

# High-Sensitivity Accelerometry with a Feedback-Cooled Magnetically Levitated Microsphere

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We show that a magnetically levitated microsphere in high vacuum can be used as an accelerometer by comparing its response to that of a commercially available geophone. This system shows great promise for ultrahigh acceleration sensitivities without the need for large masses or cryogenics. With feedback cooling, the transient decay time is reduced and the center-of-mass motion is cooled to 9 K or less. Remarkably, the levitated-particle accelerometer has a sensitivity down to  $3.6 \times 10^{-8} \text{ g}/\sqrt{\text{Hz}}$  and gives measurements similar to those of the commercial geophone at frequencies up to 14 Hz despite a test mass that is four billion times smaller. With no free parameters in the calibration, the responses of the accelerometers match within 3% at 5 Hz. The system reaches this sensitivity due to a relatively large particle mass of  $0.25 \mu\text{g}$ , a low center-of-mass oscillation frequency of 1.75 Hz, and an image-analysis method that can measure the displacement with an uncertainty of 1.6 nm in a single image.

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## I. INTRODUCTION

High-sensitivity accelerometry has myriad applications in fundamental and practical fields of physics and engineering. The ability to measure extremely small accelerations and forces has uses in absolute gravimeters [1–3], inertial navigation [4], tests of quantum gravity [5,6], gravitational wave detection [7], precision measurements of the Newtonian constant of gravitation [8], and other tests of fundamental physics [9].

Typical accelerometers are based on clamped-resonator systems [10–12]. With cryogenic temperatures, force sensitivities as low as  $S_F^{1/2} \sim 10^{-21} \text{ N}/\sqrt{\text{Hz}}$  are predicted [13]. Using a  $\text{Si}_3\text{N}_4$  membrane [14], quality factors of  $10^8$  can be achieved at room temperature with oscillation frequencies of approximately 150 kHz, and thermal-noise-limited force sensitivities of  $S_F^{1/2} \sim 10^{17} \text{ N}/\sqrt{\text{Hz}}$  are possible. Mechanical devices have the advantage of typically being extremely compact [15,16]. Systems with very large test masses, such as the LISA Pathfinder, can have acceleration sensitivities of  $S_a^{1/2} \sim 10^{-16} \text{ g}/\sqrt{\text{Hz}}$  [17], where  $g$  is standard gravity,  $g = 9.8 \text{ m/s}^2$ . Cold-atom-interferometry systems have also been proposed for measuring small changes in gravity [18–20], with acceleration sensitivities as low as  $S_a^{1/2} \sim 10^{-9} \text{ g}/\sqrt{\text{Hz}}$  [21,22].

Levitated systems avoid dissipation associated with the mechanical contact of the resonator with its environment. Force sensitivities of  $S_F^{1/2} \sim 10^{-16} \text{ N}/\sqrt{\text{Hz}}$  and  $S_F^{1/2} \sim 10^{-18} \text{ N}/\sqrt{\text{Hz}}$  have been measured with particles in optical traps [23,24]. Acceleration sensitivities of  $S_a^{1/2} \sim 10^{-10} \text{ g}/\sqrt{\text{Hz}}$  [25] have been reported using a permanent magnet levitated above a superconductor at cryogenic temperatures.

The isolation from the environment of levitated optomechanical systems makes them good candidates for high-sensitivity accelerometry but their extremely weak dissipation under vacuum may require additional steps to ensure stability. The field has been dominated by optical trapping since its development by Ashkin and Dziedzic [26], in which feedback cooling is typically required for the levitated particle to remain trapped at pressures less than approximately 0.08 Torr [27,28]. With static fields alone, magnetic traps do not generally require feedback cooling while pumping to low pressure [29]. However, feedback can increase the damping rate of the motion and cool the center-of-mass motion [30]. A magnetic trap that does not rely on gravity for confinement has been demonstrated down to a pressure of approximately 0.1 Torr [31]. Magneto-gravitational traps have been developed [29,32] and have exhibited stable trapping to a pressure of approximately  $10^{-10}$  Torr with a feedback-cooled center-of-mass motion from room temperature to  $140 \mu\text{K}$  [33]. Recent

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cooling experiments in an optical trap have demonstrated a center-of-mass motion temperature of  $50 \mu\text{K}$  for large particles (approximately  $10 \mu\text{m}$ ) [34]. Cooling to the quantum ground state of a submicrometer particle has also been shown, reaching a temperature of  $12 \mu\text{K}$  from room temperature [35].

In this paper, we demonstrate levitation of a diamagnetic borosilicate microsphere in a magneto-gravitational trap down to a pressure of approximately  $10^{-7}$  Torr at room temperature. The relatively large mass of the  $60 \mu\text{m}$  microsphere and low oscillation frequencies compared to optical trapping systems [36] make this a promising optomechanical system for high-sensitivity room-temperature accelerometry. The center-of-mass motion is cooled with feedback to damp transients on a reasonable time scale while adding less thermal noise than would result from damping to an ambient temperature bath. To check the calibration, accelerations are directly applied to the system via a surface transducer.

A critical component of the system is an offline image-analysis technique that we develop to determine the displacement of the trapped particle from images recording its motion over time. In particular, we mitigate image background noise and avoid issues with fractional pixel translations by constructing a pixel-independent “eigenframe,” against which we compute the cross-correlation.

The high acceleration sensitivity of this system, measured to be  $3.6 \times 10^{-8} \text{g}/\sqrt{\text{Hz}}$ , is an improvement over typical MEMS accelerometers with sensitivities on the order of  $10^{-5} \text{g}/\sqrt{\text{Hz}}$  [37,38]. The primary advantage of the levitated particle is its low oscillation frequency, which can be under 2 Hz and at least a thousand times lower than the typical oscillation frequencies of MEMS devices. The weak restoring force associated with the low oscillation frequency results in relatively large movement of the particle in response to low-frequency acceleration of the environment.

