


Atmospheric Aerosol Clearing by Femtosecond Filaments

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Atmospheric aerosols, such as water droplets in fog, interfere with laser propagation through scattering and absorption. Femtosecond optical filaments have been shown to clear foggy regions, improving the transmission of subsequent pulses. However, the detailed fog-clearing mechanism had yet to be determined. Here, we directly measure and simulate the dynamics of water droplets with a radius of about $5\ \mu\text{m}$, typical of fog, under the influence of optical and acoustic interactions that are characteristic of femtosecond filaments. We find that, for filaments generated by the collapse of collimated near-infrared femtosecond pulses, the main droplet-clearing mechanism is optical shattering by laser light. For such filaments, the single-cycle acoustic wave launched by filament-energy deposition in air leaves droplets intact and drives negligible transverse displacement, and therefore, negligible fog clearing. Only for tightly focused nonfilamentary pulses, where local energy deposition greatly exceeds that of a filament, do acoustic waves significantly displace aerosols.

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I. INTRODUCTION

Filamentation of short powerful laser pulses in transparent optical media occurs when self-focusing collapse from the Kerr effect is arrested by ionization. For femtosecond laser pulses in air, the dynamic interplay between self-focusing and ionization defocusing gives rise to a self-guided beam consisting of a high intensity “core” region of diameter $d_{\text{core}} \sim 200\ \mu\text{m}$ surrounded by a lower intensity “reservoir,” which continuously exchanges energy with the core during propagation [1–3]. In air, the peak core intensity is limited by plasma refraction to $< \sim 10^{14}\ \text{W}/\text{cm}^2$ [4]. Typically, the axial extent of intense core propagation is much greater than the Rayleigh range corresponding to d_{core} this is of high interest to applications of long-range propagation [5,6]. The axial extent of the filament is approximately set by the overall diameter (and therefore, Rayleigh range) of the filamenting beam [7]—for example, a 2-cm-diameter beam of sufficient peak power can generate a filament over hundreds of meters. Filaments are resistant to small blockages due their core-plus-reservoir structure: if the high-intensity core is obstructed by a water droplet or aerosol, it is reformed downstream by energy flow from the surrounding reservoir [8–10]. Atmospheric filaments have numerous applications, including long-distance laser-induced water condensation [11], atmospheric spectroscopic analysis [12],

laser-induced breakdown spectroscopy [13], electrical discharge control [14,15], quasi-steady-state air-density modulation [16], and terahertz generation [17].

In air, filaments deposit energy primarily through plasma generation and rotational excitation of O_2 and N_2 [18,19]. Inverse Bremsstrahlung heating from electron-ion collisions is negligible for the sub-picosecond pulses typically used in air filamentation [20]. Energy deposition is impulsive on the timescale of the acoustic response of air to the filament, $\tau_a \sim d_{\text{core}}/2c_s \sim 300\ \text{ns}$, using $c_s \sim 300\ \text{m/s}$ for the speed of sound in air. The impulsively heated air launches a locally cylindrical single-cycle acoustic wave, leaving behind a density depression, or “density hole,” along the laser axis that lasts for several milliseconds [21,22]. The strength of the acoustic wave and depth of the density depression are each proportional to the energy deposited per unit length [7].

One important application of filamentation is fog clearing. Prior experiments [23,24] have shown that a filament propagating in a fog chamber improves the transmission of optical pulses injected immediately afterward along the filament axis. Fog-droplet clearing is also demonstrated using a timed sequence of pump pulses that heat the air by resonantly exciting molecular rotations [25]. Such droplet clearing may have applications in optical data transmission [23] or directed energy [26]. While the physical mechanism for improved transmission is suggested to be droplet clearing by the laser-induced acoustic wave [24,25], to date, there have been no direct measurements of this or other possible mechanisms.

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Here, we directly measure and simulate the dynamics of carefully positioned water droplets with a radius of about $5\ \mu\text{m}$ under the influence of optical and acoustic interactions that are characteristic of femtosecond filaments in air. Droplets of this size are well within the typical aerosol size distribution of fog [27,28]. We find that, for filaments generated by the collapse of collimated near-infrared femtosecond pulses, the main clearing mechanism of droplets is optical shattering by the laser light. For such filaments, the single-cycle acoustic wave launched by filament-energy deposition leaves droplets intact and drives negligible radial displacement. We find that, only for tightly focused nonfilamentary pulses, where local energy deposition greatly exceeds that of a filament, can acoustic waves significantly displace aerosols.

II. MECHANISMS FOR WATER-DROPLET CLEARING

We anticipate two main droplet-clearing mechanisms and set up two experiments to study them. We consider a droplet “cleared” when it is either transversely displaced, largely intact, from the beam path of a subsequent pulse or shattered into sufficiently small fragments (in the Rayleigh-scattering regime) that scattering losses of a subsequent pulse would be greatly reduced. For both experiments, we use a Ti:sapphire ($\lambda_0 = 812\ \text{nm}$, pulse full width at half maximum $\tau = 45\ \text{fs}$, pulse rate 10 Hz) pump beam to generate a filament and a spatially filtered frequency-doubled Nd:YAG ($\lambda_0 = 532\ \text{nm}$, $\tau \sim 7\ \text{ns}$, 10 Hz) probe beam to image droplets and the hydrodynamics driven by the laser-heated air. The delay of the probe relative to the pump is electronically controlled by a digital delay box, with few-nanosecond jitter that is insignificant compared to the displacement time of the droplet. Individual distilled-water droplets with a radius of $(5 \pm 1.5)\ \mu\text{m}$ are generated by a piezoelectric driven $10\text{-}\mu\text{m}$ -inner-diameter nozzle mounted on a three-dimensional translation stage and synchronized to the pump and probe pulses [see Fig. 1(a)]. The nozzle is positioned above the laser axis and pointing down, so the droplets enter the laser beam by gravity. Rough positioning of the droplet with respect to the laser axis is controlled using the digital delay, with fine two-dimensional positioning in the transverse plane controlled with the translation stage. The droplet is positioned at the longitudinal location where the filament-energy deposition and acoustic wave amplitude are maximized.

