# Performance Projections for Two-dimensional Materials in Radio-Frequency Applications

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Given the immense attraction of using two-dimensional materials for high-frequency applications, there is a critical need for computational models that aid the production of high-frequency performance projections based on their material properties. In this work, we use the atomistic nonequilibrium Green's function approach to predict the performance of ballistic radio-frequency transistors based on a broad range of twodimensional semiconducting materials, including MoS<sub>2</sub>, WS<sub>2</sub>, WSe<sub>2</sub>, and phosphorene. Self-consistent ballistic quantum-transport simulations are performed on monolayer transistors with a 15-nm gate length and an effective gate-oxide thickness of 0.44 nm. We show that rather than the bandgap, the effective mass and the dielectric constant significantly influence the unity current gain cutoff frequency ( $f_i$ ), the maximum oscillation frequency ( $f_{max}$ ), and the intrinsic gain ( $G_{int}$ ). Phosphorene with a low effective mass and high dielectric constant is found to be the most promising material with  $f_t \simeq 10$  THz,  $f_{max} \simeq 6$  THz, and  $G_{int} \simeq 100 \ {O}/{O}$ . Results are further corroborated analytically using the Wentzel-Kramers-Brillouin approximation and also benchmarked with previous reports. Furthermore, the effect of extrinsic parameters, such as Schottky barrier height and strain on  $f_t$  and  $f_{max}$ , is discussed. This study can thus be used as a comprehensive, physics-based search guide of two-dimensional materials for radio-frequency applications.

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## I. INTRODUCTION

Low contact resistance, output current saturation, high mobility, and compatibility with CMOS processes are some of the most desirable properties for potential radiofrequency (rf) devices [1]. Silicon-on-insulator (SOI) FETs are promising for rf applications because of their easy manufacture using mainstream Si technology and improved short-channel effects [2–5]. However, the low mobility of silicon and performance degradation due to the increased role of surface roughness in the ultra-thin limit has deterred further improvements with transistor scaling [6]. At the same time, increasing bandwidths in communication systems and sensor applications [7] need devices with operating frequencies deep in the terahertz regime. Graphene with high mobility and saturation velocity has emerged as a prospective material for radio-frequency applications [8– 11]. However, the lack of a bandgap limits its maximum oscillation frequency  $f_{\text{max}}$  (approximately 200 GHz for a gate length of 60 nm) due to high output conductance [12].

Two-dimensional (2D) layered semiconducting materials with their sizeable bandgap and remarkable electronic properties have seen significant research interest for radiofrequency applications [13,14]. Further, the potential to integrate 2D materials on low-cost flexible substrates is an additional advantage over high-cost SOI and III-V semiconductors [15,16]. The ultra-thin nature and the absence of dangling bonds in 2D materials make it possible to scale the FETs down to gate lengths as low as 1 nm [17]. Previous reports on 2D material-based rf devices using MoS<sub>2</sub> [18,19] and black phosphorus [20] have demonstrated unity current gain cutoff frequency  $(f_t)$  and  $f_{max}$  values in the deep GHz regime. In a recent simulation study, Yin et al. [21] predicted the intrinsic performance limit of phosphorene transistors by varying physical parameters such as channel length, effective oxide thickness (EOT) and contact resistance. However, a comprehensive study of the dependence of the two important rf figures of merit (FOM), i.e.,  $f_t$  and  $f_{max}$ , on channel material properties and hence the rf performance projections for different 2D materials is lacking in the current literature.

In this work, a physics-based atomistic simulation platform is developed to make high-frequency performance projections based on channel material properties such as effective mass, dielectric constant, and bandgap. These simulations are performed on a Schottky barrier metal-oxide-semiconductor FET (SB MOSFET) structure with a 15-nm gate length. The nonequilibrium Green's function (NEGF) formalism within the effective mass

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approach self-consistently coupled to Poisson's equation is employed in order to extract the important FOMs for rf applications. Transfer and output characteristics of the simulated devices are compared with previous reports to validate the simulations [22,23]. Further, the variations in  $f_t$ ,  $f_{\text{max}}$  and the intrinsic gain ( $G_{\text{int}}$ ) with effective mass  $(m^*)$  and dielectric constant  $(\epsilon_r)$  are studied to develop a qualitative understanding of the dependence of the rf performance on material properties. Among the various 2D materials analyzed in this work covering a broad range of  $m^*$  and  $\epsilon_r$ , including MoS<sub>2</sub>, WS<sub>2</sub>, WSe<sub>2</sub>, and phosphorene, we find that phosphorene with a low  $m^*$  and high  $\epsilon_r$  is the most promising 2D channel material with the highest  $f_t$  and  $f_{\rm max}$ . Further, the results are analytically validated using the Wentzel-Kramers-Brillouin (WKB) approximation and also benchmarked with previous work [22,23].

This paper begins by describing the methodology and equations used in developing the atomistic simulator. Next, the transistor characteristics are benchmarked to validate the simulation framework used in this work. Then, the important FOMs for various 2D channel materials are extracted and examined in detail. Finally, the paper concludes by summarizing the important results and discussing future scope.

