

Condensation of thresholds in multimode microlasersLi Ge,^{1,2,*} Hui Cao,³ and A. Douglas Stone³¹*Department of Engineering Science and Physics, College of Staten Island, CUNY, Staten Island, New York 10314, USA*²*The Graduate Center, CUNY, New York, New York 10016, USA*³*Department of Applied Physics, Yale University, New Haven, Connecticut 06520, USA*

(Received 27 July 2016; published 27 February 2017)

We show from *ab initio* laser theory that by choosing an appropriate spatial pump profile, many different spatial modes of a typical microlaser can be turned on at the same pump energy, substantially increasing the number N of simultaneous lasing modes. The optimal pump profile can be obtained simply from knowledge of the space-dependent saturated gain profile when the system is uniformly pumped up to the N th modal threshold. We test this general result by applying it to a two-dimensional diffusive random laser and a microdisk laser. Achieving highly multimode lasing at reasonable pump powers is useful for reducing the spatial coherence of laser sources, making them suitable for use in speckle-free imaging and other applications.

DOI: [10.1103/PhysRevA.95.023842](https://doi.org/10.1103/PhysRevA.95.023842)

The laser is a well-studied driven-dissipative nonlinear system, and many aspects of the theory are well understood and tested experimentally [1,2]. In the past two decades, however, many new laser cavity designs have been introduced, both to study novel optical physics and in the search for efficient, on-chip microscale sources [3–5]. Unlike macroscopic laser cavities, where cavity design and intracavity components can be used to control the number of lasing modes, for microlasers modal control is less straightforward; moreover until recently there was no convenient theoretical approach to determining the number of lasing modes and their thresholds. Despite these challenges, modal control in microlasers offers a unique opportunity in regard to recent breakthroughs in speckle-free imaging [6–8]. While single-mode lasing is desirable in many applications, highly multimode lasing with spatially uncorrelated phases is a very convenient mechanism for reducing the spatial coherence of a bright laser source, allowing lasers to be used in full-field imaging microscopy and other applications requiring intense speckle-free sources. Compared with traditional low spatial coherence sources such as thermal lamps and light-emitting diodes, highly multimode lasers offer the advantage of higher power per mode, improved collection efficiency, and easier spectral control.

As has been known for some time [2,9], for essentially all microlasers, multimode lasing is stable due to spatial hole-burning: Different spatial modes use distinct regions of the gain medium and can reach the lasing threshold (modal gain equals loss) at different pump strengths, despite saturation of the gain by modes which turn on earlier. In addition, the large free spectral range in microlasers prevents population dynamics from effectively driving multimode laser instabilities. The modal thresholds of lasers in the absence of saturation are determined by two factors: the quality (Q) factor of the mode in the passive cavity, and the modal overlap with the gain medium, both spatially and spectrally. Previous work on achieving highly multimode lasing in microlasers has focused on passive cavity engineering to create many modes with similar Q factors, using, for example, random lasers [10] and chaotic lasers [11]. This approach, however, usually leads to relatively low Q factors and high thresholds.

In this work we propose to exploit the spatial degrees of freedom of the pump to achieve highly multimode lasing in microlasers, which can be applied to both high- Q and low- Q cavities without spoiling their quality factors. The spatial pump profile can be controlled through spatial light modulators [12], phase masks, or eventually by multiple electrical contacts [13–15], and such an approach has been used empirically to achieve single-mode lasing [16–18] and directional emission [19,20]. In contrast to these works using trial-and-error optimization to achieve modal control, here we show the existence of pump profiles leading to highly multimode lasing *analytically*, using steady-state *ab initio* laser theory (SALT), a recently developed approach to predict the modal behavior in complex microlaser geometries with arbitrary pump profiles. SALT reduces the semiclassical laser equations to a set of *time-independent* self-consistent nonlinear wave equations that include the spatial hole burning effect exactly. The SALT equations accurately find the solutions of the full semiclassical laser equations for nonuniformly pumped multimode microlasers [21–25], and they have been used to predict new phenomena, such as re-entrant lasing near exceptional points [26], which have since been observed [27,28]; hence SALT (and approximations to it) have been used to study numerically modal control through variation of the pump profile. However, due to the nonlinearity of the equations there have been no rigorous analytic results to guide these studies.

Here we present a very surprising result of this type. Suppose a laser cavity is pumped with some trial pump profile (e.g., uniform in space), and as the pump power increases, $N \gg 1$ modes turn on at thresholds $D_0^{(\mu)}$ ($\mu = 1, 2, \dots, N$). We show that for any such trial profile there exists a refined pump profile which will cause all N modes to turn on at the same “master threshold” D_m , where $D_0^{(1)} < D_m < D_0^{(N)}$. Above D_m typically many more modes will lase for the same pump power as with the trial pump profile. We also show that this approach can be effective even given practical constraints on pump control.

