Cold-Electron Bolometer as a 1-cm-Wavelength Photon Counter

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We investigate theoretically the possibility of using the cold-electron bolometer (CEB) as a counter for 1-cm-wavelength (30-GHz) photons. To reduce the flux of photons from the environment that interact with the detector, the bath temperature is assumed to be below 50 mK. At such temperatures, the time interval between two subsequent photons of 30 GHz that hit the detector is more than 100 h, on average, for a frequency window of 1 MHz. Such temperatures allow the observation of the physically significant photons produced in rare events, such as axion conversion (or Primakoff conversion) in a magnetic field. We present the general formalism for the detector's response and noise, together with numerical calculations for proper experimental setups. We observe that the current-biased regime is favorable due to lower noise and allows for photon counting at least below 50 mK. For the experimental setups investigated here, the voltage-biased CEBs may also work as photon counters but with less accuracy and, eventually, may require smaller volumes of the normal-metal island.

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I. INTRODUCTION

The search for axions [1-4] has intensified lately, since they have become good candidates for the dark matter in the Universe (see Ref. [5] and citations therein). Due to their extremely weak coupling to other massive particles, they are difficult to detect but they may be converted into photons in intense magnetic fields [6]. The photons may have low energies (eventually, of the order of 100 μ eV, which corresponds to wavelengths of the order of 1 cm) and low flux (one photon in a few hours) [5], so their detection should be attempted with extreme care. The experimental developments of single-photon counters (SPCs) that has taken place over the past decade (see, e.g., [7-9]) has eventually reached wavelengths of the order of hundreds of microns [10], whereas theoretical estimates show that detection of single photons of 1 cm wavelength may be within reach [9,11]. For the extreme requirements of axion detection, good candidates for photon counters are devices based on Josephson junctions [12,13]. Another option is the capacitively coupled cold-electron bolometer (CEB) [14-17], which is a symmetric superconductor-insulator-normalmetal-insulator-superconductor (S-I-N-I-S) structure [18], capacitively coupled to an antenna [19,20], as shown schematically in Fig. 1. In order to avoid the influence of the strong magnetic field, the detector system is moved away from the sample and the connection between the two parts may be realized by a coaxial cable. In such a setup, the photon created by the axion decay is captured by the antenna and its energy is dissipated into the central normalmetal island, increasing the temperature of the electron gas [21]. This increase in temperature is measured by the S-I-N-I-S structure and thus the photon is detected. The two normal-metal-insulator-superconductor (N-I-S) tunnel junctions that form the S-I-N-I-S structure are used as both thermometers-due to the sensitivity of their currentvoltage characteristic to the temperature-and refrigerators [18,22]—to lower the temperature of the electrons in the normal-metal island, in order to improve the sensitivity of the detector and decrease its re-equilibration time. Recently, an important development of the N-I-S thermometer has been proposed [23], in which a small gap is induced in the normal-metal island by the proximity to a superconductor. Then, a zero-bias anomaly [24] appears in the \mathcal{N} -I-S junction (where \mathcal{N} denotes the normal metal in which the small gap is induced), which may be used to determine the temperature of the $\mathcal N$ island in a temperature range that may be lower than that accessible to the simple N-I-S junction. Besides their high sensitivity and wide dynamic range, CEBs demonstrate immunity to cosmic rays, due to the tiny volume of the absorber and the decoupling of the phonon and electron subsystems [25].

Counters based on Josephson junctions are under intense investigation (see, e.g., Refs. [26–29] and citations

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FIG. 1. The detection scheme. The photon, produced by the axion in a strong magnetic field, is absorbed by the antenna and its energy is dissipated into the normal-metal island of the CEB. The antenna and the CEB are deposited on an insulating support, not shown here. SQUID, superconducting quantum-interference device.

therein), so in this paper we investigate the possibility of using the CEB as a low-energy photon counter.

In order to be able to identify photons generated by axion decay, the temperature of the environment should be low enough for the rate of "fake events" (due to photons from the environment hitting the detector) to be much smaller than the rate of the "real events" (due to photons produced by axions). If we denote by $N_{\rm ph}(\delta\omega)$ the volume density of the photons from the environment in the narrow frequency window $\delta\omega$, which includes the frequency ω , then

$$\frac{N_{\rm ph}(\delta\omega)}{\delta\omega} \equiv n_{\rm ph}(\omega) = \frac{1}{\pi^2 c^3} \frac{\omega^2}{e^{\beta\hbar\omega} - 1},\tag{1}$$

where $\beta \equiv 1/(k_B T)$, k_B is Boltzmann's constant and *T* is the bath (environment) temperature—in Eq. (1), we take into account the two photon polarizations. From Eq. (1), we obtain the flux of photons on the unit area of the detector's surface,

$$\phi(\omega) \equiv \int_0^{2\pi} d\phi \int_0^{\pi/2} d\theta \sin \theta \frac{cn_{\rm ph}(\omega)}{4\pi} = \frac{1}{2\pi^2 c^2} \frac{\omega^2}{e^{\beta\hbar\omega} - 1}.$$
(2)

For photons of wavelength of the order of 1 cm (30-GHz frequency), the area of the detector plus antenna is of the order of $A_0 = 1$ cm². The estimation of the average number of photon hits on the detector in the time interval $t_0 = 1$ h and in a unit frequency window of 1 Hz is $N_0(\nu) = A_0 t_0 \phi(2\pi\nu)$, where $\nu \equiv \omega/(2\pi)$. In Fig. 2, we show the contour plot of $\log_{10}[N_0(\nu)\delta\nu]$ for a typical bandwidth of $\delta\nu = 1$ MHz. We observe that for photons of 30 GHz we have, on average, one photon hit in more than 100 h, if the temperature of the environment is 50 mK. This allows enough room for the accurate detection of photons generated by axion decay.



FIG. 2. The estimation of the average number of hits on the detector in 1 h, by photons from the environment. The area of the antenna is considered to be 1 cm² and the bandwidth is $\delta v = 1$ MHz. The figure shows the contour plot of $\log_{10}[N_0(v)\delta v]$.

The paper is organized as follows. In the next section, we analyze the response of the CEB, namely the temperature increase due to the photon absorption, the signal produced in the measured quantity (current or voltage), and the re-equilibration time (the time scale on which the device cools down, after the photon absorption). In Sec. III, we calculate the noise in the system, to see if the signal produced by the photon can be observed. In Sec. IV, we draw our conclusions.

While, in the main body of the paper, the calculations are done for a volume of normal metal $\Omega = 0.01 \ \mu m^3$, in the Appendix A we present the main results for $\Omega = 0.1 \ \mu m^3$, to emphasize the flexibility that exists in the construction of the device and its limitations.

II. RESPONSE OF THE COLD-ELECTRON BOLOMETER

The principle of detection is presented in Fig. 1 (see, e.g., Refs. [18,21,30–32]). The superconducting antenna is coupled to the normal-metal island by two *N-I-S* tunnel junctions, forming the symmetric *S-I-N-I-S* structure. The whole detector is deposited on an insulating support (not shown in the figure). The thicknesses of the metallic layers (normal metal and superconductor) are 10–20 nm. When a photon, absorbed in the antenna, dissipates its energy into the normal-metal island, the heat diffuses in the normal metal in the characteristic time $\tau_d \approx L^2/(\pi^2 D)$, where *L* is the linear dimension of the normal metal and *D* is the diffusion constant of the electrons. For typical values of $L \sim 1 \ \mu m$ and $D = 10^{-4} \ m^2 \ s^{-1}$, we obtain $\tau_d \sim 1 \ ns$ [21], which sets the lower limit for the detection time.

At working temperatures, which are below 100 mK, the electron system in the normal metal is very weakly coupled

$$\dot{Q}_{e-\rm ph} = \Sigma_{e-\rm ph} \Omega \big(T_e^x - T_{\rm ph}^x \big), \tag{3}$$

where Σ_{e-ph} is the coupling constant, Ω is the volume of the normal metal, and the exponent *x* depends on the model and the dimensionality of the phonon system (in our case, *x* may take values between 3.5 and 5) [33–36,38]. Since the heat power exchanged between electrons and phonons is low, we assume, in general, that T_{ph} is equal to the heat-bath temperature T_b .

