# Thermodynamic, Structural, and Piezoelectric Properties of Adatom-Doped Phosphorene and Its Applications in Smart Surfaces

Lou Li,<sup>1</sup> Huiying Cao,<sup>1</sup> Bo Xu,<sup>1</sup> Junkai Deng<sup>1</sup>,<sup>1,\*</sup> Jingran Liu,<sup>2</sup> Yilun Liu,<sup>2</sup> Xiangdong Ding,<sup>1</sup> Jun Sun,<sup>1</sup> and Jefferson Zhe Liu<sup>3,†</sup>

 <sup>1</sup> State Key Laboratory for Mechanical Behavior of Materials, Xi'an Jiaotong University, Xi'an 710049, China
 <sup>2</sup> State Key Laboratory for Strength and Vibration of Mechanical Structures, School of Aerospace Engineering, Xi'an Jiaotong University, Xi'an 710049, China

<sup>3</sup> Department of Mechanical Engineering, The University of Melbourne, Parkville, VIC 3010, Australia

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Engineering the surface morphology is an effective way to obtain specific functionalities in applications of smart surfaces. Developing two-dimensional (2D) smart materials, which can undergo morphology changes under appropriate external stimuli, is a promising route to pursue for smart-surface design. In the work presented here, using density-functional-theory calculations, we systematically study the thermodynamic stability, crystal structure, and piezoelectric properties of black phosphorene (black P) doped with metallic atoms on one side with different concentrations. Particularly, Li-doped black P (P<sub>4</sub>Li<sub>2</sub>) has a  $d_{31}$  value of 6.28 pm/V, which is at least 4 times larger than that of any other 2D piezoelectric material. Via finite-element-method simulations, we show a P<sub>4</sub>Li<sub>2</sub>-based prototype design for obtaining a surface-morphology change under a vertical electric field. The surface swelling pattern can be detected by human fingers with an appropriate design of the geometry. This demonstrates the promise of 2D piezoelectric materials for use in smart-surface applications.

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## I. INTRODUCTION

Smart surfaces, which are designed to exhibit certain functionalities and performance under appropriate external stimuli, have attracted significant interest in recent years [1–7]. Engineering the surface topography is a popular and effective approach to providing some desirable functionalities [8], such as wettability [9], adhesion [10], control of aerodynamic drag [11], and molecular adsorption [12]. The design of surface topographies that are responsive to external stimuli holds great potential for applications such as tactile displays [13], controllable optical reflection [14], and reversible control of interface properties [9,10,12]. There is a growing demand for research into finding appropriate materials for use in the design of such smart surfaces.

Two-dimensional (2D) actuation and active materials are liable to exhibit shape or morphology changes under external stimuli [15–18]. Using 2D actuation and active materials in smart-surface design is a natural and promising solution. There are several advantages. First, 2D materials are atomically thin. Advances in assembly technology in the past few years allow us to integrate different 2D materials in a layer-by-layer manner, producing large-area thin-film structures [19–21], which could be suitable for smart-surface applications. Second, 2D materials are often mechanically flexible and robust [22–25]. Third, through surface functionalization, the properties of 2D materials can be designed and significantly improved [15,26]. Among 2D actuation and active materials, 2D piezoelectric materials have received the most research attention [27–30].

If we were to adopt the popular layer-by-layer heterostructures to integrate 2D piezoelectric materials with electrodes (such as graphene), the piezoelectric coefficients  $d_{33}$ ,  $d_{31}$ , and  $d_{32}$  would determine the actuation and active performance under a vertical electric field. However, the intrinsic displacement in the normal direction is unlikely to be large enough, due to the nanosized thickness and the finite value of  $d_{33}$ . Another strategy is to utilize the elastic buckling displacement in the vertical direction that occurs when the in-plane strain is above some threshold value. To achieve a detectable surface-morphology change, i.e., a larger buckling displacement, it is highly desirable to develop 2D piezoelectric materials with large piezoelectric coefficients  $d_{31}$  and  $d_{32}$ . Unfortunately, the available intrinsic 2D piezoelectric materials, such as GaP, InP, and GaInSe<sub>2</sub>, have limited  $d_{31}$  and  $d_{32}$  in the range of 0.1–0.5 pm/V [31,32].