## II. EXPERIMENTAL SETUP

### A. Loading and trapping of microspheres

The magneto-gravitational trap, designed with two samarium-cobalt (Sm-Co) permanent magnets and four iron-cobalt alloy (Hiperco-50A) pole pieces (see Fig. 1), creates a three-dimensional potential well to stably trap diamagnetic particles. The total potential energy of an object with volume  $V$  of diamagnetic material with magnetic susceptibility  $\chi$  and mass  $m$  in an external magnetic field subject to standard gravity  $g$  is

$$U = -\frac{\chi B^2 V}{2\mu_0} + mgy, \quad (1)$$

where  $B = |\vec{B}|$  is the magnitude of the magnetic field,  $\mu_0$  is the vacuum permeability, and  $y$  is the vertical displacement of the material [39]. For diamagnetic materials ( $\chi < 0$ ), a stable trap is formed at a magnetic field minimum in the absence of gravity.

The four pole pieces are configured in a quadrupole arrangement surrounding the two permanent magnets. The quadrupole field lies in the transverse-vertical ( $x$ - $y$ ) plane. Symmetry is broken in the vertical-axial ( $y$ - $z$ ) plane by cutting the top pole pieces shorter along the axial direction. This asymmetry along with gravity forms the trapping potential in the axial ( $z$ ) direction [29,30].

To reduce the effect of thermal noise while maintaining sensitivity to acceleration, larger trapped particles are preferred. A loading method is developed to allow reliable trapping of large microspheres [33]. In these experiments, we choose borosilicate microspheres (Cospheric BSGMS-2.2 53-63um-10g) with greater than 90% of particles in the diameter range of  $53 \mu\text{m}$ – $63 \mu\text{m}$ . Insulating polyimide tape is attached to the tip of an ultrasonic horn [40] to electrostatically hold large microspheres to the tip [33].

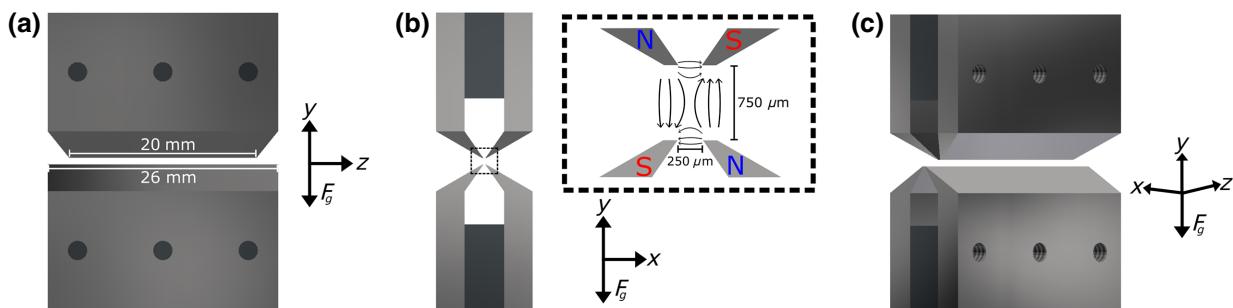


FIG. 1. (a) The linear magneto-gravitational trap as viewed from the transverse ( $x$ ) direction. The length of the bottom pole pieces is approximately 26 mm. The top pole pieces are cut shorter, to a length of approximately 20 mm. The asymmetry combined with the force of gravity constrains the particle in the axial ( $z$ ) direction. (b) The view of the trap as viewed from the axial direction, showing the quadrupole symmetry in the transverse and vertical ( $y$ ) directions. The magnetic field in the trapping region is qualitatively shown. (c) A rotated view of the trap showing the quadrupole symmetry and the broken symmetry in the vertical direction. The tapped holes pictured on the pole pieces are used to attach the trap to its mount.

The ultrasonic horn shakes the particles off and into the trapping region at atmospheric pressure.

Note that the diamagnetic trap, as described by Eq. (1), requires a large gradient in  $B^2$  to balance gravity. The large dimensions of the magneto-gravitational trap, combined with easily attained magnetic fields and the diamagnetic susceptibilities of available vacuum-compatible electrically insulating particle materials, form an extremely weak potential well. While loading a particle into the trap, an ac voltage is applied to two pole pieces, while the other two are kept isolated from the ac voltage to form a linear quadrupole ion (Paul) trap [41,42] for particles that have nonzero residual net charge. The Paul trap is much stronger than the diamagnetic trap, allowing particles to be successfully captured. A dc voltage, typically between 20 V and 40 V, is applied from the top to the bottom pole pieces to help counter gravity and center large particles in the trap (see Fig. 2). For particles in the size range used here (approximately 60  $\mu\text{m}$  diameter), the typical ac voltage amplitude is approximately 450 V oscillating at 300 Hz. Particles of this diameter are nearly the largest successfully

loaded in our trap; the limit is likely due to the conditional stability of the Paul trap [43].

The dc voltage across the top and bottom pole pieces is supplied from a 1-ppm digital-to-analog converter (DAC, Analog Devices AD5791). The DAC is floated to a voltage between  $-300$  V and 0 V using a modified stacking of Texas Instruments REF5010 high-voltage references [44] in steps of 5 V. The voltage reference circuit can be modified to allow for positive voltages as well. The DAC allows for fine tuning of the voltage and the resulting potential is estimated to be stable to  $< 3$  ppm.

After the particle is loaded into the hybrid Paul–magneto-gravitational trap, the Paul trap is turned off before pumping the system down to high vacuum. The ac voltage is slowly decreased while adjusting the dc voltage to keep the particle centered vertically in the magneto-gravitational trap. When the Paul trap is completely off, jumpers, indicated by the dashed lines in Fig. 2, are added to eliminate all of the high-resistance paths for the movement of image charges.

