Carrier-Suppressed Multiple-Single-Sideband Laser Source for Atom Cooling and Interferometry

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We present an electro-optic modulation technique that enables a single laser diode to realize a coldatom source and a quantum inertial sensor based on matter-wave interferometry. Using carrier-suppressed dual-single-sideband modulation, an in-phase and quadrature modulator generates two optical sidebands from separate radio-frequency (rf) signals. These sidebands are controlled independently in frequency, phase, and power using standard rf components. Our laser source exhibits improved rejection of parasitic sidebands compared to those based on phase modulators, which generate large systematic shifts in atom interferometers. We measure the influence of residual laser lines on an atom-interferometric gravimeter and show agreement with a theoretical model. We estimate a reduction of the systematic shift by 2 orders of magnitude compared to previous architectures and reach a long-term sensitivity of 15 ng on the gravitational acceleration with an interrogation time of only T = 20 ms. Finally, we characterize the performance of our integrated laser system and show that it is suitable for mobile sensing applications, including gravity surveys and inertial navigation.

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I. INTRODUCTION

The advent of laser cooling and atom interferometry [1,2] has hailed new classes of inertial sensors with unprecedented sensitivity, including gravimeters [3-5], gravity gradiometers [6,7], and gyroscopes [8,9]. However, these instruments are typically large complex laboratory experiments that require quiet stable conditions to operate reliably. Working in the field or on board vehicles demands a drastic reduction in the size, weight, and power consumption of these devices [10-13], while also requiring a high level of robustness and resistance to environmental disturbances [14]. Over the past few years, significant progress has been made in the commercialization of cold-atom-based sensors [15] and it is widely believed these high-performance inertial sensors will lead to a breakthrough in technology for many fields, including geophysics [16], metrology [17], and inertial navigation [18]. Laser sources represent one of the most crucial and complex parts of these systems. They require at least two frequencies (e.g., for laser-cooling alkali metals or inducing Raman

transitions), with an accuracy of approximately 100 kHz. A typical atom-interferometer sequence also demands tunability over a range of approximately 1 GHz near the atomic transition and submillisecond response times. Moreover, for a Raman interferometer, the two optical frequencies must be phase coherent, with a low relative phase noise [19].

Telecom-frequency-based architectures afford the strength of extensive development with reliable and robust off-the-shelf components and can be frequency doubled using a periodically poled lithium niobate (PPLN) crystal [20]. Within the scope of all-fibered laser systems designed for laser cooling and atom interferometry, several configurations have been demonstrated. The use of two separate laser diodes, one operating at each frequency, requires an optical phase lock [21,22]. Frequency-offset master-slave architectures offer real-time frequency agility by controlling the current of the slave diode [23] but are typically limited in bandwidth and dynamic range by the electronics. Electro-optically generated sidebands in a servo-locked system can also achieve good frequency agility [24-27]. To simplify such architectures, electro-optic phase modulation has been used to generate comblike spectra controlled by an rf source [28]. However, the use of pure

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phase modulation results in parasitic sidebands that are detrimental to atom interferometers (AIs), as they produce both a systematic measurement bias and spatial variations in fringe contrast [7,29]. Single-sideband (SSB) modulation using an in-phase and quadrature (IQ) modulator has been shown to strongly reduce the effect of parasitic lines [30]. There, however, the tunability of the laser source was realized by controlling the carrier frequency of the laser diode.

In this work, we demonstrate a 780-nm laser architecture based on carrier-suppressed dual-single-sideband (CS-DSSB) modulation in an all-fibered IQ modulator operating at 1560 nm. Here, electro-optic modulation techniques are utilized to generate two "principal" optical sidebands, while suppressing the carrier frequency and other parasitic lines. These principal sidebands are controlled in frequency, phase, and power in the rf domain-affording all the benefits of modern rf sources in terms of agility, stability, and response time. With this system, we realize a complete interferometer sequence (including atom-trap loading, sub-Doppler cooling, state preparation, interrogation, and detection) using only rf modulation, while holding the carrier frequency of the laser fixed. Using this system, we realize a quantum gravimeter with a long-term stability < 20 ng (< 1 mrad) using a modest interrogation time of T = 20 ms. Finally, we present a general model for the systematic bias of atomic gravimeters in the presence of residual laser lines. Our model is consistent with experimental measurements and highlights the fact that laser architectures with reduced parasitic laser lines (such as those based on IQ modulators [30]) can have non-negligible effects on the phase and contrast of atom interferometers.

II. LASER ARCHITECTURE

The architecture of the laser system is presented in Fig. 1(a). A reference laser diode is locked to the $|F = 2\rangle \rightarrow |F' = (2,3)\rangle$ crossover transition of ⁸⁷Rb using saturated absorption spectroscopy. The main laser (Redfern Integrated Optics external-cavity diode laser at 1560 nm, 20 mW output power) is frequency locked to the red of the reference laser via an optical beat note at $\Delta \omega \simeq 2\pi \times 1.5$ GHz. For the laser-cooling phase, two principal sidebands are generated on the main laser at frequencies $\Omega_1 = \Delta \omega + (\delta_{CO} + \Delta_C)/2$ for cooling and $\Omega_2 = \Omega_1 + (\delta_{HF} - \delta_{32})$ for repumping, both of which are blue shifted from the reference laser. Here, $\delta_{32}/2\pi \simeq$ 266 MHz is the splitting between excited states $|F' = 2\rangle$ and $|F' = 3\rangle$, $\delta_{CO} = \delta_{32}/2$ is the detuning of the crossover resonance from $|F' = 3\rangle$, $\delta_{\rm HF}/2\pi = 6.834$ GHz is the ground-state hyperfine splitting, and $\Delta_C/2\pi \simeq -20$ MHz is the detuning from $|F' = 3\rangle$ used for laser cooling. Similarly, for Raman interferometry, $\Omega_1 = \Delta \omega + (\Delta_R - \Delta_R)$



FIG. 1. (a) The architecture of the laser source: PI, proportional-integrator lock. (b) A schematic of the electro-optic IQ modulator where, for clarity, only one frequency Ω is injected into the hybrid coupler: EDFA, erbium-doped fiber amplifier; AOM, acousto-optic modulator; PPLN, periodically poled lithium niobate waveguide. $\delta_{\rm CO})/2$ and $\Omega_2 = \Omega_1 + \delta_{\rm HF}$, where Δ_R is the detuning of the Raman beams from $|F = 2\rangle \rightarrow |F' = 2\rangle$. When in CS-DSSB mode, the optical loss in the IQ modulator (approximately 12 dB in our case) depends on the total injected rf power. The remaining 500 μ W of optical power is sufficient to saturate the double-stage erbium-doped fiber amplifier (EDFA, Lumibird CEFA-C-PB-HP) after the modulator. The EDFA then outputs 2 W at 1560 nm with an approximately 1% power stability. This light subsequently undergoes second-harmonic generation (SHG) to 780 nm in a PPLN-crystal waveguide (NTT Electronics WH-0780-000-F-B-C). A fibered acousto-optic modulator (AOM, Gooch & Housego A35080-S-1/50-p4k7u), located between the EDFA and the PPLN waveguide, controls the total output power, which is 485 mW at maximum. The optical power stability is approximately 0.5% over 10^4 s [see Fig. 2(b)].



FIG. 2. (a) The Allan deviation of the optical beat note between the reference laser (blue curve) and the IQ laser source (orange curve) and a third "master" laser at 1560 nm. (b) The Allan deviation of the relative optical power emitted by the laser source. (c) The Allan deviation of the intensity ratio between principal lines $\Omega_{1,1}^{PPLN}$ and $\Omega_{2,0}^{PPLN}$ in both static (red curve) and dynamic (green curve) modes. The amplitude of each line is measured on a spectrum analyzer by beating the laser output with a local oscillator. In the static mode, the rf signals remain at fixed frequency and power, while the dynamic mode corresponds to a typical AI sequence with rf signals modulated in amplitude and frequency. The shaded areas in all plots indicates 1σ uncertainty.