In the absence of photons, the electrons equilibrate at temperature T_{e1} , determined by the balance between the heat exchanged with the phonons [Eq. (3)] and the heat extracted from the normal metal into the superconductor, through the two *N-I-S* junctions [Eq. (7b) below]—in addition to these, spurious power injection may be present, as observed in Ref. [9], but in the absence of a quantitative understanding, we do not take it into account. When a photon is absorbed, its energy is dissipated into the electron system of the normal metal, increasing its temperature to T_{e2} . In the low-temperature limit, the internal energy of the electron system is, in general, proportional to T_e^2 [39] and to the volume, so we may write

$$U(T_e) = \Omega C_e T_e^2. \tag{4}$$

For concrete systems, C_e is either a fitting parameter or is determined by the theoretical model. For simplicity, we take the value corresponding to an ideal gas, namely $C_e = (2m_e/\hbar^2)^{3/2}\epsilon_F^{1/2}k_B^2/12$, where ϵ_F is the Fermi energy of the electrons, m_e is the mass of the electron, k_B is Boltzmann's constant, and \hbar is the reduced Planck's constant. Nevertheless, significant differences may appear between the calculated values of C_e and the measured ones [9]. If we denote by $\omega_{\rm ph}$ the angular frequency of the photon, using (4) we can write the equation

$$\hbar\omega_{\rm ph} \equiv \epsilon_{\rm ph} = U(T_{e2}) - U(T_{e1}),\tag{5}$$

where $\epsilon_{\rm ph}$ is the energy of the photon.

The heat and charge transport through the *N-I-S* junctions have been extensively studied in the past (see, e.g., Refs. [18,22,31,32,40–44]). We assume that the junctions are identical, of normal resistance R_T , and that they are biased with opposite voltages, V and -V. If the tunneling resistance is big enough, Andreev reflection does not occur and particles and energy are transported by quasiparticle tunneling. We define, as in Refs. [43,44], four tunneling

currents,

$$j_1(\epsilon) \equiv \frac{g(\epsilon)}{e^2 R_T} f(\epsilon - eV, T_e) [1 - f(\epsilon, T_s)], \qquad (6a)$$

$$j_2(\epsilon) \equiv \frac{g(\epsilon)}{e^2 R_T} f(\epsilon + eV, T_e) [1 - f(\epsilon, T_s)], \qquad (6b)$$

$$j_3(\epsilon) \equiv \frac{g(\epsilon)}{e^2 R_T} [1 - f(\epsilon - eV, T_e)] f(\epsilon, T_s), \qquad (6c)$$

$$j_4(\epsilon) \equiv \frac{g(\epsilon)}{e^2 R_T} [1 - f(\epsilon + eV, T_e)] f(\epsilon, T_s), \qquad (6d)$$

where Δ and $\epsilon (\geq \Delta)$ are the energy gap and the quasiparticle energy in the superconductor, respectively, whereas $g(\epsilon) \equiv \epsilon/\sqrt{\epsilon^2 - \Delta^2}$ is proportional to the quasiparticle density of states (for a detailed description of the currents 6, see Ref. [43]). By T_s , we denote the temperature of the quasiparticles in the superconductor and, because of the low heat power exchanged between the normal metal and the superconductor, we assume that $T_s = T_b$. The density of states $g(\epsilon)$ may be generalized, to include subgap tunneling [45,46], but since this is determined by the interaction with the environment, we neglect it in this analysis (as, for example, in Refs. [9,11]). Using Eq. (6), the electrical current and the heat current through an *N-I-S* junction are [43,44,47]

$$I_J = e \int_{\Delta}^{\infty} (j_1 - j_2 - j_3 + j_4) d\epsilon$$

= $\frac{1}{eR_T} \int_{\Delta}^{\infty} g(\epsilon) [f(\epsilon - eV, T_e) - f(\epsilon + eV, T_e)] d\epsilon$
(7a)

and

$$\dot{Q}_J = \int_{\Delta}^{\infty} [(\epsilon - eV)(j_1 - j_3) - (\epsilon + eV)(j_4 - j_2)]d\epsilon,$$
(7b)

respectively. I_J and \dot{Q}_J are positive when the current and heat, respectively, flows from the electrons of the normal metal into the superconductor. The equilibrium temperature of the electron system is obtained by equating the total power $\dot{Q}_T(T_e, T_b) \equiv \dot{Q}_{e-ph}(T_e, T_b) + 2\dot{Q}_J(T_e, T_b)$ to zero (the factor of 2 appears because of the two *N-I-S* junctions attached to the normal metal), namely

$$\hat{Q}_T(T_e, T_b) = 0. \tag{8}$$

Equation (8) represents the *heat balance equation* for our system.

We consider that the normal metal is Cu and the superconductor is Al. In Fig. 3, we plot the solutions of Eq. (8) for $\dot{Q}_{e-\text{ph}}$ given by Eq. (3), with x = 5 and $\Sigma_{e-\text{ph}} = 4 \times 10^9 \text{ W m}^{-3} \text{ K}^{-5}$ [18]. The tunneling resistance is $R_T =$



FIG. 3. The theoretical estimation of the equilibrium temperature of the (ideal) electron gas in the normal-metal island, cooled by the *S-I-N-I-S* structure, starting from the bath temperature T_b and for the bias voltage V (for each *N-I-S* junction). The tunneling resistance of each of the two junctions is $R_T = 35 \text{ k}\Omega$ and the volume of the normal-metal island is 0.01 μ m³.

35 k Ω for each of the two *N-I-S* junctions, the volume $\Omega = 0.01 \ \mu m^3$, and the energy gap in the superconducting Al is $\Delta = 0.2$ meV [18,48]. We use these numerical values throughout the paper, except for the Appendix A. To emphasize the dependence of these results on the volume Ω , in the Appendix we plot the results of the same calculations, but with $\Omega = 0.1 \ \mu m^3$. We use the experimental values for x and Σ_{e-ph} , instead of the theoretical ones, calculated more recently, because the values that exist in the literature (both theoretical and experimental) vary significantly from model to model and from sample to sample (see, e.g., the diversity of results presented in Refs. [18,33–35,49–55]).

The temperature increase $\Delta T_e \equiv T_{e2} - T_{e1}$ due to the absorption of a 1-cm-wavelength photon leads to an increase of the current (at voltage bias) or a decrease of the voltage (at current bias). The photon can be detected if the variation of the measured quantity, I_J or V, is bigger than the noise (i.e., the mean-square fluctuation of the measured quantity) that we calculate in Sec. III.

A. Detector re-equilibration

We calculate the re-equilibration time of the detector, τ , which sets the time scale in which the temperature returns to the initial value after the photon absorption. Let us say that at time t = 0, the temperature of the electrons in the normal metal is varied by $\Delta T_e(0) \equiv T_{e2} - T_{e1}$, after which they cool back to T_{e1} . If $\Delta T_e(0) \ll T_{e1}$, then we can assume an exponential time dependence,

$$\Delta T_e(t) = \Delta T_e(0)e^{-t/\tau},\tag{9a}$$



FIG. 4. The relaxation time τ .

where, from the expression of Q_T , we obtain

$$\tau^{-1} = \frac{1}{C_V} \left(\frac{\partial \dot{Q}_T}{\partial T_e} \right) \equiv \tau_J^{-1} + \tau_{e\text{-ph}}^{-1} \ll \tau_d^{-1}, \qquad (9b)$$

with obvious notation. From Eqs. (7b) and (3), we obtain

$$\frac{1}{\tau_J} = \frac{2}{C_V} \left(\frac{\partial \dot{Q}_J}{\partial T_e} \right) \quad \text{and} \quad \frac{1}{\tau_{e-\text{ph}}} = \frac{5\Sigma_{e-\text{ph}}\Omega T_e^4}{C_V}, \quad (9\text{c})$$

where $C_V \equiv C_V(T_e)$ is the heat capacity of the electron system in the normal metal and $\partial \dot{Q}_J / \partial (k_B T_e)$ is calculated in Eq. (B17c). The dependence of τ on the bath temperature and the bias voltage is plotted in Fig. 4. Nevertheless, if ΔT_e is comparable with or bigger than T_{e1} —as we shall see, this happens in our case—Eq. (9) gives only the order of magnitude of the time required for the detector to reequilibrate. The time variation of the temperature in the general case is given by

$$C_V(T_e)\frac{dT_e}{dt} = \dot{Q}_T(T_e, T_b).$$
(10)

In Fig. 5, we show the time evolution of the temperature difference $\Delta T_e(t)$ for a few representative values of T_b and bias voltages or currents. We observe that, in accordance with the results plotted in Fig. 4, the relaxation time is of the order of a few tens of nanoseconds. We also observe that the relaxation time may depend strongly on the type of bias used (current or voltage bias), especially at low temperatures.

III. NOISE

Since we analyze only the CEB, in the noise calculations we neglect the fluctuations produced in the external



FIG. 5. The time evolution of the electron temperature in the normal metal at (a) voltage and (b) current bias. The volume is $\Omega = 0.01 \ \mu \text{m}^3$. The bath temperature takes three values: 30 mK (solid lines), 40 mK (dashed lines), and 50 mK (dotted lines). In (a), the voltages are fixed at V_0 , with $1 - eV_0/\Delta = 0.43 \times 10^{-3}$ (blue lines), 0.22×10^{-3} (red lines), and 0 (green lines). In (b), the currents are fixed at $I_J(T_{e1}, V_0)$, where the V_0 correspond to the same values as in (a).

circuit. These depend on the experimental setup and should be added to the fluctuations calculated here.