Before going into the proof of threshold condensation and relevant examples, we note that degenerate thresholds arising from symmetry are well-known, e.g., counterpropagating modes in ring or disk lasers. However, this case is only a pairwise degeneracy, and it is usually lifted by the nonlinearity, which randomly locks into one of the two possible states [29–31]. There are also degenerate macroscopic cavity designs

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which have many modes with the same threshold. Here, as noted, we are focusing on microlasers which can have *any* cavity design which supports many modes at high pump, and our approach requires no symmetry at all, nor any simple relationship among the condensed modes.

To understand why such a master threshold should exist, note that the pumped laser cavity itself is performing an optimization: As the pump increases, modes at different frequencies have different access to the gain, and all those which eventually lase have managed to balance gain and loss through positive feedback. However in the nonlinear steady state, the lasing modes do not respond simply to the pump profile imposed externally; instead they respond to the saturated gain profile, which is strongly affected by the spatial variation and relative intensities of each mode. Hence if one *imposes* an external pump at low power (so no modes lase) which follows spatially the *saturated gain profile* and simply increases the total pump power with this profile, at some power level all the modes will balance gain and loss with the now unsaturated gain susceptibility and start lasing together.

We now show that this simple argument is rigorously correct using the SALT equations [21–25], which find the steady-state solutions of the semiclassical Maxwell-Bloch equations [1,2] and N -level generalization thereof. SALT assumes a stationary population inversion in the gain medium (see the discussion in Ref. [32]), which requires that the relaxation rate of the gain medium γ_{\parallel} be small compared to the dephasing rate of the polarization γ_{\perp} and the free spectral range of the laser, both satisfied for most microlasers. The high accuracy of SALT in this regime has been verified by comparing with time-dependent FDTD simulations [32–35]. Although SALT, as well as the Maxwell-Bloch equations, treats homogeneously broadened gain media by construction, there is evidence that it applies qualitatively to certain inhomogeneously broadened gain media as well, such as InAs quantum dots lasers [18].

The SALT equations for the steady-state lasing modes $\Psi_{\mu}(\vec{r}; D_0)$ ($\mu = 1, \dots, N$) and their frequencies Ω_{μ} take the form [32],

$$\left[\nabla \times \nabla - [\varepsilon_c(\vec{r}) + \varepsilon_g(\vec{r}; D_0)] \frac{\Omega_{\mu}^2}{c^2} \right] \Psi_{\mu}(\vec{r}; D_0) = 0, \quad (1)$$

where c is the speed of light in vacuum and $\varepsilon_c(\vec{r})$ is the passive part of the cavity dielectric function independent of the pump strength D_0 . The electric field $\Psi_{\mu}(\vec{r}; D_0)$ is expressed in dimensionless form, measured in units $e_c = \hbar \sqrt{\gamma_{\parallel} \gamma_{\perp}} / 2g$ where g is the dipole matrix element of the lasing transition. The equations are to be solved with purely outgoing boundary conditions, and below the first threshold $D_0^{(1)}$ no solutions exist. Nontrivial solutions $\Psi_{\mu}(\vec{r}; D_0)$ appear and increase in amplitude above each threshold $D_0^{(\mu)}$, and each $\Psi_{\mu}(\vec{r}; D_0)$ oscillates at a real-valued lasing frequency Ω_{μ} , which in general varies with D_0 .

Each mode interacts with itself and the other lasing modes via nonlinear gain saturation, which appears in the “active” part of the dielectric function and takes the form [24]:

$$\varepsilon_g(\vec{r}; D_0) = \frac{\gamma_{\perp}}{\Omega_{\mu} - \omega_a + i\gamma_{\perp}} \frac{D_0 f_0(\vec{r})}{1 + \sum_{\nu=1}^N \Gamma_{\nu} |\Psi_{\nu}(\vec{r}; D_0)|^2}. \quad (2)$$

ω_a here is the atomic transition frequency, $\Gamma_{\nu} \equiv \gamma_{\perp}^2 / [\gamma_{\perp}^2 + (\Omega_{\nu} - \omega_a)^2]$ is the Lorentzian gain curve evaluated at Ω_{ν} , and $f_0(\vec{r}) \geq 0$ is the externally imposed spatial profile of the pump, which we normalize by $\int_{\text{cavity}} f_0(\vec{r}) d\vec{r} = S$, where $S = \int_{\text{cavity}} d\vec{r}$ is the area of the cavity in two dimensions. As noted, the saturated gain profile depends strongly on the amplitude, spatial variation, and frequency of the lasing modes, with the highest amplitude modes causing the most saturation.