The telecom-domain IQ modulator (iXblue MXIQER-LN-30) consists of three optically guided Mach-Zehnder interferometers (MZIs): two sub-MZIs nested inside a main one, as shown in Fig. 1(b). Each MZI has a broad modulation bandwidth of 30 GHz. An rf signal containing the two frequencies Ω_1 and Ω_2 is sent through a hybrid coupler, which equally splits the signal and phase shifts one arm by $\pi/2$. The resulting two rf signals are sent to the ac electrodes of each sub-MZI. A commercial biasvoltage controller (iXblue IQ-MBC-LAB) delivers three continuous voltages to the dc electrodes [shown in yellow in Fig. 1(b)] to control and stabilize in real time the bias phases of each MZI ($\Delta \Phi_1$, $\Delta \Phi_2$, and $\Delta \Phi_3$). This dc bias lock is realized by modulating the light passing through each sub-MZI at 1 kHz and deriving an error signal from the FFT of the corresponding optical signals. This control is critical, since these phases can drift dramatically due to temperature sensitivity and internal charge dynamics.

The primary function of each sub-MZI is to suppress the optical carrier frequency. We emphasize that the global phase shifts $\Delta \Phi_1$ and $\Delta \Phi_2 = \pm \pi$ guarantee destructive interference of the carrier, while the input rf phase φ determines the relative phase between the two remaining sidebands. A schematic of the IQ modulator, operating in carrier-suppressed single-sideband (CS-SSB) mode [31,32], is shown in Fig. 1(b). Here, for clarity, only one frequency Ω is injected into the hybrid coupler, which then modulates the two sub-MZIs with $\cos(\Omega t)$ and $\sin(\Omega t)$, respectively. This results in carrier-suppressed optical signals that are in quadrature with one another. These two signals are then combined in the main MZI, where the bias phase $\Delta \Phi_3$ determines the surviving harmonics. Specifically, the upper sideband (order +1) remains when $\Delta \Phi_3 =$ $-\pi/2$, whereas the lower sideband (order -1) survives for $+\pi/2$. CS-DSSB modulation is completely analogous to CS-SSB modulation, except that two separate rf signals are injected into the IQ modulator-generating two independent sidebands. The relative phase between these optical signals is directly controlled by the rf source.

Both rf signals Ω_1 and Ω_2 are controlled at the subhertz level with a custom-built rf source. A voltagecontrolled oscillator (VCO, Minicircuits ZX95-1750W-S+) is used to generate Ω_1 . A low-noise phase-locked dielectric resonator oscillator (PLDRO, Polaris SPLDRO-RE100-6800-P13-CP) generates 6.8 GHz and is mixed with the VCO to produce Ω_2 . Similar to the architecture described in Ref. [33], the frequency difference $\Omega_2 - \Omega_1$ (and its associated phase) is controlled by a direct digital synthesizer (Analog Devices AD9959) mixed with the PLDRO. This scheme guarantees common-mode suppression of the phase noise of the VCO. The power ratio between Ω_1 and Ω_2 is controlled using a variable-voltage rf attenuator—enabling us to suppress constant light shifts during the interferometer [4] and to optimize the optical



FIG. 3. (a) The laser source integrated in a standard 19 in. 9U rack. (b) The three-dimensional design of the laser system, including cooling fans and active temperature controllers for individual components.

molasses, state preparation, and detection phases of the atom-interferometer sequence.

The laser system is integrated into a 19-in. 9U rack, including a CPU and a graphical user interface, as shown in Fig. 3. A rubidium vapor cell is surrounded by heat tape to maintain a homogeneous temperature ($\simeq 30 \,^{\circ}$ C). The temperature of the laser diodes and PPLN waveguides is actively controlled in independent containers for use in thermally variable environments.

III. CHARACTERIZATION OF THE LASER SYSTEM

Figure 4(a) shows an example of the spectrum obtained after CS-DSSB modulation at 1560 nm using a beat note with the reference laser [34]. Here, we demonstrate suppression of the carrier ω_0 by approximately 23 dB and of all other parasitic lines below 25 dB. The two principal sidebands, labeled $\Omega_{1,0}^{IQ} = \omega_0 + \Omega_1$ and $\Omega_{0,1}^{IQ} = \omega_0 + \Omega_2$, are offset from the carrier by $\Omega_1/2\pi = 1$ GHz and are separated by $\Omega_2 - \Omega_1 = \delta_{HF}$. Similarly, the optical spectrum at 780 nm (i.e., after the PPLN) is shown in Fig. 4(b). Here, the principal laser lines used for cooling and interferometry are labeled $\Omega_{2,0}^{PPLN} = 2\omega_0 + 2\Omega_1$ and $\Omega_{1,1}^{PPLN} = 2\omega_0 + \Omega_1 + \Omega_2$. These two frequencies are generated by doubling $\Omega_{1,0}^{IQ}$ and by summing $\Omega_{1,0}^{IQ} + \Omega_{0,1}^{IQ}$, respectively.

We develop both an analytical model for the electric field (see Appendix A) and a numerical model for the spectra, which is overlaid with the measurements shown in Fig. 4. This numerical model accurately reproduces several effects, such as the level of carrier suppression, which is determined by the accuracy of bias phases $\Delta \Phi_1$ and $\Delta \Phi_2$. The suppression of all other sidebands is influenced by a combination of the bias phase $\Delta \Phi_3$ and the phase and amplitude imbalance caused by the hybrid coupler. These imbalances are measured and input into the model. The IQ modulator can also exhibit several manufacturing defects, such as asymmetries between the arms of the MZIs and irregularities in the electrodes, which can produce additional lines. The PPLN then mixes all the lines through the process of SHG. Finally, we observe several lines in the spectra that are not predicted by the numerical model. These are due to spurious frequencies generated by the rf source that arise due to harmonic distortion and mixing residues that are not completely suppressed by the rf filters within the source.



FIG. 4. The beat note spectrum after CS-DSSB modulation at (a) 1560 nm and (b) 780 nm. The blue lines show the spectra measured during Raman interferometry, obtained by beating with a stable local oscillator at 1560 nm and 780 nm, respectively. The red lines correspond to estimates from a numerical model, which are denoted $\Omega_{n,m}^{IQ} = \omega_0 + n\Omega_1 + m\Omega_2$, where *n* and *m* are integers. Here, the principal sidebands are labeled $\Omega_{1,0}^{IQ}$ and $\Omega_{0,1}^{IQ}$. Similarly, at 780 nm, the lines are labeled $\Omega_{2,0}^{PPLN} = 2\omega_0 + N\Omega_1 + M\Omega_2$, where the principal sidebands are $\Omega_{2,0}^{PPLN}$ and $\Omega_{1,1}^{PPLN}$. The input rf power is 17 dBm and 9 dBm for Ω_1 and Ω_2 , respectively, corresponding to modulation depths of 0.55 and 0.23.

Figure 2 summarizes the stability of the laser system. Here, we monitor the beat note of the main laser and the reference laser with a third "master" laser operating at 1560 nm [35]. The frequency stability of the laser source is below 10 kHz after 2×10^4 s at 1560 nm—limited only by temperature variations in the VCOs, which produce a frequency drift of approximately 15 kHz. The relative power stability (measured after a fiber-splitting bench) is at the level of 0.2% after operating for 52 h. Finally, we track the intensity of the two principal lines $\Omega_{1,1}^{PPLN}$ and $\Omega_{2,0}^{PPLN}$ in the static and dynamic operating modes. The stability of these lines contributes to time-varying light shifts in the atom interferometer and gives an indication of the stability of other lines. The intensity ratio between these lines reaches a stability below 1% in static mode, and approximately 2% in dynamic mode after 2.5 h. At this level, we estimate a phase stability of approximately 0.75 mrad (12 ng) for the atom interferometer (see Appendix B).