<sup>\*</sup>junkai.deng@mail.xjtu.edu.cn

<sup>&</sup>lt;sup>†</sup>zhe.liu@unimelb.edu.au

It has been proposed to introduce piezoelectric effects into intrinsically nonpiezoelectric graphene through atomic adsorption. Graphene has a 2D hexagonal structure with inversion symmetry and thus is not intrinsically piezoelectric. This inversion symmetry can be broken by the adsorption of atoms on the surface of graphene on only one side. This leads to piezoelectricity with piezoelectric coefficients  $d_{31}$  and  $d_{32}$ . Ong and Reed investigated the piezoelectricity of graphene doped with selected adatoms and obtained magnitudes of the piezoelectric coefficient  $d_{31}$  of around 0.3 pm/V [26]. Noor-A-Alam *et al.* found that codecoration of silicene with H and F generated a maximum  $d_{31}$  as high as 1.66 pm/V [33].

In this paper, we employ first-principles densityfunctional-theory (DFT) calculations to investigate the crystal structure, formation energy, and piezoelectric properties of black phosphorene (black P) with adatoms consisting of all metallic elements in the top three rows of the Periodic Table on its top surface, with a broad range of concentrations from  $P_{48}X_1$  to  $P_4X_2$ . The adsorptioninduced piezoelectric coefficient  $d_{31}$  varies from 0.12 to 6.28 pm/V. Notably, Li-doped black P has the largest  $d_{31}$ (6.28 pm/V), at least 4 times larger than that of any other 2D material. An in-depth analysis suggests that this considerable  $d_{31}$  value can be attributed to the low elastic modulus  $C_{11}$ . Using this material, we examine a prototypical design of surface-morphology engineering using finiteelement-method (FEM) simulations. This demonstrates the promise of 2D piezoelectric materials in smart-surface applications.

### **II. METHODS**

Our first-principles calculations are performed based on DFT, as implemented in the Vienna *ab initio* simulation package (VASP). Projector-augmented-wave pseudopotentials and the Perdew-Burke-Ernzerhof (PBE) exchangecorrelation functional are adopted. For all calculations, the plane-wave cutoff is set at 800 eV. A Monkhorst-Pack gamma-centered k-point grid of dimensions  $25 \times 15 \times 1$ is adopted for the black-P unit cell. The 2D black-P film is placed in the x-y plane. The supercell size in the zdirection is fixed at 20 Å to avoid interactions between the black-P layers and their periodic images. In all cases, the atoms are fully relaxed in all directions until the force on each atom is less than 0.001 eV/Å, ensuring accuracy of the calculated piezoelectric strain. At 0.001 eV/Å, we observe a good linear relationship between the piezoelectric strain and the electric field strength applied. But at 0.01 eV/Å, a nonlinear relationship is obtained. A van der Waals (vdW) correction using the Tkatchenko-Scheffler method with iterative Hirshfeld partitioning is also applied to make a comparison.

#### **III. RESULTS AND DISCUSSION**

We first investigate a low-concentration adatomphosphorene system with one adatom in a  $4 \times 3$ orthorhombic phosphorene supercell (containing 48 P atoms), which we refer to as  $P_{48}X_1$ . Four types of metallic atom from the first three rows of the Periodic Table, i.e., alkali metals, alkaline-earth metals, transition metals, and other metals, which are listed at the top of Fig. 1, are selected. In the inset of Fig. 1, the most stable adsorption site is the hollow site (H site), where the adatom shifts away from the center of the hexagonal cell and forms three bonds with nearby P atoms. The results are consistent with previous results [34]. To examine the stability of the relaxed structure, we calculate the formation energy per adatom  $E_f$ , which is presented in the form of bar plots in Fig. 1. The formation energy per adatom is defined as  $E_f = E_a - E_c$ . Here,  $E_a$  is the adsorption energy, defined as  $E_a = [E_{P_n X_m} - E_{P_n} - mE_X]/m$ , where  $E_{P_n X_m}$  is the total energy of the adatom-doped black-P supercell, with nphosphorene atoms and *m* metallic adatoms,  $E_{P_n}$  is the total energy of the pristine black P, and  $E_X$  is the energy of the isolated metal atom.  $E_c$  is the bulk cohesive energy of metal X, for which we use the experimental values given in Ref. [35]. Our calculated results are close to those of previous work [34], in which some metal adatoms from the first three rows of the Periodic Table (Li, Na, Mg, Al,



FIG. 1. Formation energy per adatom  $E_f$  of  $P_{48}X_1$  calculated using DFT with the PBE functional. All metallic adatoms in the first three rows of the Periodic Table are examined, as shown at the top of the figure. All alkali adatoms have a negative  $E_f$ . For transition metals, only Ni, in the middle of the Periodic Table, have a negative  $E_f$ . The inset shows the most stable adsorption site, the hollow site.