## **II. METHODS**

A schematic overview of the simulation framework is shown in Fig. 1. Various crucial parameters for rf performance such as bandgap,  $m^*$ ,  $\epsilon_r$ , thickness of the 2D channel material and the source and drain Schottky barrier heights (SBH) are given as inputs to the quantum ballistic simulator (QBS), as shown in Fig. 1(a). Bandgap,  $m^*$ , and  $\epsilon_r$ values for different materials considered in this study are available in the Supplemental Material [24–26]. A Schottky barrier SOI transistor structure with 15-nm gate length [Fig. 1(b)] is simulated using the QBS for different channel materials. A monolayer of 2D material is sandwiched between the bottom (8-nm  $SiO_2$ ) and the top oxide  $(2.8-nm HfO_2)$ . These particular device dimensions are chosen to validate the QBS with a previous report [22]. Most metals form Schottky contacts when interfaced with the 2D materials studied in this work. However, large variation is seen in published reports of SBH values for the same metal on a particular 2D material as well as across various 2D materials. Because of this reason, and to ensure that the focus of this work is on evaluating rf performance for variations in intrinsic material properties (bandgap,  $m^*$ ,  $\epsilon_r$ ), constant SBH values of 0.1 eV [22] are assumed at the source and drain contacts for all the materials analyzed in this work. However, we do show the dependence of  $f_t$  and  $f_{max}$  on SBH for specific bandgap,  $m^*$ , and  $\epsilon_r$  values later in the paper ( $f_t$ ) and also in the Supplemental Material  $(f_{\text{max}})$  [26]. Figure 1(c) depicts the schematic QBS output of the simulated devices, i.e., transfer  $(I_D - V_G)$ and output  $(I_D - V_D)$  characteristics at fixed drain bias  $(V_D)$ and gate bias  $(V_G)$ , respectively. Three important figures of merit for rf devices  $(f_t, f_{max}, and G_{int})$  are extracted from the output and transfer characteristics. The quantities  $f_t$  and  $f_{\text{max}}$  are calculated using the following equations:

$$f_t = \frac{g_m}{2\pi C_G},\tag{1}$$

$$f_{\rm max} = \frac{f_t}{2\sqrt{g_d(R_s + R_g W) + 2\pi f_t C_{GD} R_g W}}.$$
 (2)

Here, the transconductance  $(g_m)$ , the gate capacitance  $(C_G)$ , the output conductance  $(g_d)$ , and the gate-to-drain capacitance  $(C_{GD})$  are extracted from the  $I_D$ - $V_G$  and  $I_D$ - $V_D$  characteristics at fixed  $V_D = 0.9$  V,  $V_G = 0.6$  V for a channel width of  $W = 1 \ \mu$ m. Typical values of width-normalized source contact resistance  $(R_S = 500 \ \Omega \ \mu$ m) and gate resistance-width product  $(R_g W = 500 \ \Omega \ \mu$ m) are used to calculate  $f_{\text{max}}$  [23]. The QBS solves the



FIG. 1. Schematic overview of the QBS framework. (a) Database of various 2D materials taken as an input to the QBS. (b) Schematic of the Schottky barrier MOSFET simulated using the QBS. (c) Output conductance  $(g_d)$  and transconductance  $(g_m)$  extracted from  $I_D$ - $V_D$  and  $I_D$ - $V_G$  characteristics, ultimately used in calculating the  $f_t$  and  $f_{max}$ .



FIG. 2. (a),(b) Output and transfer characteristics obtained using QBS for a 15-nm gate length Schottky barrier FET with  $MoS_2$  as the channel material. Simulated characteristics are benchmarked against published data [22].

one-dimensional [along the x direction, see Fig. 1(b)] NEGF equations within the effective mass Hamiltonian framework. It is important to note that electron wave functions are assumed not to extend into the bottom and top oxides due to the large barrier between the channel material and the oxides. Transport equations based on the NEGF formalism are solved self-consistently with Poisson's equation to extract the transfer and output characteristics. The transverse direction [y axis along the width of the channel in Fig. 1(b)] is taken into account by summing over transverse momentum modes (Fig. 1), such that, the drain to source current ( $I_D$ ) is calculated using [22]

$$I_{D} = \frac{e}{\hbar} \sqrt{\frac{m_{y}^{*} k_{B} T}{2\pi^{3}}} \int dE_{k_{x}} \left\{ F_{-1/2} \left( \frac{\mu_{1} - E_{k_{x}}}{k_{B} T} \right) - F_{-1/2} \left( \frac{\mu_{2} - E_{k_{x}}}{k_{B} T} \right) \right\} T_{SD}(E_{k_{x}}),$$
(3)

where  $F_{-1/2}$  is the Fermi-Dirac integral of order -1/2and the transmission coefficient ( $T_{SD}$ ) is calculated from NEGF,  $\mu_1$  and  $\mu_2$  are the source and drain electrochemical potentials,  $\hbar$ ,  $m_y^*$ , e,  $k_B$ , T, and  $E_{k_x}$  are the reduced Planck constant, transverse effective mass, elementary charge, Boltzmann's constant, temperature, and longitudinal energy, respectively. Gate leakage current is not considered in these simulations as it is negligible compared to the drain current at large gate and drain voltages [12]. Dirichlet boundary conditions are used at the contacts, and Neumann boundary conditions are applied at all material-air interfaces [12]. The source terminal is assumed to be grounded.

