Three-dimensional limac¸on: Properties and applications

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We perform electromagnetic wave simulations of fully three-dimensional optical limacon microcavities, on the basis of their future applications in microlasers and photonic devices. The analysis of the three-dimensional modes and far fields reveals an increase of the quality factors as compared to the two-dimensional case. The structure of the far field in the third dimension shows pronounced maxima in the emission directionality inclined to the resonator plane which may be exploited for coupling the resonator modes to the environment. This triggers ideas for technical applications, such as the suggested sensor that can detect small changes in the environment based on changes in the emission profile.

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The confinement and manipulation of light using microcavites has attracted a lot of interest in basic and applied physics research over the past decades [\[1,2\]](#page-4-0), e.g., research on microlasers [\[3\]](#page-4-0), filters for communication technology [\[4\]](#page-4-0), or single molecule sensing [\[5\]](#page-4-0). Furthermore, the research on microcombs $[6–8]$ and optomechanics $[9,10]$ benefits from the progress made in the field of optical microresonators. Established examples of optical microcavites are microdisks [\[3,11\]](#page-4-0), microspheres [\[12,13\]](#page-4-0), and microtoroids [\[14,15\]](#page-4-0) which confine light in whispering gallery modes with high quality factors *Q*. The first microdisk-based microlasers had the drawback of isotropic light emission because of rotational symmetry. In order to observe a directional laser emission, deformed microcavities were investigated [\[16–18\]](#page-4-0). A promising shape to combine directional emission and high quality factors is the limaçon shape $[19]$. Here, ray and wave calculations based on a two-dimensional model system agree very well with the experimentally observed far-field characteristics [\[20–23\]](#page-4-0).

In reality, however, microcavities are three-dimensional (3D) objects with finite heights. This third dimension will be especially important when the cavity sizes are further reduced and both cavity height *h* and radius *R* become comparable to the wavelength [\[24](#page-4-0)[,25\]](#page-5-0). Here, we systematically study 3D microcavities of limaçon shape (see left inset of Fig. [1\)](#page-1-0). Its cross section in the *x*-*y* plane is given in polar coordinates (r, ϕ) (cf. Fig. [1\)](#page-1-0), by

$$
r(\phi) = R[1 + \delta \cos(\phi)], \tag{1}
$$

with mean radius *R* and deformation parameter δ . We set δ = 0*.*43, a value known [\[19\]](#page-4-0) to yield a highly directional far-field emission for two-dimensional (2D) cavities with refractive index $n = 3.3$ embedded in vacuum $(n_0 = 1)$ as used here. We first discuss modes and far fields of 3D limaçon cavities of varying height to radius ratio *h/R*, followed by outlining a sensor application based on the 3D character of the far field and its extreme sensitivity to tiny changes in the refractive index.

Using MEEP [\[26\]](#page-5-0), a free finite-difference time-domain (FDTD) software package, 3D electromagnetic wave simulations have been performed to calculate the normalized frequencies $\Omega = kR = \text{Re}(\omega)R/c$, with ω being a complex frequency and *c* the speed of light, the quality factors $Q = -0.5 \text{Re}(\omega)/\text{Im}(\omega)$, the distributions of the electric field component $E_z(x, y, z)$ (modes), and the far-field intensity *I*(ϕ , θ). As our focus is on wavelength-scale cavities, *kR* ranges from 1.9 up to 10.7, with $k = 2\pi/\lambda$ being the wave number and λ the wavelength in vacuum. We use an E_z -pointdipole source to excite the modes and focus on the study of TM-polarized modes.

We first discuss the analogies between the structures of modes of the 2D and 3D limaçon cavity, respectively. An example of a 2D mode and the (x, y) cross section of a 3D mode are shown in Figs. $2(a)$ and $2(b)$. Both modes exhibit the same azimuthal order $m = 16$ and a similar field distribution of E_z , but different normalized frequencies kR and quality factors *Q*. The higher *kR* and the much larger *Q* of the 3D mode arise from the additional confinement in the third dimension and from the faster falloff of the electromagnetic field in the resonator (x, y) plane $(1/distance r$ instead of $1/\sqrt{r}$, respectively, yielding a general increase of *Q* in finite height cavities which is of crucial experimental relevance (see the Appendix).