Cr, Fe, Co, and Ni) were studied. Most of the alkali and alkaline-earth metals have a negative  $E_f$  value, with only one exception, Mg. For transition metals, only Ni shows a negative  $E_f$  value. A negative  $E_f$  value indicates that the adatom-doped black P is thermodynamically stable against phase separation into a black-P monolayer and metallic clusters.

Adatom-phosphorene systems with higher concentrations of adatoms, namely one or two adatoms per phosphorene unit cell (referred to as  $P_4X_1$  and  $P_4X_2$ , respectively), are also investigated. For  $P_4X_1$ , the most stable adsorption site is the H site. All of the transition-metal adatoms (except Cu and Zn) are located at the center of the hollow site and form four bonds with neighboring P atoms. Other cases resemble the  $P_{48}X_1$  system, where the adatom shifts away from the center. For  $P_4X_2$ , the adsorption geometry is more complicated. There are two hollow sites on one side of the black-P unit cell: the (0.0, 0.0) and (0.5, 0.5) sites in the x-y plane, as illustrated in Fig. 2. In most cases, the two adatoms are located at these two sites. The alkali and alkaline-earth metal adatoms form two layers, as shown in Fig. 2(b). But some transition-metal adatoms (Fe, Co, and Ni) form a single layer on top of the phosphorene. This kind of adsorption causes the ratio of the lattice constants b and a to become close to one. For example, pristine phosphorene has b/a = 1.40, whereas phosphorene doped with Fe, Co, and Ni has b/a = 1.05, 1.04, and 1.05, respectively. For atoms on the right of the Periodic Table (Zn, Al, and Ga), Fig. 2(c) shows that the most stable site is on top of a P atom (T site).

Figure 2(a) shows the results for  $E_f$  of  $P_4X_1$  and  $P_4X_2$ . Most of the alkali and alkaline-earth metals have a negative



FIG. 2. (a) Formation energy per adatom  $E_f$  of  $P_4X_1$  and  $P_4X_2$ . All metallic adatoms in the first three rows of the Periodic Table are tested. The inset shows an enlarged view for the cases of Li and Na. (b) Crystal structure of  $P_4X_2$  with adatoms on two hollow sites. (c) Crystal structure of  $P_4X_2$  with adatoms on two top sites. Most alkali metals have a negative  $E_f$ . With an increase in concentration,  $E_f$  for transition-metal adatoms, Al, and Ga tends to shift to more negative values.

 $E_f$  for both compositions. But for K and Ca, the crystal structure of  $P_4X_2$  exhibits drastic changes, and the black-P lattice backbone is completely broken. For the transition metals and for Al and Ga,  $E_f$  shows a trend toward a more negative value with an increase in concentration. In some cases,  $E_f$  changes from a positive to a negative value, which is not often seen in alloy systems. As such, we have 14 cases with a negative  $E_f$  for  $P_4X_1$  and  $P_4X_2$ , whereas there are only five cases with a negative  $E_f$  for  $P_{48}X_1$ .

To examine the influence of vdW interactions on the calculated  $E_f$  values, we adopt the popular DFT–Tkatchenko-Scheffler (DFT-TS) scheme for the seven  $P_4X_2$  systems with a negative  $E_f$ . As expected, their  $E_f$  values become more negative, with a nearly constant change of -0.5 to -0.6 eV/adatom compared with the results obtained from the PBE functional. This trend is consistent with our previous study of gas adsorption in some zeolites [36]. DFT-TS calculations might identify more cases with a negative formation energy. However, it should be noted that vdW-DFT calculations tend to overcorrect for the contribution from vdW interactions [36]. Thus, in the following, we focus on the 14 thermodynamically stable cases identified from our PBE calculations.