For integrating detectors (i.e., detectors that measure the total incoming radiation flux), the figure of merit is the *noise equivalent power* (NEP). If M is the measured quantity for such a detector (e.g., the current, in a voltage-biased CEB), the NEP represents the input radiation power on the unit bandwidth $\dot{Q}_{oe}(\omega)$ that produces a signal equal in amplitude to the square root of the spectral density of noise, $[\langle |\delta M(\omega)|^2 \rangle]^{1/2}$. Concretely,

$$\text{NEP} \equiv \frac{\left[\langle |\delta M(\omega)|^2 \rangle\right]^{1/2}}{|\partial M/\partial \dot{Q}_{oe}|}.$$
 (11)

In the voltage-biased CEB, the measured quantity is the current and the spectral density of its fluctuation is [21,44]

$$\langle |\delta I_J(\omega)|^2 \rangle = \langle |\delta I_{J \text{shot}}(\omega)|^2 \rangle + \left(\frac{\partial I_J}{\partial T_e}\right)^2 \langle |\delta T_e(\omega)|^2 \rangle + \frac{1}{e^2 \omega^2} \left(\frac{\partial \epsilon_F}{\partial N} \frac{\partial I_J}{\partial (eV)}\right)^2 \langle |\delta I_J(\omega)|^2 \rangle + 2 \frac{\partial I_J}{\partial T_e} \text{Re} \left[\langle \delta I_J(\omega) \delta T_e^*(\omega) \rangle \right] + \frac{2}{e} \frac{\partial \epsilon_F}{\partial N} \frac{\partial I_J}{\partial (eV)} \frac{\partial I_J}{\partial T_e} \text{Re} \left[\left\langle \delta T_e^*(\omega) \frac{\delta I_J(\omega)}{i\omega} \right\rangle \right],$$
(12a)

where the angle brackets $\langle \cdot \rangle$ denote averages, Re(\cdot) represents the real part of a complex number, $\delta I_J(\omega)$ and $\delta T_e(\omega)$ are the Fourier transforms of the noise in current and temperature, respectively, and δT_e^* is the complex conjugate of δT_e , whereas $\delta I_{J,\text{shot}}(\omega)$ is the Fourier transform of the current shot noise (for details, see Appendix B). The first term on the right-hand side of Eq. (12a), namely $\delta I_{J,\text{shot}}(\omega)$, represents the lowest-order contribution to the noise.

In the current-biased setup, the voltage fluctuation is ultimately determined by the fluctuation of the number of electrons in the normal-metal island N (since the positive charge does not change). The charging on the normalmetal island leads to a change of its potential energy, which, in turn, influences the charges on the junction capacitances—and, therefore, the voltage on the CEB. These processes may be studied in more detail, but for a CEB the capacitance of the normal-metal island is big enough, so we use the linear approximation assuming that the voltage fluctuations are proportional to the fluctuations of the number of electrons in the normal-metal island. Concretely, we use $\delta(eV) = (\partial \epsilon_F / \partial N) \delta N$ and write the spectral density of the voltage fluctuation as [21]

$$\langle |\delta V(\omega)|^2 \rangle = \frac{1}{\omega^2} \left(\frac{1}{e^2} \frac{\partial \epsilon_F}{\partial N} \right)^2 \langle |\delta I_J(\omega)|^2 \rangle.$$
 (12b)

Nevertheless, the NEP is not directly relevant for SPCs. In our SPC, a temperature pulse with a time evolution similar to the ones presented in Fig. 5 should be discerned from the background noise and for this we need different more specific criteria than in the integrating detectors. In Appendix B, we present a short list of such criteria, used by different authors, but here we employ the one used by us in Ref. [21], which—we consider—is the most appropriate.

From Eq. (12), we may calculate the total fluctuation of the current and voltage as

$$\langle \delta^2 I_J \rangle_{\rm tot} = \int_0^\infty \langle |\delta I_J(\omega)|^2 \rangle d\omega, \qquad (13a)$$

$$\langle \delta^2 V \rangle_{\text{tot}} = \int_0^\infty \langle |\delta V(\omega)|^2 \rangle d\omega,$$
 (13b)

but the integrals in Eq. (13) are divergent (the shot noise, for example, is "white," i.e., $|\delta I_{J,\text{shot}}(\omega)|^2$ is constant) and therefore they do not represent the observed quantities. Physically, the noise may be filtered in a band $[\omega_{\text{max}}, \omega_{\text{min}}]$, whereas the readout system may have a delay τ_c , which introduces a cutoff. Due to the cutoff τ_c , the measured quantity $M_m(t)$ —which is a function of *t*—follows the real quantity M(t) with a delay, modeled by the equation [21]

$$\frac{dM_m(t)}{dt} = \frac{M(t) - M_m(t)}{\tau_c}.$$
(14)

In Fig. 6, we plot the time dependence of the current (at voltage bias) and voltage (at current bias), for the same cases as in Fig. 5, without taking the noise into account. We observe that the measured current or voltage first increases abruptly (with the time constant τ_c) and then decreases as the temperature of the normal metal decreases to the equilibrium value. Since the relaxation time is of the order of tens of nanoseconds, in the following we consider $\tau_c = 1$ ns (of the same order as the diffusion time) in all the numerical calculations. We observe that the signal (the maximum value of the measured quantity) is slightly smaller than the actual jump in current or voltage produced by the photon absorption (at T_{e2}) and depends on τ_c —the bigger τ_c , the smaller the signal.

The filtering band, together with the delay time τ_c , leads to the total *measured* fluctuations of I_J and V,

$$\langle \delta^2 I_J \rangle_m = 2 \int_{\omega_{\min}}^{\omega_{\max}} \frac{\langle |\delta I_J(\omega)|^2 \rangle}{1 + \omega^2 \tau_c^2} d\omega, \qquad (15a)$$

$$\langle \delta^2 V \rangle_m = 2 \int_{\omega_{\min}}^{\omega_{\max}} \frac{\langle |\delta V(\omega)|^2 \rangle}{1 + \omega^2 \tau_c^2} d\omega.$$
 (15b)

The relaxation time τ and the delay time τ_c impose "filtering" limits, even in the absence of ω_{\min} and ω_{\max} . That is, the noise of frequencies much lower than the inverse of the relaxation time τ does not influence the measurement because it does not influence the visibility of the pulse in the measured quantity. Similarly, we observe that due to τ_c , the integrals (15) are convergent even in the absence of ω_{\max} .

Plugging the expression (B20) into Eq. (15), we obtain

$$\begin{split} \langle \delta^2 I_J \rangle_m &\approx \frac{\pi}{\tau + \tau_c} \left(\frac{\partial I_J / \partial T_e}{\partial \dot{Q}_T / \partial T_e} \right)^2 \left[\langle | \delta \dot{Q}_{e\text{-ph shot}}(\omega) |^2 \rangle \right. \\ &\left. + 2 \langle | \delta \dot{Q}_{J\text{shot}}(\omega) |^2 \rangle - \frac{4 \langle \delta I_{J\text{shot}}(\omega) \delta \dot{Q}^*_{J\text{shot}}(\omega) \rangle}{S_I(0, V)} \right] \end{split}$$



FIG. 6. The time evolution of the current, at voltage bias (a), and of the voltage, at current bias (b), for a few significant bath temperatures and voltages (the same as in Fig. 5). The bath temperature takes three values: 30 mK (solid lines), 40 mK (dashed lines), and 50 mK (dotted lines). In (a), the voltages are fixed at V_0 , with $1 - eV_0/\Delta = 0.43 \times 10^{-3}$ (blue lines), 0.22×10^{-3} (red lines), and 0 (green lines). In (b), the currents are fixed at $I_J(T_{e1}, V_0)$, where the V_0 correspond to the same values as in (a). The measurement cutoff time used is $\tau_c = 1$ ns.

$$+\left[\frac{\pi}{\tau_c} + \frac{2}{e^2\omega_{\min}}\left(\frac{\partial\epsilon_F}{\partial N}\frac{\partial I_J}{\partial(eV)}\right)^2\right]\langle|\delta I_{Jshot}(\omega)|^2\rangle,$$
(16a)

$$\begin{split} \langle \delta^2 V \rangle_m &\approx \left(\frac{1}{e^2} \frac{\partial \epsilon_F}{\partial N} \right)^2 \frac{2}{\omega_{\min}} \left\{ \left[\langle | \delta \dot{Q}_{e\text{-ph shot}}(\omega) |^2 \rangle \right. \\ &\left. + 2 \langle | \delta \dot{Q}_{J\text{shot}}(\omega) |^2 \rangle - \frac{4 \langle \delta I_{J\text{shot}}(\omega) \delta \dot{Q}_{J\text{shot}}^*(\omega) \rangle}{S_I(0, V)} \right] \right. \\ &\left. \times \left(\frac{\partial I_J / \partial T_e}{\partial \dot{Q}_T / \partial T_e} \right)^2 + \langle | \delta I_{J\text{shot}}(\omega) |^2 \rangle \end{split}$$



FIG. 7. The current fluctuation divided by the height of the current pulse created by the photon absorption. We assume that the detector works as an SPC if this ratio is smaller than 1.

$$\times \left[1 + \frac{2}{e^2} \left(\frac{\partial \epsilon_F}{\partial N} \frac{\partial I_J}{\partial (eV)}\right)^2 \frac{1}{3\omega_{\min}^2}\right]\right\}.$$
 (16b)

where we assume $\tau \omega_{\max}, \tau_c \omega_{\max} \gg 1$ [such that $\arctan(\tau_c \omega_{\max}) \approx \arctan(\tau \omega_{\max}) \approx \pi/2$] and $\tau \omega_{\min}, \tau_c \omega_{\min} \ll 1$ [such that $\arctan(\tau_c \omega_{\min}) \approx \arctan(\tau \omega_{\min}) \approx 0$].

