left(-\frac{eV_G}{T_0}\right)\right].$$
(B4)

APPENDIX C: TUNNELING

At sufficiently high gate voltages when $e\overline{\Phi} > \Delta_C - \mu$, the energy barrier in the BL can become triangular, where $e\overline{\Phi} = \Delta_C - \Delta_M - \mu + eV_G = \mu_D - \mu + eV_G$ and The latter inequality yields $eV_G > \Delta_M$.

In this case, the electron tunneling from the GC into the gate (via the triangular barrier in question) can be substantial.

The tunneling electron current through the triangular potential barrier assumed above [see Fig. 1(b)], can be estimated as [54]

$$\overline{j}^{\text{tunn}} \simeq j^{\max} \exp\left[-\frac{4\sqrt{2m}(\Delta_C - \mu)^{3/2}W}{3e\hbar\overline{\Phi}}\right], \quad (C1)$$

where m is the electron effective mass in the BL.

Accounting for Eqs. (2) and (B4), for the net DC current at large gate voltages we obtain

$$\frac{\overline{j}}{j^{\max}} \simeq \exp\left(\frac{\mu - \Delta_C}{\overline{T}}\right) + \exp\left[-\frac{4\sqrt{2m}(\Delta_C - \mu)^{3/2}W}{3e\hbar\overline{\Phi}}\right].$$
(C2)

Considering that a $e\overline{\Phi} = \mu_D - \mu + eV_G \simeq eV_G$, Eq. (C2) becomes

$$\frac{\overline{j}}{j^{\max}} \simeq \exp\left(\frac{\mu - \Delta_C}{\overline{T}}\right) + \exp\left[-\frac{4\sqrt{2m}(\Delta_C - \mu)^{3/2}W}{3\hbar eV_G}\right].$$
(C3)

Hence, the thermionic current exceeds the tunneling current if

$$V_G < \frac{4\sqrt{2m(\Delta_C - \mu)}T}{3e\hbar}W.$$
 (C4)

Accounting for that the responsivity maximum corresponds to $\Delta_C - \mu = T$, we obtain

$$V_G < V_G^{\text{tunn}} = \frac{4\sqrt{2m}T^{3/2}}{3e\hbar}W.$$
 (C5)

Assuming $m = 0.22m_0 = 2 \times 10^{-28}$ g and W = 10 nm for room temperature we find $V_G^{\text{tunn}} \simeq 0.14$ V.

In devices with relatively large Δ_M (in which even at $V_G = 0$ the energy barrier in the BL is triangular, i.e., $e\overline{\Phi} > 0$ at $V_G = 0$), the quantity $\overline{\Phi}$ can be small even at high bias voltages V_G , so that V_G^{tunn} might be fairly large.

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