A mechanical roughing pump along with a turbomolecular pump achieve a pressure of  $10^{-7}$  Torr in the vacuum chamber. To eliminate vibrations from these pumps, they are closed off from the chamber and turned off while pumping continues with an ion-sputter pump. A pressure of approximately  $10^{-7}$  Torr is maintained for all measurements reported. The natural damping rate does not decrease in tests with a further reduction in pressure, so we do not pursue ultrahigh vacuum.

## B. Table stabilization

Changes in the tilt of the optical table cause the equilibrium position of the levitated particle to shift. In the weak direction of the trap, very small changes in tilt can have a significant effect on the equilibrium position. For small tilts, the shift in equilibrium position is described by

$$\Delta z_{eq} \approx \frac{g}{\omega_0^2} \Delta\theta. \quad (2)$$

To avoid any large shifts in the equilibrium position, a method is developed to feedback stabilize the relative tilt of the optical table in real time [45]. The tilt of the table is measured with an ultrahigh-sensitivity tiltmeter (Jewell Instruments A603-C) and read on a computer. Using two mass-flow controllers, air is added or removed from one side of the floating table to keep it level.

Without stabilization, the relative tilt of the table can change by  $\pm 150$   $\mu\text{rad}$  or more. For a levitated particle with an axial oscillation frequency  $\omega_0/(2\pi) = 2$  Hz, this corresponds to a  $\pm 9.5$ - $\mu\text{m}$  shift in equilibrium, which is much larger than the typical oscillation amplitudes due to environmental vibrations. With feedback stabilization, this value can be 200 times smaller, resulting in only negligible shifts in equilibrium position.

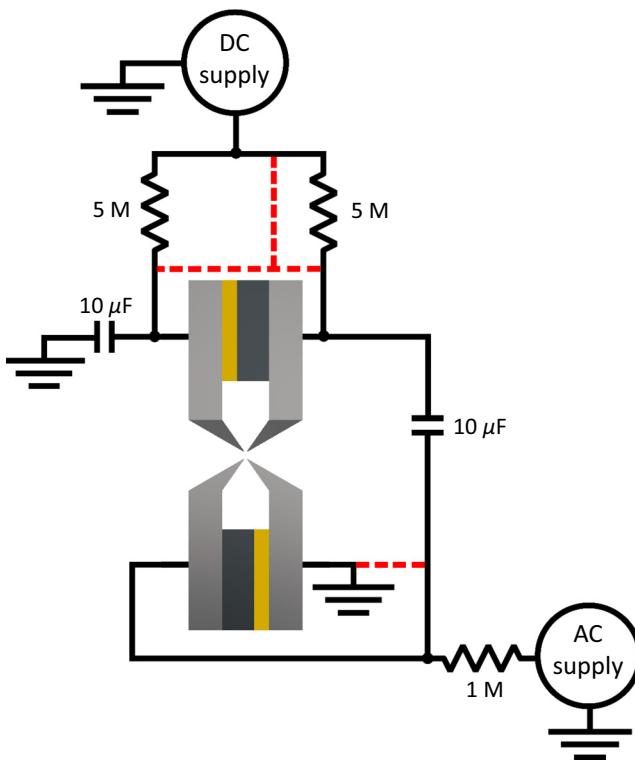


FIG. 2. A simple schematic of the circuit used to apply the ac voltage for the Paul trap and the dc bias to help counteract gravity. A 50 s filter prevents the addition of high-frequency noise. The red dashed lines indicate where jumpers are added to prevent image-charge currents from going through high-resistance paths when the Paul trap is not in use. The pole pieces are electrically isolated using polyether ether ketone (PEEK) film, indicated in gold with exaggerated thickness. The PEEK is not visible in Fig. 1.

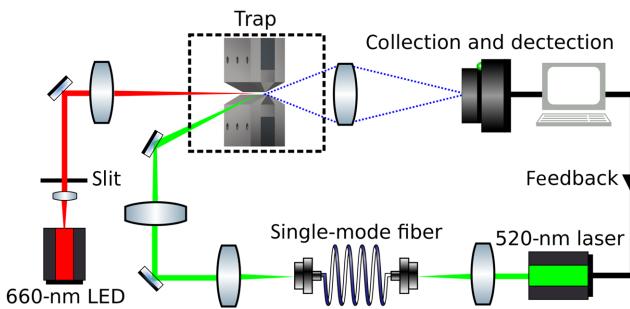


FIG. 3. Light from a pulsed 660-nm light-emitting diode (LED) illuminates a slit that is imaged onto the particle, as indicated by the red path. The control laser beam, indicated by the green path, originates from a 520-nm diode laser. Radiation pressure from the laser applies a force that heats or cools the center-of-mass motion of the particle, depending on the phase of the drive relative to the motion of the particle. The scattered green light is blocked by a long-pass filter, while the scattered illumination light is collected and imaged onto a CMOS camera. The images are analyzed in real time to apply the feedback drive to the particle.

### C. Real-time image analysis and feedback cooling

The particle is stroboscopically illuminated using a 660-nm light-emitting diode (LED) with a repetition rate of 100 Hz and a pulse duration of 1 ms. As shown in Fig. 3, light from the LED is collimated using an aspheric lens

and passed through a 100- $\mu\text{m}$  slit. The slit is imaged onto the particle and magnified to illuminate the entire region of interest. The particle is imaged onto the CMOS camera with a 0.09-NA telecentric objective (Mitutoyo 375-037-1). All recorded images (or frames) are 256  $\times$  128 pixels, corresponding to a field of view of 300  $\times$  150  $\mu\text{m}$ . The camera frame rate is 100 Hz, with an exposure time of 2 ms. The LED pulse is initiated 10  $\mu\text{s}$  after the camera exposure starts.