The terms that appear in Eq. (16) are calculated in the Appendix A; in Sec. 1 a we give analytical expressions in terms of polylogarithmic functions. In the numerical calculations, we choose $\omega_{\min} = 2\pi/(10\tau)$ (i.e., we consider that noise of frequencies lower than $1/(10\tau)$ does not obstruct the observation of the signal), where τ is plotted in Fig. 4. In this way, we observe that in Eq. (16a) the dominant terms are those proportional to $\langle |\delta \dot{Q}_{e-\text{ph} \text{ shot}}(\omega)|^2 \rangle$ and $\langle \delta I_{J \text{ shot}}(\omega) \delta \dot{Q}^*_{J \text{ shot}}(\omega) \rangle$] being smaller by at least 2 and 3 orders of magnitude. Furthermore, in the second square bracket of Eq. (16a), the first term (π/τ_c) is more than 2 orders of magnitude bigger than the second term, for the most part of the parameter range.

In the expression (16b), the dominant terms are also those proportional to $\langle |\delta \dot{Q}_{e\text{-ph} \text{shot}}(\omega)|^2$ and $\langle |\delta I_{J\text{shot}}(\omega)|^2 \rangle$, with the electron-phonon noise being the larger one in the greater part of the parameter range—but not everywhere. The sum of these two terms is 2 orders of magnitude larger than the sum of the terms proportional to $\langle |\delta \dot{Q}_{J\text{shot}}(\omega)|^2 \rangle$ and $\langle \delta I_{J\text{shot}}(\omega) \delta \dot{Q}_{J\text{shot}}^*(\omega) \rangle$.

In Fig. 7, we plot the current noise, divided by the height of the current pulse $\Delta I_{J,\text{max}}$, as exemplified in Fig. 6(a). This ratio should be below 1, to ensure that the pulse may be observed from the noise. We see that the SPC could function at voltage bias in the low-temperature limit (around 30 mK) but in general, in the parameter range



FIG. 8. The voltage fluctuation divided by the height of the voltage pulse produced by the photon absorption. We assume that the detector works as an SPC if this ratio is smaller than 1.

investigated, the noise may hide the signal produced by the photon.

The situation is better for current-biased measurements. In Fig. 8, we plot the voltage noise divided by the height of the voltage pulse [see Fig. 6(b)]. We see that the detector permits the counting of 1-cm-wavelength photons in the whole range of parameters analyzed.

IV. CONCLUSIONS

We investigate the possibility of using the cold-electron bolometer (CEB) as a counter for photons of wavelengths up to 1 cm. The CEB consists of a normal-metal island, coupled to the superconducting antenna by two symmetric normal-metal-insulator-superconductor (*N-I-S*) tunnel junctions, realizing the so-called *S-I-N-I-S* structure (see Fig. 1). We present the general formalism and the numerical calculations for a bath temperature (T_b) range from 30 mK to 50 mK. In this temperature range, the flux of 1-cmwavelength photons that hit the detector, coming from the environment, is less than one photon in 100 h (see Fig. 2). This makes the detector suitable for counting low-energy photons generated by rare events.

We investigate both the voltage-biased setup—when the measured quantity is the current—and the current-biased setup—when the measured quantity is the voltage. We compare the response of the detector (shown in Figs. 5 and 6) with the fluctuation of the measured quantity (see Figs. 7–10).

Due to the intrinsic shot noise of the current, the voltagebiased setup is more noisy than the current-biased setup. For a volume $\Omega = 0.01 \ \mu m^3$, both current- and voltagebiased CEBs may detect 1-cm-wavelength photons, but the current-biased detectors are more accurate. The signal (due to photon absorption) is bigger than the noise in



FIG. 9. The current fluctuation divided by the height of the current pulse created by the photon absorption, for $\Omega = 0.1 \ \mu \text{m}^3$. The fluctuation is bigger than the pulse for the whole range of parameters.

the current-biased CEB for the whole temperature range investigated (see Fig. 8), whereas for the voltage-biased CEBs, the signal is bigger than the noise only in a part of the parameter range, as can be seen in Fig. 7.

If the volume of the normal-metal island is $\Omega = 0.1 \ \mu m^3$, in the temperature range investigated, the noise in current in the voltage-biased setup is bigger than the current pulse produced by the photon absorption (see Fig. 9). Therefore, the detection of 1-cm-wavelength photons does not seem to be possible. On the other hand, in the current-biased setup, the counter may work, since the voltage pulse produced by the photon absorption is bigger than the noise,



FIG. 10. The voltage fluctuation divided by the height of the (absolute value of the) voltage pulse created by the photon absorption, for $\Omega = 0.1 \ \mu m^3$. The fluctuation is smaller than the pulse—so the detector may work as an SPC—in the lower part of the temperature range.

at least in some ranges of the parameters, as seen in Fig. 10. Nevertheless, the system may be improved. For example, by reducing the tunneling resistance R_T , the cooling properties of the *N-I-S* junctions are improved (if the quasiparticles in the superconductor are properly removed from the vicinity of the junction) and the detector becomes more sensitive. On the other hand, the reduction of the tunneling resistance would increase the noise as well, so the optimization of the SPC is not straightforward and requires a detailed analysis.

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APPENDIX A: RESULTS FOR A VOLUME OF THE NORMAL METAL OF 0.1 μ m³

For comparison, we present the relative fluctuations of current and voltage for a detector with $\Omega = 0.1 \ \mu m^3$. The relative fluctuation of the current (the fluctuation of current, divided by the current pulse) in the voltage-biased setup is presented in Fig. 9 and the relative fluctuation of the voltage (the voltage fluctuation divided by the voltage pulse) is presented in Fig. 10. We observe that in the voltage-biased setup $\sqrt{\langle \delta^2 I_J \rangle_m} / \Delta I_{J,\max} > 1$, so the signal is smaller than the noise. In principle, in such a situation the signal cannot be distinguished from the noise. On the other hand, in the current-biased setup, in some ranges of parameters, the signal is bigger than the noise [i.e., $\sqrt{\langle \delta^2 (eV) \rangle_m} / |\Delta eV_{\max}| < 1$] and the device may function as a photon counter, even for such a relatively large volume.

APPENDIX B: FLUCTUATIONS AND THE NEP IN INTEGRATING DETECTORS AND SPCs

1. Integrating detectors

Noise in integrating detectors has been calculated before (see, e.g., Refs. [44,47]). The figure of merit for such detectors is the NEP, which represents the signal power that gives a signal-to-noise ratio equal to 1. To calculate the NEP, one has to calculate the added contributions of all the sources of noise in the detector. In Ref. [47], the NEP

of a voltage-biased junction was given as (we change the notation slightly, to adapt it to ours)

$$NEP^2 \equiv NEP_{e-ph}^2 + NEP_J^2, \qquad (B1a)$$

where we omit a term $\langle |\delta I_{Jamp}|^2 \rangle / S_I^2(0, V)$ [S_I is defined in Eq. (B1g)], representing the contribution due to the sensitivity of the amplifier, which we cannot calculate and therefore do not take into account (as mentioned before)—this term has to be added to the final result. In Eq. (B1a), NEP_J^2 is the noise associated with the transport through the junctions (in Ref. [47] there was only one *N*-*I*-*S* junction, whereas we have two) and NEP_{e-ph}^2 is the shot noise due to electron-phonon interaction. In our model, both junctions are identical and, according to [47], each contributes with

$$\frac{\text{NEP}_{J}^{2}}{2} = \langle |\delta \dot{Q}_{J\text{shot}}(\omega)|^{2} \rangle - 2 \frac{\langle \delta \dot{Q}_{J\text{shot}}(\omega) \delta I_{J\text{shot}}^{*}(\omega) \rangle}{S_{I}(0, V)} + \frac{\langle |\delta I_{J\text{shot}}(\omega)|^{2} \rangle}{S_{I}^{2}(0, V)}, \quad (B1b)$$

whereas [47,56]

$$\mathrm{NEP}_{e\text{-ph}}^{2} = 10k_{B}\Sigma_{e\text{-ph}}\Omega(T_{e}^{6} + T_{ph}^{6}) \equiv \langle |\delta \dot{Q}_{e\text{-ph}}(\omega)|^{2} \rangle$$
(B1c)