In order to investigate the mode structure perpendicular to the resonator plane (*z* direction), we analyze $E_z(z)$ in Fig. 2(*c*) at one (x, y) position marked by a cross in Fig. $2(b)$. The mode confinement between the top and bottom surface is clearly visible, as well as the expected exponential decay of *Ez* outside this dielectric slab. The finite value $E_z(z = \pm h/2)$ reflects the boundary condition—the dielectric displacement field *D* has to be continuous at the top (t) and bottom (b) surfaces [\[27\]](#page-5-0), $(D_{\text{out}} - D_{\text{in}}) \cdot \dot{N}_{t,b} = 0$, where $\dot{N}_{t,b}$ is the normal vector at the top and bottom surface, respectively.

We analyze the exponential decay of $E_z(z)$ using the so-called effective refractive index model [\[28\]](#page-5-0) [cf. inset of Fig. $2(c)$]. The key idea is to decompose the 3D wave vector *nk* into its horizontal (index *xy*) and its vertical (index *z*) components

$$
n\vec{k} = nk_{xy}\vec{e}_{xy} + nk_z\vec{e}_z,\tag{2}
$$

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FIG. 1. Left inset shows the limacon shape from Eq. [\(1\)](#page-0-0) and for comparison a circle with radius *R* centered at $x = \delta R$. Note that the origin (0,0) of the polar coordinate system for the limaçon is quite off its center. The right figure displays the 3D limaçon cavity with mean radius *R* and height *h*. ϕ is the azimuthal and θ the inclination angle; (ϕ, θ) determine the far-field direction. The blue plane indicates the resonator plane (*x*-*y* plane, $z = 0$ or $\theta = 0$).

where \vec{e}_{xy} (\vec{e}_z) is the unit vector in the *x*-*y* plane (in the *z* direction). We make the following ansatz for the exponential decay of $E_z(z)$:

$$
E_z(z) = \begin{cases} a_1 \exp(ink_z z) + a_2 \exp(-ink_z z) & : |z| \le h/2\\ a_3 \exp(-q_z|z|) & : |z| \ge h/2 \end{cases}
$$
 (3)

FIG. 2. 3D mode structure. Comparison of (a) a 2D and (b) a 3D limaçon mode taken at $z = 0$. Both modes have the same radial order $l = 1$ and azimuthal order $m = 16$. (c) shows E_z parallel to the *z* axis piercing through the point marked by the cross in (b). The inset in (c) illustrates a dielectric slab and the decomposition of the wave vector *nk*.

where the vertical component q_z outside the cavity is related to the horizontal component nk_{xy} inside and the wave number *k* by $q_z^2 = (nk_{xy})^2 - k^2 = k^2(n_{xy}^2 - 1)$ according to the boundary conditions. The effective refractive index n_{xy} in the *x*-*y* plane follows from the Pythagorean decomposition, using Eq. (2) ,

$$
n^{2} =: n_{xy}^{2} + n_{z}^{2} = \left(\frac{nk_{xy}}{k}\right)^{2} + \left(\frac{nk_{z}}{k}\right)^{2}.
$$
 (4)

The n_{xy} represents the ratio of the speed of light in vacuum to that of a horizontally guided mode, and is a measure of the inclination angle $cos(\chi) = n_{xy}/n$ of the 3D wave vector *nk* with regard to the *x*-*y* plane. It runs from $n_{xy} = 1$ (total internal reflection on the top and bottom areas) up to $n_{xy} = n$ (light propagation in the *x*-*y* plane). An analytical form of $n_{xy} = n_{xy}(kh)$ for the dielectric slab was derived, e.g., in [\[27–29\]](#page-5-0).

It is tempting to compare $(kR)_{2D}$ of the 2D mode with the horizontal component $k_{xy}R$ of the 3D mode. The exponential fit yields $n_{xy} = 2.245$, which corresponds to $k_{xy}R = 5.7130$. This result is very close to $(kR)_{2D} = 5.7646$ confirming the similar mode structures, as seen in Fig. 2.

We now apply the effective refractive index model in order to investigate the confinement in the third dimension in more detail. To this end, we use numerics to fit n_{xy} from the exponential decay as a function of the (x, y) position, and make the connection to the 3D far field. We distinguish between (I) whispering-gallery-type modes, as seen in Fig. 2 and (II) modes characterized by higher field amplitudes in the center of the cavity. We will see below that modes of type II display truly 3D far-field features in contrast to type I (cf. Figs. [3](#page-2-0) and [4\)](#page-2-0).

