Optomechanically induced carrier-envelope-phase-dependent effects and their analytical solutions

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To date, investigations of carrier-envelope-phase (CEP)-dependent effects have been limited to optical pulses with few cycles and high intensity and have not been reported for other types of pulses. Optomechanical systems are shown to have the potential to go beyond these limits. We present an approach using optomechanics to extend the concept of the traditional CEP in the few-cycle regime to mechanical pulses and develop a two-step model to give a physical insight. By adding an auxiliary continuous optical field, we show that a CEP-dependent effect appears even in the multicycle regime of mechanical pulses. We obtain the approximated analytical solutions providing full understanding for these optomechanically induced CEP-dependent effects. In addition, our findings show that one can draw on the optomechanical interaction to revive the CEP-dependent effects on optical pulses with an arbitrary number of cycles and without specific intensity requirements. The effects of CEP, broadly extended to encompass few- and multicycle optical and mechanical pulses, may stimulate a variety of applications in the preparation of a CEP-stabilized pulse, the generation of ultrasonic pulses with a desired shape, the linear manipulation of optical combs, and more.

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I. INTRODUCTION

The simple premises behind an optomechanical system (OMS), where a mechanical resonator interacts with an optical field via radiation pressure force, offer untold opportunities that were even hard to imagine until recent years. The rapid development of optical control in optomechanical devices [1-4] brings applications of OMS to the cutting edge of metrology, such as precision measurements of acceleration [5], magnetic fields [6], weak forces [7], and electrical charges [8]. New frontiers are also targeted for position measurements, with pioneering research aiming to push the precision towards the standard quantum limit [9]. In fact, the applications of OMSs in the field of metrology are too many to be listed comprehensively, and there is always potential for further extension to other significant physical quantities. The carrier-envelope phase (CEP) of a given pulse is one example.

The CEP is the phase between the envelope of a pulse and the carrier frequency at which the pulse is modulated. In the field of ultrafast optics, the rapid progress of CEP measurement techniques has made it possible to fully manipulate laser pulses, paving the way to numerous novel physical phenomena and applications. Some of these include, for example, super-high-resolution measurements on atomic and molecular systems [10], efficient tomography of molecular orbitals [11], and generation of intensive femtosecond electron beams [12–14]. Despite their manifest popularity, so far CEP-dependent effects have mostly been limited to pulses with few oscillations within the envelope (few-cycle pulses), and the measurement techniques involved result in impossible for pulses whose intensity is too low to excite tunneling ionization [15,16]. Sparked by the growing importance of

CEP measurements, recent works extended the exploration of CEP effects towards multicycle [17] and low-intensity [15] regimes, finding interesting applications in the generation of CEP-stabilized ultrashort laser pulses [18,19] and the coherent control of molecular and electron collisions [20]. The CEP-dependent effects of laser pulses with both an arbitrary number of cycles and arbitrary intensity are, nevertheless, still an open issue that needs to be explored.

It is also worth noting that almost all the current research on CEPs is focused only on pulses of an optical nature, missing the potential significance of CEPs for other types of pulses. The generation and manipulation of ultrasonic pulses are currently topics of intense research [21–24], accounting for a number of recent achievements such as superresolution imaging [25,26], control of microfluidics [27], and coherent magnetization precession [28]. Remarkable advancements in the generation, detection, and control of magnetic [29] and electric [30,31] pulses are also pushing for the development of new applications [29,32,33]. In view of the compelling demand, an extension of CEP measurement and control techniques to new types of pulses is very appealing. From this perspective, the diversity of experimental setups in optomechanics [34] makes an OMS become an incredibly useful platform that can act as a transducer between different types of pulses generated in various systems. For example, ultrasonic pulses can be transformed into mechanical pulses by the acoustic radiation pressure force generated by the ultrasound [27], while electric or magnetic pulses can be changed to mechanical actuation by piezoelectric [35] or piezomagnetic effects. This indicates that, in principle, one can focus the study of CEP measurements and control of a pulse on a generic mechanical pulse while at the same time benefiting from the profusion of applications associated with pulses of different natures.