In Experiment 1 [Fig. 1(a)], the pump beam is a filament generated using a near-collimated beam, where self-focusing is not assisted by a focusing optic (in contrast to Refs. [23,24]). The collimated-beam configuration is most likely to be used for long-range filament applications in the field. The goal in this experiment is to observe the relative contributions of radial droplet displacement

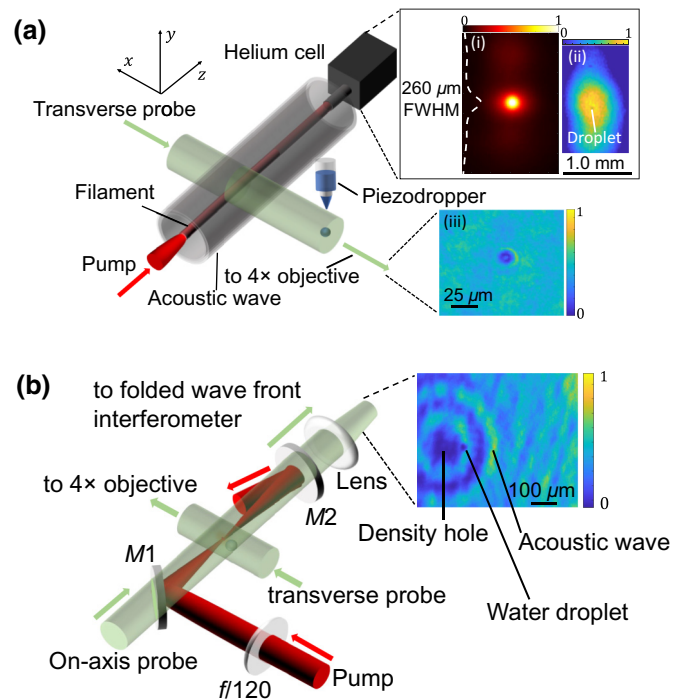


FIG. 1 (a) Diagram of Experiment 1. Beam is down-collimated by a reflective telescope to a $w_0 = 1\ \text{mm}$ waist (e^{-2} intensity radius) to generate a filament with peak intensity $I_0 \sim 80\ \text{TW}/\text{cm}^2$ [estimated from panel (a)(i) and simulations], radiating a single-cycle acoustic wave. Filament is terminated mid-flight by a helium cell, enabling linear imaging of the filament cross section [29,30]. Piezodropper places a $5\text{-}\mu\text{m}$ -radius droplet a controlled distance from the center of the filament core; droplet interaction is imaged from the side using a $\lambda_0 = 532\text{-nm}$ 7-ns transverse probe. (i) End-on image of filament core-intensity profile, using the He cell, with the y line out plotted. (ii) End-on image of the droplet in a low-power beam. (iii) Side image of an unperturbed $5\text{-}\mu\text{m}$ -radius droplet. All color maps are in arbitrary units. (b) Diagram of Experiment 2. Dielectric mirror ($M1$) is used to copropagate the pump and on-axis probe, and a second dielectric mirror ($M2$) filters out the pump to image the probe. Peak intensity for this $f/120$ focusing geometry is $I_0 \sim 160\ \text{TW}/\text{cm}^2$ at the highest pump energy. Inset, end-on image showing the density hole, radial acoustic wave, and water droplet. Color map is in arbitrary units.

and droplet shattering to clearing by a filament without lens assistance.

To generate single filaments in the lab, a 2.8-mJ pump pulse is down-collimated by a reflective telescope to a $w_0 = 1\ \text{mm}$ waist (e^{-2} intensity radius). The filament is terminated mid-flight about 40 cm after collapse and immediately after interaction with the droplet by an abrupt about 4-mm air-to-helium transition in the $0.5''$ diameter nozzle of a slowly outflowing helium cell [29,30] maintained at a slight positive pressure to the ambient air. Helium-cell termination of the filament enables end-on imaging of the filament-intensity profile and calibration of the droplet

position with respect to the center of the filament. The intensity profile is further attenuated by wedges in and after the helium cell to ensure linear propagation for imaging. Insets of Fig. 1(a) show images from the helium cell: an end-on image and line out of a filament core (with $d_{\text{core}} \sim 260 \mu\text{m}$, in good agreement with propagation simulations for these conditions [31]), and an image of an unfilamented lower-energy beam with a droplet $50 \mu\text{m}$ away from the beam axis. A side-imaging system with $4\times$ magnification [see Figs. 1(a) and 1(b)] uses the transverse $\lambda_0 = 532 \text{ nm}$ probe beam to image filament-droplet interaction dynamics.