Adatom adsorption on one side breaks the inversion symmetry of black P, generating an out-of-plane electric polarization and consequent piezoelectricity. We calculate the piezoelectric coefficients of those 14  $P_4X_1$  and  $P_4X_2$ cases. Figure 3 shows the in-plane piezoelectric strains  $\varepsilon_{11}$  and  $\varepsilon_{22}$  as functions of an applied electric field in the z direction. The electric field varies from -0.1 to 0.1 eV/Å for the seven  $P_4X_2$  systems; this range of values can be achieved in experiments [37]. Figures 3(a) and 3(b) depict a good linear relationship between the strain and the electric field strength. The strain piezoelectric coefficients  $d_{31}$  and  $d_{32}$  can then be determined from the slope. The calculated values of  $d_{31}$  and  $d_{32}$  for  $P_4X_1$  and  $P_4X_2$ are listed in Fig. 4 and Table I. The results for  $P_4X_2$ obtained from the DFT-TS calculations are also included in Table I.

Figure 4 compares the piezoelectric coefficients  $d_{31}$  of our materials with all previously reported values for 2D piezoelectric materials. Note that P<sub>4</sub>Li<sub>2</sub> has a coefficient  $d_{31}$  much higher than that of other 2D materials, such as adatom-doped graphene (0.002–0.3 pm/V) [26], graphene oxide (0.24 pm/V) [27], InP (0.39 pm/V) [31], and Hand F-codecorated silicene (0.22–1.66 pm/V) [33]. The filled and unfilled bars represent adatom-induced piezoelectric materials and intrinsic piezoelectric materials, respectively. We find that the extrinsic adatom-induced materials often have larger  $d_{31}$  values than the intrinsic piezoelectric materials. A high adatom concentration usually leads to a higher  $d_{31}$ , except for V and Co. Such a coverage-concentration dependence is consistent with results for the adatom-doped graphene system [26]. The piezoelectric anisotropy is also significant for both  $P_4X_2$ 



FIG. 3. In-plane piezoelectric strains in the x and y directions under an electric field applied perpendicular to the black-P plane (along the z direction) for  $P_4X_2$ .

and  $P_4X_1$ .  $P_4Li_2$  has the largest  $d_{31}/d_{32}$  ratio, with a value of 21.

Compared with the PBE results, our DFT-TS calculations show that the  $d_{31}$  values of  $P_4V_2$  and  $P_4Mn_2$  increase, while for the other  $P_4X_2$  materials,  $d_{31}$  is reduced. Besides, the  $d_{31}$  values of  $P_4Na_2$  and  $P_4Ni_2$  change from a positive to a negative value. There is no clear trend in the change in  $d_{31}$  obtained using different DFT computational methods. Although the  $d_{31}$  value of  $P_4Li_2$  is reduced from 6.28 to 2.5 pm/V, it is still the highest among all reported materials. It is worth noting that the piezoelectric coefficients of the other 2D materials were calculated without a vdW correction [26,27,31–33].

TABLE I. Piezoelectric coefficients of  $P_4X_2$  calculated using DFT. Units: pm/V. The PBE functional is adopted. To correct for the van der Waals interaction, we also perform DFT-TS calculations.

|                                | <i>d</i> <sub>31</sub> (PBE) | <i>d</i> <sub>32</sub> (PBE) | $d_{31}$ (DFT-TS) | $d_{32}$ (DFT-TS) |
|--------------------------------|------------------------------|------------------------------|-------------------|-------------------|
| P <sub>4</sub> Li <sub>2</sub> | 6.28                         | 0.30                         | 2.50              | -0.42             |
| $P_4Na_2$                      | 0.95                         | -0.26                        | -0.32             | 0.07              |
| $P_4V_2$                       | 0.27                         | 0.13                         | 0.27              | 0.36              |
| P <sub>4</sub> Mn <sub>2</sub> | 0.67                         | 0.33                         | 0.74              | 0.42              |
| P <sub>4</sub> Fe <sub>2</sub> | 0.24                         | 0.39                         | 0.16              | 0.36              |
| P <sub>4</sub> Ni <sub>2</sub> | 0.73                         | 0.56                         | 0.54              | 0.40              |
| P <sub>4</sub> Co <sub>2</sub> | 0.37                         | 0.41                         | 0.25              | 0.36              |



FIG. 4. Comparison of piezoelectric coefficients  $d_{31}$  of our adatom-doped black P with previously known values for 2D piezoelectric materials. The orange and green bars represent values of  $d_{31}$  calculated using the PBE functional and the DFT-TS scheme, respectively. GO denotes the graphene oxide. The color-filled and unfilled bars represent adatom-induced piezoelectric materials and intrinsic piezoelectric materials, respectively. The superscript labels "(a)," "(b)," "(c)," "(d)," and "(e)" refer to Refs. [26], [33], [27], [31], and [32], respectively.