(in our case, $T_{\rm ph} = T_b$). The terms appearing in Eq. (B1b) are the shot noise of the heat power through one *N-I-S* junction [44,47],

$$\langle |\delta \dot{Q}_{J \text{shot}}(\omega)|^2 \rangle = 2 \int_{\Delta}^{\infty} [(\epsilon - eV)^2 (j_1 + j_3) - (\epsilon + eV)^2 \times (j_4 + j_2)] d\epsilon, \qquad (B1d)$$

the current shot noise,

$$\langle |\delta I_{J \text{shot}(\omega)}|^2 \rangle = 2e^2 \int_{\Delta}^{\infty} [j_1(\epsilon) + j_2(\epsilon) + j_3(\epsilon) + j_4(\epsilon)],$$
(B1e)

the correlation between the heat-power shot noise and the current shot noise,

$$\langle \delta \dot{Q}_{J \text{shot}}(\omega) \delta I_{J \text{shot}}^{*}(\omega) \rangle$$

= $2e \int_{\Delta}^{\infty} [(\epsilon - eV)(j_{1} + j_{3})] - (\epsilon + eV)(j_{4} + j_{2})] d\epsilon$
= $\langle \delta \dot{Q}_{J \text{shot}}^{*}(\omega) \delta I_{J \text{shot}}(\omega) \rangle$, (B1f)

and the current responsivity,

$$S_I(\omega, V) = \frac{\partial I_J / \partial T_e}{-i\omega C_V + \partial \dot{Q}_T / \partial T_e} \equiv \frac{S_I(0, V)}{-i\omega \tau + 1}, \quad (B1g)$$

where $S_I(0, V) \equiv (\partial I_J / \partial T_e) / (\partial \dot{Q}_T / \partial T_e)$.

Nevertheless, in Ref. [44] it has been shown that other terms contribute to the total fluctuations, as we explain below. The fluctuation of the power exchange between the electrons of the normal metal and the other subsystems leads to fluctuations of the electron temperature, whereas the fluctuation of the (electron) current leads to the fluctuation of the Fermi energy, which may be interpreted as a fluctuation of the applied voltage. These fluctuations should also be taken into account in the calculation of the NEP of the detector, since they lead to extra contributions to the fluctuations of the measured quantity I_J . In this way, one arrives at a self-consistent set of equations, which may be solved for an exact solution, or one may only plug in the different sources of shot noise, for a perturbative calculation. These extra contributions may be obtained by writing the detailed energy-balance equations in the normal metal (for details, see Ref. [44]). Applying the Fourier transformation, these equations may be formally written as

$$\Delta_T(\omega) = \Delta'_T(\omega), \tag{B2a}$$

where the fluctuation of temperature,

$$\Delta_T(\omega) = \delta T_e(\omega) \left[-i\omega C_V + \frac{\partial}{\partial T_e} (2\dot{Q}_J + \dot{Q}_{e\text{-ph}}) \right]$$

$$\equiv \delta T_e(\omega) Z_T, \qquad (B2b)$$

is related to the fluctuation of power,

$$\Delta_T'(\omega) = -\delta \dot{Q}_{J1}(\omega) - \delta \dot{Q}_{J2}(\omega) - \delta \dot{Q}_{e-\text{ph}}(\omega) + \delta \dot{Q}_{oe}(\omega) + \frac{1}{e} \frac{\partial \epsilon_F}{\partial N} \frac{\partial \dot{Q}_{J1}}{\partial (eV)} \frac{\delta I_{J1}(\omega)}{i\omega} + \frac{1}{e} \frac{\partial \epsilon_F}{\partial N} \frac{\partial \dot{Q}_{J2}}{\partial (eV)} \frac{\delta I_{J2}(\omega)}{i\omega},$$
(B2c)

and we define the thermal impedance of the electron system, $Z_T(\omega)$ —in Eq. (B2c) we take into account that we have two junctions, J1 and J2. Comparing Eqs. (B2b) and (B1g), we observe that

$$Z_T(\omega) = \frac{1}{S_I(\omega, V)} \frac{\partial I_J}{\partial T_e}.$$
 (B3)

In addition to Ref. [47], one should also take into account the fluctuation due to the incoming radiation, denoted here by $\dot{Q}_{oe}(\omega)$, since this produces shot noise at the very least. Equations (B2) are a simplified version of Eqs. (10)–(12) of Ref. [44]. The difference comes from the fact that here we consider $T_{\rm ph} = T_b$ = constant and we assume that the incoming radiation does not directly interact with the lattice (phonons). Under these simplifying assumptions, calculation of the mean-square fluctuations gives

$$\begin{aligned} \langle |\Delta_T(\omega)|^2 \rangle &= \langle \delta^2 T_e \rangle_\omega \, |Z_T(\omega)|^2 \\ &= \langle |\delta \dot{Q}_{e\text{-ph shot}}(\omega)|^2 \rangle + \langle |\delta \dot{Q}_{oe \text{ shot}}(\omega)|^2 \rangle + \Upsilon(\omega) \\ &\equiv \langle |\Delta'_T(\omega)|^2 \rangle, \end{aligned} \tag{B4a}$$

where $\delta \dot{Q}_{e-\text{ph shot}}(\omega)$ is the shot noise of the incoming (optical) power and we denote

$$\Upsilon(\omega) \equiv 2 \left\langle \left| -\delta \dot{Q}_{J \text{ shot}}(\omega) + \frac{1}{e} \frac{\partial \epsilon_F}{\partial N} \frac{\partial \dot{Q}_J}{\partial (eV)} \frac{\delta I_{J \text{ shot}}(\omega)}{i\omega} \right|^2 \right\rangle$$
$$= 2 \left\langle |\delta \dot{Q}_{J \text{ shot}}(\omega)|^2 \right\rangle + \frac{2}{\omega^2 e^2} \left(\frac{\partial \epsilon_F}{\partial N} \frac{\partial \dot{Q}_J}{\partial (eV)} \right)^2$$
$$\times \left\langle |\delta I_{J \text{ shot}}(\omega)|^2 \right\rangle. \tag{B4b}$$

In Eq. (B4b), we take into account that the correlation between $\delta \dot{Q}_{J\text{shot}}(\omega)$ and $\delta I_{J\text{shot}}(\omega)/i\omega$ is zero because of the $\pi/2$ phase difference. In Eq. (B4b), we drop the separate subscripts J1 and J2 used in Eq. (B2c), by making the simplifying assumption that the noise contributions are uncorrelated between the two junctions.

From Eqs. (B2)-(B4), we can calculate the spectral density of the temperature noise, which may be used further for the calculation of the fluctuation of the junction current, as shown in Eq. (12a). In Eq. (12a), we use Re $\left| \langle |\delta I_J(\omega)|^2 / (ie\omega) \rangle \right| =$ 0 and we assume that the changes in the chemical potential μ due to temperature fluctuations are negligible. The correlations Re $\left[\langle \delta I_J(\omega) \delta T_e^*(\omega) \rangle\right]$ and Re $\left[\langle \delta I_J(\omega) \delta T_{\rho}^*(\omega) / (ie\omega) \rangle \right]$ = Im $\left[\langle \delta I_J(\omega) \delta T_{\rho}^*(\omega) \rangle \right]$ $/(e\omega)$ should be calculated using Eq. (B2)—by Im (·), we denote the imaginary part of a complex number. Having the fluctuation of the current, we can calculate the NEP. For this, we have to calculate the energy of the incoming radiation (in the unit bandwidth), which produces a signal equal to the fluctuation of the current (12a). The incoming radiation produces a change in the electron temperature $\delta_s T_e(\omega)$, which produces a signal $\delta_s I_I(\omega)$. The two quantities are related by

$$\delta_s I_J(\omega) = \frac{\partial I_J}{\partial T_e} \delta_s T_e \equiv \frac{\partial I_J}{\partial T_e} \frac{\dot{Q}_{oe}}{Z_T(\omega)} \equiv S_I(\omega, V) Q_{oe}.$$
 (B5)