Figure 2 shows a sequence of side shadowgrams at 0.1 and $500 \mu\text{s}$ after the filament of the droplet interaction as the droplet is translated closer to the filament core center from directly above. The $500\text{-}\mu\text{s}$ delay is chosen to match that for optimal transmission of a pulse following the filament in a prior fog-clearing experiment [23]. It is seen from the $0.1\text{-}\mu\text{s}$ -delay panels that at about $750 \mu\text{m}$ from the center the droplet is unaffected, but as the droplet is moved closer, it increasingly deforms and cavitates owing to mass ejection from its far side (away from the laser). In the corresponding $500\text{-}\mu\text{s}$ delay panels, the droplet is seen to reform its shape and move along the optical axis *toward* the laser, owing to a momentum boost from the mass ejection. At less than $200 \mu\text{m}$ ($150 \mu\text{m}$) from the core in the vertical (horizontal) direction, the droplet completely disintegrates; in the $500\text{-}\mu\text{s}$ panel, there is no evidence of probe scattering by droplet fragments. The vertical-horizontal asymmetry originates from the slight asymmetry of the filament cross section, as seen in Fig. 1(a)(i). At no droplet position is there any evidence of *radial* droplet

displacement away from the filament, which is what one would expect if the cylindrical acoustic wave contributed significantly to droplet clearing [24]. Since droplet shattering occurs at the edge of the filament core but well inside the reservoir radius ($w_0 \sim 1 \text{ mm}$), with cavitation and mass expulsion occurring on the far side of the droplet, we conclude that laser light from the filament reservoir is focused by the droplet, with strong heating on the far side. This scenario has been discussed in Ref. [32], where the geometric focus of a droplet with $ka = 2\pi a/\lambda \gg 1$ ($ka \sim 40$ for radius $a = 5 \mu\text{m}$ droplets) leads to a radius-independent intensity enhancement of about 7.6 times [32] at the far side, promoting cavitation and mass expulsion. Optical breakdown in water droplets has also been simulated in Ref. [33], which shows the same focusing effect with additional free electrons generated on the front face of the droplet at filament core intensities ($> 10 \text{ TW}/\text{cm}^2$).

To verify that the laser fluence in the filament reservoir is sufficient to initiate breakdown and plasma formation in a droplet, we simulate filamentary propagation with a unidirectional-pulse-propagation code [31,34] using our experimental parameters. We determine the radius at which the filament intensity drops below $1.3 \text{ TW}/\text{cm}^2$; this is our estimated damage threshold based on a water-ionization breakdown intensity of $10 \text{ TW}/\text{cm}^2$ [35] and the 7.6 times intensity enhancement from droplet focusing. We see in these simulations that the filament reservoir fluence falls below $1.3 \text{ TW}/\text{cm}^2$ at a radial position of $580 \mu\text{m}$ from the beam axis. This is significantly larger than the measured shattering radius, but water breakdown occurs in both shattered *and* deformed droplets. It is worth noting that we see significant deformation out to $400 \mu\text{m}$ and no

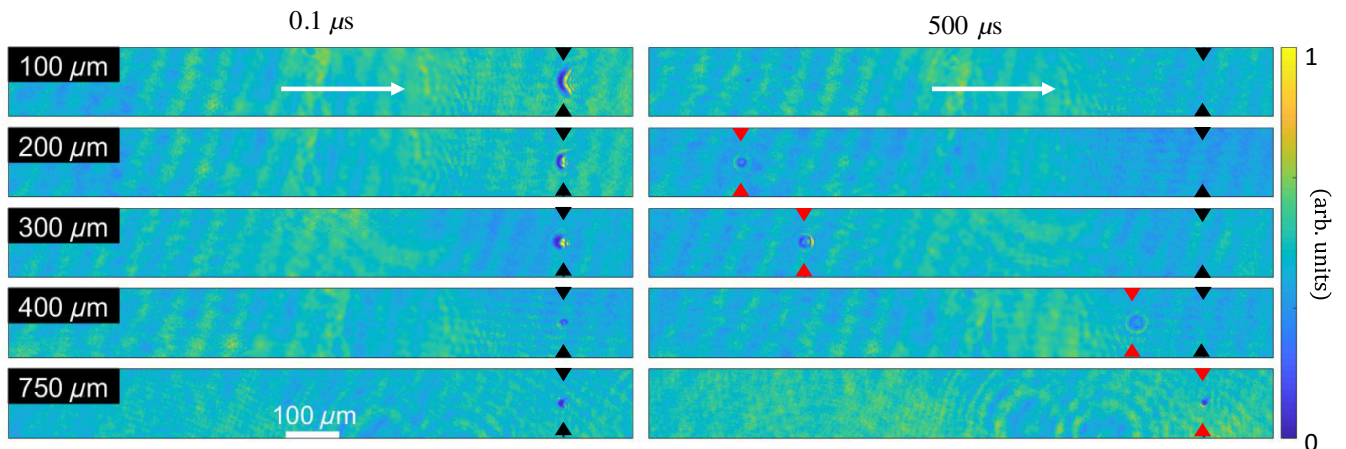


FIG. 2. Shadowgrams of filament-induced dynamics for droplets with a radius of about $5 \mu\text{m}$ placed at varying radial distances (labels at left) from the center of the filament core. Filament propagates from left to right (white arrows). Two columns show droplet images at 0.1 and $500 \mu\text{s}$ after filament arrival. Black arrows mark the initial droplet axial location, while red arrows mark the droplet location (if a droplet is still present) $500 \mu\text{s}$ after the filament interaction. As the droplet is moved closer to the beam axis, the images at $0.1 \mu\text{s}$ show droplet distortion and far-side cavitation, while the $500\text{-}\mu\text{s}$ images show axial droplet displacement toward the laser and the complete disintegration of droplets placed closer than about $200 \mu\text{m}$ from the core center.

deformation at $750 \mu\text{m}$ in Fig. 2, so our results match well with this breakdown estimate.