## **III. RESULTS AND DISCUSSION**

To validate the QBS, the simulated I-V curves of a top gate MoS<sub>2</sub> transistor with a gate length of 15 nm and EOT of 0.44 nm are compared with a previous report [22]. Figures 2(a) and 2(b) show the output and transfer characteristics extracted from OBS and the previous work, respectively [22]. The results are in good agreement at small gate and drain voltages. A slight deviation in the output and transfer characteristics for larger gate voltages could possibly be from differences in device details such as the Fermi energy of the metal, the number of valleys considered, and the metal work function, which were not mentioned in the previous report [22]. In addition to the QBS validation,  $f_t$  for MoS<sub>2</sub> at fixed drain (0.4 V) and gate (0.4 V) voltages is calculated using Eq. (1). Results are further compared and validated with the analytical expression for  $f_t$  calculated using the  $k \cdot p$  model which includes band-to-band tunneling (BTBT), as shown in Fig. 3(b) [23]. A decrease in the channel length leads to a shorter source-to-drain transit time, thereby increasing  $f_t$ . The slight overestimation in  $f_t$  extracted using QBS compared to the  $k \cdot p$  model [23] is due to the absence of a BTBT model in QBS. The BTBT-assisted current



FIG. 3. (a) Various parasitic elements of the Schottky barrier FET crucial to high-frequency performance (i.e.,  $f_t$  and  $f_{max}$ ). (b) Unity current gain cutoff frequency  $f_t$  calculated for monolayer MoS<sub>2</sub> channel from the  $k \cdot p$  model [23] and the effective mass Hamiltonian used in this work.



FIG. 4. Important FOMs for rf performance. (a) Cutoff frequency, (b) maximum oscillation frequency, and (c) intrinsic gain for various 2D channel materials.

reduces the transconductance and thus  $f_t$ . Various parasitics involved in  $f_t$  and  $f_{max}$  extraction are shown in Fig. 3(a). Besides MoS<sub>2</sub> we also simulate DC characteristics and rf performance for BP transistors using QBS and find the results to be in close agreement with recently published work [27]. This reinforces the credibility in QBS to be able to accurately predict the rf performance for a large variety of 2D materials.

We now extract  $f_t$ ,  $f_{max}$ , and  $G_{int}$  for various 2D materials, namely, TiS<sub>2</sub>, silicane, ZrS<sub>2</sub>, HfS<sub>2</sub>, PtS<sub>2</sub>, NiS<sub>2</sub>, SiC, MoS<sub>2</sub>, WS<sub>2</sub>, WSe<sub>2</sub>, and phosphorene, as shown in Figs. 4(a)–4(c), respectively. The thickness of the channel material and the electron barrier height are kept constant, whereas the bandgap,  $m^*$  and  $\epsilon_r$  are varied. A table for the material properties is given in the Supplemental Material. The highest  $f_t$ ,  $f_{max}$ , and  $G_{int}$  values for phosphorene among the 2D materials considered here stems from its low  $m^*$  and high  $\epsilon_r$ . Moreover, the  $f_t$  values are benchmarked with previous studies as shown in Table I. Almost a tenfold improvement in  $f_t$  in this work as compared to previous work [19,28,29] results from the lack of scattering in the channel. The presence of scattering in previous experimental and theoretical studies for long

TABLE I. Unity current gain cutoff frequencies for monolayer transistors with different channel materials reported previously and in this work.

Channel material	Previous work		This work
	v <sub>sat</sub> (cm/s)	$f_t$ (THz) at 15 nm	$f_t$ (THz) at 15 nm
MoS <sub>2</sub>	$4.8 \times 10^{6}$ [28] $1.1 \times 10^{6}$ [19] $1.8 \times 10^{6}$ [29]	0.51 0.12 0.2	4.15
$WS_2$	$5.1 \times 10^{6}$ [28]	0.54	5.4
WSe <sub>2</sub>	$4 \times 10^{6}$ [28]	0.42	5.1
Phosphorene	$9.6 \times 10^{6}$ [20] $2.5 \times 10^{7}$ [21]	1 5	9.7 9.7

channel length transistors (>250 nm) limits the intrinsic  $f_t$ . Therefore, for the previous reports, we extrapolate the  $f_t$  for 15-nm gate length using  $v_{sat} = L_g/\tau = 2\pi L_g f_t$  [19] and compare it with  $f_t$  reported in this work. Hence,  $f_t$  reported in this work can be considered as the intrinsic ballistic limit for a 15-nm gate length transistor. The higher  $f_t$  for phospherene reported in this work compared to Yin *et al.* [21], can be attributed to the reduced EOT (0.44 vs 1.3 nm).