Equating $|\delta_s I_J(\omega)|^2$ with $\langle |\delta I_J(\omega)|^2 \rangle$ obtained from Eq. (12a), we finally get the full expression of the NEP,

$$\operatorname{NEP}_{t}^{2}(\omega) \equiv \frac{\langle |\delta I_{J}(\omega)|^{2} \rangle}{|S_{I}(\omega, V)|^{2}} = \langle |\Delta_{T}'(\omega)|^{2} \rangle + 2 \frac{\langle |\delta I_{J \operatorname{shot}}(\omega)|^{2} \rangle}{|S_{I}(\omega, V)|^{2}}$$

$$+ \frac{2}{e^2 \omega^2} \left(\frac{\partial \epsilon_F}{\partial N} \frac{\partial I_J}{\partial (eV)} \right)^2 \frac{\langle |\delta I_J(\omega)|^2 \rangle}{|S_I(\omega, V)|^2} + \frac{2 \text{Corr}(\omega)}{|S_I(\omega, V)|^2}, \tag{B6}$$

where $Corr(\omega)$ denotes the two correlation terms from Eq. (12a). From Eq. (B6), we arrive at

N

$$\begin{split} \mathrm{EP}_{t}^{2}(\omega) &= \langle |\delta \dot{Q}_{e\text{-ph shot}}(\omega)|^{2} \rangle + \langle |\delta \dot{Q}_{oe \text{ shot}}(\omega)|^{2} \rangle \\ &+ 2 \langle |\delta \dot{Q}_{J\text{ shot}}(\omega)|^{2} \rangle + 2 \frac{\langle |\delta I_{J\text{ shot}}(\omega)|^{2} \rangle}{|S_{I}(\omega, V)|^{2}} \\ &+ \frac{2}{\omega^{2}e^{2}} \left(\frac{\partial \epsilon_{F}}{\partial N} \frac{\partial \dot{Q}_{J}}{\partial (eV)} \right)^{2} \langle |\delta I_{J\text{ shot}}(\omega)|^{2} \rangle \\ &+ \frac{2}{e^{2}\omega^{2}} \left(\frac{\partial \epsilon_{F}}{\partial N} \frac{\partial I_{J}}{\partial (eV)} \right)^{2} \frac{\langle |\delta I_{J}(\omega)|^{2} \rangle}{|S_{I}(\omega, V)|^{2}} \\ &+ 4 \frac{\partial I_{J}}{\partial T_{e}} \frac{\mathrm{Re}}{|S_{I}(\omega)|^{2}} \frac{\langle \delta I_{J}(\omega) \delta T_{e}^{*}(\omega) \rangle}{|S_{I}(\omega, V)|^{2}} \\ &+ \frac{4}{e\omega} \frac{\partial \epsilon_{F}}{\partial N} \frac{\partial I_{J}}{\partial (eV)} \frac{\partial I_{J}}{\partial T_{e}} \frac{\mathrm{Im}}{|S_{I}(\omega, V)|^{2}}, \end{split}$$
(B7)

Using Eq. (B2), we calculate, in the lowest order [i.e., taking only the shot noise contributions to $\delta I_J(\omega) \equiv \delta I_{J\text{shot}}(\omega)$ and $\delta \dot{Q}_J(\omega) \equiv \delta \dot{Q}_{J\text{shot}}(\omega)$], the correlation

$$\langle \delta I_{J}(\omega) \delta T_{e}^{*}(\omega) \rangle = \left\langle \frac{\delta I_{J \text{shot}}(\omega)}{Z_{T}^{*}(\omega)} \left[-\delta \dot{Q}_{J \text{shot}}(\omega) + \frac{1}{e} \frac{\partial \epsilon_{F}}{\partial N} \frac{\partial \dot{Q}_{J1}}{\partial (eV)} \frac{\delta I_{J \text{shot}}(\omega)}{i\omega} \right]^{*} \right\rangle$$

$$= -\left\langle \frac{\delta I_{J \text{shot}}(\omega) \delta \dot{Q}_{J \text{shot}}^{*}(\omega)}{Z_{T}^{*}(\omega)} \right\rangle$$

$$- \frac{1}{e} \frac{\partial \epsilon_{F}}{\partial N} \frac{\partial \dot{Q}_{J1}}{\partial (eV)} \left\langle \frac{|\delta I_{J \text{shot}}(\omega)|^{2}}{i\omega Z_{T}^{*}(\omega)} \right\rangle.$$
(B8a)

Using Eq. (B8a), we obtain

$$\operatorname{Re}\left[\langle \delta I_{J}(\omega) \delta T_{e}^{*}(\omega) \rangle\right] = -\frac{Z_{T}(0)}{|Z_{T}(\omega)|^{2}} \langle \delta I_{J \operatorname{shot}}(\omega) \delta \dot{Q}_{J \operatorname{shot}}^{*}(\omega) \rangle + \frac{1}{e} \frac{\partial \epsilon_{F}}{\partial N} \frac{\partial \dot{Q}_{J1}}{\partial (eV)} \frac{C_{V}}{|Z_{T}(\omega)|^{2}} \times \langle |\delta I_{J \operatorname{shot}}(\omega)|^{2} \rangle \quad (B8b)$$

and

$$\operatorname{Im} \left[\langle \delta I_{J}(\omega) \delta T_{e}^{*}(\omega) \rangle \right]$$

= $\frac{\omega C_{V}}{|Z_{T}(\omega)|^{2}} \langle \delta I_{J \operatorname{shot}}(\omega) \delta \dot{Q}_{J \operatorname{shot}}^{*}(\omega) \rangle$
+ $\frac{1}{e} \frac{\partial \epsilon_{F}}{\partial N} \frac{\partial \dot{Q}_{J}}{\partial (eV)} \frac{Z_{T}(0)}{\omega |Z_{T}(\omega)|^{2}} \times \langle |\delta I_{J \operatorname{shot}}(\omega)|^{2} \rangle$ (B8c)

[note that $\langle \delta I_{J\text{shot}}(\omega) \delta \dot{Q}_{J\text{shot}}^*(\omega) \rangle$ is real, as specified in Eq. (B1f)]. Combining Eq. (B7) with Eq. (B8), we obtain the expression for the total noise, which we formally write as

$$NEP_t^2(\omega) = \sum_{i=0}^{8} NEP_i,$$
 (B9a)

where

$$\text{NEP}_{0} \equiv \langle |\delta \dot{Q}_{e\text{-ph shot}}(\omega)|^{2} \rangle + \langle |\delta \dot{Q}_{oe \text{ shot}}(\omega)|^{2} \rangle, \qquad (\text{B9b})$$

$$NEP_1 \equiv 2\langle |\delta \hat{Q}_{Jshot}(\omega)|^2 \rangle, \tag{B9c}$$

$$NEP_2 \equiv 2 \frac{\langle |\delta I_{Jshot}(\omega)|^2 \rangle}{|S_I(\omega, V)|^2},$$
(B9d)

$$\text{NEP}_{3} \equiv -4\langle \delta I_{J \text{shot}}(\omega) \delta \dot{Q}_{J \text{shot}}^{*}(\omega) \rangle / S_{I}(0, V), \qquad (\text{B9e})$$

$$\mathrm{NEP}_{4} \equiv \frac{2}{e^{2}\omega^{2}} \left(\frac{\partial \epsilon_{F}}{\partial N} \frac{\partial \dot{Q}_{J}}{\partial (eV)} \right)^{2} \langle |\delta I_{J\mathrm{shot}}(\omega)|^{2} \rangle, \qquad (\mathrm{B9f})$$

$$\text{NEP}_{5} \equiv \frac{2}{e^{2}\omega^{2}} \left(\frac{\partial\epsilon_{F}}{\partial N} \frac{\partial I_{J}}{\partial(eV)}\right)^{2} \frac{\langle |\delta I_{J\,\text{shot}}(\omega)|^{2} \rangle}{|S_{I}(\omega,V)|^{2}}, \qquad (B9g)$$

$$\text{NEP}_{6} \equiv \frac{4C_{V}}{e} \left(\frac{\partial I_{J}}{\partial T_{e}}\right)^{-1} \frac{\partial \epsilon_{\text{F}}}{\partial N} \frac{\partial \dot{Q}_{J}}{\partial (eV)} \langle |\delta I_{J\text{shot}}(\omega)|^{2} \rangle, \quad (B9h)$$

$$NEP_{7} \equiv \frac{4C_{V}}{e} \frac{\partial \epsilon_{F}}{\partial N} \frac{\partial I_{J}}{\partial (eV)} \left(\frac{\partial I_{J}}{\partial T_{e}}\right)^{-1} \\ \times \langle \delta I_{J\text{shot}}(\omega) \delta \dot{Q}_{J\text{shot}}^{*}(\omega) \rangle,$$
(B9i)

$$\text{NEP}_{8} \equiv \frac{4}{e^{2}\omega^{2}} \left(\frac{\partial\epsilon_{F}}{\partial N}\right)^{2} \frac{\partial I_{J}}{\partial(eV)} \frac{\partial \dot{Q}_{J}}{\partial(eV)} \frac{\langle |\delta I_{J\text{shot}}(\omega)|^{2} \rangle}{S_{I}(0,V)}.$$
(B9j)