As shown in Fig. 4(a), the illuminated microsphere appears as a dark disk in each frame. The microsphere diameter of approximately 60  $\mu\text{m}$  corresponds to a diameter of approximately 60 pixels in each frame. In the data that we analyze, the microsphere never leaves the frame.

The frames from the CMOS camera are analyzed in real time to track the motion of the particle. Each frame is thresholded to isolate the particle and the apparent center-of-mass is calculated. The movement from frame to frame is used to calculate the velocity of the particle, which is then passed through a second-order infinite-impulse-response (IIR) peak bandpass filter with a bandwidth of 1.0 Hz, centered at 1.5 Hz, to eliminate high-frequency noise.

The measured and filtered velocity of the particle is used to damp and cool the center-of mass motion of the particle via algorithmic feedback [46,47]. A damping force is applied to the particle using the radiation pressure of the light from a modulated 520-nm diode laser with an average power of 1 mW and a beam waist of approximately 18  $\mu\text{m}$ .

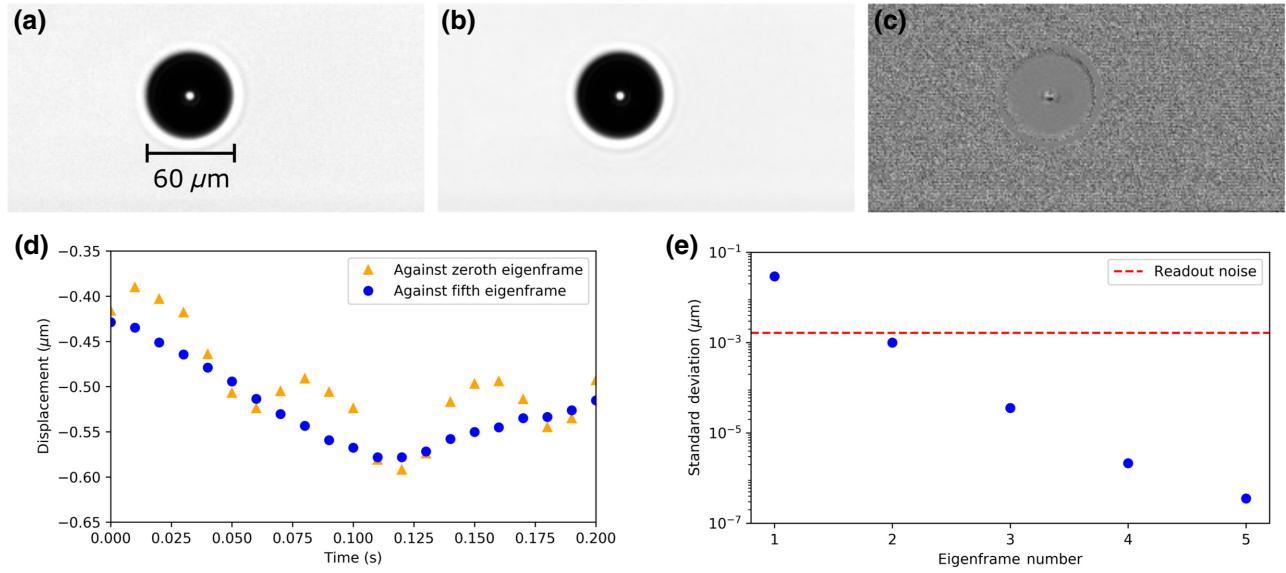


FIG. 4. (a) Raw data: a dark microsphere on a light background with an approximate scale. (b) The fifth eigenframe, built by averaging frames as described in Sec. III. Note the smoothing of the background features in comparison to the raw data in (a). (c) The difference in pixel values between the zeroth eigenframe, shown in (a), and the fifth eigenframe, shown in (b), scaled by a factor of 9 to make the differences more visible. Note that gray pixels denote small differences; dark and light pixels represent the fifth eigenframe having a darker or brighter pixel than the zeroth eigenframe, respectively. (d) The displacement comparison between correlation against the zeroth and fifth eigenframes. Note in particular the discontinuities appearing throughout the zeroth-eigenframe displacement time series. (e) The standard deviation of the displacement differences between eigenframes  $n$  and  $n - 1$ .

Light from this control laser that scatters off the particle is blocked by a long-pass filter before the objective lens used for imaging.

### III. OFFLINE IMAGE ANALYSIS

If limited to a resolution of 1 pixel, we can only track the microsphere's position to about 1  $\mu\text{m}$ . Sophisticated image-analysis techniques exist, however, that measure displacement versus some reference frame to a small fraction of a pixel by incorporating *all* pixel data from each frame. While the image analysis for feedback must be completed in real time, a more accurate but more computationally intensive algorithm can be used for offline analysis of the data. As our first approach, we adopt the cross-correlation function `REGISTER_TRANSLATION()`, available in the SCIKIT-IMAGE PYTHON package [48,49], to determine the displacement of the particle relative to the first recorded frame of data (which we refer to as the “zeroth eigenframe”). While this approach largely seems to work well, we note jump discontinuities in the microsphere displacement versus time, as can be seen in Fig. 4(d).