IV. LASER COOLING AND ATOM INTERFEROMETRY

We now discuss the results of laser-cooling and atominterferometry experiments carried out with this laser system. Our experimental setup has been previously described in Ref. [18]. A vapor-loaded three-dimensional magneto-optical trap (MOT) accumulates approximately 5×10^{8} ⁸⁷Rb atoms in 250 ms. This is followed by a gray-molasses stage using the D_2 transition [36], where the atoms are cooled to 2.5 μ K. In our retroreflected three-beam MOT, this technique is particularly effective compared to a standard red molasses because the beams are further detuned from the cycling transition-resulting in an improved intensity balance between the beams and a lower cloud temperatures. During the gray molasses, cold atoms are coherently transferred to the dark state $|F = 1\rangle$. After 10 ms of gray molasses, the light is turned off and the atoms are released in free fall. A magnetic bias field of approximately 70 mG is then turned on and the atoms are prepared in the magnetically insensitive $|F = 1, m_F = 0\rangle$ state using a series of optical pulses. Each preparation subsequence lasts approximately 300 μ s and involves two 100 μ s pulses of copropagating Raman light separated by 100 μ s [37]. At the same time, the Raman frequency is swept across the two-photon Zeeman resonances-coherently transferring atoms from $|F = 1, m_F = \pm 1\rangle$ to $|F = 2, m_F = \pm 1\rangle$, where they are subsequently removed with a short blowaway pulse near $|F = 2\rangle \rightarrow |F' = 3\rangle$. This subsequence is repeated three times, which enables us to reach 95% purity in $|F = 1, m_F = 0\rangle$ with no residual heating. During each of these stages, the principal lines produced by the laser source are modulated in amplitude and frequency using only rf control.

The atom interferometer is configured as a three-pulse Mach-Zehnder-type gravimeter [3-5,15] with vertically

oriented Raman beams that are retroreflected by a mirror below the MOT. In this configuration, the phase shift of the interferometer is $\Delta \Phi = (\alpha - k_{\text{eff}}g)T^2$, where α is the chirp rate applied to one of the Raman sidebands, $k_{\rm eff} \simeq 4\pi/\lambda$ is the effective wave vector of Raman light at wavelength $\lambda = 780$ nm, g is the gravitational acceleration, and T is the free-fall time between Raman pulses. For the atom-interferometry experiments, the two pairs of counterpropagating Raman beams have orthogonal linear polarizations to suppress velocity-insensitive copropagating transitions. Using microwave components, we adjust the intensity ratio between the two Raman lines to minimize the ac Stark shift between the two ground states. We typically measure shifts $< 20 \text{ Hz}/(\text{mW/cm}^2)$. A magnetically shielded mechanical accelerometer (Thales EMA 1000) monitors vibrations of the reference mirror and is used to correct for vibration-induced phase noise [4,11,37].

Figure 5 shows interference fringes obtained for different interrogation times. Here, the relative population in $|F=2\rangle$ is measured as a function of α and the dark fringe common to all values of T gives a measure of local gravity through $\alpha = k_{\text{eff}}g$. To suppress noninertial shifts due to the ac Stark and quadratic Zeeman effects, we combine measurements of g with opposite wave vectors $\pm k_{\rm eff}$ [4]. At T = 31 ms, the fringes exhibit a contrast of C = 0.43(1), offset noise $\sigma_P = 0.0079(1)$, contrast noise $\sigma_C = 0.0033(1)$, and phase noise of $\sigma_{\phi} = 0.141(4)$ rad per shot (limited by the self-noise of the mechanical accelerometer, of approximately 360 ng/ $\sqrt{\text{Hz}}$ [38]). These noise parameters are estimated by minimizing the negative log-likelihood distribution associated with the sinusoidal fit function-similar to the method presented in Ref. [18]. For a cycling time of $T_{\rm cyc} = 1.6$ s (including dead times of approximately 1.3 s between experiments), we estimate a short-term acceleration sensitivity of $\sigma_a = \sigma_\phi \sqrt{T_{\rm cyc}} / k_{\rm eff} T^2 = 1.2 \ \mu {\rm g} / \sqrt{{\rm Hz}}.$

To characterize the stability and ultimate sensitivity limit of our setup, we implement a central fringe lock using a protocol similar that used in atomic clocks. Here, the phase of the interferometer is modulated between opposite midfringe positions $(\pm \pi/2)$, where the sensitivity to phase fluctuations is largest [39]. We also alternate between momentum-transfer directions $(\pm k_{\text{eff}})$ and combine the measurements such that noninertial effects are rejected on the fly. Hence, one lock cycle is complete every $T_{\text{lock}} = 4T_{\text{cyc}} \simeq 6.4$ s. The chirp rate is steered onto the central fringe using a simple proportional-integrator feedback loop, with a time constant of approximately $10T_{lock} = 64$ s. This scheme has the advantage of being insensitive to fringe offset and contrast variations and optimizes the short-term sensitivity of the sensor. Figure 5(c)shows the Allan deviation of the acceleration measurements after tracking the central fringe for 15 h. After a few time constants, the measurement sensitivity integrates as roughly $1/\sqrt{t}$, as expected for white Gaussian phase noise.



FIG. 5. Interference fringes for opposite directions of momentum transfer (a) $-k_{\text{eff}}$ and (b) $+k_{\text{eff}}$, obtained by scanning the chirp rate α . Data are shown for interrogation times T = 19 ms (blue), 25 ms (orange), and 31 ms (green). The solid lines are least-squares fits to the data. The horizontal axis is centered on the local reference of gravity $g = 9.805\,642$ m/s² [15]. (c) The Allan deviation of raw acceleration measurements for T = 20 ms (blue curve) and after subtraction of tides (red curve). The shaded regions correspond to the 1σ statistical uncertainty in the Allan deviation and the black dotted line is a fit of the form σ_a/\sqrt{t} . Other parameters are as follows: π -pulse duration $2\tau = 6 \mu$ s; detuning $\Delta_R/2\pi = -0.88$ GHz.

From a fit to these data, we obtain a short-term sensitivity of $\sigma_a = 2.4 \ \mu g/\sqrt{\text{Hz}}$ —consistent with our estimates of the phase noise from the interference fringes. The tidal gravitational anomaly appears after approximately 1 h and is subtracted using a global model for tidal effects [40]. We reach a statistical precision of 15 ng after 10⁴ s of integration—corresponding to a phase stability of approximately 0.95 mrad.

V. INFLUENCE OF RESIDUAL LINES

The impact of additional laser lines on atominterferometric sensors has previously been studied in the case of phase-modulated light in free space [7,29] and more recently in an optical cavity [41]. The presence of these lines adds several spatial components to the effective Rabi frequency for counterpropagating

Raman transitions, resulting in a small spread of momenta transferred to the atom on each Raman pulse. This leads to a multipath interferometer, as illustrated in Fig. 6. Interference between the different momentum components leads to a spatially varying Rabi frequency and phase shift, which depend on the relative line intensities and the position of the atoms relative to the reference mirror. The largest contributors to these effects are the two pairs of lines nearest the principal Raman pair. In Fig. 4(b), these lines correspond to $(\Omega_{3,-1}^{PPLN}, \Omega_{2,0}^{PPLN})$, and $(\Omega_{1,1}^{PPLN}, \Omega_{0,2}^{PPLN})$. In a phase modulator, the intensity of these lines is typically of the same order of magnitude as the principal pair. With our method, we are able to suppress these lines at the 20-dB level, which strongly reduces their effects on the atom interferometer. Additionally, we show that the two Raman couplings associated with these residual lines have opposite signs; hence their



FIG. 6. The effect of an additional laser line on an atom interferometer. (a) Two-photon Raman transitions between ground states $|a\rangle$ and $|b\rangle$ coupled by two pairs of laser lines; one with principal Rabi frequency $\chi_{0,0}$ and one residual $\chi_{p,q}$. The momentum transferred in each case is $\hbar k_{p,q} = \hbar (k_{\text{eff}} + q\Delta k_1 + p\Delta k_2)$, where $\Delta k_1 = 2\Omega_1/c$, $\Delta k_2 = 2\Omega_2/c$, and $\Omega_2 - \Omega_1 = \delta_{\text{HF}}$ is the splitting between ground states. (b) An illustration of the multipath interferometer that results from an additional laser line. For sufficiently cold atoms, these pathways are within the de Broglie wavelength of the diffracted wave packets—causing spatial interference that leads to a phase shift.

contributions to the interferometer phase tend to cancel out (see Appendix B).