The goal of Experiment 2 is to observe droplet-clearing effects using a laser-intensity profile resembling the most intense part of the filament core ($\sim 100 \mu\text{m}$, or approximately half the core diameter) where laser energy is deposited from plasma generation. The setup, shown in Fig. 1(b), uses an $f/120$ lens-focused pulse so that the beam waist diameter ($2w_0 \sim 100 \mu\text{m}$) matches this. With little to no laser flux radially outside about w_0 , any droplet clearing from that region would not be directly optically driven; a strong candidate would be clearing by the laser-induced acoustic wave. In the experiment, the pulse energy, $\varepsilon_{\text{pump}}$, is adjusted in the range of $100 - 500 \mu\text{J}$ to match and exceed the energy deposition per unit length, $\partial_z \varepsilon_{\text{dep}}$, of a real filament core, and thus, launch an acoustic wave of at least equal amplitude. The energy deposition is measured interferometrically using a portion of the $\lambda = 532\text{-nm}$ pulse transmitted through the $\lambda = 800\text{-nm}$ mirror, $M1$, and directed along the pump-beam axis. This on-axis probe picks up a phase shift, $\Delta\Phi(\mathbf{r}_\perp)$, from the long-lasting air-density depression left by pump heating, as described in Ref. [7]. The energy deposition per unit length is given by [7] $\partial_z \varepsilon_{\text{dep}} = -c_v T_0 \rho_0 k^{-1} L^{-1} (n-1)^{-1} \int d^2 \mathbf{r}_\perp \Delta\Phi(\mathbf{r}_\perp)$, where the integral is over the cross section of the density hole, the simulated [31] axial FWHM of air heating is $L \sim 2 \text{ cm}$ (less than the confocal parameter of $2z_0 \sim 2.8 \text{ cm}$ owing to the strongly nonlinear heating), $c_v = 0.72 \text{ kJ}/(\text{kg K})$ is the isochoric specific heat of air [36], $T_0 = 297 \text{ K}$ is the ambient air temperature, $\rho_0 = 1.23 \text{ kg}/\text{m}^3$ is the air mass density [37], $k^{-1} = 84.7 \text{ nm}$ is the inverse wave number

of the probe, and $(n-1) = 2.8 \times 10^{-4}$ is the air index of the refraction increment [38].

Energy deposition, $\partial_z \varepsilon_{\text{dep}}$, versus $\varepsilon_{\text{pump}}$ is plotted in Fig. 3(a). For $\varepsilon_{\text{pump}} = 450 \mu\text{J}$, $\partial_z \varepsilon_{\text{dep}}$ exceeds, by about 40%, our prior measurements of a maximum deposition of $3.5 \mu\text{J}/\text{cm}$ in a real filament [7]. Therefore, near the focus in Experiment 2, the launched acoustic wave for $\varepsilon_{\text{pump}} = 450 \mu\text{J}$ is stronger than an acoustic wave from a real filament; we use this experiment to determine an upper bound on acoustically induced droplet displacement.

The droplet's initial and final positions, R_{init} and R_{final} , are imaged using the transverse $\lambda_0 = 532\text{-nm}$ $\tau \sim 7\text{-ns}$ probe pulse. To enable sensitive detection of potentially small laser-induced position changes, every other pump pulse is blocked for collection of a pump-off droplet image. These are then binned based on the droplet's blocked-pump position (R_{init}) with respect to the pump axis. The mean droplet displacement ($\overline{\Delta R_{\text{drop}}} = \overline{R_{\text{final}}} - \overline{R_{\text{init}}}$) after $500\text{-}\mu\text{s}$ delay is plotted in Fig. 3(b) as a function of $\varepsilon_{\text{pump}}$ for R_{init} in the range $100 - 110 \mu\text{m}$, which encompasses the slight shot-to-shot variations in initial droplet location. The overbars represent a mean over about 100 shots at each point. For $\varepsilon_{\text{pump}} = 450 \mu\text{J}$, the droplet is shattered by the beam focus for $R_{\text{init}} < 100 \mu\text{m}$. Figure 3(c) plots $\overline{\Delta R_{\text{drop}}}$ versus $\overline{R_{\text{init}}}$ at $500\text{-}\mu\text{s}$ delay for $\varepsilon_{\text{pump}} = 450 \mu\text{J}$. In both Figs. 3(b) and 3(c), the error bars represent the displacement variance, $\pm \Delta R_{\text{var}}$, over about 100 shots at each point. The red bands in these panels are results from a hydrocode simulation of acoustically driven droplet displacement (as discussed in Sec. III).