Further,  $f_t$  and  $f_{\text{max}}$  with varying  $m^*$  and  $\epsilon_r$  are extracted to understand their trends for different channel materials (Fig. 4). Variations in  $f_t$ ,  $f_{max}$ , and  $G_{int}$  with  $m^*$  and  $\epsilon_r$  for a constant energy bandgap (1.5 eV) are shown in Figs. 5(a)-5(c), respectively. Solid yellow spheres in Fig. 5 represent various materials considering their specific bandgaps in the QBS. Almost all spheres lie on the same trend that houses the  $f_t$  and  $f_{max}$  variations for a constant bandgap. The fact that this trend is not dependent of the actual bandgap suggests a negligible effect of bandgap on  $f_t$ ,  $f_{\text{max}}$ , and  $G_{\text{int}}$ . A small electronic barrier (0.1 eV) gives rise to a dominant electronic current through the conduction band and a negligible hole current for sizeable bandgap due to a large hole barrier. Reduction in bandgap lowers the hole barrier and below a critical value that depends on  $m^*$  and  $\epsilon_r$ , the hole current increases and affects  $f_t$  and  $f_{\text{max}}$ . However, most of the monolayer 2D materials considered in this study have a bandgap above their respective critical bandgaps. Therefore, no considerable effect of bandgap on  $f_t$  and  $f_{max}$  is observed. A detailed analysis on the effect of bandgap on  $f_t$  and  $f_{max}$  is provided in the Supplemental Material [26]. Figures 5(a) and 5(b) show that lower  $m^*$  and higher  $\epsilon_r$  lead to higher  $f_t$  and  $f_{\text{max}}$ . In these simulations,  $\epsilon_r$  is varied from 1 to 15 and  $m^*/m_0$  from 0.13 to 6 spanning a wide range of relevant 2D materials. Variations in  $f_t$  and  $f_{max}$  are attributed to the modulation of the source-channel barrier width and the DOS with  $m^*$  and  $\epsilon_r$ . Detailed explanations of the effect of  $m^*$  and  $\epsilon_r$  on  $f_t$  and  $f_{\rm max}$  are presented in the following sections.

To understand the variation in  $f_t$  for different channel materials, we study the  $g_m$  and  $C_G$  trends for varying  $m^*$ 



FIG. 5. (a)  $f_t$ , (b)  $f_{max}$ , and, (c)  $G_{int}$  with varying  $m^*/m_0$  and  $\epsilon_r$  for a constant energy bandgap of 1.5 eV. Yellow spheres represent the various channel materials with their respective bandgaps.

and  $\epsilon_r$ , since  $f_t$  depends on these two crucial parameters. Figure 6(a) depicts a significant variation in  $f_t$  with  $m^*$ , but only a small variation with  $\epsilon_r$ . First, consider the effect of  $\epsilon_r$  on  $f_t$  for constant  $m^*$ .  $f_t$  varies with  $\epsilon_r$  only for small  $m^*$  and remains nearly constant for larger values of  $m^*$ . Therefore, normalized  $f_t$  along the  $\alpha$ - $\alpha'$  curve shown in Fig. 6(a) is plotted for small and constant  $m^*$  ( $m^*/m_0 =$ 0.13) in Fig. 6(b). Figure 6(b) shows  $f_t$  increasing monotonically for increasing  $\epsilon_r$ . We further look at the variation of  $g_m$  and  $C_G$  with  $\epsilon_r$  for constant  $m^*/m_0 = 0.13$ . Both  $g_m$ and  $C_G$  increase up to a certain  $\epsilon_r$  and then start decreasing for higher  $\epsilon_r$ , as shown in Fig. 6(c). However, since their ratio continues increasing monotonically with  $\epsilon_r$ ,  $f_t$  also increases monotonically with  $\epsilon_r$  [Fig. 6(b)]. The initial increase in both  $g_m$  and  $C_G$  is attributed to the improved effective gate control of the source-channel barrier for  $\epsilon_r$ increasing up to a value of approximately 5 [30]. However, a further increase in  $\epsilon_r$  reduces both  $g_m$  and  $C_G$  due



FIG. 6. (a)  $3D f_t$  phase diagram for varying  $m^*/m_0$  and  $\epsilon_r$ . (b) Normalized  $f_t$  vs  $\epsilon_r$  at constant  $m^*/m_0 = 0.13$ . Initially  $f_t$  increases fast with  $\epsilon_r$  due to increased gate-to-channel coupling. A further increase in  $\epsilon_r > 5$  leads to enhanced drain control over the source-channel barrier that dominates over the gate-to-channel coupling. (c) Normalized  $C_G$  and  $g_m$  for varying  $\epsilon_r$ . (d) Energy band diagrams along the channel for different  $\epsilon_r = 1$ , 5, 15 and gate voltages (0.55 and 6 V) show the bands shifting downwards (thinner barrier) for  $\epsilon_r$  increasing from 1 to 5 but pulled up by the drain (thicker barrier) for  $\epsilon_r > 5$ . (e) Conduction band profiles near the source end. Change in total charge (dQ) for a 50 mV change in the gate voltage and for different  $\epsilon_r$  is shown in the inset.