Now consider $f_0(\vec{r})$, as the “pilot” profile we wish to refine to cause all of the modes up to a target number N_t to lase at the same threshold. This trial problem for $\Psi_{\mu}(\vec{r}; D_0), \Omega_{\mu}$ up to the N_t th threshold D_t can be solved either by expanding $\Psi_{\mu}(\vec{r}; D_0)$ in a complete, biorthogonal, and frequency-dependent basis (i.e., the constant flux states [22]) and solving a set of nonlinear equations for the expansion coefficients and Ω_{μ} , or by a direct nonlinear numerical solver based on the Newton-Raphson algorithm [32]. As noted, for those N_t modes the *saturated* gain profile balances gain and loss. Hence we take our refined pump profile to be proportional to the saturated gain profile,

$$f_m(\vec{r}; D_t) = \frac{C(D_t) f_0(\vec{r})}{1 + \sum_{\mu=1}^{N_t} \Gamma_{\mu} |\Psi_{\mu}(\vec{r}; D_t)|^2}, \quad (3)$$

where $C(D_t)$ is a constant determined by the normalization $\int_{\text{cavity}} f_m(\vec{r}; D_t) d\vec{r} = S$. After replacing $f_0(\vec{r})$ by $f_m(\vec{r}; D_t)$ in Eqs. (1) and (2), we insist that the *unsaturated* susceptibility with the new profile be identical to the saturated susceptibility of the original pilot problem at D_t . This requires that the appropriate pump value for the refined problem be

$$D_m = \frac{D_t}{C(D_t)}, \quad (4)$$

which uniquely determines a master threshold, at which all N_t modes turn on under the new pump profile. At D_m all the lasing modes have the same spatial pattern and frequency as in the trial problem. This construction was first noted in passing in Ref. [36], and it relies on the fact that the SALT equations are *homogeneous* nonlinear differential equations. To exemplify this construction in a much simpler case, we discuss its analog using a nonlinear matrix problem in Appendix A.

The above result on threshold condensation is exact for the SALT equations, and therefore applies to many lasers, particularly microlasers as noted above. However, while this result rigorously proves that all N_t modes are at threshold at D_m , it does not prove that above D_m , all modes are lasing, and below D_m none are. It is possible in principle that one or more of the modes have turned on at a lower pump value, acquired a negative slope before D_m , and stop lasing at D_m , which would be their “off threshold”. However, while negative power slope due to modal interactions is possible, it requires special relationships between the modal profiles and lasing frequencies and typically also some optimization of the pump profile [35]. Since the modes involved here are arbitrary and the pump profile has been set by the requirement of degeneracy, it is highly unlikely that negative power slopes will occur at or near D_m (see Appendix B).

As a first demonstration of threshold condensation following this construction, we show in Fig. 1 the condensation of $N_t = 6$ modes in a two-dimensional (2D) diffusive random laser [21,37–39], calculated via SALT. [For 2D geometries

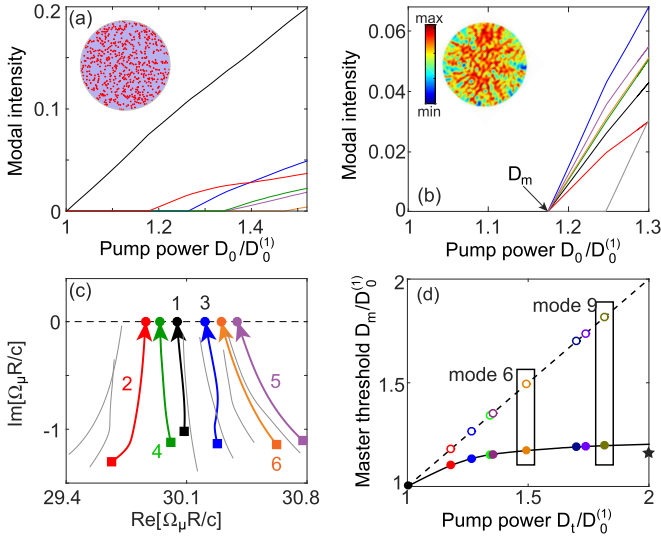


FIG. 1. Condensation of multiple thresholds in a 2D random laser. (a) Modal intensity $I_\mu \equiv \int_{\text{cavity}} |\Psi_\mu(\vec{r}; D_0)|^2 d\vec{r}/S$ as a function of pump power D_0 with uniform pumping. (Inset) A disk pump of radius R over an aggregate of scatterers with refractive index $n = 1.2$. The background index is 1. The gain medium is characterized by $\omega_\perp R/c = 30$ and $\gamma_\perp R/c = 1$. (b) Simultaneous onset of six modes above $D_m = 1.17D_0^{(1)}$ with the refined pump profile $f_m(\vec{r}; D_t = 1.48D_0^{(1)})$. An additional mode (thin gray line) also turns on in the range of pump power shown. (Inset) Refined pump profile and its color scale. (c) The lasing frequencies of the six modes in (a) at D_t are shown by filled circles, where the trajectories of the corresponding QB modes end up as the pump power increases from 0 (squares) to the master threshold D_m with the refined pump profile. The trajectories of six other QB modes that have not reached their thresholds are also shown (thin gray lines). The horizontal line indicates the threshold condition $\text{Im}[\Omega_\mu R/c] = 0$. (d) D_m as a function of D_t . Filled circles show the values of D_m when N_t increases by 1, and open circles show the threshold of this new mode with uniform pumping. Two pairs of such values for $N_t = 6$ and 9 are enclosed by boxes.