Both Figs. 3(b) and 3(c) show a very weak trend of increasing droplet displacement for increasing $\varepsilon_{\text{pump}}$ and

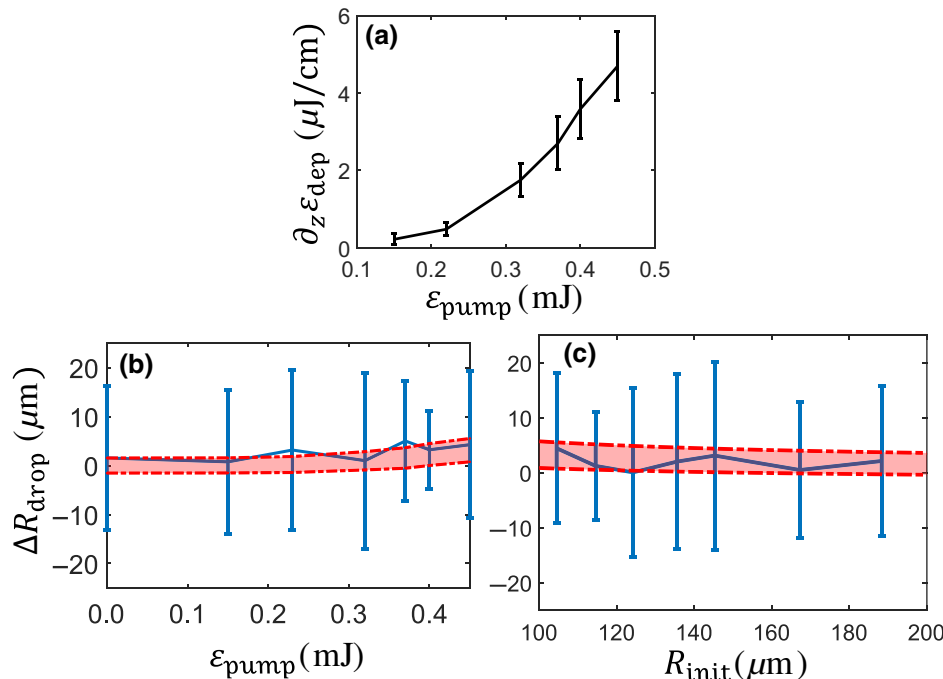


FIG. 3. (a) Energy deposition per unit length, $\partial_z \varepsilon_{\text{dep}}$, versus pump energy, $\varepsilon_{\text{pump}}$. (b) Droplet displacement, ΔR_{drop} , as a function of pump energy for initial position $R_{\text{init}} = 100 - 110 \mu\text{m}$. Blue trace is the mean displacement, $\overline{\Delta R_{\text{drop}}}$, and error bars represent variance over 100 shots at each point. Red region is ΔR_{drop} from simulations (see Sec. III). (c) ΔR_{drop} versus R_{init} for $\varepsilon_{\text{pump}} = 450 \mu\text{J}$. Each value of R_{init} plotted corresponds to the average at that point, with standard deviation $< 4.5 \mu\text{m}$.

decreasing R_{init} . In both cases, however, the maximum ΔR_{drop} of about $5 \mu\text{m}$ is small compared to both ΔR_{var} and the variation of initial droplet positions. Even if we consider a maximum acoustic clearing displacement of $\Delta R_{\text{var}} \sim 20 \mu\text{m}$, this is still insufficient for acoustic droplet clearing by a real filament: for $R_{\text{init}} = 100 \mu\text{m}$, the displaced droplet would still be well within the filament's optical shattering radius ($150 - 200 \mu\text{m}$), as discussed earlier for Experiment 1. We therefore conclude that, in a real filament, the intense core alone will not generate an acoustic wave of sufficient strength to clear a water droplet with a radius of about $5 \mu\text{m}$, typical of fog.

III. SIMULATIONS AND ADDITIONAL EXPERIMENTS

Our experimental results for acoustic droplet clearing are compared with a one-dimensional + time cylindrically symmetric hydrocode. Because energy deposition by a filament is impulsive [18,21], we assume that the initial excitation of the air is a heated region with a radial temperature profile, $\Delta T(r, t=0) = \Delta T_{\text{peak}} \exp(-2(r/r_h)^2)$, where $r_h = 60 \mu\text{m}$ (unless otherwise stated) and $\Delta T_{\text{peak}} = 2(\pi r_h^2 \rho_0 c_v)^{-1} \partial_z \varepsilon_{\text{dep}}$ is given by the measured energy deposition of Fig. 3, and plotted versus $\partial_z \varepsilon_{\text{dep}}$ in Fig. 4(a).

The simulation then computes the gas evolution and the resulting drag and pressure-gradient forces on the droplet.

The hydrocode solves (using Ref. [39]) the fluid conservation equations:

$$\frac{\partial \xi_i}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} r(\xi_i v + \phi_i) = 0, \quad (1)$$

where ξ_i are the conserved densities and ϕ_i are their forced fluxes. Here, $\xi_1 = \rho(r, t)$ is the air mass density, $\xi_2 = \rho v(r, t)$ is the momentum density, and $\xi_3 = \epsilon + \rho v^2/2$ is the energy density, where the air is taken as an ideal gas of internal energy density $\epsilon(r, t) = 3(\rho/m)k_B T(r, t)/2$ and pressure $P(r, t) = 2\epsilon/3$, with an average molecular mass $m = 0.8m_{N_2} + 0.2m_{O_2}$. The corresponding source fluxes are $\phi_1 = 0$, $\phi_2 = P + \tau$, and $\phi_3 = (P + \tau)v + q$, where $\tau = (4/3)\eta(T)\partial v/\partial r$ is the shear stress and $q = -\kappa(T)\partial T/\partial r$ is the thermal flux. Here, η is the dynamic viscosity and κ is the thermal conductivity of air [40].