to more dominant drain coupling to the source-channel barrier [31]. Figures 6(d) and 6(e) show the barrier width modulation at the source-channel interface for various  $\epsilon_r$ values at different drain voltages. Device performance at high drain voltage is largely dependent on the sourcechannel barrier due to negligible contribution to  $I_D$  from the drain contact. The conduction band profiles of Fig. 6(d)are magnified near the source-channel interface to understand barrier width variation with  $V_G$  and  $\epsilon_r$ , as shown in Fig. 6(e). The change in conduction band profiles for  $V_G$  varying from 0.55 to 0.6 V determines the change in channel charge [inset of Fig. 6(e)]. This change in charge represents  $C_G (= dQ_{ch}/dV_g)$  and is consistent with the  $C_G$ trend depicted in Fig. 6(c). Further, the variation in conduction band profiles is also consistent with the  $g_m$  trend in Fig. 6(c) and explained in detail via Fig. 7. Figure 7(a)depicts the electric field lines emanating from the gate and drain for three different  $\epsilon_r$  values (1, 5, and 15). The field strength from the gate to the source increases for an initial increase in  $\epsilon_r$  (higher density of gate field lines) from 1 to 5 resulting in improved gate control, a thinner sourcechannel barrier and thus a higher  $g_m$ . With further increase in  $\epsilon_r > 5$ , the field lines from the drain start affecting the source-channel barrier, resulting in the barrier becoming wider and hence reducing  $g_m$  [31]. Figure 7(b) shows the conduction band profiles for these three  $\epsilon_r$  conditions. An initial increase in  $\epsilon_r$  shifts the bands down [from the pink to the brown profile in Fig. 7(b)] due to a high gate field effect and a further increase in  $\epsilon_r$  pulls the bands in the channel towards the drain (brown to black) due to a strong drain field. These results are also validated using the WKB analytic approximation, [32] using a factor  $F_G$  proportional



to  $g_m$ , as plotted in the inset of Fig. 7(c). The factor  $F_G$  is given by

$$F_G = -I\left(\frac{2}{W_B} + \frac{\sqrt{m^*}}{C}\right)\frac{dW_B}{dV_G},\tag{4}$$

where C is a constant independent of channel material parameters,  $W_B$  is the width of the barrier at source Fermi level as obtained from simulations,  $dW_B$  is the change in  $W_B$  for the  $dV_G$  voltage bias change, and I is the drain-to-source current. The above calculation results from the WKB approximation assuming that the current is being controlled by a triangular source-channel barrier. An increase in  $F_G$  for an initial increase in  $\epsilon_r$  (1 to 5) can be attributed to reduction in  $W_B$  and increased  $dW_B/dV_G$  [inset of Fig. 7(c)]. A further increase in  $\epsilon_r$ (5 to 15) increases  $W_B$  and reduces  $dW_B/dV_G$ , thereby reducing  $F_G$ . The variation in  $F_G$  is in complete agreement with the  $g_m$  vs  $\epsilon_r$  trend shown in Fig. 6(c). Detailed information about  $F_G$  is given in the Supplemental Material [26]. The variation in  $f_t$  with  $m^*$  is more pronounced, as shown in Fig. 8. For a constant  $\epsilon_r$ ,  $f_t$  along the  $\beta$ - $\beta'$  curve of Fig. 8(a) decreases monotonically with an increase in  $m^*$  [Fig. 8(b)]. Figure 8(c) shows the change in  $g_m$  and  $C_G$  with  $m^*$  with an equivalent gate capacitance model in the inset. As detailed in [33], this capacitance model represents the intrinsic behavior of any semiconductor material including the quantum capacitance  $(C_{O})$ . An increase in the normalized  $C_G$  with  $m^*$  results from increasing  $C_O$  due to an increased DOS for large  $m^*$ . However,  $g_m$  decreases due to reduced gate-assisted tunneling at the source-channel barrier resulting from degrading gate

> FIG. 7. (a) Electric field lines for varying  $\epsilon_r$  of the channel material. An increase in  $\epsilon_r$  from 1 to 5 allows electric field lines to travel deeper inside the channel, thereby improving the gate control of the source-channel barrier. A further increase in  $\epsilon_r$  deteriorates the gate control due to an increase in the drain field at the source. Electric field lines flow from drain to source through the channel for higher  $\epsilon_r$ . (b) Conduction energy band profiles from source to drain at  $V_D = 0.9$  V and  $V_G = 0.6$  V for different  $\epsilon_r$ . (c) Normalized  $g_m$ for varying  $\epsilon_r$ . Initial increase in  $\epsilon_r$  from 1 to 5 increases the  $g_m$ due to better gate control, a further increase in  $\epsilon_r$  from 5 to 15 reduces the  $g_m$  because of the increase in drain-to-source coupling. Factor  $F_G$  (in the inset) shows the same variation as  $g_m$ .