Figure 7 shows the predicted Rabi frequency and AI phase shift due to additional laser lines for the case of a standard phase modulator (PM) and an IQ modulator operating in CS-DSSB mode. The model for these effects is based on the multichromatic field produced by our laser system (see Appendix A), along with measurements of the residual line intensities [Fig. 4(b)], and a precise determination of the initial atom-mirror distance z_M (see Appendix C). For the phase-shift model, we also take into account the k-reversal process used in the experiment, which removes direction-independent systematic effects. Specifically, $\Delta \Phi = \frac{1}{2}(\Delta \phi_{\uparrow} - \Delta \phi_{\downarrow})$, where $\Delta \phi_{\uparrow\downarrow}$ is the phase shift for upward (downward) momentum kicks. From Figs. 7(a) and 7(b), both χ_{eff} and $\Delta \Phi$ are periodic with the mirror position z_M . The shape of these oscillations features a complex dependence on the relative line intensities and their phase relationships. The key feature of the IQ modulator is that these modulation effects are highly suppressed compared to the phase modulator—especially for the spatial component corresponding to $\delta_{\rm HF}/2\pi = 6.834$ GHz (i.e., a spatial period of 21.9 mm). An additional spatial modulation with period 157 mm is present in the IQ modulator due to residual lines at an offset frequency of $\Omega_1/2\pi = 0.955$ GHz. The phase shift due to the IQ modulator is primarily due to these lines. Figure 7(c)



FIG. 7. A comparison of (a) the normalized Rabi frequency $\chi_{eff}/\chi_{0,0}$ and (b),(c) the AI phase shift $\Delta \Phi$ produced by a phase modulator (red curves) and an IQ modulator (blue curves). The phase shift is shown as a function of z_M (b) for fixed T = 20 ms and (c) as a function T for a fixed atom-mirror distance $z_M = 122$ mm. The IQ modulator line intensities are taken from Fig. 4(b). For the phase modulator, we use relative line intensities $I_{0,m}/I_{0,0} = (-30, -12, -2, 0, -2, -12, -30)$ dB for modulation frequencies $m\delta_{\rm HF}$, with $m = -3, -2, \ldots, 3$. These intensities are based on measurements in a similar laser system employing a phase modulator with $\beta = 1.254$. Other AI parameters are as follows: TOF = 15 ms, $2\tau = 6 \ \mu$ s, $\Delta_R = -0.88$ GHz, and the initial velocity $v_0 = -15$ mm/s.

shows the phase shift as a function of the interrogation time *T*. Here, the IQ modulator offers several advantages in terms of systematic effects over a phase modulator. First, the amplitude of the phase oscillations is reduced by more than a factor 5 up to T = 100 ms. Second, due to the larger spatial modulation period, $\Delta \Phi$ accumulates on a much longer scale and with a moderate variation. This reduces the level at which experimental parameters (e.g., line intensities, Rabi frequency, and mirror position) must be known in order to accurately determine this systematic shift or to operate where it crosses zero.

To confirm the validity of our model for the IQ modulator and its effects on the AI, we measure the spatial variation of the Rabi frequency. Figure 8(a) shows measurements of this variation as a function of the cloud position relative to the mirror. The central cloud position is varied by changing the time of flight before the AI. We then measure the Rabi frequency at a fixed position by varying the duration of the pulse and fitting the resulting Rabi oscillations. The normalized Rabi frequency $(\chi_{eff}/\chi_{0.0})$ is estimated by dividing the measurements by their mean value. Our model for the Rabi frequency (see Appendix B) shows excellent agreement with the data and demonstrates that the residual laser lines spatially modulate the Raman coupling by approximately 5% peak to peak. This corresponds to a reduction by a factor of approximately 3.5 compared to a phase modulator. We expect this to have a small effect on the AI fringe contrast but we do not observe significant contrast modulations within our operating parameters.

Based on our model, we estimate a phase shift of $\Delta \Phi \simeq$ 6 mrad for typical experimental conditions (see Fig. 7), which corresponds to an acceleration bias of 95 ng. Compared to a phase modulator, this systematic is reduced by a factor of approximately 100. However, it is challenging to measure phase shifts at this level (for our conditions, it would require averaging for several hours). To enhance the phase shift due to residual laser lines, we modify the Doppler-compensation protocol for the AI. Instead of using a frequency chirp $\alpha \simeq k_{\text{eff}}g$, we apply a sequence of phase-continuous frequency steps of $\alpha(T+2\tau)$ between each Raman pulse (similar to the first atomic gravimeters [42]). With this method, the Doppler shift is canceled between pulses but remains during the pulses. This creates a slight imbalance between the phase contributions from atomic motion and the laser frequency (see Appendix D). The result is a phase shift $\Delta \Phi_{FS}$ that is proportional to the difference between the Rabi frequencies $\chi_{eff}^{(1)}$ and $\chi_{eff}^{(3)}$ at each $\pi/2$ pulse:

$$\Delta \Phi_{\rm FS} = \alpha (T + 2\tau) \left[\frac{\tan \left(\frac{\chi_{\rm eff}^{(3)} \tau}{2}\right)}{\chi_{\rm eff}^{(3)}} - \frac{\tan \left(\frac{\chi_{\rm eff}^{(1)} \tau}{2}\right)}{\chi_{\rm eff}^{(1)}} \right]$$
(1a)
$$\simeq \alpha (T + 2\tau) (\pi/2 - 1) \left(\chi_{\rm eff}^{(3)} - \chi_{\rm eff}^{(1)}\right) / \chi_{0,0}^2.$$
(1b)



FIG. 8. (a) Measurements of the normalized Rabi frequency $(\chi_{eff}/\chi_{0,0})$ as a function of the cloud position. The blue (red) points correspond to mirror position 1 (2). The solid black curve corresponds to our model for the IQ modulator. (b) Measurements of the induced frequency-step bias due to the spatial variation of the Rabi frequency for an interrogation time T = 20 ms. (c) A schematic of the setup. The atom-mirror distance is varied by letting the cloud (black dot) fall for different heights over a maximum of 35 mm (constrained by our vacuum system). The mirror is then moved from position 1 to position 2 between data sets.

Here, the last line is a first-order expansion about $\chi_{eff}^{(1)} = \chi_{eff}^{(3)} = \chi_{0,0}$. This phase shift is much larger than $\Delta \Phi$ (typically several hundred milliradians) due to the spatial variation of the Rabi frequency. Hence, this technique allows us to validate the influence of the IQ modulator on the AI.

Figure 8(b) shows measurements of the acceleration bias due to the laser-frequency steps $(\Delta \Phi_{\rm FS}/k_{\rm eff}T^2)$ as a function of the atom-mirror distance at the time of the first pulse. The data are first corrected for the two-photon light shift [43] and subsequently compared with the predicted frequency-step bias using our spatially varying Rabi frequency as input. We note that the atomic trajectories differ for interferometers employing $\pm k_{\text{eff}}$ and this must be accounted for in the model. We obtain good agreement between the model and the data in both mirror positions when constant biases of $-0.9 \ \mu g$ and $-1.4 \ \mu g$ are added to the model for mirror positions 1 and 2, respectively. These biases are attributed to slight tilts of the collimator (approximately 0.67 mrad) and the mirror (approximately 0.35 mrad) relative to the vertical between the two positions. We also shift the model by -3.5 mm on the position axis. This shift is attributed to effects related to averaging over the spatial and velocity distribution of the cloud. Such effects are beyond the scope of this paper and require further study. We emphasize that the modulation amplitude and spatial period of the frequency-step bias show good agreement with predictions. These results verify our model for the Rabi frequency and, by extension, the phase shift $\Delta \Phi$ due to residual laser lines.

VI. CONCLUSION

We present a dual-frequency modulated laser source with reduced parasitic sidebands, where the control of two independent optical signals is realized using microwave signals. The key component is an IQ modulator that enables optimal suppression of the carrier and the production of two single sidebands, with a rejection of the parasitic lines better than 20 dB. With this laser source, we demonstrate a complete cold-atom measurement sequence, including laser cooling, state preparation and atom interferometry, and detection, using only rf control. The laser system is tunable over a range of 15 GHz in typically 1 μ s using a microwave waveform generator with a large time bandwidth [44]. This architecture can be employed for many cold-atom techniques, such as atom launching, high Doppler-shift compensations, and zero-velocity atom interferometry [45]. The dual-single-sideband modulation can be generalized to any multiple single-sideband generation, while limiting the influence of unwanted frequencies.