In this work, we present a model addressing the CEP-dependent effects for both mechanical pulses and optical pulses using optomechanics. Even though several theoretical

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pioneering works [36–39] in the field of ultrafast optics have qualitatively and quantitatively described the CEP-dependent effects appearing in atoms or molecules, the analytical description and physical insight of CEP-dependent effects emerging in an optomechanical system are still not well understood. We set down the approximated analytical results that are strongly supported by accurate numerical simulations, leading us towards a clear physical picture of optomechanically induced CEP-dependent effects. In the resolved-sideband regime where the resonance frequency of the mechanical oscillator is much larger than the linewidth of the cavity, our analysis starts from few-cycle mechanical pulses, showing that the plateau width (PW) of the cavity output spectrum directly depends on the CEP. In the multicycle regime of mechanical pulses, where the traditional CEP-dependent effects are washed out, we introduce an auxiliary continuous field to reveal a CEPdependent effect: the plateau height difference (PHD) between the Stokes and the anti-Stokes sidebands in the spectrum. The outcomes are easily adapted to the case of optical pulses with an arbitrary number of cycles and without specific intensity requirements. As a consequence, CEP measurements are extended to the domain of ultraweak, multicycle optical pulses, as well as all other types of pulses that an OMS can interact with. Along lines similar to applications of the CEP of optical pulses, the CEP measurement of mechanical pulses has the potential to be applied to shape detection and manipulation of ultrasonic, electric, or magnetic pulses.

II. CEP-DEPENDENT EFFECT IN THE FEW-CYCLE REGIME

We consider a cavity OMS [see Fig. 1(a)] consisting of a fixed mirror and a movable mirror (i.e., mechanical resonator), with characteristics similar to a recent pioneering experimental scheme [40]. The system is driven by a continuous optical input with frequency ω_l and an external mechanical pulse with carrier frequency ω_m , and its Hamiltonian in the rotating frame

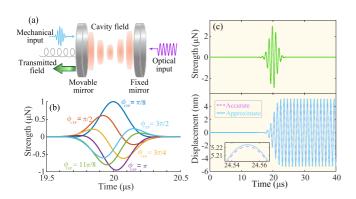


FIG. 1. (a) Schematic diagram of the optomechanical system. (b) Different shapes of pulsed mechanical forces depending on the CEP. We set $A=1~\mu N$ and $t_p=0.2~\mu s$. (c) The dynamical evolution of a mechanical pulse and the corresponding mechanical displacement. The other relevant parameters used in this work are borrowed from a recent state-of-the-art experiment [40]: $\gamma_m=2\pi\times 140~{\rm Hz}$, $\kappa=2\pi\times 215~{\rm kHz}$, $\omega_m=2\pi\times 947~{\rm kHz}$, $m=145~{\rm ng}$, $g_0=2\pi\times 2.7~{\rm Hz}$, $G=-g_0/\sqrt{\hbar/(m\omega_m)}$.

of ω_l is

$$H = \left(\frac{\hat{p}^2}{2m} + \frac{m\omega_m^2 \hat{q}^2}{2}\right) - \hbar \Delta \hat{c}^{\dagger} \hat{c} + \hbar G \hat{q} \hat{c}^{\dagger} \hat{c} + H_{\text{md}} + H_{\text{od}},$$

$$\tag{1}$$

with $H_{\rm md}$ and $H_{\rm od}$ being, respectively, the mechanical drive and optical drive, which are chosen as in this section: $H_{md} =$ $A \exp[-2 \ln 2(\frac{t-t_0}{t_p})^2] \cos(\omega_m t + \phi_{\rm CEP})\hat{q}$ and $H_{\rm od} = i\hbar(\varepsilon_l \hat{c}^\dagger - {\rm H.c.})$. Here, \hat{q} and \hat{p} are, respectively, the position and momentum operators of a mechanical resonator of mass m, and \hat{c} (\hat{c}^{\dagger}) is the bosonic annihilation (creation) operator of the optical mode. For simplicity, we consider the case that the mechanical pulse matches the mode of the mechanical resonator by assuming the mechanical eigenfrequency to be ω_m . The parameter $\Delta = \omega_l - \omega_c$ is the cavity detuning (where ω_c denotes the cavity resonant frequency), and κ is the cavity decay rate. The input field inside the cavity ε_l is obtained using $\varepsilon_l = \sqrt{2\kappa P_l/(\hbar\omega_l)}$, with P_l being the input laser power. The term $\hbar G \hat{q} \hat{c}^{\dagger} \hat{c}$ describes the optomechanical interaction, with the coupling strength G. For the input pulse, we consider, in a representative form, a Gaussian envelope such as the ultrasonic pulse discussed in Ref. [41], with A being the amplitude, t_p being the FWHM, and t_0 being the arrival time of the center point, set to 20 μs in all the following simulations. The parameter ϕ_{CEP} represents the carrier-envelope phase, whose importance in determining the pulse shape [see Fig. 1(b)] is essential for the control of a few-cycle pulse. In obtaining the dynamics from the Hamiltonian we ignore the quantum fluctuations [1,42,43] and consider the classical Langevin equations as follows by adding the mechanical (γ_m) and optical (κ) dissipation terms:

$$\ddot{q} + \gamma_m \dot{q} + \omega_m^2 q$$

$$= -\frac{\hbar G}{m} |c|^2 + \frac{A}{m} e^{-\beta^2 (t - t_0)^2} \cos(\omega_m t + \phi_{\text{CEP}}), \quad (2)$$

$$\dot{c} = -[\kappa + i(-\Delta + Gq)]c + \varepsilon_l, \quad (3)$$

where $\beta = \sqrt{2 \ln 2}/t_p$. Since both differential equations are nonlinear, an analytical solution to both is nontrivial. However, we shall derive the approximated analytical solutions if we consider a *strong-drive approximation*, where the drive to the mechanical motion is typically much more intense than the effect of the radiation pressure force, and thus we are able to drop the term $-\frac{\hbar G}{m}|c|^2$ from Eq. (2). Ignoring the effects of light on the mechanics does not completely eliminate the optomechanical interaction: the position of the mirror still exerts its influence on the cavity field, acting as a "transducer" for the mechanical pulse. For the subsequent analysis we focus on two time windows, one during which the pulse is interacting with the system and the other starting right after the end of the mechanical pulse and ending before the damping of the displacement becomes appreciable.

We start the analysis from the later time window, in which strong-drive and negligible-damping approximations are considered. The relatively small impact of the approximations is shown in the numerical results [see Fig. 1(c)] for the dynamics of the system driven by a pulse of even a micronewton.

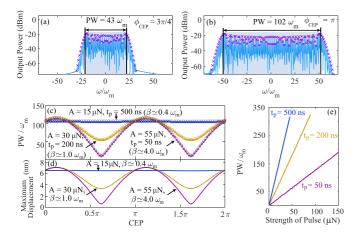


FIG. 2. (a) and (b) The optical power spectrum obtained from the analytical solution of Eq. (4) (crosses) compared with the accurate numerical solution of Eqs. (2) and (3) (lines). The relevant parameters are set to $P_l=10~\rm mW$, $A=200~\mu N$, and $t_p=20~\rm ns$. (c) The plateau width (PW) as a function of CEP. The lines and the crosses indicate the PW obtained from the numerical and analytical solutions, respectively, as before. The circles are obtained from the more concise definition of Eq. (5). (d) The CEP dependence of maximum mechanical displacement. (e) The numerical results for the linear relation of the PW to the amplitude of the input mechanical pulse.

The spectrum for the cavity field is then given as follows (detailed calculations are available in the Appendixes):

$$c_N(\omega_m) = \varepsilon_l e^{iN\phi_m} \sum_{n=-\infty}^{+\infty} \frac{J_n(\alpha)J_{N+n}(\alpha)}{i(n\omega_m - \Delta) + \kappa},$$
 (4)

where $\alpha = Gq_0/\omega_m$, N symbolizes the order of the optical sidebands, and $J_n(\alpha)$ is the Bessel function of the first kind, with n for its integer order. The parameters q_0 and ϕ_m are the amplitude and the initial phase of the mechanical oscillation, respectively, and their values are extracted from numerical results. Given the property of the Bessel function $\sum_{n=-\infty}^{+\infty} J_n(\alpha) J_{N+n}(\alpha) = \delta_{N0}$ (where δ_{N0} is the Kronecker delta function), it is shown from Eq. (4) that $c_N(\omega_m)(N \neq 0)$ goes to zero when the cavity decay κ is much larger than the mechanical frequency ω_m . This means that the higher-order sidebands and associated effects are absent in such a regime, and thus our following work will be focused only on the regime where $\kappa \ll \omega_m$, i.e., the resolved-sideband regime. From now on we choose $\Delta = -\omega_m$ and consider the power spectrum of the transmitted field to avoid the interference between the output field and the input field by applying the input-output relation: $c_N^{\text{out}}(\omega_m) = \sqrt{2\kappa} c_N(\omega_m)$. The output power spectrum is shown in Figs. 2(a) and 2(b), in which a plateau is formed by the emergence of high-order sidebands [44,45] that ends swiftly at a specific cutoff frequency. The PW is a convenient quantity to consider for a characterization of the system's conditions. We define it from the difference between the highest and lowest frequencies corresponding to the sidebands whose amplitudes are greater than half of the maximum value, determining the cutoff frequencies of the anti-Stokes and Stokes sidebands, respectively. When the mechanical pulse contains only a few cycles, the PW oscillates