After a careful study of the results shown in Fig. 4 and Tables I, we do not find clear clues about how  $d_{31}$  depends on the adatom type. To obtain some understanding of the high  $d_{31}$  value of P<sub>4</sub>Li<sub>2</sub>, we perform the following analysis. The piezoelectric coefficients  $e_{31}$  and  $e_{32}$  describe the change in electric polarization as a result of applied in-plane mechanical strains. They are the key physical properties for mechanical-sensing applications. The most reliable way to calculate the electric polarization is to use the Berry-phase method. However, this requires a highly symmetric nonpolarized phase as a reference, which is not available in our study. Therefore, we adopt another way to calculate these coefficients. For 2D materials, there is a relation between the piezoelectric coefficients  $d_{ij}$  and  $e_{ij}$ ,

$$e_{31} = d_{31}C_{11} + d_{32}C_{21},$$
  

$$e_{32} = d_{31}C_{12} + d_{32}C_{22},$$
(1)

where  $C_{11}$ ,  $C_{22}$ , and  $C_{12}$  (=  $C_{21}$ ) are the elastic stiffness constants. We determine the elastic constants of  $P_4X_2$  by fitting the strain energy density  $U(\varepsilon_{11}, \varepsilon_{22})$  calculated using the DFT method via

$$U(\varepsilon_{11},\varepsilon_{22}) = \frac{1}{2}C_{11}\varepsilon_{11}^2 + \frac{1}{2}C_{22}\varepsilon_{22}^2 + C_{12}\varepsilon_{11}\varepsilon_{22}.$$
 (2)

| A  |                                |                                |          |           |                                |                                |                                |  |  |
|--|--------------------------------|--------------------------------|----------|-----------|--------------------------------|--------------------------------|--------------------------------|--|--|
|  | P <sub>4</sub> Li <sub>2</sub> | P <sub>4</sub> Na <sub>2</sub> | $P_4V_2$ | $P_4Mn_2$ | P <sub>4</sub> Fe <sub>2</sub> | P <sub>4</sub> Ni <sub>2</sub> | P <sub>4</sub> Co <sub>2</sub> |  |  |
| $\overline{e_{31} (10^{-10} \text{ C/m})}$ | 0.84                           | 0.12                           | 0.25     | 0.59      | 0.48                           | 0.62                           | 0.45                           |  |  |
| $e_{32}$ (10 <sup>-10</sup> C/m)           | 0.90                           | -0.09                          | 0.27     | 0.56      | 0.71                           | 0.59                           | 0.58                           |  |  |
| $C_{11}$ (N/m)                             | 13.01                          | 18.11                          | 78.80    | 72.58     | 115.76                         | 76.99                          | 98.61                          |  |  |
| $C_{22}$ (N/m)                             | 110.28                         | 112.61                         | 144.61   | 103.53    | 150.52                         | 91.26                          | 123.59                         |  |  |
| $C_{12}$ (N/m)                             | 9.03                           | 21.68                          | 30.50    | 32.66     | 52.89                          | 10.44                          | 20.93                          |  |  |
| $E_{\rm r}$ (N/m)                          | 11.85                          | 14.06                          | 72.29    | 62.47     | 95.78                          | 77.11                          | 92.74                          |  |  |
| $E_{v}$ (N/m)                              | 107.52                         | 85.87                          | 132.80   | 88.84     | 128.11                         | 88.29                          | 122.06                         |  |  |
| v <sub>rv</sub>                            | 0.08                           | 0.19                           | 0.21     | 0.32      | 0.35                           | 0.11                           | 0.17                           |  |  |
| $v_{yx}$                                   | 0.69                           | 1.20                           | 0.39     | 0.45      | 0.35                           | 0.14                           | 0.21                           |  |  |

TABLE II. Piezoelectric coefficients, elastic stiffness constants, Young's modulus, and Poisson's ratio for  $P_4X_2$  calculated using DFT computational method with PBE functional.