The output of the fluid simulation is then used to compute the acoustically driven motion of a spherical water droplet of radius a , mass M , and radial R , where the force, F_{drop} , on the droplet is taken as the sum of the local

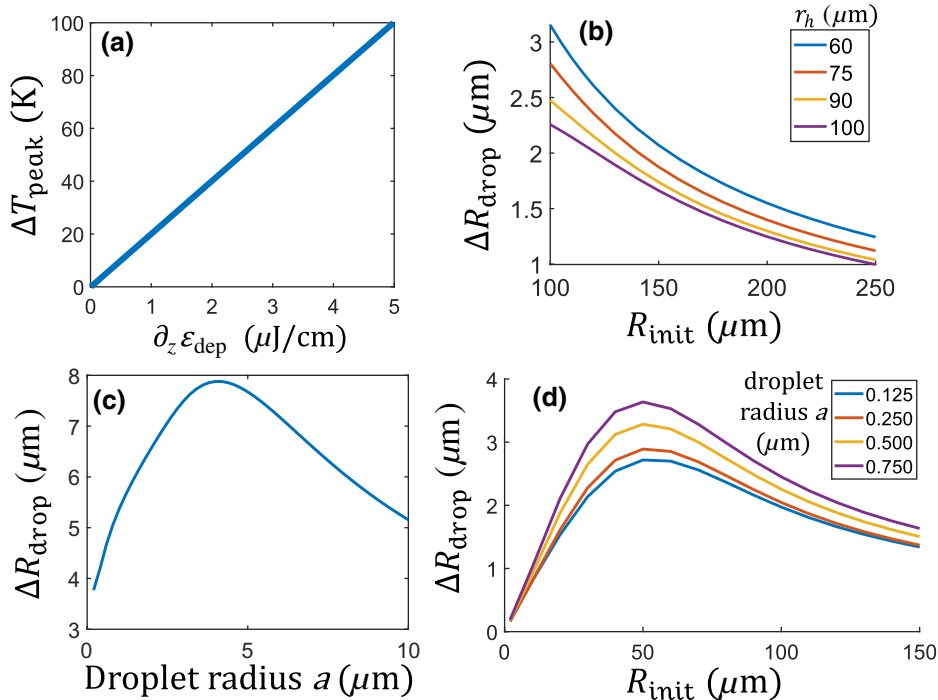


FIG. 4. (a) Peak temperature rise versus laser energy deposited per unit length, $\partial_z \varepsilon_{\text{dep}}$. (b) Droplet displacement, ΔR_{drop} , at 500- μs delay for droplet radius $a = 5 \mu\text{m}$; $\partial_z \varepsilon_{\text{dep}} = 4.8 \mu\text{J}/\text{cm}$ for various r_h (heated-region radius) labeled in the legend. (c) ΔR_{drop} at 500- μs delay versus droplet radius a for $\partial_z \varepsilon_{\text{dep}} = 4.8 \mu\text{J}/\text{cm}$, initial droplet position $R_{\text{init}} = 50 \mu\text{m}$, and $r_h = 60 \mu\text{m}$. (d) ΔR_{drop} at 500- μs delay versus R_{init} for $r_h = 60 \mu\text{m}$ and droplet radii $a = 0.125, 0.25, 0.5, \text{ and } 0.75 \mu\text{m}$ and $\partial_z \varepsilon_{\text{dep}} = 4.8 \mu\text{J}/\text{cm}$. ΔR_{drop} decreases for $R_{\text{init}} < \sim 50 \mu\text{m}$ because the acoustic wave reaches its maximum amplitude just inside the heated region.

pressure gradient and drag force from the acoustic wave:

$$M \frac{d^2 R}{dt^2} = F_{\text{drop}},$$

$$F_{\text{drop}}(t) = \pi a^2 \left(\frac{\partial P}{\partial r} + 0.5 C_d \rho \left[\frac{dR}{dt} - v \right]^2 \text{sgn} \left(v - \frac{dR}{dt} \right) \right). \quad (2)$$

Here, $p = p(R(t), t)$, $v = v(R(t), t)$, $\rho = \rho(R(t), t)$ are the fluid pressure, velocity, and density evaluated at the droplet position $R(t)$, respectively. The drag coefficient, C_d , is a strong function of the Reynolds number ($\text{Re} = 2a\rho v\eta^{-1}$) of the flow around small droplets. We consider two drag regimes: $\text{Re} \leq 0.2$, for which $C_d = 24/\text{Re}$ follows Stokes law [40], and $\text{Re} > 0.2$, for which $C_d = 21.12/\text{Re} + 6.3/\sqrt{\text{Re}} + 0.25$ is a fit between the static $C_d = 0.47$ for $\text{Re} > 1000$ and Stokes law [40]. We note that $\text{Re} > 1000$ is unreachable with the droplet sizes and air and droplet velocities in this paper.

The simulation results are shown in the red bands overlaid on the experimental results in Figs. 3(b) and 3(c), showing excellent overlap, and verifying that filament-induced acoustic clearing of water droplets with a radius of about $5 \mu\text{m}$ is negligible. The bands plot the simulated droplet displacement incorporating experimental shot-to-shot variations in energy deposition and initial droplet position, R_{init} , and the uncertainty in droplet size. The

energy-deposition fluctuations are accounted for by initiating the hydrocode simulations by varying ΔT_{peak} for each $\varepsilon_{\text{pump}}$ in Fig. 3(a). The variation in droplet displacement owing to measurement uncertainty in droplet radius a is accounted for by simulating the smallest and largest a within a standard deviation of the mean. Additionally, the mean displacement, $\overline{\Delta R}_{\text{drop}}$, at $\varepsilon_{\text{pump}} = 0$ is added to the upper bound and subtracted from the lower bound of the simulated range, since any acoustic displacement would add onto that detected (but not acoustic-induced) movement.