periodically with period π as the value of CEP changes [see Fig. 2(c)]. This is a clear CEP-dependent effect that can be utilized to infer the shape of the pulse and prompt the necessary actions for its control. Figure 2(c) shows in particular that the CEP-dependent effect is weakened as the temporal width of the pulse t_p becomes larger (i.e., the pulse contains more cycles) and ultimately vanishes when t_p is large enough. We note that the Bessel function $J_n(\alpha)$ decays very quickly when $n > \alpha$. Applying this property to Eq. (4), we see that higher-order terms in the series reduce to zero rapidly once $N > \alpha$. This means that the cutoff frequencies in the output power spectrum can be approximated to $\pm \alpha \omega_m$. We can therefore redefine the PW ϖ in a more concise equation:

$$\varpi = 2\alpha\omega_m = 2Gq_0. \tag{5}$$

As seen in the overlap of the PW traces in Fig. 2(c), this new definition distinctly agrees with the previous one. Equation (5) reminds us that it is essential to fully understand the behaviors of the maximum displacement q_0 for the sake of obtaining the physical picture of the CEP-dependent effect. For this reason, in the following discussions we focus on the analysis of the mechanical spectrum in the time window during which the pulse drives the system.

By dropping the radiation pressure term as in the previous calculation and considering the Fourier transform of q(t) $[q(t) = \int_{-\infty}^{+\infty} q(\omega)e^{i\omega t}d\omega]$, we give the displacement spectrum (see the Appendixes):

$$|q(\omega)|^{2} = \left| \frac{A}{4\beta\sqrt{\pi}} \right|^{2} \frac{1}{|\chi(\omega)|^{2}} \left(e^{-\frac{(\omega - \omega_{m})^{2}}{2\beta^{2}}} + e^{-\frac{(\omega + \omega_{m})^{2}}{2\beta^{2}}} \right.$$

$$\left. + 2e^{-\frac{\omega^{2} + \omega_{m}^{2}}{2\beta^{2}}} \cos[2(\omega_{m}t_{0} + \phi_{CEP})] \right), \tag{6}$$

where $\chi(\omega) = [m(\omega_m^2 - \omega^2 + i\gamma_m \omega)]^{-1}$ is the susceptibility of the mechanical oscillator. This spectrum shows that the maximum values of the mechanical displacement are found at the mechanical sidebands, i.e., $\omega \approx \omega_m$ and $\omega \approx -\omega_m$. The term including the CEP in Eq. (A15) reduces to $2 \exp(-\omega_m^2/\beta^2) \cos[2(\omega_m t_0 + \phi_{\text{CEP}})]$ if one looks at these two mechanical sidebands. Since the PW is linearly related to the maximum mechanical displacement [see Eq. (5)], such a term indicates that both are modulated periodically by the CEP with period π when the parameter β is much greater than ω_m (i.e., $t_p \ll \sqrt{2 \ln 2}/\omega_m$). Moreover, the dependence of the PW (and maximum displacement) on the CEP fades with decreasing β (increasing t_p), and such dependence completely dies out when $\beta \ll \omega_m$. These features agree very well with previous discussions about CEP-dependent effects (see Fig. 2). Furthermore, we find that the numerical result for the maximum mechanical displacement as a function of CEP [see Fig. 2(d)] shows the same dynamics as the analytical results. We therefore identify the regime where $\beta \gg \omega_m$ (pulse contains few cycles) as the *few-cycle* regime and the regime where $\beta \ll \omega_m$ (pulse contains many cycles) as the *multicycle* regime. We note from Eq. (A15) that the mechanical displacement linearly depends on the amplitude of the mechanical pulse (i.e., A), implying that the PW is also proportional to A [see Fig. 2(e)]. Such dependence provides a potential and concise way to linearly manipulate the line number of an optical comb. Since the line spacing of the optical

comb observed in Figs. 2(a) and 2(b) is determined by the mechanical frequency (the value is taken from an experiment to be $2\pi \times 947$ kHz [40]), it is, in principle, possible to beat the challenge of narrow-line spacing [46]. Current experiments in optomechanics have achieved mechanical frequencies lower than kilohertz [34,47], meaning that this technique would open access to new regimes of optical comb manipulation.

Based upon the analysis above, we devise a two-step interpretation of the appearance of high-order sidebands induced in the OMS: (i) an intense mechanical pulse is sent to the mechanical resonator to drive high-amplitude oscillations; (ii) the strong oscillations of the mechanical resonator induce Stokes and anti-Stokes scattering of the cavity field. The requirement for the first step is embodied in Eq. (A15), according to which the higher-order sidebands forming the plateau can be excited only when $\alpha \gg 1$, or, equivalently, $q_0 \gg \omega_m/G$. The second step is represented by Eq. (4), describing how both the Stokes and anti-Stokes fields build up the power spectrum. The two-step model can also be used to obtain physical insight into the appearance of CEP-dependent effects. The first step introduces an intense mechanical pulse to drive the oscillations of the mechanical resonator. Since the amplitude of the oscillations depends on the CEP [see Eq. (A15) and Fig. 2(b)], one can thus infer a similar dependence on the optical spectrum of the cavity, thanks to Eq. (5). The second step relates to the appearance of sidebands on the optical output spectrum due to the impact of the modulation from the mechanical oscillation. Observation of the PW of the output power spectrum will therefore give, thanks to Eq. (5), a direct measurement of the CEP.

