Extracting work from quantum states of radiation

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Quantum optomechanics opens a possibility to mediate a physical connection between quantum optics and classical thermodynamics. We propose and theoretically analyze a one-way chain starting from various quantum states of radiation. In the chain, the radiation state is first ideally swapped to a sufficiently large mechanical oscillator (membrane). Then the membrane mechanically pushes a classical almost massless piston, which is pressing a gas in a small container. As a result, we observe strongly nonlinear and nonmonotonic transfer of the energy stored in classical and quantum uncertainty of radiation to mechanical work. The amount of work and even its sign depend strongly on the uncertainty of the radiation state. Our theoretical prediction would stimulate an experimental proposal for such optomechanical connection to thermodynamics.

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I. INTRODUCTION

The recent development of quantum optomechanics has stimulated many proposals and experiments testing the possibility of mechanical systems to mediate physical connections between physical platforms [1–7]. These physical connections bring together different physics and translate many physical notions beyond their mathematical analogies. Already from university studies, one would say that the most natural connection of classical mechanics is to classical thermodynamics [8]. On the other hand, quantum optics is already directly connected to quantum mechanics by a pressure of light [9,10] in many recent experimental achievements [11–18]. Therefore, it is natural to think about the physical connection between quantum optics and classical thermodynamics mediated by mechanical systems. Theoretical thoughts about it and planning of future experiments have been stimulated by the recent fast progress in quantum optomechanics and many discussions about quantum thermodynamics in this context [19-27].

In contrast to many of these discussions, we focus on the basic but important quantum-to-classical transition between quantum modes of light, mechanical oscillators at that border, and the fully classical system of the piston manipulating thermodynamic states of gas in the closed container [8]. It is a kind of quantum-classical transition typical for the detectors registering light at the quantum level. The mediating mechanical oscillator feels a position projection from the classical system and environment [28]. The quantum quadrature of light is therefore connected to the mechanical position and, furthermore, to the position of a classical piston. Altogether, it is a theoretical limit of a one-way von Neumann chain, where one part drives the next one, but not vice versa. At this point, we simply ignore all the backactions, which could be the subject of further studies. Our first goal is to describe how the inherent quantum uncertainty of the states of light translates into a classically uncertain position of the classical piston and classical average work on the ensemble of independently repeated experiments. It is a gedanken experiment going towards more complicated and realistic considerations at this mechanical border between quantum and classical.

At the beginning of the challenging experiment, both classical and quantum uncertainty of virtual position and momentum quadrature variables of an electric field of light or microwaves have to be translated to the real uncertainty of the mechanical position and momentum of the mechanical system. Quantum optomechanics has already experimentally tested the dedicated preparation and precise estimation of mechanical position with small uncertainty approaching quantum limits [29–37]. Recently, quantum entanglement between radiation and mechanical systems and also quantum squeezing of mechanical uncertainty have been demonstrated [14,16,17]. These experiments can be extended to prepare various quantum states of the mechanical system [38-45]. To reach a high quality of transfer for any state of light to mechanical systems, universal interfaces have been proposed as well [46-49]. The remaining main experimental challenge, therefore, is the direct coupling of the mechanical system at the quantum level to a classical thermodynamic system. A direct coupling between mechanical oscillators has been investigated in [50-53]. Alternatively, mediated coupling between two mechanical systems, possibly representing the mechanical oscillator (or cantilever) and mechanical piston in the future, has been proposed [54-60]. Currently, progress in the research of levitating mechanical oscillators opens the door to such types of mechanical couplings [37,61–66].

All of these points fully legitimate theoretical thoughts of a future experiment testing the simplest physical connection between quantum optics and classical thermodynamics. In this way, different forms of energy of light represented by thermal, coherent, squeezed, and Fock states of light [67] can be *physically* translated to thermodynamic work performed by a real device. It is a novelty for quantum optics because classical and nonclassical states of light can be seen from a perspective of classical thermodynamics through a specific physical chain. The simplest classical version of this chain (an interconnection between mechanics and thermodynamics) can be considered in terms of a mechanical cantilever whose single variable (mechanical position or momentum) drives a piston compressing an ideal gas in a solid container during a standard isothermal process. This process of energy transformation interestingly has a nonlinear response, although the optomechanical coupling between the light and mechanical oscillator remains typically linear.

Considering an ensemble of such independent chains, the classical or quantum uncertainty of light translates to an uncertainty of the piston position and, finally, to an uncertainty of work in the classical isothermal process. In principle, this uncertainty can be present only on the ensemble, and hence any individual chain in the ensemble does not principally fluctuate in time [68]. The piston-gas container can therefore follow the simplest isothermal process in standard thermodynamics [8]. On the ensemble, the position of the piston and accessible work on the testing body, however, have to be fully characterized by a statistical distribution over the ensemble. Classical average work on the ensemble of the repeated experiments can therefore be seen as an operational thermodynamic characterization of the uncertainty present in the light. Beyond this basic level, analysis of the piston fluctuations driven by an environment can be added. In this sense, the piston can be understood as an overdamped particle under a Brownian motion [68]. This can be viewed as an equivalent of the noise in a detector, which can affect the results of the detection process. It is an important test of stability of this chain under the fluctuations in time at the border of thermodynamics.