First (I), we analyze a whispering-gallery-type mode, as depicted in Fig. $3(a)$ where the crosses mark the position at which the n_{xy} were fitted from the exponential decay of the electric field outside the cavity (cf. Fig. 2). In addition, Fig. $3(c)$ illustrates the electric field and displays the values of n_{xy} at the marked positions. We clearly observe a similar exponential decay at all positions, denoting a high confinement between the top and bottom areas. The resulting n_{xy} vary within a relatively small range from $n_{xy} = 2.969$ up to $n_{xy} = 3.305$, which indicates that the mode propagates homogeneously and with a large $k_{xy}R$ component since $n_{xy} \approx 3$ corresponds to an inclination angle of the wave vector *nk* with regard to the *x*-*y* plane of about 25◦.

Having analyzed the mode propagation, we now make the connection to the 3D far field of this mode that is depicted in Fig. [3\(b\).](#page-2-0) It shows a parametric plot of the intensity $I(\phi, \theta)$ in the Fraunhofer region $r \gg 2(2R)^2/\lambda$ (far field) that displays a main lobe centered along the *x* axis. The intensity of the main lobe is maximal in the plane of the resonator $(x - y)$ plane, $\theta = 0$) and decays away from this plane. We checked that this behavior is very similar to that of a plane wave diffracted at a single slit whose width is the cavity height. The inset of Fig. $3(b)$ shows a polar plot of the far-field intensity of this mode in the plane of the resonator that clearly exhibits directional emission. Thus, we can think of the main components that determine the 3D far field of this mode: (i) The 2D limacon-shaped cross section of the 3D cavity induces a characteristic, inherent emission

FIG. 3. Modes and far fields in 3D of a whispering-gallery-type mode. (a) A cross section of a 3D limaçon mode at $z = 0$. (b) 3D far field and its cross section in the resonator plane (inset). (c) Electric field component E_z above the cavity at positions numbered in (a) and the deduced effective refractive indices n_{xy} . The plot markers and solid lines show numerical data and the fit of the exponential decay, respectively.

profile (directional emission of the limacon). (ii) 3D limacon modes experience diffraction at the side area due to its finite height.

Next (II), we focus on modes which exhibit higher field amplitudes in the center of the cavity, as depicted in Fig. 4(a).

FIG. 4. As in Fig. 3, but for a mode characterized by higher field amplitudes in the center of the cavity. Note the oscillations of E_z in (c), e.g., at position 1. See the text for details.

This mode exhibits a much more complex field distribution inside the cavity as well as outside the cavity, as shown in Fig. $4(c)$. The resulting n_{xy} vary within a wide range from $n_{xy} = 1.807$ up to $n_{xy} = 3.288$, whereas $n_{xy} = 5.518$ is an example of a failed exponential fit because the electric field at position 1 propagates even outside the cavity. This propagation indicates refractive output and as a result of a reduced confinement between the top and bottom areas, reflected also in a diminished quality factor *Q*. The wide range of observed n_{xy} reflects the complexity of the mode that consists of whispering-gallery-type features at positions 2 and 3, as well as zigzagging (between the top and bottom areas) features at position 4 since $n_{xy}(4) = 1.807$ corresponds to an inclination angle of the wave vector $n\vec{k}$ with regard to the *x*-*y* plane of about 57 \degree .

Based on this analysis, we now address the 3D far field of this mode, shown in Fig. $4(b)$. We observe two main lobes that are inclined with regard to the resonator (x, y) plane. The inset confirms that directional emission still exists in the (x, y) plane and into the expected direction, but the maximum intensity is emitted along an inclined direction highlighting the 3D character of the far field. This inclined and directional emission is a truly 3D effect and originates in the output detected around position 1 marked in Fig. $4(a)$. Therefore, for type-II modes we complement the far-field determining mechanisms (i), (ii) discussed above by (iii) refractive escape of electromagnetic waves through the top and bottom areas.

We point out that all far fields are for freestanding cavities. For a substrate-mounted cavity, additional reflections at the substrate could interfere with the direct light emissions from the cavity and could thus modify the far fields [\[30\]](#page-5-0).

In the following, we use the truly 3D far-field features described above to design a sensor that can detect particles or gases in the environment based on a change of the emission characteristics, e.g., for a laboratory-on-a-chip application $[31]$. An optical resonator, such as the 3D limaçon cavity, can be very sensitive against tiny changes at the boundary. Thus, changes in the environment could affect mode structures [\[15\]](#page-4-0) and consequently the far fields, too. Since we focus on wavelength-scale cavities, bidirectional emission is possible [\[25\]](#page-5-0) unlike in large cavities where universal emission directionality is determined by chaotic ray dynamics. Here, we investigate the extent of the changes in the environment necessary to change the far-field direction significantly.