III. CEP-DEPENDENT EFFECT IN THE MULTICYCLE REGIME

As mentioned earlier, traditional CEP-dependent effects are weakened in the presence of multiple cycles. In this section, we demonstrate how the inclusion of an auxiliary continuous optical field in the system lifts any requirement linked to the number of cycles for observing CEP-dependent effects. We consider the following inputs to the OMS: a mechanical pulse containing a large number of cycles, one continuous reddetuned laser, and another continuous auxiliary laser of a different wavelength. The Hamiltonian for the optical drives [see Eq. (1)] reads $H_{\rm od}=i\hbar[(\varepsilon_l+\varepsilon_a e^{-i\Omega t-\phi_o})\hat{c}^\dagger-{\rm H.c.}]$, where ε_a is determined by the input power of the auxiliary laser using $\varepsilon_a = \sqrt{2\kappa P_a/(\hbar\omega_a)}$; Ω is its optical frequency in the rotating frame of ω_l , i.e., $\Omega = \omega_a - \omega_l$ (from here, we choose $\Omega = l\omega_m$, with $l = \pm 0, 1, 2, ...$); and ϕ_o is the phase difference of the two lasers at t=0. Considering approximations and calculation methods similar to those in the previous section (see the Appendixes), we obtain the cavity-field spectrum:

$$c_{N}(\omega_{m}) = e^{iN\phi_{m}} \sum_{n=-\infty}^{+\infty} \frac{\left[\varepsilon_{l} J_{n}(\alpha) + \varepsilon_{a} e^{-i(\phi_{a} - l\phi_{m})} J_{n+l}(\alpha)\right] J_{N+n}(\alpha)}{i(n+1)\omega_{m} + \kappa}.$$

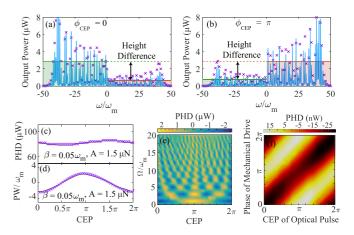


FIG. 3. (a) and (b) The output power spectrum from Eq. (7) (crosses) compared with its numerical results (lines) under no approximation. The parameters are set to $P_l=2$ mW, $P_a=3$ mW, $A=6~\mu N$, and $\beta=0.2\omega_m$. (c) and (d) Dependence of the plateau parameters (PW and PHD) on CEP. The input powers of the two lasers are the same as in (a) and (b). (e) PHD as a function of the CEP and the frequency of the auxiliary laser Ω . (f) For a pulsed *optical* input in the multicycle regime, PHD is shown to depend on its CEP. The parameters are $P_l=1~\mu W$, $P_a=100~\rm nW$, $A=40~\rm nN$, and $B=0.005\omega_m$.

The output power spectrum [see Figs. 3(a) and 3(b) with l = 1] for such a setup displays a striking asymmetric feature: the sidebands from Stokes scattering differ in intensity from the sidebands due to anti-Stokes processes. Such an effect cannot be found in the absence of the auxiliary laser (see Fig. 2) and has the very important quality of depending on the CEP. Therefore, in this multicycle regime where the dependence of PW on CEP vanishes [see Fig. 3(c)], we can still define a parameter that identifies and characterizes the CEP: the plateau *height difference* between the average height of the anti-Stokes and Stokes sidebands in the output power spectrum. In contrast to PW, which is periodic by π [see Fig. 2(e)], the PHD reveals a dependence periodic by 2π [see Fig. 3(d) and Eq. (7)]. Equation (7) offers a clear physical picture for such an effect. The origin of the PHD lies in the interference between the two optical fields. As the auxiliary laser enters the cavity, it acquires high-order sidebands due to the interaction with the mechanical motion, similar to the original field with amplitude ε_l . The Stokes and anti-Stokes sidebands from the two lasers interfere unevenly, leading to the difference in amplitude between the two. Furthermore, Eq. (7) also reveals that the CEP dependence period would be $2\pi/l$ if the frequency of the auxiliary laser were $l\omega_m$, as demonstrated by the numerical results shown in Fig. 3(e).