We note that the terms (B9b)–(B9e) contain all the terms of Eq. (B1) [47]. But, besides the term $\langle |\delta \dot{Q}_{oe shot}(\omega)|^2 \rangle$, which is not taken into account in Eq. (B1), we note another difference. The term NEP₂ $\equiv 2\langle |\delta I_{Jshot}(\omega)|^2 \rangle / |S_I(\omega, V)|^2$, which *is* ω *dependent*, appears in Eq. (B1)–and in Ref. [47]–as NEP'₂ $\equiv 2\langle |\delta I_{Jshot}(\omega)|^2 \rangle / |S_I(0, V)|^2$, which *is* ω *independent*. This mathematical difference, although well justified in our formalism, has also a simple intuitive explanation: to produce the same current oscillations, the amplitude of the power oscillations should increase with frequency due to the thermal inertia of the electron gas. This leads to the increase of the contribution of $\delta I_{Jshot}(\omega)$ with ω in our expression for NEP.

a. Evaluation of the contributions to the NEP in the low-temperature limit

Let us derive simplified expressions for the terms of NEP_t²(ω) (B9), which are valid at low temperatures, $T_e, T_b \ll \Delta/k_B$ (approximately 2.32 K, for $\Delta = 0.2$ meV in Al). At such temperatures, we ignore the currents of holes and the population of quasiparticle states in the superconductor by using the approximation

$$f(\epsilon + eV, T_e) \approx f(\epsilon, T_b) \approx 0.$$
 (B10)

Then, the current I_J through one junction (7a) may be simplified to

$$I_J \approx \frac{1}{eR_T} \int_{\Delta}^{\infty} \frac{\epsilon}{\sqrt{\epsilon^2 - \Delta^2}} \frac{d\epsilon}{e^{\beta_e(\epsilon - eV)} + 1}.$$
 (B11)

We introduce the notation $x \equiv \beta_e(\epsilon - \Delta)$, $a_e \equiv \beta_e(\Delta - eV)$, and $A_e \equiv \beta_e \Delta$, in order to write

$$I_J = \frac{1}{eR_T} \frac{k_B T}{\sqrt{2A_e}} \int_0^\infty \frac{x + A_e}{\sqrt{x[1 + x/(2A_e)]}} \frac{dx}{e^{x + a_e} + 1}$$

Using the Taylor expansion $1/\sqrt{1+\delta} \approx 1-\delta/2$ [in this case, $\delta \equiv x/(2A_e)$], we obtain

$$I_J \approx \frac{1}{eR_T} \frac{(k_B T)^{3/2}}{\sqrt{2\Delta}} \int_0^\infty \left(\sqrt{x} + \frac{A_e}{\sqrt{x}}\right) \left(1 - \frac{x}{4A_e}\right)$$
$$\times \frac{dx}{e^{x+a_e} + 1} \approx \frac{1}{eR_T} \frac{(k_B T)^{3/2}}{\sqrt{2\Delta}} \left[\frac{3}{4} \int_0^\infty \frac{\sqrt{x} \, dx}{e^{x+a_e} + 1}\right]$$
$$+ A_e \int_0^\infty \frac{dx}{\sqrt{x} \left(e^{x+a_e} + 1\right)} = -\frac{\sqrt{k_B T \Delta}}{eR_T} \sqrt{\frac{\pi}{2}}$$
$$\times \left[\operatorname{Li}_{1/2} \left(-e^{-a_e}\right) + \frac{3}{8} \frac{k_B T}{\Delta} \operatorname{Li}_{3/2} \left(-e^{-a_e}\right)\right], \quad (B12)$$

where we keep only the two highest-order terms in A_e and $\operatorname{Li}_m(x)$ is the polylogarithm of order *m* in *x* [57–60] [note that $\operatorname{Li}_l(-e^{-a_e}) < 0$; hence the global "–" sign in the equations involving polylogarithms]. Similarly, the heat power through a *N-I-S* junction (7b) is reduced to [44]

$$\dot{Q}_{J} \approx \frac{1}{e^{2}R_{T}} \int_{\Delta}^{\infty} \frac{(\epsilon - eV)\epsilon}{\sqrt{\epsilon^{2} - \Delta^{2}}} \frac{d\epsilon}{e^{\beta_{e}(\epsilon - eV)} + 1}$$

$$\approx -\frac{1}{e^{2}R_{T}} \sqrt{\frac{\pi (k_{B}T)^{3}\Delta}{2}} \left[\frac{1}{2} \left(1 + \frac{3}{4} \frac{a_{e}}{A_{e}} \right) \operatorname{Li}_{3/2}(-e^{-a_{e}}) + a_{e} \operatorname{Li}_{1/2}(-e^{-a_{e}}) + \frac{3}{4A_{e}} \operatorname{Li}_{5/2}(-e^{-a_{e}}) \right]. \quad (B13)$$

If one neglects the terms proportional to $1/A_e$ in the square brackets of Eq. (B13), one can obtain the so-called *optimum cooling power*, for $a_e \approx 0.66$.

The current shot noise through one junction is given by Eq. (B1e). Ignoring again the tunneling of holes and the populations of the quasiparticle states in the superconductor, this reduces to

$$\langle |\delta I_{J \text{shot}}(\omega)|^2 \rangle \approx \frac{2e^2}{e^2 R_T} \int_{\Delta}^{\infty} \frac{\epsilon}{\sqrt{\epsilon^2 - \Delta^2}} \frac{d\epsilon}{e^{\beta_e(\epsilon - eV)} + 1}$$

= 2eI_J. (B14)

The heat-current fluctuation through one junction, in the approximation (B10), is

$$\langle |\delta \dot{Q}_{J \text{shot}}(\omega)|^{2} \rangle \approx \frac{2}{e^{2} R_{T}} \int_{\Delta}^{\infty} \frac{\epsilon(\epsilon - eV)^{2}}{\sqrt{\epsilon^{2} - \Delta^{2}}} \frac{d\epsilon}{e^{\beta_{e}(\epsilon - eV)} + 1}$$

$$\approx -\frac{2(k_{B}T)^{5/2}}{e^{2} R_{T}} \sqrt{\frac{\pi \Delta}{2}} \left[\frac{45}{32A_{e}} \text{Li}_{7/2} \left(-e^{-a_{e}} \right) \right]$$

$$+ \frac{3}{4} \left(1 + \frac{3}{2} \frac{a_{e}}{A_{e}} \right) \text{Li}_{5/2} \left(-e^{-a_{e}} \right)$$

$$+ a_{e} \left(1 + \frac{3}{8} \frac{a_{e}}{A_{e}} \right) \text{Li}_{3/2} \left(-e^{-a_{e}} \right)$$

$$+ a_{e}^{2} \text{Li}_{1/2} \left(-e^{-a_{e}} \right)], \qquad (B15)$$

whereas the correlation between the heat and current fluctuations is

$$\begin{split} \langle \delta \dot{I}_{J \text{shot}}(\omega) \delta \dot{Q}_{J \text{shot}}^{*}(\omega) \rangle &\approx \frac{2}{eR_{T}} \int_{\Delta}^{\infty} \frac{\epsilon(\epsilon - eV)}{\sqrt{\epsilon^{2} - \Delta^{2}}} \frac{d\epsilon}{e^{\beta_{e}(\epsilon - eV)} + 1} \\ &\approx -\frac{2(k_{B}T)^{3/2}}{eR_{T}} \sqrt{\frac{\pi \Delta}{2}} \\ &\times \left[\frac{9}{16A_{e}} \text{Li}_{5/2} \left(-e^{-a_{e}} \right) \right. \\ &\left. + \frac{1}{2} \left(1 + \frac{3}{4} \frac{a_{e}}{A_{e}} \right) \text{Li}_{3/2} \left(-e^{-a_{e}} \right) \right. \\ &\left. + a_{e} \text{Li}_{1/2} \left(-e^{-a_{e}} \right) \right]. \end{split}$$
(B16)