the vector equation (1) reduces to a nonlinear Helmholtz form [24]. Using a uniform pilot pump profile $f_0(\vec{r}) = 1$, we ramp up the pump power until six modes are lasing [see Fig. 1(a)]. Expressed in terms of the first threshold $D_0^{(1)}$, the thresholds of the other five modes are 1.18, 1.27, 1.34, 1.35, and 1.48. Now using $D_t = 1.48D_0^{(1)}$ and the corresponding saturated gain profile $f_m(\vec{r}; D_t)$ as the refined pump profile, we find that the master threshold is given by $D_m = 1.17D_0^{(1)}$. At this pump value only one mode lases with uniform pumping, while with the refined pump there are now six [see Fig. 1(b)]. As a separate verification, we plot the trajectories of the corresponding resonance poles [quasibound (QB) mode frequencies] with increasing pump strength in Fig. 1(c); the pump value at which a pole first reaches the real axis denotes the lasing threshold [24], and here all six poles reach the real axis simultaneously.

The same procedure can be applied to a larger target number of lasing modes in the same laser. For example, for this random laser the ninth mode starts lasing at $D_0^{(9)} = 1.81D_0^{(1)}$ with uniform pumping. Now using this different value as D_t , and the different saturated gain profile as the refined pump profile, the master threshold is given by $D_m = 1.20D_0^{(1)}$,

a value where there are only two modes lasing with uniform pumping, whereas now there are nine. Strikingly, the master threshold increases much more slowly with N_t than does the N_t th threshold with uniform pumping [see Fig. 1(d)]. For example, D_m only increases by $0.03D_0^{(1)}$ when N_t increases from 6 to 9, while the difference between the sixth and ninth thresholds with uniform pumping is $0.33D_0^{(1)}$.

The reason for this behavior is as follows: The ratio of D_m and D_t is given by the normalization constant $C(D_t)$ [Eq. (4)]. By integrating both sides of Eq. (3) and using the normalization of $f_m(\vec{r}; D_t)$, we find

$$C(D_t)^{-1} = \int_{\text{cavity}} \frac{f_0(\vec{r}) d\vec{r}}{1 + \sum_{\mu=1}^{N_t} \Gamma_\mu |\Psi_\mu(\vec{r}; D_t)|^2}. \quad (5)$$

On average, the saturation term in the denominator increases linearly with pump, so that (averaging over space) $\sum_{\mu=1}^{N_t} \Gamma_\mu I_\mu(D_t) \approx aD_t/D_0^{(1)} - b$, [where $I_\mu(D_t) \equiv \int_{\text{cavity}} |\Psi_\mu(\vec{r}; D_t)|^2 d\vec{r}/S$]. Thus $D_m \approx D_t/[1 - b + aD_t/D_0^{(1)}] \rightarrow D_0^{(1)}/a$, when the pump power $D_t \gg D_0^{(1)}$, indicating that D_m remains of order $D_0^{(1)}$ even when D_t becomes very large. The asymptote of D_m in Fig. 1(d) is captured well by this approximation ($1.16D_0^{(1)}$; marked by the star), using $a = 0.86$ extracted from the modal intensities in Fig. 1(a).

The saturated gain profile used to generate the refined pump typically varies on the scale of the wavelength of light in the cavity, whereas approaches to shape the pump profile mentioned in the introduction will have limited resolution due to the diffraction limit, carrier diffusion, and other effects. In addition, the saturated gain profile is typically not directly measurable but must be calculated from some model of the cavity, and will be subject to corresponding inaccuracies. Thus there will be limits on our ability to generate the ideal pump profile leading to exact degeneracy. To estimate this effect, we perform a Gaussian smoothing of the refined pump profile used in Fig. 1:

$$\tilde{f}_m(\vec{r}; D_t) = \frac{\tilde{C}(D_t)}{2\pi\sigma^2} \int_{\text{cavity}} f_m(\vec{\zeta}; D_t) e^{-\frac{(\vec{r}-\vec{\zeta})^2}{2\sigma^2}} d\vec{\zeta}, \quad (6)$$

where $\tilde{C}(D_t)$ is a normalization constant similar to $C(D_t)$. We note that a quite noticeable reduction of pump details already takes place at $\sigma = R/40$ [compare the insets in Figs. 1(b) and 2(b)]. Nevertheless, we still find a significant enhancement of multimode lasing [see Fig. 2(b)]: While the sixth threshold is now at $1.27D_0^{(1)}$ and higher than the master threshold ($1.17D_0^{(1)}$), it is still much lower than its value with uniform pumping ($1.48D_0^{(1)}$). $D_0^{(1)}$ here refers the first threshold under the pilot pump profile.