Young's modulus E and Poisson's ratio v are then calculated using

$$E_x = \frac{C_{11}C_{22} - C_{12}C_{21}}{C_{22}}, E_y = \frac{C_{11}C_{22} - C_{12}C_{21}}{C_{11}},$$
$$\nu_{xy} = \frac{C_{21}}{C_{22}}, \quad \nu_{yx} = \frac{C_{12}}{C_{11}}.$$
(3)

By substituting the calculated elastic constants into Eq. (1), the piezoelectric coefficients  $e_{31}$  and  $e_{32}$  can be determined. The results are summarized in Table II. Combining Eqs. (1) and (3) yields

$$d_{31} = \frac{e_{31}C_{22} - e_{32}C_{21}}{C_{11}C_{22} - C_{12}^2} = \frac{e_{31} - v_{xy}e_{32}}{C_{11} - v_{xy}C_{12}},$$
 (4)

$$d_{32} = \frac{e_{31}C_{12} - e_{32}C_{11}}{C_{12}^2 - C_{11}C_{22}} = \frac{-C_{11}(e_{31}\nu_{yx} - e_{32})}{C_{11}C_{22} - C_{12}^2}.$$
 (5)

In Table II, we note that these  $P_4X_2$  materials have  $C_{11} \gg v_{xy}C_{12}$  and  $e_{31} \gg v_{xy}e_{32}$ . Hence Eq. (4) can be simplified to  $d_{31} \approx e_{31}/C_{11}$ .  $P_4Li_2$  has the highest  $e_{31}$  but the smallest  $C_{11}$  among all the cases. It thus has the highest  $d_{31}$  value. The low stiffness  $C_{11}$  of  $P_4Li_2$  might be related to its significantly increased lattice constant *a* compared with pristine black P, 4.88 Å vs 4.62 Å. The Li adatoms could significantly distort the chemical bonds in black P, leading to a reduced stiffness  $C_{11}$ .

Finally, we carry out FEM simulations to demonstrate a prototypical smart-surface design using the 2D piezoelectric material P<sub>4</sub>Li<sub>2</sub>. Figure 5(a) illustrates the prototype, where a square film of monolayer P<sub>4</sub>Li<sub>2</sub> with an edge size L is placed on a substrate. The four edges are fixed to the substrate. A local voltage is applied in the vertical direction to a selected square region of the thin film with an edge size l. The large piezoelectric coefficient  $d_{31}$  of P<sub>4</sub>Li<sub>2</sub> should lead to a large in-plane strain  $\varepsilon_{11}$  in the selected region and a subsequent large out-of-plane buckling displacement. This could generate a detectable morphology change on the surface.

In our FEM model [Fig. 5(b)], four-point shell elements with a mesh size of about 0.008-0.01 mm and a thickness of  $4.6 \times 10^{-4} \ \mu m$  are employed to simulate a thin film with the elastic properties of P<sub>4</sub>Li<sub>2</sub> listed in Table II. The substrate is assumed to be rigid. The filmsubstrate interface is modeled assuming a cohesion mode with normal stiffness  $K_n = 120$  MPa/mm, shear stiffness  $K_t = 120$  MPa/mm, maximum normal separation stress  $\delta n = 0.008$  MPa, maximum shear separation stress  $\delta t =$ 0.01 MPa, and adhesive energy  $e = 8 \times 10^{-5}$  mJ. These effective parameters depend on the properties of the cohesive surfaces and the substrate [38,39]. They are selected to mimic the case of separating a bilayer of black P. A film-substrate separation could take place when the interfacial normal stress or energy-release rate is above a critical value. In our FEM simulations, the in-plane piezoelectric strain is simulated by a thermal-expansion strain with an appropriate expansion coefficient and temperature field applied in the  $P_4Li_2$  film. We perform the FEM simulations using Abaqus/Explicit. A periodic boundary condition is applied to the four edges. The left plot in Fig. 5(b) shows the initial undeformed geometry. The right plot shows the swollen surface morphology obtained as a result of the out-of-plane elastic buckling displacement (for L = 1 mmand l = 0.4 mm). The arched swelling profile generated shows differences between the x and y directions. This can be attributed to the intrinsic elastic and piezoelectric anisotropy of P<sub>4</sub>Li<sub>2</sub>. The maximum swelling height is denoted by H.