We now calculate the partial derivatives:

$$\frac{\partial I_J}{\partial (k_B T_e)} \approx \frac{\beta_e^2}{eR_T} \int_{\Delta}^{\infty} \frac{\epsilon(\epsilon - eV)}{\sqrt{\epsilon^2 - \Delta^2}} \frac{e^{\beta_e(\epsilon - eV)}}{[e^{\beta_e(\epsilon - eV)} + 1]^2} d\epsilon$$
$$\approx -\frac{1}{eR_T} \sqrt{\frac{\pi \Delta}{2k_B T}} \left[\frac{9}{16A_e} \text{Li}_{3/2} \left(-e^{-a_e} \right) \right.$$
$$\left. + \frac{1}{2} \left(1 + \frac{3}{4} \frac{a_e}{A_e} \right) \text{Li}_{1/2} \left(-e^{-a_e} \right) \right.$$
$$\left. + a_e \text{Li}_{-1/2} \left(-e^{-a_e} \right) \right], \qquad (B17a)$$

$$\frac{\partial I_J}{\partial (eV)} \approx \frac{\beta_e}{eR_T} \int_{\Delta}^{\infty} \frac{\epsilon}{\sqrt{\epsilon^2 - \Delta^2}} \frac{e^{\beta_e(\epsilon - eV)}}{[e^{\beta_e(\epsilon - eV)} + 1]^2} d\epsilon$$
$$\approx -\frac{1}{eR_T} \sqrt{\frac{\pi \Delta}{2k_B T}} \left\{ \frac{3}{8A_e} \mathrm{Li}_{1/2} \left(-e^{-a_e} \right) + \mathrm{Li}_{-1/2} \left(-e^{-a_e} \right) \right\}, \tag{B17b}$$

$$\begin{aligned} \frac{\partial \dot{Q}_J}{\partial (k_B T_e)} &\approx \frac{\beta_e^2}{e^2 R_T} \int_{\Delta}^{\infty} \frac{\epsilon (\epsilon - eV)^2}{\sqrt{\epsilon^2 - \Delta^2}} \frac{e^{\beta_e (\epsilon - eV)} d\epsilon}{[e^{\beta_e (\epsilon - eV)} + 1]^2}, \\ &\approx -\frac{k_B T_e}{e^2 R_T} \sqrt{\frac{\pi A_e}{2}} \left[\frac{3}{4} \left(1 + \frac{3}{2} \frac{a_e}{A_e} \right) \operatorname{Li}_{3/2} \left(-e^{-a_e} \right) \right. \\ &\left. + \left(a_e + \frac{3}{8} \frac{a_e^2}{A_e} \right) \operatorname{Li}_{1/2} \left(-e^{-a_e} \right) \right. \\ &\left. + a_e^2 \operatorname{Li}_{-1/2} \left(-e^{-a_e} \right) + \frac{45}{32A_e} \operatorname{Li}_{5/2} \left(-e^{-a_e} \right) \right], \end{aligned}$$
(B17c)

and

$$\frac{\partial \dot{Q}_J}{\partial (eV)} \approx \frac{\beta_e}{e^2 R_T} \int_{\Delta}^{\infty} \frac{\epsilon(\epsilon - eV)}{\sqrt{\epsilon^2 - \Delta^2}} \frac{e^{\beta_e(\epsilon - eV)} d\epsilon}{[e^{\beta_e(\epsilon - eV)} + 1]^2}$$
$$= k_B T_e \frac{\partial I_J}{\partial (k_B T_e)}.$$
(B17d)

In Eq. (B17), we use the general derivation rules for polylogarithms to define

$$\mathrm{Li}_{-1/2}\left(-e^{-a_{e}}\right) \equiv -\frac{d\mathrm{Li}_{1/2}\left(-e^{-a_{e}}\right)}{da_{e}}.$$
 (B18)

Using Eqs. (B9)–(B17), we can calculate NEP_t, which is plotted in Fig. 11, for ω taking values in a relevant interval, $\omega \in [2\pi/(10\tau), 2\pi/(\tau/10)]$, and for $T_b = 30$ mK and 50 mK.

Among the terms NEP_i (i = 0, ..., 8), the dominant one in most of the frequency range of interest is NEP₂. In Fig. 12, we compare NEP₂ with NEP₀ and with the absolute value |NEP₁ + NEP₃ + NEP₅|, for $T_b = 30$ mK—for T_b between 30 and 50 mK, the plots are rather similar. All the other terms, namely NEP₄, NEP₆, NEP₇, and NEP₈, are over 20 orders of magnitude smaller than NEP₀ + NEP₁ + NEP₂ + NEP₃ + NEP₅, so we neglect them in all the calculations. The term $\langle |\delta \dot{Q}_{oe \text{ shot}}(\omega)|^2 \rangle$ is relevant only for integrating detectors, so we also disregard it in our analysis of SPCs. Therefore, the relevant terms may be grouped in three categories, according to their ω dependence:

NEP_t² =
$$A + \frac{B}{|S_I(\omega, V)|^2} + \frac{C}{\omega^2 |S_I(\omega, V)|^2}$$
, (B19a)



FIG. 11. The NEP_t (without taking into consideration $\langle |\delta \dot{Q}_{oe\,\text{shot}}(\omega)|^2 \rangle$) vs $\omega/(2\pi/\tau) \equiv \nu\tau$ and $1 - eV/\Delta$ for two values of the bath temperature: $T_b = 30$ mK and $T_b = 50$ mK, as indicated.

where

$$A \equiv \langle |\delta \dot{Q}_{e\text{-ph shot}}(\omega)|^2 \rangle + 2 \langle |\delta \dot{Q}_{J\text{shot}}(\omega)|^2 \rangle - \frac{4 \langle \delta I_{J\text{shot}}(\omega) \delta \dot{Q}^*_{J\text{shot}}(\omega) \rangle}{S_I(0, V)}, \quad (B19b)$$

$$B \equiv 2 \langle |\delta I_{J \text{shot}}(\omega)|^2 \rangle, \qquad (B19c)$$

and

$$C \equiv \frac{2}{e^2} \left(\frac{\partial \epsilon_F}{\partial N} \frac{\partial I_J}{\partial (eV)} \right)^2 \langle |\delta I_{J \text{shot}}(\omega)|^2 \rangle.$$
(B19d)

Vice versa, from Eq. (B19) and the definition of NEP, we get the expression for the current fluctuation,

$$\langle |\delta I_J(\omega)|^2 \rangle = |S_I(\omega, V)|^2 \operatorname{NEP}_t^2 = |S_I(\omega, V)|^2 A + B + \frac{C}{\omega^2}.$$
(B20)



FIG. 12. The ratios NEP_0/NEP_2 and $|NEP_1 + NEP_3 + NEP_5|/NEP_2$, for two values of T_b —NEP₀, NEP₁, NEP₂, NEP₃, and NEP₅ are the only relevant contributions to NEP_t. We observe that in the greater part of the parameter range, NEP₂ is the most dominant term.

2. Single-photon counters

The calculation of the NEP is just a prerequisite and cannot be directly compared to the signal produced by the photon absorption in a SPC [7,9,11,21,61]. For example, Hadfield proposes two different definitions for the NEP [61],

$$\operatorname{NEP}_{H1} \equiv (h\nu/\eta)\sqrt{2D}$$
 and $\operatorname{NEP}_{H2} \equiv \eta/(D\Delta t)$,
(B21)

to qualitatively adapt it to the SPC. In Eq. (B21), hv is the energy of the photon, η is the detection efficiency (number of detected photons divided by the number of incident photons), D is the dark-count rate, and Δt is the timing jitter of the detector (the variation of the time interval between the absorption of a photon and the generation of the output electrical pulse)—note that while NEP_{H1} has units of W Hz^{-1/2}, NEP_{H2} is dimensionless. While both definitions (B21) represent qualitative scales for the performance of the detectors, they are of no practical use for our SPC, since they cannot discern between the cases when the photon can or cannot be observed.

Another estimation of the energy resolution of the SPC was used in Ref. [9], as $\delta E_G = \text{NEP}_G \tau^{-1/2}$, where $NEP_G \equiv NET_G C_V$, is the noise-equivalent power, NET_G is the noise-equivalent temperature, and τ is the reequilibration time of the detector. This formula for the energy resolution represents the contribution of the NEP in a frequency window equal to τ^{-1} . However, in Sec. III we show that in order to detect the photon, the current signal produced by its absorption should be bigger than the fluctuation of the current in the frequency window of the filter. The use of an excessively low frequency cutoff (such as $1/\tau$, in this case), would drastically reduce not only the noise but also (and especially) the pulse height-as seen, for example, in Eqs. (14) and (15)—and therefore would decrease the detection capabilities of the SPC (in Fig. 6 we use a cutoff time $\tau_c = 1$ ns, for a time constant τ more than an order of magnitude bigger). To put it simply, using NEP_G as an estimation of the noise in a SPC gives a unrealistic (too optimistic) estimation of the detector's capabilities.

The importance of recognizing the signal produced by the photon (in the measured quantity) from the detector noise has been shown theoretically in Ref. [21] and has been concretely emphasized by Santavicca et al. in Ref. [7]. In accordance with this, Brange et al. [11] theoretically compare the temperature spike produced by the photon absorption with the Monte Carlo simulation of the noise in the detector. Nevertheless, in both Refs. [7] and [11], concrete criteria for the possibility of detecting the photon are not provided—for example, in Ref. [11], only the temperature variation is visually compared with the temperature noise. Therefore, in addition to this, here and in Ref. [21], we propose a concrete calculation method to compare the measured signal with the average fluctuation of the measured quantity in the relevant time scale of the experiment.

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