In addition, we can perform further optimization by treating the refined pump profile itself as a variational function, and using the intensities in the denominator of Eq. (3) as variational parameters to compensate much of the threshold splitting. For example, the dominant effect of pump smearing in Fig. 2(a) is a much lower threshold of mode 1. To reverse this change, we increase the suppression of mode 1 in the refined pump profile (before smearing) by increasing the intensity $|\Psi_1(\vec{r}; D_t)|^2$ [and $I_1(D_t)$]. Due to cross-saturation, this treatment also changes the thresholds of the other modes but typically to a lesser extent. Hence by adjusting each modal

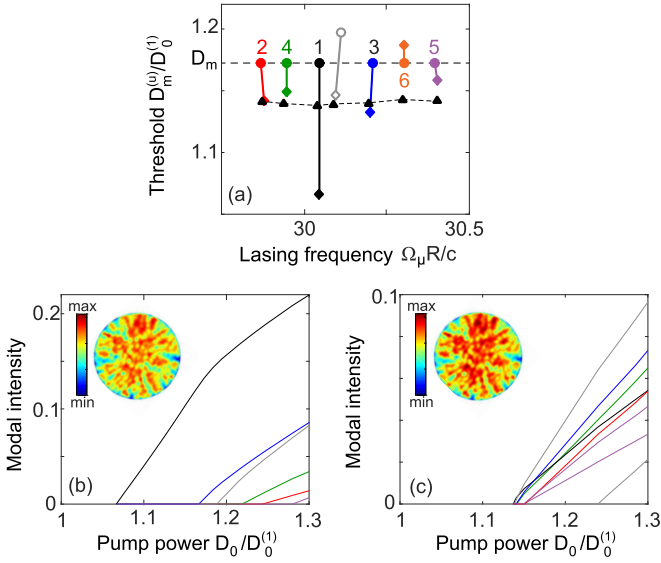


FIG. 2. Effect of a deviated pump profile and its correction. (a) Filled diamonds: lifting of the sixfold threshold degeneracy (filled circles) in Fig. 1(b) due to a Gaussian smoothing of the refined pump profile with $\sigma = R/40$ [see inset in (b)]. Open symbols show an additional mode (mode 7). Connected black triangles: restoration to a quasidegeneracy after an “error correction” procedure with modal-intensity changes $\Delta I_{1-7}(D_t) = 0.82, 0.01, 0.25, 0.08, -0.05, -0.10, 0.13$. Modal interactions under the smeared pump profiles are neglected in calculating the degeneracy-lifted thresholds $D_m^{(u)}$ but included in (b) and (c). (b) Modal intensity I_μ as a function of pump power D_0 with $\tilde{f}_m(\vec{r}; D_t)$ before “error correction”. (c) Same as (b) but after “error correction”.

intensity in the appropriate direction to compensate its splitting due to smearing, quasidegeneracy can be restored as shown in Figs. 2(a) and 2(c). Note that the quasidegenerate master threshold after “error correction” is given by $\bar{D}_m \approx 1.15D_0^{(1)}$, which is even lower than the degenerate one. This illustrates the point that D_m is not a lower bound on the pump value where N_t modes can lase, but it is an excellent starting point for optimization.

As a final example, we apply the threshold condensation procedure to a microdisk laser (see Fig. 3), a well-studied

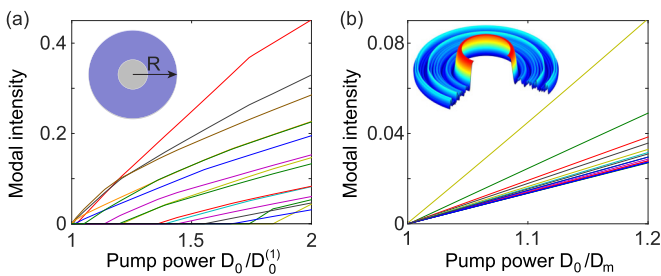


FIG. 3. Condensation of multiple thresholds in a microdisk laser of radius R . (a) Modal intensity I_μ as a function of pump power D_0 with a ring-shaped pilot pump profile (inset). The 16th mode starts lasing at $D_0 = 1.83D_0^{(1)}$, and $\gamma_\perp R/c = 0.5$ is used. (b) Simultaneous onset of all 16 modes above $D_m = 1.08D_0^{(1)}$ with the refined pump profile $f_m(\vec{r}; D_t = 1.83D_0^{(1)})$. The 3D rendering of the latter is shown as the inset, one quarter of which is removed to show its radial profile.

multimode microlaser of technological interest. We choose a high index contrast typical of semiconducting devices although we assume an atomiclike gain medium (e.g., quantum dots). The relevant electromagnetic modes are high- Q whispering-gallery modes (WGMs), confined by near total internal reflection. For the reason discussed already in the introduction, we only consider WGMs of one symmetry, e.g., the clockwise rotation (positive azimuthal quantum number m), which preserves the rotational symmetry of the system when gain saturation is considered. With $n = 3.3 + 10^{-4}i$ and $\omega_a R/c = 30$, this microdisk laser supports WGMs of m up to 100. It is natural here to choose a nonuniform pilot profile, and we take a ring-shaped pump profile [$f_0(\vec{r}) = 0$ for $r < R/3$]. With this choice the first mode has $m = 80$ and the 16th mode of $m = 37$ starts lasing at $D_0^{(16)} = 1.83D_0^{(1)}$ [see Fig. 3(a)]. Using this pump value as D_t , the master threshold occurs at $D_m = 1.08D_0^{(1)}$, beyond which all 16 modes start lasing simultaneously [see Fig. 3(b)].