IV. FROM MECHANICAL TO OPTICAL PULSES

To complete our analysis we explore the effect of multicycle *optical* pulses, as opposed to mechanical pulses, as considered so far. We take, as inputs, a continuous high-amplitude mechanical drive, a continuous red-detuned laser, and an optical pulse. The Hamiltonians describing the drives are $H_{\text{od}} = i\hbar[(\varepsilon_l + \varepsilon_a e^{-i\Omega t - \phi_{\text{CEP}}} e^{-\beta^2 (t - t_0)^2})\hat{c}^{\dagger} - \text{H.c.}]$ and $H_{\text{md}} = A\cos(\omega_m t + \phi)\hat{q}$.

Like in the scenario for the mechanical pulse, the output power spectrum shows again the emergence of a dependence of the power spectrum on the CEP in the form of a PHD [see Fig. 3(f)], even in the regime where the optical pulse contains many cycles and traditional CEP-dependent effects are washed out. It should be noted that, additionally, traditional CEP-dependent effects in an ion platform can be observed only when the optical pulse is intense enough that the tunneling ionization can take place [15]. In the OMS, this condition is generally transferred onto the drive for the mechanical resonator, which is required to be intense to generate a strong mechanical oscillation leading to higher-order sidebands. In a previous relevant work, the optical pulse was required to be intense to meet such a requirement [44]. Here, it is the continuous mechanical drive that takes the responsibility to intensely drive the mechanical resonator. The new CEP measurement for the optical pulse based upon an interferometric process is therefore technically free from any intensity requirements.

V. CONCLUSION

We extended the observation of CEP-dependent effects from ultrafast optics to the realm of mechanical pulses using optomechanics. Approximated analytical solutions robustly supported by accurate numerical solutions were delivered, revealing a clear physical picture of the model. We developed a two-step model to describe the physical processes linking the optical spectrum to the CEP of few-cycle mechanical pulses and then identified an effect that delivers information on the CEP regardless of how many cycles the envelope of the mechanical pulse contains. Importantly, such a method functions even for ultraweak optical pulses. The method described applies extensively to a variety of pulses: mechanical or optical, in the few- or multicycle regime, and without specific requisites for optical intensity. The diverse development of an experimental optomechanical setup [34] may enable our scheme to be implemented for the measurement of the CEP and manipulation of optical combs in a very wide frequency range, and the versatility of optomechanical platforms could be used to stretch these advantages to unexplored grounds (such as ultrasonic pulses [48]).

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APPENDIX A: MECHANICAL PULSES IN THE FEW-CYCLE REGIME

We consider a cavity OMS driven by a continuous optical input with frequency ω_l and an external mechanical pulse with carrier frequency ω_m , and its Hamiltonian in the rotating frame

$$H = \left(\frac{\hat{p}^2}{2m} + \frac{m\omega_m^2 \hat{q}^2}{2}\right) + \hbar \Delta \hat{c}^{\dagger} \hat{c} + \hbar G \hat{q} \hat{c}^{\dagger} c + H_{\text{md}} + H_{\text{od}},$$
(A1)

with

$$H_{\rm md} = A \exp\left[-2\ln 2\left(\frac{t - t_0}{t_p}\right)^2\right] \cos(\omega_m t + \phi)\hat{q}, \quad (A2)$$

$$H_{\rm od} = i\hbar(\varepsilon_l \hat{c}^{\dagger} - \text{H.c.}). \quad (A3)$$

In this work, the classical Langevin equations are given as

$$\ddot{q} + \gamma_m \dot{q} + \omega_m^2 q = -\frac{\hbar g}{m} |c|^2 + \frac{A}{m} e^{-\beta^2 (t - t_0)^2} \cos(\omega_m t + \varphi),$$
(A4)

$$\dot{c} = -[\kappa + i(-\Delta + gq)]c + \varepsilon_l. \tag{A5}$$

The approximated analytical solution of the two nonlinear differential equations can be calculated if we consider a strongdrive approximation, where the drive to the mechanical motion is typically much more intense than the effect of the radiation pressure force, and thus we are able to drop the term $-\frac{\hbar G}{m}|c|^2$ from Eq. (A4). If we focus on the time window that starts right after the end of the mechanical pulse and ends before the damping of the displacement becomes appreciable, Eq. (A4) becomes $\ddot{q} + \omega_m^2 q = 0$, and its solution is easily obtained as

$$q(t) = q_0 \cos(\omega_m t + \phi_m), \tag{A6}$$

where q_0 and ϕ_m are the amplitude and the initial phase of the mechanical oscillation, respectively. We define h(t) = $-[\kappa + i(-\Delta + Gq)]$ and suppose the solution of c(t) is as follows:

$$c(t) = e^{\int h(t)dt} g(t) = f(t)g(t), \tag{A7}$$

with $f(t) = e^{\int h(t)dt}$. Substituting this equation into Eq. (A5), we have

$$f(t)g(t)h(t) + f(t)\dot{g}(t) = h(t)f(t)g(t) + \varepsilon_l,$$

$$g(t) = \varepsilon_l \int f(t)^{-1}dt.$$
 (A8)