To evaluate the dependence of H on the parameters Land l, a series of FEM calculations are carried out. Figure 5(c) summarizes the calculated results for H, with L varying from 0.5 to 5 mm and the ratio l/L varying from 0.1 to 0.8. Note that the in-plane piezoelectric strains are  $\varepsilon_{11} = 0.628\%$  and  $\varepsilon_{22} = 0.03\%$  in all cases. The swelling height H can reach up to 0.22 mm for L = 5 mm and a/L = 0.8. Previous studies have shown that receptors in the human finger can feel a texture by detecting surface roughness with a spatial resolution of about 40  $\mu$ m over a contact area of 1 cm<sup>2</sup> [40]. Tactile features have been introduced in many banknotes to assist visually disabled people,



FIG. 5. Prototypical smart-surface design where P<sub>4</sub>Li<sub>2</sub> is used to generate morphology changes under an external electric field, simulated via FEM. (a) Illustration of the design. A 2D P<sub>4</sub>Li<sub>2</sub> monolayer thin film is placed on a rigid substrate with a vertical electric field applied locally. (b) Top view of our FEM model. The P<sub>4</sub>Li<sub>2</sub> thin film has an edge length of L. The four edges are fixed to the substrate. The vertical electric field is applied to a local region in the center with edge size l. See the main text for details of our FEM model. The right part of (b) shows the surface swelling profile. (c) Maximum swelling height H as a function of L and l/L. The piezoelectric strains are  $\varepsilon_{11} = 0.628\%$ and  $\varepsilon_{22} = 0.03\%$ . (d) Four arrays of  $9 \times 9$  building blocks (pixels) assembled together. Each building block follows the prototypical design shown in (b). When a voltage is applied to selected blocks, the swollen blocks form patterns with special morphologies. In this case, the patterns are "X," "J," "T," "U."

for whom the depth that can be felt is about 50  $\mu$ m [41]. These requirements can be feasibly achieved by selecting appropriate *L* and *l/L* values using Fig. 5(c).

Taking the prototype of the square thin film in Fig. 5(b)as one building block (or pixel), we can combine many such building blocks together to form an array, e.g., a  $9 \times 9$ array as shown in Fig. 5(d). As a demonstration, here L and l/L are set to 5 mm and 0.5, respectively. Applying a vertical electric field to selected pixels leads to a designed morphology pattern on the surface. Figure 5(d) shows an example of patterns "X," "J," "T," "U," representing the initials of Xi'an Jiaotong University. Piezoelectric strains are applied only to the green blocks shown in the top plot in Fig. 5(d). The swelling patterns "X," "J," "T," "U" in our FEM simulations are observed in the bottom part (which shows a top view). In a side view, the height H generated is about 0.19 mm, which is large enough for many applications (e.g., detection by fingers). Recently, layerby-layer assembly of multilayer 2D materials, e.g., vdW heterostructures, has been widely demonstrated in many publications [19]. This can be used to fabricate a heterostructure composed of a  $P_4X_2$  layer on top of a graphene electrode layer. The lithographic technology for patterning graphene layers and layers of other conductive 2D materials is also mature [42]. This technology can be used to fabricate top electrode layers with required patterns, e.g., a 9 × 9 pixel array. Using available transfer techniques [43], a patterned top electrode layer could be placed on top of  $P_4X_2$ . All of these experimental technologies are readily available, suggesting the feasibility of our proto-typical design based on piezoelectric  $P_4X_2$  (or other 2D piezoelectric materials) in experiments. Using 2D piezo-electric materials to design surface-morphology changes is promising for smart-surface applications.

## **IV. CONCLUSIONS**

In summary, using DFT-PBE calculations, we investigate the crystal structure, formation energy, and piezoelectric properties of adatoms doped on the top surface of black phosphorene. Adatoms X consisting of all metallic elements in the top three rows of the Periodic Table, and concentrations ranging from  $P_{48}X_1$  to  $P_4X_2$  are considered. In most cases, the metal adatoms occupy the H sites. But at high concentrations, in  $P_4X_2$ , Zn, Al, and Ga adatoms occupy the T sites. For  $P_{48}X_1$ ,  $P_4X_1$ , and  $P_4X_2$ , there are five, seven, and seven types, respectively, of adatoms with a negative formation energy. We find that the piezoelectric coefficient  $d_{31}$  of  $P_4Li_2$  is at least 4 times higher than those of all other 2D materials. Detailed analysis attributes the superior piezoelectric properties of this material to its small elastic constant  $C_{11}$ . The excellent piezoelectricity of adatom-doped black P could be used to generate significant in-plane strain under an applied electric field in the vertical direction. The elastic-buckling-induced out-of-plane swelling patterns can be used in smart-surface applications. We use FEM simulations to successfully demonstrate a prototypical smart-surface design. The design of surface morphologies using 2D piezoelectric materials is a promising avenue for smart surfaces.

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