Our theoretical model predicts a systematic error due to residual laser lines below 100 ng at T = 20 ms, which is confirmed by measurements of the Rabi frequency at different cloud positions. We also measure the influence of residual lines on an atomic gravimeter via the acceleration bias induced by a sequence of phase-continuous laser-frequency steps. We anticipate that the contribution due to residual lines can be reduced to 10 ng by further optimizing the operating parameters of the laser system (see Appendix B). The tunability of the IQ modulator implies that our architecture can also be adapted for other atomic species, such as potassium [23] or cesium [46], or upgraded to operate with a single diode. The simplicity of our architecture, along with the dramatic improvement in accuracy over phase-modulator-based designs, makes it a suitable alternative for systems employing two phase-locked lasers [21,22]. It is also easily transportable—making it ideal for a large range of onboard applications, including mobile gravity surveys [47], inertial navigation [18], or fundamental physics in space [48].

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APPENDIX A: MODEL OF THE ELECTRIC FIELD PRODUCED BY CS-DSSB MODULATION

In this appendix, we present a derivation of the modulated optical field obtained using the CS-DSSB modulation technique in an electro-optic IQ modulator. For the purposes of this derivation, we use a plane wave at the input of the IQ modulator: $E_0e^{i(\omega_0t+\phi_0)}$, with carrier frequency ω_0 , optical phase ϕ_0 , and electric field amplitude E_0 . We ignore the spatial part of the field for the moment but we discuss its effects in Appendix B. Following the scheme shown in Fig. 1(b), injecting two rf signals in phase quadrature into the IQ modulator, the electric field at the output of the two sub-MZIs can be written as

$$E_{1}(t) = \frac{E_{0}}{4} e^{i(\omega_{0}t + \phi_{0})} \left(e^{i[\beta_{1}\cos(\Omega_{1}t + \phi_{1}) + \beta_{2}\cos(\Omega_{2}t + \phi_{2}) + \Delta\Phi_{1}/2]} + e^{-i[\beta_{1}\cos(\Omega_{1}t + \phi_{1}) + \beta_{2}\cos(\Omega_{2}t + \phi_{2}) + \Delta\Phi_{2}/2]} \right).$$
 (A1a)

$$E_{2}(t) = \frac{E_{0}}{4} e^{i(\omega_{0}t + \phi_{0})} \left(e^{i[\beta_{1}\sin(\Omega_{1}t + \phi_{1}) + \beta_{2}\sin(\Omega_{2}t + \phi_{2}) + \Delta\Phi_{1}/2]} + e^{-i[\beta_{1}\sin(\Omega_{1}t + \phi_{1}) + \beta_{2}\sin(\Omega_{2}t + \phi_{2}) + \Delta\Phi_{2}/2]} \right).$$
 (A1b)

Here, Ω_1 and Ω_2 represent the two rf frequencies, ϕ_1 and ϕ_2 are arbitrary phases, and β_1 and β_2 are the respective rf modulation depths given by $\beta_i = \pi (V_i/V_\pi)$, where V_i is the signal amplitude and V_π is the half-wave voltage of the two sub-MZIs. This quantity depends on the dimensions of the optical waveguide, which is optimized to reduce

 V_{π} as much as possible. $\Delta \Phi_1$ and $\Delta \Phi_2$ are the phase differences between the arms of each sub-MZI and the main MZI contains a phase difference $\Delta \Phi_3$. All of these phases are controlled by dc bias voltages within each MZI. The total electric field at the output of the IQ modulator is $E_{IQ} = E_1 e^{i\Delta\Phi_3/2} + E_2 e^{-i\Delta\Phi_3/2}$. In CS-DSSB mode, we tune the phases $\Delta \Phi_1 = \Delta \Phi_2 = \pi$ in order to suppress the carrier. Using the Jacobi-Anger expansion, it follows that

$$E_{1}(t) = \frac{E_{0}}{2} e^{i(\omega_{0}t + \phi_{0})} \sum_{n,m \in \mathbb{Z}} \cos\left((n + m + 1)\frac{\pi}{2}\right)$$

$$\times J_{n}(\beta_{1})J_{m}(\beta_{2})e^{i[(n\Omega_{1} + m\Omega_{2})t + n\phi_{1} + m\phi_{2}]}, \quad (A2a)$$

$$E_{2}(t) = \frac{E_{0}}{2}e^{i(\omega_{0}t + \phi_{0})} \sum_{n,m \in \mathbb{Z}} \cos\left((n + m + 1)\frac{\pi}{2}\right)$$

$$\times J_{n}(\beta_{1})J_{m}(\beta_{2})e^{i[(n\Omega_{1} + m\Omega_{2})t + n\phi_{1} + m\phi_{2}]}e^{-i(n + m)\pi/2}, \quad (A2b)$$

where $J_n(z)$ is a Bessel function of the first kind. One can easily verify that the amplitude of the carrier frequency (corresponding to indices n = m = 0) vanishes for both E_1 and E_2 . Combining Eq. (A2) in quadrature (i.e., with $\Delta \Phi_3 = -\pi/2$) we can suppress the lower sidebands at the output of the IQ modulator. It is convenient to write this electric field as a series of plane waves in the following form:

$$E_{\mathrm{IQ}}(t) = E_0 e^{i(\omega_0 t + \phi_0)} \sum_{n,m \in \mathbb{Z}} A_{n,m}^{\mathrm{IQ}} e^{i\left(\Omega_{n,m}^{\mathrm{IQ}} t + \phi_{n,m}^{\mathrm{IQ}}\right)}, \qquad (A3)$$

where the amplitude, frequency, and relative phase of each line are

$$A_{n,m}^{\text{IQ}} = \cos\left((n+m+1)\frac{\pi}{2}\right)\cos\left((n+m-1)\frac{\pi}{4}\right)$$
$$\times J_n(\beta_1)J_m(\beta_2), \qquad (A4a)$$

$$\Omega_{n,m}^{\rm IQ} = n\Omega_1 + m\Omega_2, \tag{A4b}$$

$$\phi_{n,m}^{\text{IQ}} = n\phi_1 + m\phi_2 - (n+m)\frac{\pi}{4}.$$
 (A4c)

According to Eq. (A4a), all harmonics corresponding to even n + m or odd (n + m - 1)/2 are suppressed. For example, the harmonics with indices (n, m) =(-2, 0), (-1, 0), (0, 0), (0, -1), (1, 1), (1, 2) are all suppressed due to our choice of $\Delta \Phi_3 = -\pi/2$. The principal lines used for laser cooling and interferometry in our case correspond to (n, m) = (0, 1) and (1, 0). The electric field at the output of the PPLN is proportional to the square of the input field: $E_{\text{PPLN}}(t) = \eta \epsilon_0 \chi^2 E_{\text{IQ}}^2(t)$, where η is the efficiency of SHG [49], ϵ_0 is the vacuum permittivity, and χ is the susceptibility of the medium. Squaring Eq. (A3), we obtain

$$E_{\text{PPLN}}(t) = \eta \epsilon_0 \chi^2 E_0^2 e^{i(2\omega_0 t + 2\phi_0)} \sum_{n,m,l,k \in \mathbb{Z}} \cos\left((n+m+1)\frac{\pi}{2}\right) \cos\left((n+m-1)\frac{\pi}{4}\right) \cos\left((l+k+1)\frac{\pi}{2}\right) \\ \times \cos\left((l+k-1)\frac{\pi}{4}\right) J_n(\beta_1) J_m(\beta_2) J_l(\beta_1) J_k(\beta_2) e^{i\left[\left((n+l)\Omega_1 + (m+k)\Omega_2\right)t + (n+l)\phi_1 + (m+k)\phi_2 - (n+m+l+k)\pi/4\right]}.$$
 (A5)