The idea of a particle sensor is illustrated in Fig. $5(a)$. A 3D limaçon is placed on a glass substrate that has a typical refractive index $n_g = 1.5$. The upper half space is enclosed by a chamber which could contain a gas or cloud of particles with a refractive index n_p higher than the vacuum index of $n_0 = 1.0$. Initially, we assume the chamber to be vacuum or filled with air (refractive index 1.0). A laser (red arrow) excites a mode in the 3D limacon; its far-field direction is indicated by the blue arrow. Next, the cavity is exposed to a gas of particles raising the refractive index outside from $n_0 = 1.0$ to $n_p > 1.0$. The change of the refractive index influences the mode and the far-field pattern resulting, e.g., in a reversed far-field emission direction (green arrow) as the sensor measurement signal (cf. Fig. [5\)](#page-3-0).

FIG. 5. 3D limaçon sensor. (a) sketches the idea of a 3D limaçon sensor. (b), (c), and (d) show calculated far fields and the horizontal mode structures at $z = 0$ (insets). Increasing the n_p results in reversed and bidirectional emission in (d) compared to (b).

Figures $5(b)$ – $5(d)$ show the calculated far fields and the horizontal mode structures at $z = 0$ (insets). Note that the far fields show exclusively positive inclinations, because we are interested in far fields in the upper half space. Remarkably, increasing the refractive index n_p by 2% [\[32\]](#page-5-0) and 5% [Figs. $5(c)$ and $5(d)$] completely changes the far-field characteristics. It leads to a modified field distribution in the center of the cavity as well as to higher output indicated by black arrows. Consequently, the quality factor *Q* decreases successively and an additional far-field lobe appears, pointing in the opposite direction compared to the initial far field for $n_p = 1.0$ in Fig. 5(b). This allows for a relative measurement of the intensities of the two far-field modes which promises more stable and reliable sensor performance, or alternatively to use one lobe to couple in and out, respectively.

To summarize, we have performed 3D FDTD wave simulations in order to investigate 3D mode structures and 3D far fields of wavelength-scale 3D optical microresonators that in view of the ongoing miniaturization of photonic devices will soon become of experimental relevance. In particular, we show that *Q* factors can be expected to be higher in 3D systems. While we find that the mode distribution looks similar inside the cavity for the 2D and 3D cases, the far fields can differ significantly, implying that 2D far-field simulations can be highly misleading.

Our results on 3D far fields embed those obtained for 2D microcavities by explicitly showing how the emission pattern looks perpendicular to the resonator plane. Besides a mere diffractive spreading due to the finite height of the lateral area, we predict a type of far field where the directions of maximum far-field emission are not in the resonator plane, but inclined to it, forming an angle of almost 60◦. It arises for modes with a slightly increased intensity in the cavity center as compared to whispering-gallery-type modes. This suggests that the far-field properties can be customized by adjusting the mode structure, e.g., via the 3D resonator geometry.

The unique emission characteristics of the 3D microresonators can potentially be exploited in sensors and highly integrated optical microsensors [\[33\]](#page-5-0). We discuss a sensor that can detect tiny changes in the environment via characteristic far-field signal. Furthermore, we plan to utilize integrated optical microsystems to optically address individual microdisk resonators. The 3D simulations presented here enable the optimization of the coupling efficiencies. Coherently coupled microcavities can be fabricated by carefully aligning arrays of individual resonators, which is feasible using lithographic fabrication technologies. This will help to further enhance the sensitivity of the microdisk sensors.

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APPENDIX: ORIGIN OF INCREASED QUALITY FACTORS IN FLAT 2D VS 3D CAVITIES

We consider a cylinder of height *h*, radius *R*, and refractive index *n* with circular cross section in the *x*-*y* plane, and the cylinder axis perpendicular to this plane in the *z* direction. We will restrict our considerations to the case of TM polarization (generalization to the TE case is straightforward) where the electric field $E(r)$ is parallel to the *z* axis. The magnetic field lies in the *x*-*y* (or cavity) plane and is transverse both to the *z* axis and the field propagation direction. The electric field **E**(**r**) is then fully described by its *z* component $E_z(\mathbf{r})$ that has to fulfill the Helmholtz (wave) equation

$$
[\nabla^2 + n(\mathbf{r})^2 k^2]E_z(\mathbf{r}) = 0,
$$
 (A1)

where $k = \omega/c$ is the vacuum wave number, ω the angular frequency, and *c* the speed of light.