In summary, we have shown that the spatial hole-burning nonlinearity of a laser can be utilized to refine the pump profile, resulting in the simultaneous lasing of many modes at relatively low pump power. This analytic property of the lasing equations is a consequence of their nature as a set of homogeneous nonlinear differential equations, which is independent of the laser cavity itself. Therefore, this approach can be used as a guide to find spatial profiles leading to control of multimode lasing properties, for both high- Q and low- Q cavities, even if there are limitations on the spatial precision or resolution of the pump profile as illustrated in Fig. 2. For a stable pump source, its temporal fluctuation, even if noticeable, has a time scale longer than the laser dynamics. Then the laser can be viewed as subjected to multiple realizations of a spatial noise sequentially. For each instance the effect of the noise is captured by what we have discussed in Fig. 2, and as a function of time we may see lasing of different subgroups of the intended modes. Nevertheless, this “subgroup hopping” does not impose a problem for our purpose of speckle-free imaging, since we only require a large group of modes lasing simultaneously (that have uncorrelated phases), without requiring constant lasing of a particular group of modes.

L.G. acknowledges partial support by PSC-CUNY under Grant No. 68698-0046 and NSF under Grant No. DMR-1506987. H.C. acknowledges support by NSF under Grant No. DMR-1205307. A.D.S. acknowledge support by NSF under Grant No. DMR-1307632.

APPENDIX A: NONLINEAR MATRIX MODEL

To exemplify the construction of the refined pump profile in a much simpler setting, here we consider the following nonlinear matrix problem:

$$\begin{pmatrix} 1 + \frac{D_0 f_a}{1+I_a} & -1 \\ -1 & 1 + \frac{D_0 f_b}{1+I_b} \end{pmatrix} \begin{pmatrix} a \\ b \end{pmatrix} = 0, \quad I_{a(b)} = a^2(b^2). \quad (\text{A1})$$

Here $f = (f_a, f_b)$ resembles the pump profile and the fractions $D_a \equiv D_0 f_a / (1 + I_a)$, $D_b \equiv D_0 f_b / (1 + I_b)$ resemble the saturated gain profile. With a uniform “pump profile”

$f_a = f_b = 1$ and at “pump strength” $D_0 = 4$, we find $a = (1 + \sqrt{5})/2$, $b = (1 - \sqrt{5})/2$ give a nonlinear solution of the matrix problem above, resulting in a saturated “gain profile” $D_a = 4/[1 + (\sqrt{5} + 1)^2/4] \equiv d_a$ and $D_b = 4/[1 + (\sqrt{5} - 1)^2/4] \equiv d_b$. Now if we choose a new “pump profile” $f = (d_a, d_b) \equiv f_m$, we immediately find that

$$\begin{pmatrix} a \\ b \end{pmatrix} = \begin{pmatrix} 1 + \sqrt{5} \\ 1 - \sqrt{5} \end{pmatrix} \epsilon \quad (\text{A2})$$

is a solution of Eq. (A1) at $D_0 = 1 \equiv D_m$, when $\epsilon \rightarrow 0$. This solution indicates that D_m is the threshold of the “laser” with the new “pump profile” f_m .

We note that this simplified example differs from the SALT equations in the main text in two important aspects. First, it is a “single-mode” model, where $I_{a,b}$ represents the intensity of this mode at two different locations. Second, we did not normalize f_m and hence the value of D_m cannot be compared directly with the threshold with uniform pumping. Nevertheless, the essential feature of this simplified example is exactly the same as that in the main text, where we have a set of homogeneous nonlinear equations and take the saturated “gain profile” at a certain pump strength with uniform pumping to be the pump profile in a second setup, resulting in a laser at its threshold.

APPENDIX B: NEGATIVE POWER SLOPE AT THE MASTER THRESHOLD

With a refined pump profile $f_m(\vec{r}; D_t)$, we have shown in the main text that all N_t modes lase simultaneously once the pump power is increased beyond the resulting master threshold D_m . There are two rare scenarios where this behavior breaks down, with one or more of the N_t mode suppressed beyond D_m . We discuss these two scenarios in this appendix.

The first scenario in which one or more of the N_t modes could in principle be suppressed beyond their condensed threshold D_m is a linear effect, where the trajectory of the corresponding quasibound mode frequency $\Omega_\mu(D_0)$ crosses the real axis at $D_0 = D_m$ from above. This behavior is caused by an exceptional point [26,40,41], and such an $\Omega_\mu(D_0)$ has another crossing with the real axis at a lower pump power (see the schematics in Fig. 4). We have not found a case where this rare scenario takes place, which requires fine tuning of the system parameters close to an exceptional point.