FIG. 8. (a)  $3D f_t$  phase diagram for varying  $m^*/m_0$  and  $\epsilon_r$ . (b) Normalized  $f_t$  vs  $m^*/m_0$  at constant  $\epsilon_r = 5$ . We note that  $f_t$  decreases monotonically with increasing  $m^*$  due to an increase in the DOS leading to a reduction in the gate capacitance. (c) Normalized  $C_G$  and  $g_m$  vs  $m^*/m_0$  showing a decrease in the gate capacitance with increasing  $m^*$  as the gate capacitance can be modeled [33] using oxide capacitance in series with a parallel combination of the material capacitance and the quantum capacitance ( $C_Q$ ) shown in the inset. The quantum capacitance is directly proportional to the DOS and,  $C_M$ , the material capacitance is directly proportional to  $\epsilon_r$ . (d) Energy band diagrams from source to drain for different  $V_G$  (0.55 and 0.6 V) and  $m^*/m_0$  (0.13, 0.46, 6). (e) Magnified conduction band profile near the source end shows that the bands shift upward with  $m^*$  leading to a reduction in  $g_m$ . In the inset, the analytical WKB factor  $F_G$ , which is proportional to  $g_m$ , reveals the same trend as shown by  $g_m$ .

control of the source-channel barrier with increasing  $m^*$ [34]. Energy band profiles for different  $m^*$  (0.13, 0.46, and 6) and for different  $V_G$  are shown in Fig. 8(d). Figure 8(e) shows the enlarged conduction band profiles near the source, where besides widening of the source-channel barrier, the gate-assisted change in the conduction band profile decreases with increasing  $m^*$  leading to a reduction in  $g_m$ . Further, the analytical WKB factor  $F_G$  plotted for different  $m^*$  is in agreement with the  $g_m$  trend, as shown in the inset of Fig. 8(e). The decrease in  $F_G$  with  $m^*$  can be attributed to reduction in  $dW_B/dV_G$ ,  $1/W_B$ , and I for increasing  $m^*$ .

Another important FOM for rf applications is the maximum oscillation frequency  $f_{\text{max}}$ . Variations in  $f_{\text{max}}$  with  $m^*/m_0$  and  $\epsilon_r$  are depicted in Fig. 9. We notice that similar to  $f_t$ ,  $f_{\text{max}}$  is also a strong function of  $m^*$ . First, we look at the change in  $f_{\text{max}}$  by varying  $\epsilon_r$  for a constant  $m^*/m_0 =$ 0.13. The normalized  $f_{\text{max}}$  and  $f_t$  along the  $\alpha$ - $\alpha'$  curve in Fig. 9(a) with varying  $\epsilon_r$  are shown in Fig. 9(b). Unlike  $f_t$ , which is monotonically increasing,  $f_{\text{max}}$  initially decreases with  $\epsilon_r$  and then increases for higher values of  $\epsilon_r > 5$ . As shown in Eq. (2), besides  $f_t$ ,  $f_{\text{max}}$  also depends on  $g_d$ ,  $C_{GD}$ , etc. which in turn depend on  $\epsilon_r$ . Figure 9(c) shows that  $g_d$  increases initially with  $\epsilon_r$  and then decreases for  $\epsilon_r > 5$ . Similar to  $g_d$ ,  $C_{GD}$  and  $f_tC_{GD}$  also follow a similar trend, i.e., both initially increase and then decrease for larger values of  $\epsilon_r$ , as seen in Fig. 9(d). A factor  $F_D$  proportional to  $g_d$  is plotted for three different  $\epsilon_r$  and is shown in the inset of Fig. 9(c). The factor  $F_D$ , also derived from WKB approximation, is given by,

$$F_D = -I\left(\frac{2}{W_B} + \frac{\sqrt{m^*}}{C}\right)\frac{dW_B}{dV_D},\tag{5}$$

where  $dW_B/dV_D$  is the change in  $W_B$  for  $dV_D$ . The variation in  $F_D$ , similar to  $F_G$ , can be explained by an initial increase in  $1/W_B$  and  $dW_B/dV_D$  for  $\epsilon_r$  increasing from 1 to 5 due to improved gate-channel coupling and reduction in  $1/W_B$  and  $dW_B/dV_D$  for  $\epsilon_r$  increasing from 5 to 15 due to increased drain-to-channel coupling. The variations in  $g_d$ ,  $C_{GD}$ , and  $f_tC_{GD}$  with  $\epsilon_r$  can be explained by barrier width modulation at the source-channel interface, as shown in Figs. 6(e) and 9(e). An initial increase in  $\epsilon_r$  strengthens the