We attribute these discontinuities to noise in the zeroth eigenframe. As this frame is chosen arbitrarily, we anticipate that any other choice of reference frame will result in similar displacement discontinuities. To minimize the effects of this noise, we devise an “eigenframe” approach that proceeds as follows: we first compute the translation in  $z$  and  $y$  of each frame against the zeroth eigenframe in the spatial domain using `REGISTER_TRANSLATION()`. These spatial translations are used to compute the corresponding phase shifts in the Fourier domain, so that each image can be overlaid onto the zeroth eigenframe. After overlaying all images atop the zeroth eigenframe, we then compute the average value of each pixel and call the resulting frame the “first eigenframe.” The images are overlaid and averaged in the Fourier domain to avoid information loss when an image is translated by a noninteger number of pixels in the position domain. The averaging smears out the noise present in the zeroth eigenframe and smooths the displacement data, as illustrated in Fig. 4(d) [compare also Figs. 4(a) and 4(b); the difference between them is illustrated in Fig. 4(c)]. We then refine the translation values by correlating each frame against a translation of the first eigenframe (again in the Fourier domain) to the inferred particle location. The resulting translations may be used to build a second eigenframe in a manner analogous to building the first and this process can be iterated as many times as we like.

To further refine our position resolution, we modify `REGISTER_TRANSLATION()` to fit a slice of the correlation surface through the peak in the  $z$  direction to a quadratic function using SciPy’s `OPTIMIZE.CURVE_FIT()` function. Locating the peak of this quadratic gives a finer estimate

of the particle translation between each frame and the eigenframe.

To demonstrate that the translation values converge with the eigenframe number, denote by  $d_n(t_i)$  the axial displacement of the microsphere at time  $t_i$  when correlated against eigenframe  $n$  ( $n = 1, 2, \dots, 5$ ). We compute the standard deviation of  $d_n(t_i) - d_{n-1}(t_i)$  over all  $t_i$  [see Figs. 4(c) and 4(e)]. Incredibly, the position differences quickly reach a standard deviation of less than 1 nm, thus falling well below the physical-resolution limit. After repeating this eigenframe approach five times, the standard deviation of the change in displacements drops to below 1 pm. As this is far below other sources of displacement error in our experiment and demonstrates rapid convergence of position values, the fifth eigenframe is the final one we compute.

### IV. ACCELERATION MEASUREMENT

We measure the acceleration sensitivity of the trapped particle by examining the effect of movement of the pneumatically isolated optical table (on which the trap and optics are mounted) on the particle. In the frame of the laboratory, consider the displacement of the particle in the axial direction,  $z$ , and the displacement of the camera,  $z_0$ . The camera directly measures  $z' = z - z_0$ . The equation of motion for the particle in the laboratory frame is then

$$\ddot{z} + \Gamma\dot{z} + \omega_0^2 z = \Gamma\dot{z}_0 + \omega_0^2 z_0, \quad (3)$$

where  $\Gamma$  is the damping rate and  $\omega_0$  is the resonant angular frequency of the particle.

The displacement of the optical table, for example, from vibrations, can be written as an integral over all frequencies,

$$z_0(t) = \int_{-\infty}^{\infty} d\omega' A_0(\omega') \sin[\omega't + \phi(\omega')], \quad (4)$$

where  $A_0$  is the strength of the drive as a function of frequency. The phase  $\phi(\omega')$  has no impact on the power spectra of the linear systems analyzed here.

After substituting Eq. (4) into Eq. (3), we can take the Fourier transform of Eq. (3). Simplifying the resulting expression, we find that the magnitude of the transfer function is [50]

$$\left| \frac{Z'(\omega)}{A_0(\omega)} \right| = \frac{\omega^2}{[(\omega_0^2 - \omega^2)^2 + \Gamma^2 \omega^2]^{1/2}}, \quad (5)$$

where  $Z'(\omega)$  is the Fourier transform of the motion of the particle with respect to the camera.

The minimum acceleration that can be detected for an oscillator in thermal equilibrium is [51]

$$S_a^{1/2} = \sqrt{\frac{4k_B\Gamma T}{m}}, \quad (6)$$

where  $k_B$  is Boltzmann's constant,  $m$  is the mass,  $\Gamma$  is the damping rate of the oscillator for a particular degree of freedom under investigation, and  $T$  is the temperature of the center-of-mass motion of the same degree of freedom. The results presented in this paper are obtained using the axial motion. Feedback cooling at best keeps  $\Gamma T$  constant, damping out potentially long-lived transients without a significant impact on sensitivity [52].

### A. Results

A 60-μm-diameter borosilicate microsphere, shown in Fig. 4(a), is levitated with a dc bias across the vertical gap of the magneto-gravitational trap of -37.2313 V. Using this diameter, measured using the calibrated CMOS camera (described below) the mass of the microsphere is calculated to be  $m = 2.5 \times 10^{-10}$  kg (assuming a typical density for borosilicate glass of 2230 kg/m<sup>3</sup>). Note that the microsphere mass is not needed for calibrating the system response as an accelerometer; it is only used for calculating the magnitude of the thermal noise. Throughout the measurements, a vacuum pressure of 10<sup>-7</sup> Torr is maintained and the tilt of the optical table is stabilized to within ±0.75 μrad. With the measured resonant frequency of the microsphere, Eq. (2) yields the result that the equilibrium position of the particle is stabilized to within ±60 nm.

Before acquiring acceleration data, the system magnification, a critical calibration parameter, is measured. By analyzing the recorded image of a USAF1951 calibration target (Edmund Optics 58-198) through the system optics, the scaling factor  $S_c = 1.15$  μm per pixel is determined. For frequency calibration, the digital delay generator used to control all of the timing in the experiment is tied to a rubidium frequency standard (Stanford Research Systems, Inc. FS725). The on-off times of the LED, the start-stop time of each frame acquired on the CMOS camera (recorded and used for cooling), and the triggering of the data acquisition system for voltage and tilt monitoring are all controlled by pulse outputs of the delay generator.