We give f(t) as follows:

$$f(t) = e^{\int h(t)dt}$$

$$= \exp(-\kappa t) \exp(-i\omega_m t) \exp[-i\alpha \sin(\omega_m t + \phi_m)],$$

$$= \varepsilon_l \sum_{n=-\infty}^{+\infty} J_n(\alpha) e^{in\phi_m} \frac{\exp[i(n+1)\omega_m t + \kappa t]}{i(n+1)\omega_m + \kappa}.$$
 (A9)

We thus obtain c(t):

$$c(t) = f(t)g(t)$$

$$= \varepsilon_l \sum_{k=-\infty}^{+\infty} \sum_{n=-\infty}^{+\infty} J_n(\alpha) J_k(\alpha) e^{i(n-k)\phi_m} \frac{\exp[i(n-k)\omega_m t]}{i(n+1)\omega_m + \kappa}$$

$$= \sum_{N=-\infty}^{+\infty} c_N(\omega_m) \exp[-iN\omega_m t], \tag{A10}$$

with

$$c_N(\omega_m) = \varepsilon_l e^{iN\phi_m} \sum_{n=-\infty}^{+\infty} \frac{J_n(\alpha)J_{N+n}(\alpha)}{i(n+1)\omega_m + \kappa}.$$
 (A11)

Subsequently, we calculate the spectrum of the mechanical displacement for the time window during which the pulse is interacting with the system. By dropping the radiation pressure term like in the previous calculation, Eq. (A4) takes the form

$$\ddot{q} + \gamma_m \dot{q} + \omega_m^2 q = \frac{A}{m} e^{-\beta^2 (t - t_0)^2} \cos(\omega_m t + \varphi). \tag{A12}$$

The right side of the equation above is expanded as follows:

$$\ddot{q} + \gamma_m \dot{q} + \omega_m^2 q$$

$$= \frac{A}{m} e^{-\beta^2 (t - t_0)^2} \cos(\omega_m t + \varphi)$$

$$= \frac{A}{m} \int_{-\infty}^{+\infty} \frac{1}{2\beta \sqrt{\pi}} \exp\left(-\frac{\omega^2}{4\beta^2}\right) \exp[i\omega(t - t_0)]$$

$$\times \left[\frac{e^{i\omega_m t + i\varphi} + e^{-i\omega_m t - i\varphi}}{2}\right] d\omega$$

$$= \frac{A}{m} \int_{-\infty}^{+\infty} \frac{1}{4\beta \sqrt{\pi}} \exp\left[-\frac{(\omega - \omega_m)^2}{4\beta^2}\right] e^{-i(\omega t_0 - \omega_m t_0 - \varphi)} e^{i\omega t} d\omega$$

$$+ \frac{A}{m} \int_{-\infty}^{+\infty} \frac{1}{4\beta \sqrt{\pi}} \exp\left[-\frac{(\omega + \omega_m)^2}{4\beta^2}\right]$$

$$\times e^{-i(\omega t_0 + \omega_m t_0 + \varphi)} e^{i\omega t} d\omega. \tag{A13}$$

We substitute the ansatz $q(t)=\int_{-\infty}^{+\infty}q(\omega)e^{i\omega t}d\omega$ into the left side of the Eq. (A12) and obtain

$$m\ddot{q} + m\gamma_m\dot{q} + m\omega_m^2 q$$

$$= \int_{-\infty}^{+\infty} q(\omega) \left(-\omega^2 + i\gamma_m\omega + \omega_m^2\right) e^{i\omega t} d\omega. \quad (A14)$$

Comparing Eqs. (A13) and (A14), $q(\omega)$ is easily given as follows:

$$q(\omega) = \frac{A}{4m\beta\sqrt{\pi}}e^{-i\omega t_0}$$

$$\times \frac{e^{-\frac{(\omega-\omega_m)^2}{4\beta^2}}e^{i(\omega_m t_0+\varphi)} + e^{-\frac{(\omega+\omega_m)^2}{4\beta^2}}e^{-i(\omega_m t_0+\varphi)}}{-\omega^2 + i\gamma_m\omega + \omega_m^2},$$

$$|q(\omega)|^2 = \left|\frac{A}{4\beta\sqrt{\pi}}\right|^2 \frac{1}{|\chi(\omega)|^2} \left(e^{-\frac{(\omega-\omega_m)^2}{2\beta^2}} + e^{-\frac{(\omega+\omega_m)^2}{2\beta^2}}\right.$$

$$+ 2e^{-\frac{\omega^2+\omega_m^2}{2\beta^2}}\cos[2(\omega_m t_0 + \phi_{\text{CEP}})], \tag{A15}$$

where $\chi(\omega) = [m(\omega_m^2 - \omega^2 + i\gamma_m\omega)]^{-1}$ is the susceptibility of the mechanical oscillator.