gate control due to an increasing density of field lines from the gate to the source-channel barrier; hence resulting in an increase in  $g_d$ , gate to drain capacitance ( $C_{GD}$ ), and  $f_t C_{GD}$ . A further increase in  $\epsilon_r$  reduces the gate control, as the field lines from the drain are more strongly coupled to the source-channel barrier resulting in a wider barrier width and a reduction in  $g_d$ ,  $C_{GD}$ , and  $f_t C_{GD}$  [Fig. 9(d)]. Figure 9(e) shows the variation in the conduction band profiles from source to drain as  $\epsilon_r$  and  $V_D$  are varied. An increase in the barrier width due to the conduction band floating up for very large  $\epsilon_r$  results in a reduction in  $g_d$ . The inset in Fig. 9(e) shows the variation of charge integrated from the drain contact to the middle of the channel, which corresponds to the  $C_{GD}$  variation shown in Fig. 9(d). The  $C_{GD}$ is extracted by assuming that the left half of the channel is controlled by the source whereas the right half is controlled by the drain ( $\alpha = 0.5$ ). Here,  $\alpha$  is defined as the ratio of length of the source-controlled channel to the total channel length. Figure 4 in the Supplemental Material [26] shows that even a large change in  $\alpha$  from 0.1 to 0.5 does not affect  $f_{\rm max}$  for phosphorene significantly.

The variation in  $f_{\text{max}}$  with  $m^*$  is shown in Fig. 10. Similar to  $f_t$ ,  $f_{\text{max}}$  decreases monotonically with an increase

in  $m^*$  along the  $\beta$ - $\beta'$  curve shown in Fig. 10(a) for a constant  $\epsilon_r = 5$ . Figure 10(b) shows the normalized  $f_t$  and  $f_{\rm max}$  for varying  $m^*$  at a constant  $\epsilon_r$ . As discussed earlier,  $f_{\text{max}}$  depends strongly on  $g_d$  and  $C_{GD}$ . Figure 10(c) shows that  $g_d$  initially increases for low  $m^*$  and then decreases for high  $m^*$ . A very low  $m^*$  makes the source-channel barrier almost transparent to carriers and the significant tunneling implies reduced drain control and low  $g_d$ . However, with increasing  $m^*$  the current becomes more sensitive to the drain voltage due to reduced tunneling, thereby increasing  $g_d$ . A further increase in  $m^*/m_0$  (>0.46) leads to a larger DOS, along with which the conduction band also floats up as shown in Fig. 10(e) (increasing the difference between  $E_F$  and  $E_C$  near the source). This increase in barrier width due to the conduction band floating up in turn reduces the drain control over the source-channel barrier and leads to a reduction in  $g_d$ . Unlike  $F_G$ , the factor  $F_D$  [inset of Fig. 10(c)] initially increases due to an increase in  $\sqrt{m^*}/C$  and then decreases due to a decrease in  $1/W_B$  and  $dW_B/dV_D$  resulting from the increased DOS. The trend depicted by factor  $F_D$  is in complete agreement with the  $g_d$  vs  $m^*$  trend in Fig. 10(c). Figure 10(d) shows that  $C_{GD}$  increases with  $m^*/m_0$  due to the increase in DOS



FIG. 9. (a) Phase diagram showing the change in  $f_{\text{max}}$  with  $m^*/m_0$  and  $\epsilon_r$ . (b) Normalized  $f_{\text{max}}$  and  $f_t$  vs  $\epsilon_r$  at constant  $m^*/m_0 = 0.13$ . (c)  $g_d$  vs  $\epsilon_r$  shows that initially  $g_d$  increases and then decreases with  $\epsilon_r$ . In the inset, the analytical WKB factor  $F_D$  proportional to  $g_d$  shows a similar variation as  $g_d$  at different  $\epsilon_r$ . (d) Plot of  $f_tC_{GD}$  and  $C_{GD}$  vs  $\epsilon_r$ . (e) Conduction band diagrams showing the variation with  $\epsilon_r$  for different  $V_D$ . In the inset,  $Q_D - \epsilon_r$  variations are shown for a 50 mV change in the drain voltage bias that are consistent with the  $C_{GD}$  trends in (d).



FIG. 10. (a) 3D  $f_{\text{max}}$  phase diagram for varying  $m^*/m_0$  and  $\epsilon_r$ . (b) Normalized  $f_{\text{max}}$  and  $f_t$  vs  $m^*/m_0$  at constant  $\epsilon_r = 5$ . (c)  $g_d$  vs  $m^*/m_0$  shows initially  $g_d$  increases and then decreases with  $m^*/m_0$ . Inset shows analytical WKB factor  $F_D$  showing similar variation as  $g_d$ . (d) Variation of  $C_{GD}$  and  $f_t C_{GD}$  for varying  $m^*/m_0$ . (e) Energy band diagrams for different  $m^*/m_0$  and at different drain voltages. Inset shows  $Q_D$  variation with  $m^*/m_0$  for 50 mV change in drain voltage.

for high values of  $m^*/m_0$ . However,  $f_t C_{GD}$  decreases with an increase in  $m^*/m_0$  due to a strong dependence of  $f_t$  on  $m^*$ . Figure 10(e) shows the conduction band energy profiles for various  $m^*/m_0$  at different drain voltages and the inset shows corresponding  $Q_D$  variation consistent with the  $C_{GD}$  trend in Fig. 10(d).