In order to eliminate any free parameters of the system, the transient response of the microsphere is measured after a small excitation in the axial direction, shown in Fig. 5. The resonant frequency of the particle is measured to be  $\omega_0/(2\pi) = 1.75$  Hz. While feedback cooling the center-of-mass motion of the microsphere, the damping rate is measured to be  $\Gamma = 6.26 \times 10^{-2}$  s<sup>-1</sup>.

For comparison, we also place an L-4C geophone (Sercel, Inc. [53]) on the optical table. The sensitivity of this instrument and other critical parameters are given by the manufacturer. We add an additional amplification circuit

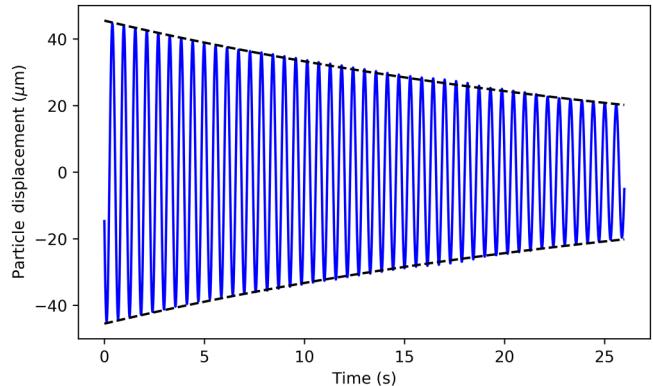


FIG. 5. The transient motion of the particle after excitation with feedback cooling applied. Analysis of the motion gives an axial ( $z$ ) oscillation frequency of  $\omega_0/(2\pi) = 1.75$  Hz and the decay rate is  $\Gamma = 6.26 \times 10^{-2}$  s<sup>-1</sup> (black dashed lines). The amplitude range plotted and analyzed is chosen so that vibrational noise is negligible.

with a gain of approximately 180 to boost the signal before digitization (modeled after that in Ref. [54]). The data acquired with the geophone are started synchronously with the camera.

The response of the particle to movement of the optical table is tested by applying a 5 Hz sinusoidal drive with a surface transducer, oriented to push the table in the axial direction. While applying this external drive, a set of five 60-s measurements are recorded. Each measurement consists of 6000 images from the CMOS camera, which are analyzed with the algorithm described above. The averaged spectrum of the resulting particle acceleration over five data sets is shown in Fig. 6(a). For comparison, the measured acceleration of the test mass of the geophone is shown on the same plot. The vibration between 1 Hz and 2 Hz is believed to be a resonance of the optical table and overlaps with the resonance of the particle, causing an on-resonance excitation illustrated by the large peak at 1.75 Hz. The transverse and vertical motion of the particle are at 10.2 Hz and 15.2 Hz, respectively, likely creating peaks at the corresponding frequencies due to misalignments in the system.

To calculate the acceleration of the environment from the measured acceleration of the particle and geophone test masses, the harmonic oscillator response [Eq. (5)] of each is divided out of the Fourier spectrum of the test-mass acceleration, resulting in the acceleration shown in Fig. 6(b). The two spectra match over a broad frequency range of approximately 14 Hz. The amplitudes of the two peaks at the external drive frequency, 5 Hz, are within 3% of each other, confirming the calibration between the two systems. Above 14 Hz, the geophone response diverges from the particle response due to increasing noise in the particle-acceleration measurement.

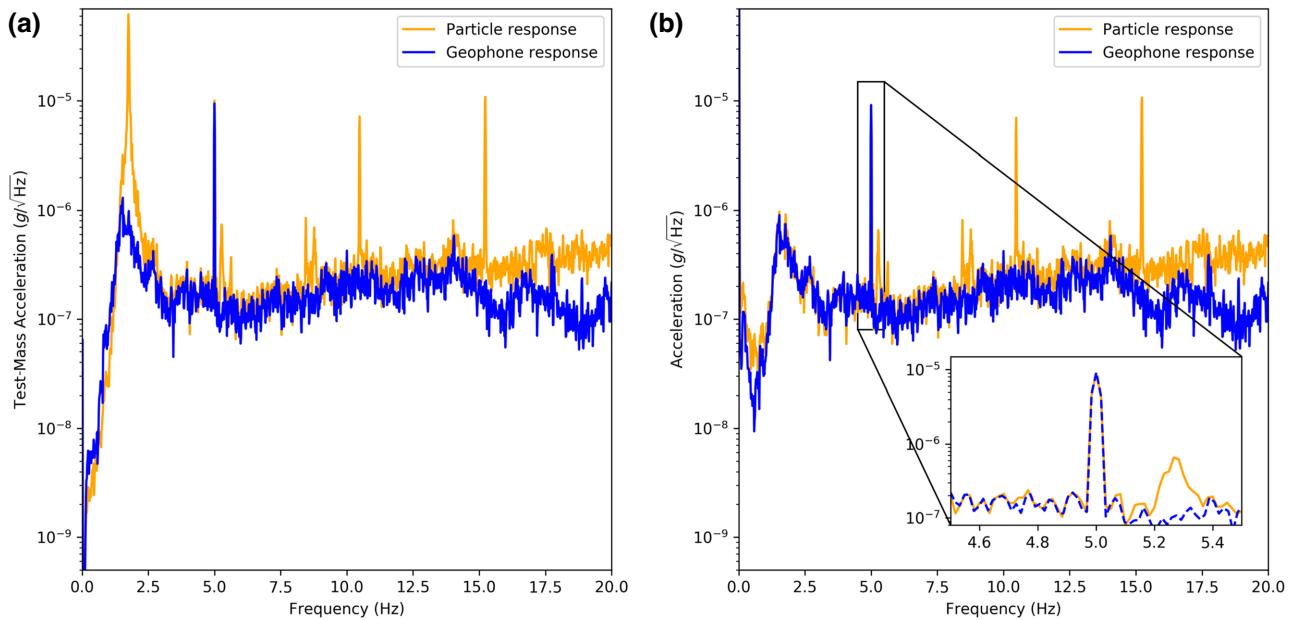


FIG. 6. (a) A comparison of the test-mass acceleration of the particle and geophone. A 5-Hz drive is used to verify the calibration. The large peak at 1.75 Hz is due to the axial motion and the peaks at 10.5 Hz and 15.2 Hz are due to the transverse and vertical motions of the particle, respectively. (b) The particle and geophone responses from (a) divided by their harmonic oscillator responses. The amplitude of the peaks at 5 Hz differ from each other by less than 3%. The blue line in the inset is dashed so that both peaks are visible.