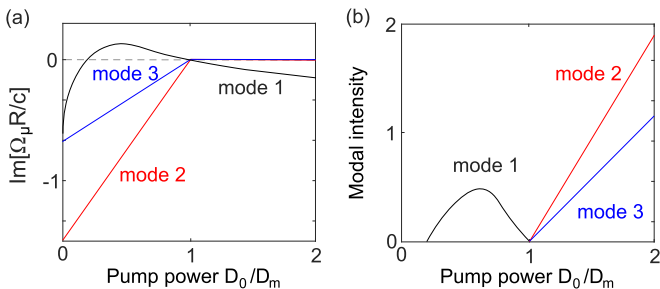


FIG. 4. Schematics showing that the master threshold in principle can be where a mode is turned off instead of turned on. D_m in this case is the “on” threshold of modes 2 and 3 and “off” threshold of mode 1.

The second scenario is a nonlinear effect. It occurs if the onset of mode competition above D_m would lead to a negative power slope of one or more modes. To study this scenario analytically, we assume the cavity has a high- Q factor and consider first the $N_t = 2$ case for simplicity. For a high- Q cavity SALT can be approximated by a simple set of intensity equations [24], which take the following form here:

$$\frac{D_0}{D_m} - 1 = \chi_{11}\mathcal{J}_1 + \chi_{12}\mathcal{J}_2 = \chi_{22}\mathcal{J}_2 + \chi_{21}\mathcal{J}_1. \quad (\text{B1})$$

Although $\mathcal{J}_\mu \equiv \Gamma_\mu \int_{\text{cavity}} f_m(\vec{r}) \Psi_\mu(\vec{r}; D_0)^2 d\vec{r}/S$ is defined differently from the modal intensity I_μ introduced in the main text, they are proportional to each other in a high- Q cavity, and the normalized spatial mode profile $\varphi_\mu(\vec{r}) = \Psi_\mu(\vec{r}; D_0) \sqrt{\Gamma_\mu/\mathcal{J}_\mu}$ is approximately real and varies little above threshold. $\chi_{\mu\nu} = \int_{\text{cavity}} f_m(\vec{r}) \varphi_\mu(\vec{r})^2 |\varphi_\nu(\vec{r})|^2 d\vec{r}/S$ gives the self-interaction coefficients when $\mu = \nu$ and the