## IV. EFFECT OF SCHOTTKY BARRIER HEIGHT AND STRAIN ON $f_t$

In this section, we briefly discuss the effects of variation in extrinsic parameters such as SBH and strain. The effective SBH for  $MoS_2$  can be controlled either by interfacial engineering or chemical doping [35,36]. This analysis is performed for the best performing material (phosphorene), but similar arguments can be made for other 2D materials as well.

Figure 11(a) shows the trends in  $g_m$ ,  $C_G$ , and  $f_t$  with varying electron SBH ( $\phi_B$ ) for phosphorene.  $f_t$  decreases monotonically with increasing SBH due to a reduction in  $g_m$  resulting from the increasing contact resistance. In addition, the effect of strain on rf performance is also of interest from the viewpoint of flexible electronics. Figure 11(b) shows the change in  $f_t$  for phosphorene under different



FIG. 11. (a) Variation in  $g_m$ ,  $C_G$ , and  $f_t$  with SBH for phosphorene. (b) Effect of strain on  $f_t$  for phosphorene with SBH of 0.1 eV.

strain conditions with a fixed SBH of 0.1 eV. Values for the bandgap and directional electron and hole effective masses for phosphorene under strain are obtained from [37] and available in the Supplemental Material [26]. The inset in Fig. 11(b) shows the top view of the simulated device with indicated directions for strain. The effective mass in y direction is used as the transport effective mass whereas effective mass in x direction is used to calculate the transverse modes available for current transport, and hence both affect the  $f_t$  performance. Pristine phosphorene gives the best  $f_t$  performance and the effect of effective mass in x direction on  $f_t$  is found to be more significant when compared to the effective mass in the y direction. Similar analysis for  $f_{max}$  is available in the Supplemental Material [26].

### V. CONCLUSIONS

This work reports a comprehensive study of the rf performance of 2D materials and identifies the contributions of different intrinsic material properties to standard rf FOMs, namely,  $f_t$  and  $f_{max}$ . Unlike conventional bulk semiconductors, 2D materials offer the benefit of controllably scaling channel thickness. Superior electrostatics in sub-1-nm 2D monolayers can enable gate-length scaling for enhanced rf performance. Reduced scattering due to the absence of dangling bonds in pristine 2D materials can also benefit rf performance in comparison to conventional rf semiconductors. In addition, high mechanical stability under strain and optical transparency make 2D materials suitable for flexible and wearable rf electronics [38]. By analyzing the variation in  $m^*$  and  $\epsilon_r$  and their effect on  $f_t$ ,  $f_{max}$ , and  $G_{int}$ , we demonstrate that a lower  $m^*$  and higher  $\epsilon_r$  provide the best combination for rf applications. We demonstrate that this is due to the high degree of gate control over the source-channel barrier. An increase in the DOS for larger effective masses  $m^*$  reduces the modulation of the potential in the channel resulting in a poorer gate control. In the chosen set of materials, phosphorene emerges as the best material for rf applications due to its low  $m^*$  and high  $\epsilon_r$ . Although not comprehensive, the list of 2D materials studied in this work covers a broad range of  $m^*$  and  $\epsilon_r$  to enable performance predictions for other, known and yet to be discovered, 2D materials covered by it. Hence, this study could work as a guide for choosing specific materials for rf applications. To establish the credibility of our analysis, we also repeated the simulations for parameter  $(m^*, m^*)$ bandgap) values obtained by the GW method (see the Supplemental Material) [26]. It is important to note that the rf performance predicted in these simulations requires significant experimental improvements in (i) scaling gate dielectric thickness [25-nm Al<sub>2</sub>O<sub>3</sub> (EOT approximately 10 nm) in [38] vs 2.8-nm HfO<sub>2</sub> (EOT approximately 0.44 nm) in this work], as well as (ii) scaling gate length from

100s of nm in recent experimental rf reports to 15 nm in this work. Another critical challenge is to develop techniques for improving the air stability of 2D materials, phosphorene in particular [39,40], since material degradation in ambient air can lead to loss of rf performance. Although the simulations account for contact resistance of the Schottky source and drain contacts, reduction in contact resistance through source and drain doping and/or metal work-function engineering can also help improve rf performance. From a simulation perspective, as a future extension of this work, the effect of scattering on  $f_t$  can be studied via the use of the incoherent NEGF formalism and the impact of extrinsic parameters related to device processing on rf performance, such as the Schottky barrier height, strain, and the substrate, can be looked at in more detail.

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