APPENDIX B: MECHANICAL PULSES IN THE MULTICYCLE REGIME

Here, we introduce another laser to release the few-cycle restriction. Similarly, the Hamiltonian of the drives can be written as

$$H_{\rm md} = A \exp\left[-2\ln 2\left(\frac{t - t_0}{t_p}\right)^2\right] \cos(\omega_m t + \phi)\hat{q}, \quad (B1)$$

$$H_{\rm od} = i\hbar[(\varepsilon_l + \varepsilon_a e^{-i\Omega t - i\phi_a})\hat{c}^{\dagger} - \text{H.c.}]. \quad (B2)$$

We give the equations of motion as follows:

$$\ddot{q} + \gamma_m \dot{q} + \omega_m^2 q = -\frac{\hbar g}{m} |c|^2 + \frac{A}{m} e^{-\beta^2 (t - t_0)^2} \cos(\omega_m t + \phi),$$
(B3)

$$\dot{c} = -[\kappa + i(-\Delta + gq)]c + (\varepsilon_l + s_a e^{-i\Omega t - i\phi_a}).$$
 (B4)

When the interaction between the pulse and the system ends, Eq. (B3), under the strong-drive and negligible-damping approximations, can be reduced to the following form as in Appendix A:

$$q(t) = q_0 \cos(\omega_m t + \phi_m). \tag{B5}$$

Like in Appendix A, we define $h(t) = -[\kappa + i(-\Delta + Gq)]$ and suppose the solution of c(t) is as follows:

$$c(t) = e^{\int h(t)dt}g(t) = f(t)g(t).$$
 (B6)

Substituting this equation into Eq. (B4), we can obtain

$$f(t)g(t)h(t) + f(t)\dot{g}(t)$$

$$= h(t)f(t)g(t) + \sqrt{\eta_c \kappa}(\varepsilon_l + s_a e^{-i\Omega t - i\phi_a}),$$

$$g(t) = g_1(t) + g_2(t),$$

where

$$g_1(t) = \varepsilon_l \int f(t)^{-1} dt,$$

$$g_2(t) = s_a e^{-i\phi_a} \int e^{-i\Omega t} f(t)^{-1} dt.$$

We give f(t) and $g_1(t)$ as follows:

$$f(t) = e^{\int h(t)dt}$$

$$= \exp(-\kappa t) \exp(-i\omega_m t) \exp\left[-\frac{iGq_0}{\omega_m} \sin(\omega_m t + \phi_m)\right]$$

$$= \exp(-\kappa t) \exp(-i\omega_m t) \sum_{n=-\infty}^{+\infty} J_n(\alpha) e^{-in(\omega_m t + \phi_m)} dt,$$

$$g_1(t) = \varepsilon_l \int f(t)^{-1} dt$$

$$= \varepsilon_l \sum_{n=-\infty}^{+\infty} J_n(\alpha) e^{in\phi_m} \frac{\exp[i(n+1)\omega_m t + \kappa t]}{i(n+1)\omega_m + \kappa},$$

where $\alpha = \frac{Gq_0}{\omega_m}$.

Similarly, $g_2(t)$ is obtained as

$$g_2(t) = \varepsilon_a e^{-i\phi_a} \int e^{-il\omega_m t} f(t)^{-1} dt = \varepsilon_a e^{-i\phi_a} \sum_{n=-\infty}^{+\infty} J_{n+l}(\alpha) e^{i(n+l)\phi_m} \frac{\exp[i(n+1)\omega_m t + \kappa t]}{i(n+1)\omega_m + \kappa}.$$

As a result, we obtain c(t):

$$c(t) = f(t)[g_1(t) + g_2(t)],$$

with

$$c_N(\omega_m) = e^{iN\phi_m} \sum_{n=-\infty}^{+\infty} \frac{\left[\varepsilon_l J_n(\alpha) + \varepsilon_a e^{-i(\phi_a - l\phi_m)} J_{n+l}(\alpha)\right] J_{N+n}(\alpha)}{i(n+1)\omega_m + \kappa}.$$

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