### B. Noise analysis

The noise contributions for both the geophone and particle are plotted in Fig. 7 along with the (undriven) acceleration of the table as determined by the geophone and levitated particle.

The noise of the L-4C geophone and its accompanying amplification circuit can be broken down into four terms [54]. As displacement-equivalent noise sources, they are as follows:

$$n_{\text{therm}}(\omega) = \sqrt{\frac{4k_B T \omega_0}{m Q}} \frac{1}{\omega^2}, \quad (7)$$

$$n_{\text{Johnson}}(\omega) = \frac{\sqrt{4k_B T R(\omega)}}{G(\omega)}, \quad (8)$$

$$n_{\text{voltage}}(\omega) = \frac{N_V(\omega)}{G(\omega)}, \quad (9)$$

$$n_{\text{current}}(\omega) = \frac{N_A(\omega) R(\omega)}{G(\omega)}. \quad (10)$$

The thermal noise of the damped harmonic oscillator is given by Eq. (7), where  $T$  is the temperature of the oscillator,  $m$  is the mass,  $\omega_0$  is the resonant angular frequency, and  $Q$  is the quality factor. The thermal fluctuations are

approximately  $2.4 \times 10^{-11} g/\sqrt{\text{Hz}}$  for the geophone with the parameters listed in Table I. The Johnson noise of the geophone coil is given by Eq. (8), where  $R$  is the real part of the complex impedance of the coil, given by

$$R(\omega) = R_c + \frac{i S_g^2 \omega}{\omega_0^2 - \omega^2 + i \Gamma \omega}, \quad (11)$$

and where  $R_c$  is the resistance of the coil,  $S_g$  is the sensitivity of the oscillator, and  $\Gamma$  is the damping rate of the oscillator. The harmonic oscillator response  $G$  is given by

$$G(\omega) = \frac{\omega^3 S_g}{\sqrt{(\omega_0^2 - \omega^2)^2 + \Gamma^2 \omega^2}}. \quad (12)$$

The input voltage and current noise of the amplification circuit are given by Eqs. (9) and (10), respectively.  $N_V$  is the input-referred voltage noise of the OPA188 operational amplifier [55] used in the amplification circuit, assumed to be constant over the frequency range of interest. The current noise of the amplification circuit is negligible compared to all other noise sources for the geophone. The noise sources add in quadrature to give the total noise of the geophone system  $n_{\text{total},g}$  as

$$n_{\text{total},g}^2 = n_{\text{therm}}^2 + n_{\text{Johnson}}^2 + n_{\text{voltage}}^2 + n_{\text{current}}^2. \quad (13)$$

The noise of the levitated-particle accelerometer has two contributions. First, the thermal noise of the particle

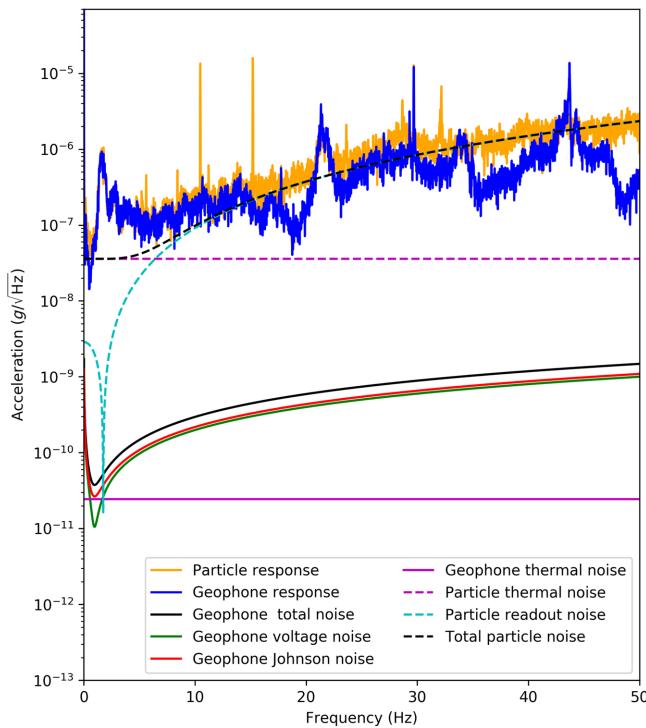


FIG. 7. The particle and geophone test-mass acceleration spectra divided by their harmonic oscillator responses with no drive over the full frequency range measured. Contributions to the noise for the geophone and particle are also shown.

is given by Eq. (7), where the parameters are now those of the particle (given in Table I). With feedback cooling applied, we measure the damping rate to determine the  $Q$  to be 175 (reduced from approximately  $10^4$  without feedback) but the effective temperature may be significantly reduced relative to the ambient temperature. An upper limit of the acceleration noise is conservatively estimated to be  $3.6 \times 10^{-8} \text{ g}/\sqrt{\text{Hz}}$  using the particle signal near its minimum (around 0.5 Hz) by assuming that the signal at this

frequency is entirely due to noise, not the targeted acceleration of the environment. Assuming this noise to be entirely thermal in origin, the upper limit on the effective temperature associated with the damping of the particle is 9 K.