To simplify this expression, we define new indices N = n + l and M = m + k and substitute them in Eq. (A5). The electric field after SHG can then be written as

$$E_{\text{PPLN}}(t) = \eta \epsilon_0 \chi^2 E_0^2 e^{i(2\omega_0 t + 2\phi_0)} \sum_{N,M \in \mathbb{Z}} A_{N,M}^{\text{PPLN}} e^{i\left(\Omega_{N,M}^{\text{PPLN}} t + \phi_{N,M}^{\text{PPLN}}\right)},\tag{A6}$$

where the amplitude, frequency, and relative phase are

$$A_{N,M}^{\text{PPLN}} = \sum_{n,m\in\mathbb{Z}} \cos\left((n+m+1)\frac{\pi}{2}\right) \cos\left((N+M-n-m+1)\frac{\pi}{2}\right) \cos\left((n+m-1)\frac{\pi}{4}\right) \\ \times \cos\left((N+M-n-m-1)\frac{\pi}{4}\right) J_n(\beta_1) J_{N-n}(\beta_1) J_m(\beta_2) J_{M-m}(\beta_2),$$
(A7a)

$$\Omega_{N,M}^{\rm PPLN} = N\Omega_1 + M\Omega_2, \tag{A7b}$$

$$\phi_{N,M}^{\text{PPLN}} = N\phi_1 + M\phi_2 - (N+M)\frac{\pi}{4}.$$
(A7c)

Equation (A7a) determines the relative power ratio between the harmonics and allows us to cancel constant light shifts by precisely controlling the intensity ratio of the two principal lines [4]. We emphasize that the sum over the individual line indices n, m appears only in the amplitude, while the frequency and phase of each second harmonic is determined by indices N, M from the SHG process. The principal Raman lines in our case correspond to (N, M) = (2, 0) and (1, 1). The most significant parasitic lines shown in Fig. 4(b) are $\Omega_{0,2}^{\text{PPLN}}$ and $\Omega_{3,-1}^{\text{PPLN}}$. The first of these arises from doubling $\Omega_{0,1}^{\text{IQ}}$, while the second is derived from summing $\Omega_{2,-1}^{IQ}$ and $\Omega_{1,0}^{IQ}$. The amplitude of all lines is controlled experimentally by the modulation depths β_1 and β_2 . Typically, these two parameters are set by (i) zeroing the one-photon light shift by optimizing the ratio between the two principal lines $\Omega_{2,0}^{PPLN}$ and $\Omega_{1,1}^{PPLN}$ and (ii) minimizing the amplitude of all other lines. This is achieved by minimizing both β_1 and β_2 while preserving the correct ratio. Although all other lines are suppressed, each pair of lines separated by $\delta_{\rm HF}$ is resonant with a twophoton Raman transition. Using Eq. (A7b) and the fact that $\Omega_2 = \Omega_1 + \delta_{\text{HF}}$, this condition can be summarized as

$$\delta_{\rm HF} = \Omega_{N',M'}^{\rm PPLN} - \Omega_{N,M}^{\rm PPLN},$$

= $(N' - N)\Omega_1 + (M' - M)(\Omega_1 + \delta_{\rm HF}).$ (A8)

It follows that only pairs $(\Omega_{N,M'}^{PPLN}, \Omega_{N,M}^{PPLN})$ with N' = N - 1and M' = M + 1 can drive Raman transitions. The phase difference between any of these Raman lines can be deduced from Eq. (A7c):

$$\Delta \phi = \phi_{N'M'}^{\text{PPLN}} - \phi_{NM}^{\text{PPLN}} = \phi_2 - \phi_1, \qquad (A9)$$

which is equal to the phase difference between the two input rf signals. This key property enables precise control of the atom-interferometer phase via the optical Raman interaction.

APPENDIX B: EFFECTS OF RESIDUAL LASER LINES ON THE ATOM INTERFEROMETER

Each pair of residual laser lines separated by δ_{HF} is resonant with a two-photon Raman transition and can lead to a parasitic phase shift in the atom interferometer, as illustrated in Fig. 6. Using our model for the electric field in the previous section, here we develop a model for the phase shift and contrast loss in the atom interferometer produced by the IQ modulator. We adopt the approach of Ref. [29], where the impact of additional laser lines has previously been studied in the case of an electro-optic phase modulator.

The counterpropagating Rabi frequency associated with any two pairs of lines is proportional to the product of their electric field amplitudes and inversely proportional to the detuning from the excited state. For all resonant pairs of lines $(\Omega_{2+p,q}^{PPLN}, \Omega_{1+p,1+q}^{PPLN})$, where the indices (p,q) denote the offset from the principal Raman lines $(\Omega_{2,0}^{PPLN}, \Omega_{1,1}^{PPLN})$, the Raman coupling parameter can be written as

$$\Lambda_{p,q} \sim \frac{E_{2+p,q}(t)E_{1+p,1+q}^{*}(t-2z/c)}{\Delta_{R} + p\,\Omega_{1} + q\,\Omega_{2}},\tag{B1}$$

where $E_{N,M}(t) = E_0 e^{i2\omega_0 t} A_{N,M}^{\text{PPLN}} e^{i(\Omega_{N,M}^{\text{PPLN}} t + \phi_{N,M}^{\text{PPLN}})}$ is an electric field amplitude, z is the distance between the atoms and the mirror at time t, and 2z/c is the round-trip time required for the light to reflect off the mirror. It follows that

$$\Lambda_{p,q} \sim e^{i(k_{\text{eff}}z - \delta_{\text{HF}}t - \Delta\phi)} \chi_{p,q} e^{i(p\,\Delta k_1 + q\,\Delta k_2)z}, \qquad (B2a)$$

$$\chi_{p,q} \propto \frac{A_{2+p,q}^{\text{PPLN}} A_{1+p,1+q}^{\text{PPLN}}}{\Delta_R + p \,\Omega_1 + q \,\Omega_2},\tag{B2b}$$

where $\chi_{p,q}$ is a Rabi frequency and the effective wave vector is

$$k_{\text{eff}} = (2\omega_0 + \Omega_{2,0}^{\text{PPLN}} + 2\omega_0 + \Omega_{1,1}^{\text{PPLN}})/c$$

= $(4\omega_0 + 3\Omega_1 + \Omega_2)/c.$ (B3)

The first term in $\Lambda_{p,q}$ describes the energy ($\hbar \delta_{\text{HF}}$), momentum ($\hbar k_{\text{eff}}$), and phase ($\Delta \phi$) transferred to the atoms by the principal Raman lines during each pulse. These lines are associated with the principal Rabi frequency $\chi_{0,0} \equiv \pi/2\tau$, where τ is the $\pi/2$ -pulse duration. For other pairs of lines, the energy and phase are identical but due to additional spatial harmonics present in the field, the momentum transfer is modified to $\hbar(k_{\text{eff}} + p\Delta k_1 + q\Delta k_2)$, where $\Delta k_1 = 2\Omega_1/c$ and $\Delta k_2 = 2\Omega_2/c$. This slightly different momentum kick for each pair of laser lines is the origin of the parasitic phase shift in the atom interferometer.

The Rabi frequencies $\chi_{p,q}$ associated with each resonant pair of laser lines can be determined from experimental parameters using the following ratio:

$$\frac{\chi_{p,q}}{\chi_{0,0}} = \frac{A_{2+p,q}^{\text{PPLN}} A_{1+p,1+q}^{\text{PPLN}}}{A_{2,0}^{\text{PPLN}} A_{1,1}^{\text{PPLN}}} \times \left(\frac{\frac{1}{\Delta_{R2} + p\Omega_1 + q\Omega_2} + \frac{1}{3(\Delta_{R1} + p\Omega_1 + q\Omega_2)}}{\frac{1}{\Delta_{R2}} + \frac{1}{3\Delta_{R1}}}\right), \quad (B4)$$

where $\Delta_{R2} = \Delta_R$ and $\Delta_{R1} = \Delta_R + 2\pi \times 157$ MHz are the single-photon Raman detunings from the $|F = 2\rangle \rightarrow$ $|F' = 2\rangle$ and $|F' = 1\rangle$ transitions in ⁸⁷Rb, respectively. Table I provides a list of the Rabi frequencies and detunings used in our calculations.

During each Raman pulse, the light-matter interaction imprints a phase on the atoms that depends on the position z relative to the retroreflection mirror. The effective Rabi frequency χ_{eff} determines the strength of this interaction. In the presence of additional laser lines, this quantity is given

TABLE I. The Rabi frequencies and detunings for $\Omega_1/2\pi = 0.96$ GHz, $\Omega_2/2\pi = 7.79$ GHz, $\Delta_R/2\pi = -0.88$ GHz, and line intensities measured from Fig. 4(b). Here, $\Omega(p,q) = p\Omega_1 + q\Omega_2$ and $\Delta_{R1,2}(p,q) = \Delta_{R1,2} + p\Omega_1 + q\Omega_2$. Other quantities are as defined in the text.