In the *2D case*, we make use of the rotational symmetry of our problem, apply ∇^2 in cylindrical coordinates r, ϕ, z , and perform a separation of variables. Assuming a *φ* dependence of $e^{im\phi}$ and a *z* dependence $e^{ik_z z}$ of $E_z(\mathbf{r})$, its radial part $E(r)$ has to fulfill the equation

$$
\left[\frac{d^2}{dr^2} + \frac{1}{r}\frac{d}{dr}\right]E(r) + V_{\text{eff}}(r)E(r) = 0 \tag{A2}
$$

with the effective potential (assuming $k_z = 0$ for simplicity)

$$
V_{\text{eff}}^{2\text{D}}(r) = n^2 k^2 - \frac{m^2}{r^2},\tag{A3}
$$

where *m* is the angular momentum quantum number that, via the conservation of angular momentum, contributes to the effective potential barrier.

In the *3D case*, although the use of cylindrical coordinates seems suggestive, we rather use spherical coordinates *r,φ,θ* where the polar angle θ runs within a small range at the cavity boundaries in the case of the flat resonator geometries we are interested in here. We assume again the separation of variables, now with the radial part $U(r)$ of $E_z(\mathbf{r})$ deduced from

the Helmholtz equation in spherical coordinates, to be of the form

$$
\left[\frac{d^2}{dr^2} + \frac{2}{r}\frac{d}{dr}\right]U(r) + \left(n^2k^2 - \frac{l(l+1)}{r^2}\right)U(r) = 0.
$$
 (A4)

The azimuthal (ϕ) and polar (θ) parts are given by the spherical harmonics $Y_{l,m}(\theta, \phi)$. Since we wish to consider flat disks, we are interested in those $Y_{l,m}(\theta, \phi)$ that possess nodal lines only along the ϕ , but not along the θ direction [i.e., regions of the same sign of $Y_{l,m}(\theta,\phi)$ form sectors, divided by meridians, on the sphere; and these spherical harmonics are referred to as sectoral]. As a consequence, the relation $l = |m|$ holds in this case, a crucial property that allows one to directly compare to the 2D case, as we will see below.

In order to find the analogy to Bessel's differential equation as in the 2D case [cf. Eq. $(A2)$], we substitute further $x = nkr$ and $U(x) = U(x)/\sqrt{x}$, and find

$$
\left[\frac{d^2}{dx^2} + \frac{1}{x}\frac{d}{dx}\right]\tilde{U}(x) + \left(1 - \frac{(l+1/2)^2}{x^2}\right)\tilde{U}(x) = 0.
$$
 (A5)

This yields, in analogy to Eqs. $(A2)$ and $(A3)$, the effective potential in the three-dimensional case as

$$
V_{\text{eff}}^{3D}(r) = n^2 k^2 - \frac{(l+1/2)^2}{r^2}.
$$
 (A6)

The crucial difference is the angular momentum barrier that is proportional to m^2 in the 2D case, but proportional

to $(l + 1/2)^2$ in 3D (instead of l^2 when adopting the 2D situation). Thinking in terms of the effective potential, it will be deeper in 3D (note the minus sign in front of the angular momentum barrier term), thereby directly explaining the better confinement of resonances that corresponds to longer lifetimes and provides one part of the analytical proof of the higher *Q* factors seen in the 3D case.

We finish by pointing out the relation between the spherical and the ordinary Bessel functions that reflects precisely the difference between the effective potentials in 3D and 2D, respectively. In the 3D situations, the complete solutions of the radial part $U(x)$ are given by the spherical Bessel functions j_l which are related to the ordinary Bessel functions J_l by

$$
j_l(x) = \sqrt{\frac{2\pi}{x}} J_{l+1/2}(x).
$$
 (A7)

We notice that the spherical Bessel function j_l is related to the ordinary Bessel function, with the order increased by one half, $J_{l+1/2}$, corresponding to the effective potential argument outlined above. Moreover, $J_{l+1/2}$ is divided by the square root of *x* (normalized radial distance), which already causes a faster falloff in the 3D case and provides the second part of the analytical explanation for the higher *Q* factors seen in the 3D case. This enhances the effect that Bessel functions of higher order show a faster falloff as a function of the argument. Altogether, the radial component $U(r)$ in 3D (in the *x*-*y* plane of the resonator) of the electric field $E_z(\mathbf{r})$ decays faster than its 2D analog $E(r)$.

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