The second noise source is readout noise from the camera and image analysis, which is expected to be dominated by shot noise of the light and camera noise within each individual image, since most noise is averaged out of the eigenframe. To place a lower bound on the readout noise, we consider the precision to which a diffraction-limited spot can be determined in the presence of shot noise. This is described by

$$\langle (\Delta z)^2 \rangle \geq \frac{\sigma_{\text{PSD}}^2}{N}, \quad (14)$$

where  $\sigma_{\text{PSD}}$  is the standard deviation of the point-spread function (PSF) of the imaging optics and  $N$  is the number of photons collected—or in our case, blocked—by the particle.

For the lower bound on the noise, the PSF is calculated for a diffraction-limited spot. The standard deviation is  $\sigma_{\text{PSD}} = 0.225\lambda/\text{NA}$ , where  $\lambda$  is the wavelength of the scattered light and NA is the numerical aperture of the collection objective. For our system,  $\sigma_{\text{PSD}} = 1.65 \mu\text{m}$ . The number of photons is estimated from the brightness of the illumination in the CMOS camera and the number of pixels blocked by the  $30\text{-}\mu\text{m}$ -radius particle, resulting in an uncertainty in the location of the point of  $\langle (\Delta z)^2 \rangle^{1/2} \approx 0.4 \text{ nm}$ . Given that the particle is much larger than the diffraction limit, the readout noise is expected to be significantly higher than this.

From 14 Hz to 50 Hz, the levitated-particle acceleration spectrum is not vibration limited. Instead, it follows the expected shape of readout noise, which is a white-noise source (in displacement) with the harmonic oscillator response divided out. We fit the spectrum in the frequency

TABLE I. The critical parameters for the amplified L-4C geophone and levitated-particle accelerometers. The geophone values are from the data sheets of the L-4C geophone and the OPA188 operational amplifier used in the geophone amplifier.

Parameter	Description	Geophone value	Particle value
$T$	Temperature	300 K	9 K
$\omega_0/2\pi$	Resonant frequency of oscillator	0.97 Hz	1.75 Hz
$m$	Mass of oscillator	0.957 kg	$2.5 \times 10^{-10} \text{ kg}$
$Q$	Quality factor of oscillator	1.845	175
$S_g, S_c$	Sensitivity (note different units)	281.7 Vs/m	1.15 $\mu\text{m}$ per pixel
$R_c$	Resistance of geophone coil	5546 $\Omega$	
$S_g$	Sensitivity of geophone oscillator	281.7 Vs/m	
$G_a$	Gain of amplification circuit	180.2	
$N_V$	Input-referred voltage noise	8.8 nV/ $\sqrt{\text{Hz}}$	
$N_A$	Input-referred current noise	Negligible	
$I_0$	Energy density of scattered light		$2.76 \times 10^{-4} \text{ J/m}^2$
$\Delta z$	Readout noise		$160 \text{ pm}/\sqrt{\text{Hz}}$

range of 35 Hz to 50 Hz to find the apparent readout noise of  $\Delta z = 1.6$  nm per image or  $160 \text{ pm}/\sqrt{\text{Hz}}$ , reasonably above the point-source diffraction limit. The two noise sources add in quadrature, so that the total noise of the particle response is

$$n_{\text{total},p}^2 = n_{\text{therm}}^2 + (\Delta z)^2. \quad (15)$$

We associate the readout noise with the particle-position uncertainty of each image, as computed by the eigenframe approach (presented in Sec. III) in the presence of shot noise and camera noise.

## V. DISCUSSION AND CONCLUSIONS

We experimentally demonstrate levitation of a  $2.5 \times 10^{-10}$  kg borosilicate microsphere in high vacuum. This system shows great promise for ultrahigh acceleration sensitivities without the need for large masses or cryogenics. Feedback cooling reduces the transient decay time of the system, while also cooling the center-of-mass motion. With no free parameters in the calibration, the acceleration determined from the apparent motion of the particle both follows that of a commercial geophone below 14 Hz and matches the response to an external drive within 3% at 5 Hz, despite the particle having a mass that is  $4 \times 10^9$  times smaller than the test mass in the geophone.

The sensitivity limit in the levitated-particle accelerometer is estimated to be below  $3.6 \times 10^{-8} \text{ g}/\sqrt{\text{Hz}}$  at low frequencies, limited by either the vibrations being measured or thermal noise associated with damping at 9 K; a quieter environment would be needed to unambiguously determine the limiting factor and the effective temperature. Much lower center-of-mass temperatures have been reached with trapped particles in other systems, so there is room for significant improvement. For example, feedback cooling to  $140 \mu\text{K}$  of a  $1.5\text{-}\mu\text{m}$ -diameter silica microsphere (with a 7.5-Hz oscillation frequency) in a magnetogravitational trap [33] and to  $50 \mu\text{K}$  of a  $10\text{-}\mu\text{m}$ -diameter silica microsphere (with a 65-Hz oscillation frequency) in an optical trap [34] is demonstrated. Lower center-of-mass temperatures in the current system could result in a sensitivity improvement of at least an order of magnitude and might be reached by using a more precise real-time image-analysis system for feedback cooling. Further improvements are possible using an even lower center-of-mass oscillation frequency or a higher camera frame rate. By increasing the natural  $Q$ , an improvement in sensitivity of several orders of magnitude could be achieved. A complete accelerometer based on the reported system could be much more sensitive than MEMS or nanoelectromechanical systems (NEMS) devices, while also being simpler and lighter than precision accelerometers based on cold atoms. This high-sensitivity self-calibrating system with negligible test mass may be particularly valuable for space-based accelerometry at low frequencies.

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