р	q	$ \chi_{p,q}/\chi_{0,0} $ (dB)	$\operatorname{sign}(\chi_{p,q})$	$\begin{array}{c} \Omega(p,q) \\ (\mathrm{GHz}) \end{array}$	$\begin{array}{c} \Delta_{R1}(p,q) \\ (\text{GHz}) \end{array}$	$\begin{array}{c} \Delta_{R2}(p,q) \\ (\text{GHz}) \end{array}$
-2	0	-25.5	1	-1.91	-2.63	-2.79
-1	0	-23.2	-1	-0.96	-1.67	-1.83
-1	1	-18.5	-1	6.84	6.12	5.96
0	0	0.0	1	0.00	-0.72	-0.88
1	-1	-18.5	-1	-6.84	-7.56	-7.71
1	0	-15.6	1	0.96	0.24	0.08
2	0	-27.4	1	1.91	1.19	1.03

by the sum over all Rabi frequencies—each coupled with a phase term describing the modified momentum transfer

$$\chi_{\text{eff}}(z) = \sum_{p,q \in \mathbb{Z}} \chi_{p,q} e^{i(p \,\Delta k_1 + q \,\Delta k_2)z}.$$
 (B5)

This sum results in a spatially varying Rabi frequency due to the interference between different spatial harmonics. In addition to the rf phase $\Delta \phi$, the atoms are imprinted with the following phase during each Raman pulse:

$$\varphi(z) = \arg\left[\chi_{\text{eff}}(z)\right]. \tag{B6}$$

In a three-pulse Mach-Zehnder interferometer, the total phase shift is

$$\Delta \Phi = \varphi(z_A) - \varphi(z_B) - \varphi(z_C) + \varphi(z_D), \quad (B7)$$

where z_A, \ldots, z_D denote the vertices of the interferometer at times t = TOF, TOF + T, and TOF + 2T (see Fig. 6). In a gravimeter configuration, where the atoms fall within a vertically aligned laser beam at a constant acceleration $a_z = -g$, these vertices are

$$z_A = z_M + v_0 \text{TOF} + \frac{1}{2}a_z (\text{TOF})^2,$$
 (B8a)

$$z_B = z_A + (v_0 + a_z \text{TOF})T + \frac{1}{2}a_z T^2,$$
 (B8b)

$$z_C = z_A + (v_0 + a_z \text{TOF} + v_{\text{rec}})T + \frac{1}{2}a_z T^2,$$
 (B8c)

$$z_D = z_A + \left(v_0 + a_z \text{TOF} + \frac{1}{2}v_{\text{rec}}\right)(2T) + \frac{1}{2}a_z(2T)^2.$$
(B8d)

Here, v_0 is the initial velocity of the atomic cloud, TOF is the time of flight before the first Raman pulse, z_M is the position of the mirror (nominally 122 mm below the initial cloud position), T is the interrogation time, and $v_{\rm rec} = \hbar k_{\rm eff}/M$ is the two-photon recoil velocity.



FIG. 9. (a) The contribution of each parasitic Raman transition to the phase shift as a function of the atom-mirror distance z_M . (b) The predicted AI phase shift due to residual parasitic lines for the current laser parameters (solid black curve), with optimized Ω_1 (dashed curve), and with optimized modulation depths β_1 and β_2 (dotted line). The AI parameters are as follows: TOF = 15 ms, T = 20 ms, and $\Delta_R/2\pi = -0.88$ GHz.

Figure 9 shows the predicted phase shift $\Delta \Phi$ due to residual lines as a function of the atom-mirror distance z_M . For each line, we compute the phase contribution $\Delta \Phi_{p,q}$ using the corresponding parameters listed in Table I. It is clear from Fig. 9(a) that the largest contributors ($\Delta \Phi_{-1,1}$ and $\Delta \Phi_{1,-1}$) have opposite sign—hence their sum tends to zero. We emphasize that this is a direct result of our frequency-doubled CS-DSSB architecture [37]. The total phase shift depicted in Fig. 9(b) presents locally an amplitude of approximately 10 mrad (162 ng) and for a constant offset of approximately 2.3 mrad (10 ng). The main contribution to this shift derives from the Rabi frequency $\chi_{1,0}$, where the Raman detunings are relatively small $[\Delta_{R1}(1,0) \simeq 240 \text{ MHz} \text{ and } \Delta_{R2}(1,0) \simeq 80 \text{ MHz}].$ By increasing Ω_1 to 1.1 GHz, the acceleration shift is decreased and can be locally approximated as a sinusoidal oscillation with an amplitude and a constant offset of 68 and -9 ng, respectively. Further optimization of the modulation depths to $\beta_1 = 0.573$ and $\beta_2 = 0.255$ reduces the contributions from $\Delta \Phi_{-1,1}$ and $\Delta \Phi_{1,-1}$ —resulting in an amplitude and offset of 26 and -11 ng, respectively.

APPENDIX C: MEASUREMENT OF ATOM-MIRROR DISTANCE USING OPTICAL RAMAN SPECTROSCOPY

To precisely determine the initial position of the atomic cloud relative to the reference mirror, as well as the residual launch velocity after the preparation stage, we take advantage of an interference effect using optical Raman spectroscopy. Two counterpropagating pairs of copropagating Raman beams excite velocity-insensitive transitions, as shown in Fig. 10(b). These two orthogonally polarized pairs of beams are simultaneously resonant but the retroreflected pair accumulates an additional phase proportional to the round-trip distance to the mirror. This results in a spatial modulation of the Rabi frequency analogous to the previous analysis with additional laser lines. Adding the electric fields for each pair of beams (ignoring residual lines), the effective Rabi frequency can be shown to be

$$\chi_{co}(z) = \chi_i e^{i\Delta kz} + \chi_r e^{-i\Delta k(z-2z_M)},$$

= 2|\chi|e^{i\Delta kz_M} \sin \Delta k(z-z_M), (C1)

where $\chi \equiv \chi_i = -\chi_r$ are Rabi frequencies for the incident and reflected beams and $\Delta k = \delta_{\rm HF}/c \simeq 2\pi \times 22.8 \text{ m}^{-1}$ is the effective wave number for copropagating transitions. This provides a powerful method to measure the initial atom-mirror distance z_M , as well as the initial velocity of the cloud v_0 .

Figure 10(a) shows measurements of the copropagating transition probability between magnetically insensitive



FIG. 10. (a) Measurements of the copropagating transition probability between $|F, m_F = 0\rangle$ states as a function of the atom-mirror distance. The red (blue) points correspond to the nominal (shifted) mirror position. The solid curves are sinusoidal fits to the data. (b) A schematic of the experiment and level diagram for copropagating transitions.

states as a function of the atom-mirror distance. We use a similar measurement strategy as for Fig. 8: the atom-mirror distance is varied using the time of flight before the Raman pulse and we repeat the measurement for two different mirror positions. Here, we fix the intensity and duration of the π pulse and record Raman spectra for each time of flight. We extract the peak amplitude from fits to these spectra [37], which provide a direct measurement of the copropagating transition probability shown in Fig. 10(a). This probability varies spatially as $P_{co}(z) \propto \sin^2[\chi_{co}(z)\tau]$, with a period of $\pi/\Delta k = 21.9$ mm. Assuming a parabolic trajectory for the cloud $z(t) = v_0t - \frac{1}{2}gt^2$, a fit to these data provides a precise estimate of the initial atom-mirror distance $z_M = 121.96(18)$ mm, as well as the initial vertical velocity of $v_0 = -15.5(3.1)$ mm/s.