To assess whether the radius of the filament-heated region can affect droplet movement, we perform additional simulations varying r_h , the $1/e^2$ radius of the initial temperature profile. A wider heated region may apply, for example, when laser energy is deposited through rotational excitations [18,21] outside of the highest-intensity region of the filament core where optical field ionization primarily occurs. Simulation results plotted in Fig. 4(b) for an $a = 5 \mu\text{m}$ droplet show that a fixed energy deposition, $\partial_z \varepsilon_{\text{dep}}$, over a larger radius r_h has a reduced effect on droplet displacement, as one might expect from the reduced radial pressure gradient and lower peak fluid velocity. In all cases, the droplet displacement is negligible.

One possibility of interest is whether the acoustic wave can displace much smaller droplets, such as the fragments generated by optical shattering. Figure 4(c) plots droplet displacement as a function of droplet radius for $\partial_z \varepsilon_{\text{dep}} = 4.8 \mu\text{J}/\text{cm}$ [$\Delta T_{\text{peak}} \sim 100 \text{ K}$ from Fig. 4(a)] and

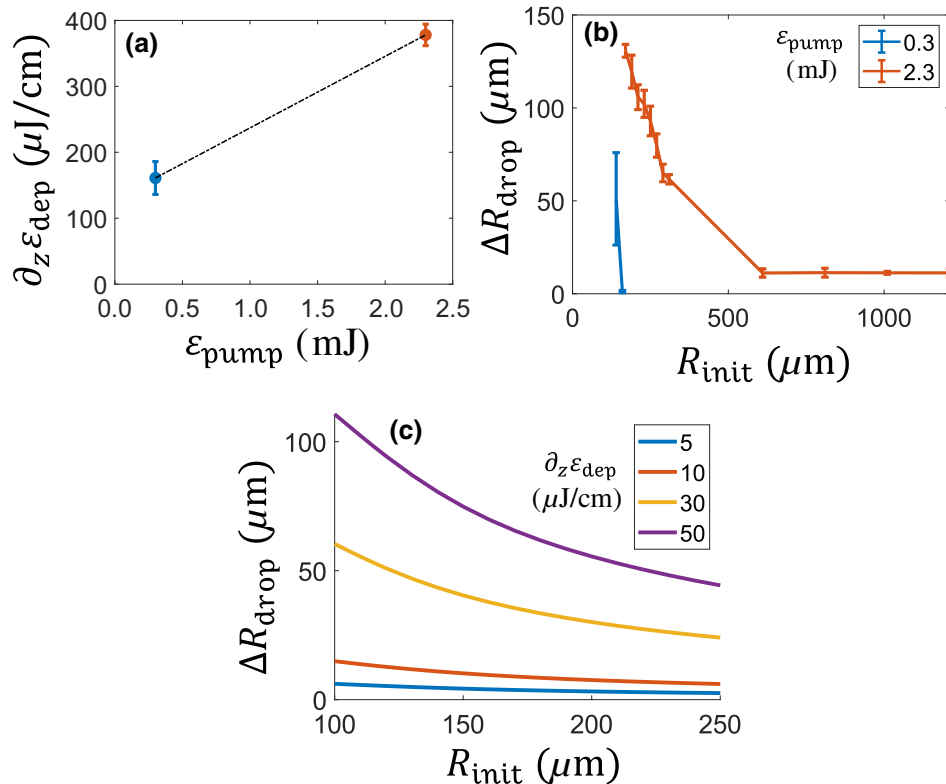


FIG. 5. (a) Peak energy deposition per unit length for each pump-pulse energy. For $\varepsilon_{\text{pump}} = 0.3$ mJ, $L \sim 1$ mm, and for $\varepsilon_{\text{pump}} = 2.3$ mJ, $L \sim 5$ mm [31]. (b) Droplet displacement for each pump energy after 105- μs delay. (c) Droplet displacement after 500 μs simulated by the hydrocode for $r_h = 60 \mu\text{m}$ and droplet diameter $a \sim 10 \mu\text{m}$, for energy depositions labeled in the legend.

$R_{\text{init}} = 50 \mu\text{m}$ (a position where a droplet would normally be optically shattered), where it is seen that the greatest displacement is for droplets with radii in the range of about $5 \mu\text{m}$ of our experiment. While smaller droplets accelerate more due to their smaller masses and larger drag coefficients, overriding the decrease in drag from their lower cross sections, they also experience a stronger drag deceleration from the background air. This leads to the overall decrease of ΔR_{drop} as the droplet radius decreases below about $5 \mu\text{m}$. For droplet radii beyond about $5 \mu\text{m}$, ΔR_{drop} decreases because of larger droplet inertia and reduced drag coefficient.

If the initial water droplet is shattered into fragments in a range of radii at different radial positions, Fig. 4(d) shows their possible displacements, neglecting the initial fragment velocity upon shattering (which is in all directions [41]). Here, the heated-region radius is $r_h = 60 \mu\text{m}$. The smallest fragment simulated (radius $a = 0.125 \mu\text{m}$) is similar to the upper-bound radius ($0.135 \mu\text{m}$) of laser-shattered water-droplet fragments estimated in Ref. [41]. For fragments of that size, ΔR_{drop} is negligible and remains small for all fragments in Fig. 4(d), ranging to the larger droplets of Fig. 4(c). Therefore, we conclude that acoustic clearing is insignificant, even for droplet fragments generated by optical shattering.