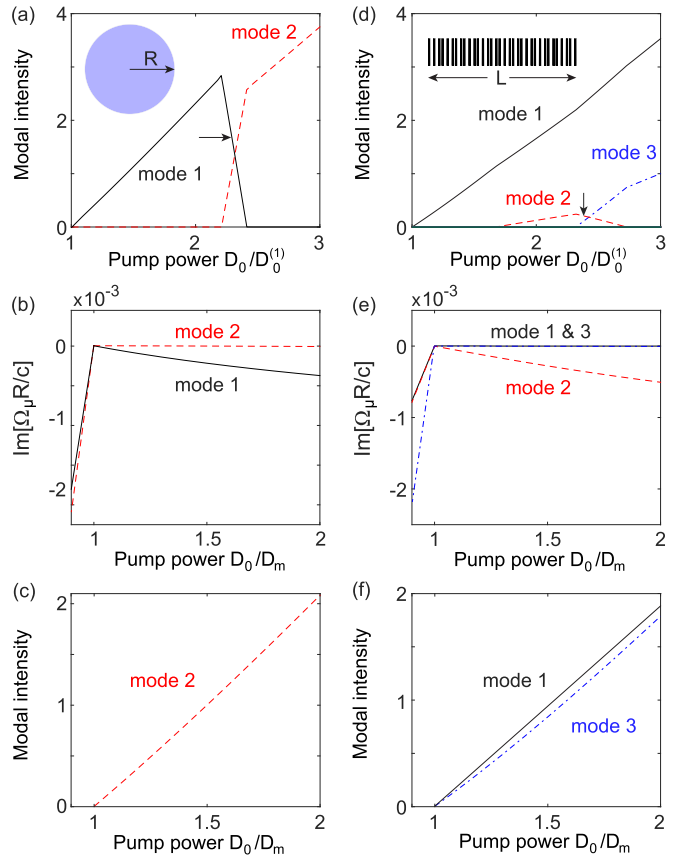


FIG. 5. Mode suppression beyond the master threshold in a microdisk laser (a)–(c) and an aperiodic laser (d)–(f). (a) and (d) Modal intensity I_μ as a function of pump power D_0 with uniform pumping. Both cases feature an interaction-induced mode switching (IMS), for the first and second modes, respectively. The arrows point to their negative power slopes at $D_t = 2.29D_0^{(1)}$ in (a) and $D_t = 2.38D_0^{(1)}$ in (c). (Insets) Schematics of a microdisk laser with $n_c = 2 + 0.01i$, $\omega_a R/c = 4.83$, and $\gamma_\perp R/c = 1$ in (a) and an aperiodic laser with dielectric layers of $n_c = 1.5$ (in air), $\omega_a R/c = 122.51$, and $\gamma_\perp R/c = 17.46$ in (d). (b) and (e) $\text{Im}[\Omega_\mu R/c]$ as a function D_0 with the refined pump profile $f_m(\vec{r}; D_t)$. $N_t = 2, 3$ and $D_m/D_0^{(1)} = 1.54, 1.37$ in (b) and (e), respectively. (c) and (f) Same as (a) and (d) but with their respective $f_m(\vec{r}; D_t)$.

cross-interaction coefficients when $\mu \neq \nu$, and we note that $\chi_{21} \approx \chi_{12}$ holds in a high- Q cavity. It is straightforward to see that a negative power slope for either \mathfrak{J}_1 or \mathfrak{J}_2 requires

$$\frac{\chi_{22} - \chi_{12}}{\chi_{11} - \chi_{21}} = \frac{\mathfrak{J}_1}{\mathfrak{J}_2} < 0. \quad (\text{B2})$$

In other words, the cross-interaction coefficients χ_{12}, χ_{21} need to be larger than one of the self-interaction coefficients and smaller than the other. This condition is again very rare in a high- Q cavity which features $\chi_{11}, \chi_{22} \gg \chi_{12}, \chi_{21}$ in general; only recently was the condition (B2) reported that leads to interaction-induced mode switching (IMS) [35]. Using the multimode form of Eq. (B1), the criterion (B2) can be generalized to $N_t > 2$ cases straightforwardly, i.e.,

$$\mathfrak{J}_\mu \propto \sum_{\nu=1}^{N_t} [\chi^{-1}]_{\mu\nu} < 0, \quad (\text{B3})$$

for one or more of the N_t modes, where χ^{-1} is the inverse matrix of χ .

In Fig. 5 we apply the condensation procedure to the microdisk laser studied in Ref. [35] that exhibits IMS: The second mode turns on at $D_0^{(2)} = 2.21D_0^{(1)}$ before it switches off the first mode via a negative power slope at $D_0 = 2.41D_0^{(1)}$ [see Fig. 5(a)]. We choose $D_t = 2.29D_0^{(1)}$ in the cross-over region, which leads to $D_m = 1.54D_0^{(1)}$. As Fig. 5(b) shows, $\Omega_{1,2}$ reach the real axis simultaneously as the pump power is ramped up to D_m with the pump profile $f_m(\vec{r}; D_t)$. But as soon as D_0 goes beyond D_m , Ω_1 is forced into the lower half of the complex plane again due to mode competition, leading to single-mode lasing of the second mode only [see Fig. 5(c)].

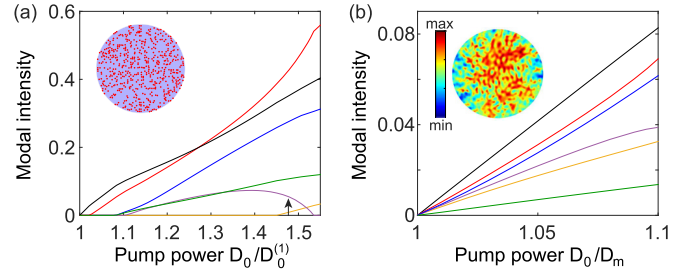


FIG. 6. Condensation of multiple thresholds in a 2D random laser. (a) Modal intensity I_μ as a function of pump power D_0 with uniform pumping. The arrow points to the negative power slope of the fifth mode at $D_t = 1.48D_0^{(1)}$ chosen for $N_t = 6$. (Inset) Schematics of the 2D random laser. The parameters are the same as in Fig. 1 of the main text except for a different disorder of scatterers. (b) Simultaneous onset of all six modes above $D_m = 1.35D_0^{(1)}$ with the refined pump profile $f_m(\vec{r}; D_t)$. The latter is shown in the inset with its color scale.

While Eq. (B1) and the criterion (B3) do not apply to low- Q cavities, the correlation between IMS and the suppression of certain mode(s) beyond D_m still seems to hold. In Figs. 5(d)–5(f) we show such an example in a one-dimensional aperiodic cavity. The second mode exhibits a negative power slope after the onset of the third mode at $D_0 = 1.66D_0^{(1)}$, and it is switched off at $D_0 = 2.73D_0^{(1)}$. When taking any pump value in this range as D_t , we find that the second mode is suppressed beyond D_m with the refined pump profile $f_m(\vec{r}; D_t)$.

We note that IMS does not only feature a negative power slope; this negative power slope must be induced suddenly by the onset of a new lasing mode. If the negative power slope is due to mode mixing [21], we find that all N_t modes still lase simultaneously above D_m . One example is shown in Fig. 6 for a 2D random laser.

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