APPENDIX D: THE AI PHASE SHIFT DUE TO PHASE-CONTINUOUS FREQUENCY STEPS

To amplify the effects of residual laser lines while also compensating the Doppler effect, we apply a series of phase-continuous frequency steps to the Raman frequency. This simulates a frequency chirp *between* pulses but maintains a constant frequency *during* the pulses. Figure 11 shows the frequency profile $\omega_{FS}(t)$ used in the experiment, which is described by

$$\omega_{\rm FS}(t) = \begin{cases} \omega_0, & t < -\delta t, \\ \omega_1, & -\delta t \le t < T + 2\tau - \delta t, \\ \omega_2, & T + 2\tau - \delta t \le t < 2T + 4\tau - \delta t, \\ \omega_3. & t \ge 2T + 4\tau - \delta t. \end{cases}$$
(D1)

Here, ω_0 is an arbitrary frequency, ω_n is the frequency during the *n*th Raman pulse, and δt is a small temporal offset that defines when the frequency steps occur before each pulse. Since $\omega_{FS}(t)$ is a phase-continuous frequency



FIG. 11. The timing diagram for the frequency steps used in the experiments (blue) and the corresponding frequency chirp (red) usually employed in atomic gravimeters.

profile, in order to avoid undesired AI phase shifts proportional to δt , the frequency steps must be triggered symmetrically with respect to the center of the interferometer at $t = T + 2\tau$ (as shown in Fig. 11). The resulting phase shift due to the laser is given by

$$\phi_{\rm las} = \int g_s(t) \omega_{\rm FS}(t) dt. \tag{D2}$$

Here, $g_s(t)$ is the generalized sensitivity function [50]:

$$g_{s}(t) = \begin{cases} 0, & t \leq 0 \text{ or } t > 2T + 4\tau, \\ -\frac{\sin(\chi_{\text{eff}}^{(1)}t)}{\sin(\chi_{\text{eff}}^{(1)}\tau)}, & 0 < t \leq \tau, \\ -1, & \tau < t \leq T + \tau, \\ \frac{\sin[\chi_{\text{eff}}^{(2)}(t - T - 2\tau)]}{\sin(\chi_{\text{eff}}^{(2)}\tau)}, & T + \tau < t \leq T + 3\tau, \\ +1, & T + 3\tau < t \leq 2T + 3\tau, \\ -\frac{\sin[\chi_{\text{eff}}^{(3)}(t - 2T - 4\tau)]}{\sin(\chi_{\text{eff}}^{(3)}\tau)}, & 2T + 3\tau < t \leq 2T + 4\tau, \end{cases}$$
(D3)

where $\chi_{\text{eff}}^{(n)}$ is the effective Rabi frequency during the *n*th pulse. Evaluating Eq. (D2) for the frequency profile in Eq. (D1), we obtain

$$\phi_{\text{las}} = (\omega_2 - \omega_1)T + (\omega_1 - 2\omega_2 + \omega_3)(\delta t - \tau) + \omega_3 \frac{\tan\left(\frac{\chi_{\text{eff}}^{(3)}\tau}{2}\right)}{\chi_{\text{eff}}^{(3)}} - \omega_1 \frac{\tan\left(\frac{\chi_{\text{eff}}^{(1)}\tau}{2}\right)}{\chi_{\text{eff}}^{(1)}}.$$
 (D4)

To compensate the Doppler shift $k_{\text{eff}gt}$ during the AI, we step the frequency such that $\omega_n = \omega_{n-1} + \alpha(T + 2\tau)$ with $\alpha = k_{\text{eff}g}$. Under these conditions, the second term in Eq. (D4) vanishes and we obtain

$$\phi_{\text{las}} = \omega_1 \left[\frac{\tan\left(\frac{\chi_{\text{eff}}^{(3)}\tau}{2}\right)}{\chi_{\text{eff}}^{(3)}} - \frac{\tan\left(\frac{\chi_{\text{eff}}^{(1)}\tau}{2}\right)}{\chi_{\text{eff}}^{(1)}} \right] + k_{\text{eff}}g(T+2\tau) \left[T+2\frac{\tan\left(\frac{\chi_{\text{eff}}^{(3)}\tau}{2}\right)}{\chi_{\text{eff}}^{(3)}} \right]. \quad (D5)$$

The kinematic component of the phase shift (i.e., that due to atomic motion assuming a constant acceleration -g and velocity v_1 at the first Raman pulse) is given by

$$\phi_{\rm kin} = k_{\rm eff} \int g_s(t)(v_1 - gt) dt,$$
(D6a)
$$\simeq k_{\rm eff} v_1 \left[\frac{\tan\left(\frac{\chi_{\rm eff}^{(1)}\tau}{2}\right)}{\chi_{\rm eff}^{(1)}} - \frac{\tan\left(\frac{\chi_{\rm eff}^{(3)}\tau}{2}\right)}{\chi_{\rm eff}^{(3)}} \right] - k_{\rm eff} g(T + 2\tau) \left[T + \frac{\tan\left(\frac{\chi_{\rm eff}^{(1)}\tau}{2}\right)}{\chi_{\rm eff}^{(1)}} + \frac{\tan\left(\frac{\chi_{\rm eff}^{(3)}\tau}{2}\right)}{\chi_{\rm eff}^{(3)}} \right],$$
(D6b)

where the last line is a leading-order approximation. Summing Eqs. (D5) and (D6), we obtain the total interferometer phase shift:

$$\phi_{\text{tot}} = (\omega_1 - k_{\text{eff}} v_1) \left[\frac{\tan\left(\frac{\chi_{\text{eff}}^{(3)} \tau}{2}\right)}{\chi_{\text{eff}}^{(3)}} - \frac{\tan\left(\frac{\chi_{\text{eff}}^{(1)} \tau}{2}\right)}{\chi_{\text{eff}}^{(1)}} \right] + k_{\text{eff}} g(T + 2\tau) \left[\frac{\tan\left(\frac{\chi_{\text{eff}}^{(3)} \tau}{2}\right)}{\chi_{\text{eff}}^{(3)}} - \frac{\tan\left(\frac{\chi_{\text{eff}}^{(1)} \tau}{2}\right)}{\chi_{\text{eff}}^{(1)}} \right].$$
(D7)

In the ideal case of a frequency chirp that cancels the Doppler shift at all times during the interferometer, the laser and kinetic phases are equal and opposite when $\alpha = k_{\text{eff}g}$ —resulting in $\phi_{\text{tot}} = 0$. In the case of phasecontinuous frequency steps, we obtain two terms. The first term in Eq. (D7) vanishes when the Raman frequency during the first pulse is equal to the Doppler shift ($\omega_1 = k_{\text{eff}}v_1$). The remaining term is equivalent to Eq. (1) in the main text, which can be approximated as $k_{\text{eff}}gT(\pi/2 - 1)(\chi_{\text{eff}}^{(3)} - \chi_{\text{eff}}^{(1)})(2\tau/\pi)^2$. Since this quantity scales as the difference between Rabi frequencies, it is a powerful tool to amplify any imbalance between them. In our case, it is ideal to indirectly measure the effects of residual laser lines as they produce a spatial modulation in the Rabi frequency.

Equation (D7) can also be interpreted as an imbalance between the AI scale factors for the laser and kinematic phases. The laser phase can be written as $\phi_{\text{las}} = S_{\text{las}}(\alpha/k_{\text{eff}})$, where S_{las} is the laser scale factor. This phase aims to compensate the kinetic phase which, for a constant acceleration *a*, is $\phi_{\text{kin}} = S_{\text{kin}}a$. When employing phasecontinuous frequency steps, S_{las} differs from the kinetic scale factor S_{kin} :

$$\frac{S_{\rm kin}}{k_{\rm eff}} = (T+2\tau) \left[T + \frac{\tan\left(\frac{\chi_{\rm eff}^{(1)}\tau}{2}\right)}{\chi_{\rm eff}^{(1)}} + \frac{\tan\left(\frac{\chi_{\rm eff}^{(3)}\tau}{2}\right)}{\chi_{\rm eff}^{(3)}} \right],$$
(D8a)

$$\frac{S_{\text{las}}}{k_{\text{eff}}} = (T+2\tau) \left[T+2\frac{\tan\left(\frac{\chi_{\text{eff}}^{(3)}\tau}{2}\right)}{\chi_{\text{eff}}^{(3)}} \right].$$
 (D8b)

When operating at the Doppler-compensating chirp rate $\alpha = k_{\text{eff}}a$, this leads to a bias on the acceleration measurement, since the total phase shift $\phi_{tot} = (S_{kin} - S_{las})a \neq 0$.

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