Although there is negligible acoustic clearing of water droplets from a collimated filament, there are nonfilamentary conditions where acoustic clearing can be significant. We study this by using a setup identical to that of Experiment 2 [Fig. 1(b)], except with $f/10$ focusing instead of $f/120$ and with larger water droplets of radius $a \sim 12.5 \mu\text{m}$. This setup produces a smaller heated region (for $\varepsilon_{\text{pump}} = 2.3 \text{ mJ}$, simulation [31] gives $r_h \sim 45 \mu\text{m}$ and $L \sim 5 \text{ mm}$) with significantly higher energy deposition and higher ΔT_{peak} . In Fig. 5(a), the measured $\partial_z \varepsilon_{\text{dep}}$ is plotted for two values of $\varepsilon_{\text{pump}}$, with an absorption of about $380 \mu\text{J}/\text{cm}$ ($\Delta T_{\text{peak}} \sim 5000 \text{ K}$) at $\varepsilon_{\text{pump}} = 2.3 \text{ mJ}$, roughly about 100 times higher than $\partial_z \varepsilon_{\text{dep}}$ in a filament. In Fig 5(b), the measured ΔR_{drop} at 105- μs delay is plotted versus R_{init} . The displacement driven by a 2.3-mJ pulse is significant, with the droplet moving radially from about 170 to 300 μm . For results more directly comparable to a filament, Fig. 5(c) plots results from the hydrocode using a $a = 5 \mu\text{m}$ radius droplet and $r_h = 60 \mu\text{m}$, as in Fig. 3, but higher $\partial_z \varepsilon_{\text{dep}}$. The results show that a heated region with the same spatial profile as a filament but with 10 times higher energy deposition can radially displace droplets significantly. For example, when $R_{\text{init}} = 150 \mu\text{m}$ and $\partial_z \varepsilon_{\text{dep}} = 50 \mu\text{J}/\text{cm}$, the droplet displacement is $\Delta R_{\text{drop}} = 75 \mu\text{m}$. However, in the deposition range for a filament ($\partial_z \varepsilon_{\text{dep}} < 5 \mu\text{J}/\text{cm}$), droplet displacement is only $\Delta R_{\text{drop}} \sim 4 \mu\text{m}$. This result shows that acoustic clearing is constrained mainly by the limited laser-energy deposition in a near-IR femtosecond filament generated by collapse of a collimated beam.

We note that there may be self-guided propagation regimes in which acoustic clearing is more effective. For example, our recent simulations of self-guided propagation of 1 TW, about $10 \mu\text{m}$, 3.5-ps pulses in air [33], show that peak values of $\partial_z \varepsilon_{\text{dep}}$ greater than about $100 \mu\text{J}/\text{cm}$ are achievable from avalanche ionization and heating of ambient submicron aerosols by the self-guided pulse. This scenario may apply to recent experiments demonstrating self-guiding of long-wavelength infrared pulses over tens of meters [42].

IV. CONCLUSIONS

The self-guiding of short powerful pulses in the atmosphere is proposed as a method for clearing atmospheric aerosols in fog for pulses that propagate after them, for applications including optical communications and directed energy. Our experiments and simulations show that, for single filaments generated by collimated near-infrared femtosecond pulses, clearing of water droplets with a radius of about $5 \mu\text{m}$, typical of fog, is caused mainly by optical shattering for droplets closer than about $200 \mu\text{m}$ from the filament axis. Under these conditions, the filament reforms and continues to propagate and shatter droplets, clearing a path for a follow-on laser pulse or beam. ‘‘Clearing’’ in this case means reduced scattering losses of the follow-on beam owing to the much smaller radii of the shattered droplet fragments, a transition from Mie scattering to Rayleigh scattering. Droplets outside the shattering radius ($>200 \mu\text{m}$) undergo varying levels of distortion and cavitation as laser light is internally focused in the droplet, with heating and mass ejection on the far side, driving the surviving portion of the droplet back toward the laser, but not cleared from the optical path. Detailed scattering losses from optically shattered droplets need to be explored experimentally to reach a definitive conclusion on this method’s clearing efficacy. We do not consider energy losses from droplet shattering, which, by some estimates [43], make fog clearing with a single near-IR filament over long distances impractical.

We find that acoustic forces are largely ineffective as a droplet-clearing mechanism by near-infrared femtosecond filaments, mainly because the filament-energy deposition of $< 5 \mu\text{J}/\text{cm}$ cannot drive an acoustic wave of sufficient amplitude to move a $5 - \mu\text{m}$ droplet more than about $10 \mu\text{m}$ at best. Filament-induced acoustic waves are of little help to clear even the small droplet fragments generated by optical shattering—these experience offsetting drag forces by the ambient air.

Other fog-clearing systems may be worth exploring. Long-wavelength infrared (LWIR) filaments with few-picosecond pulses [34,42] have large cross-section areas and high energies and heat the air via avalanche ionization and collisional heating. This can lead to larger droplet-shattering regions and greater energy deposition

for acoustic clearing. LWIR pulses may also induce plasma-free droplet shattering [44], potentially decreasing laser-energy losses. Finally, the resonant excitation of molecular rotations using pulse trains [19,25] can deposit energy per unit length exceeding that from plasma generation in a typical near-IR filament, increasing the acoustic wave amplitude and potentially enhancing clearing.

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Correction: The verb tense in the second sentence of the abstract has been restored to match that present in the original manuscript.