In this paper, we describe a gedanken but fully physical chain going from quantum optics to classical equilibrium thermodynamics. We investigate a position uncertainty of the piston and, consequently, average work from the isothermal process for several quadrature distributions of light. Our results show that the amount and even the sign of work obtained from the energy transfer through the chain depends nontrivially and nonmonotonically on the uncertainty of the radiation state. That is, contrary to what one might expect, the increase of uncertainty can cause either an increase or decrease of the average output work. In Sec. II, we describe the components of our physical model of the chain. Section III describes the approach of the piston subsystem to the thermal equilibrium. Section IV describes the ensemble-averaged work as the partial outcome of the light to piston+gas energy transfer through the chain. Direct comparison for thermal, Fock, coherent, squeezed, and phase-randomized states of light is performed. The coherent states are the candidates for the most efficient average-energy-to-work transfer.

II. DESCRIPTION OF THE MODEL

Initially, we assume that the quantum state of light mode is *ideally* transferred onto the state of the mechanical membrane. This fact causes the virtual absence of the light mode in



FIG. 1. Schematic of the physical model of the chain. Initially, the quantum state of the light is *ideally* transferred to the state of the mechanical membrane. This assumption causes the virtual absence of the light in our chain. The membrane position (together with its uncertainty) is transferred to the classical piston sealing the container with a classical ideal gas.

our model and allows us to keep our toy model consisting of only three components, namely, the membrane subsystem, where the quantum projection to mechanical position happens, described quantum mechanically, the piston subsystem with stochastic description, and the classical nonfluctuating gas subsystem described in the thermodynamic language. Our model therefore describes a one-way transfer of energy from the different quantum states of the membrane through the classically (and possibly stochastically) evolving piston, into the compression of the ideal gas stored in a container enclosed by the low-mass piston (Fig. 1).

A. The membrane

We describe the quantum part of the system, i.e., the membrane, by the quantum mechanical Hamiltonian of a harmonic oscillator,

$$\hat{H}_{M} = \frac{\hat{P}_{M}^{2}}{2m_{M}} + \frac{m_{M}\omega^{2}}{2}\hat{X}_{M}^{2},$$
(1)

where X_M is measured from the membrane potential minimum. The quantum nature of X_M can be omitted in the following, since we consider position distribution after perfect quantum projection of the membrane state by its environment, destroying any information about P_M . Therefore, we use only its position distribution. However, X_M does represent the variable with a position uncertainty. We assume the membrane to be coupled to a piston (described below) by the position-position type of coupling, typical for coupled harmonic oscillators. We consider this linear coupling to ensure that it cannot itself generate any nonlinear effects on the piston position. This type of coupling can be used for both quantum mechanical and classical oscillators. It reads

$$H_{MP} = \kappa X_M X. \tag{2}$$

This interaction Hamiltonian leads to the equation of motion for the piston position operator X which contains the linear force $-\kappa X_M$ acting on the piston.

The membrane is a conceptually important part of our gedanken experiment. It mediates the quantum-to-classical transition from the quantum state of light to the classical position distribution of the piston. The membrane undergoes a collapse in the position pointer basis on a time scale smaller than any other time scale assumed in the chain. After this projection, the membrane description is effectively classical. The direct transfer of quantum states of light onto the piston would be difficult to describe.

B. The piston

As the next level of our chain, we assume that the membrane acts on a very light microscopic piston. The one-way chain structure of our model implies that the backaction of the piston on the membrane can be neglected. In other words, we assume that the mass of the piston is much smaller compared to the membrane mass, $m_P \ll m_M$. This is the standard physical limit in which the large membrane drives the smaller piston. The piston represents a moving boundary used to compress a certain amount of a classical ideal gas in a cylinder. To test the basic robustness of the chain under fluctuations of the piston in time, we introduce stochastic Brownian motion of the piston caused by the piston environment. We assume that the dynamics of the piston position X is described by the classical overdamped Langevin equation [69]

$$\gamma \dot{X} = F(X,t) + \sqrt{2\gamma k_B T} \,\xi(t). \tag{3}$$

Thus, we model the fluctuations of the piston as if it would be a classical overdamped Brownian particle immersed in a heat bath of temperature *T*. In Eq. (3), γ stands for the damping coefficient, k_B is the Boltzmann constant, F(X,t) is the nonfluctuating, but possibly uncertain, force acting on the piston, and $\xi(t)$ is the Gaussian white noise which accounts for the thermal fluctuations of the surroundings $[\langle \xi(t) \rangle = 0,$ $\langle \xi(t)\xi(t') \rangle = \delta(t - t')]$. The force F(X,t) is specified below in Eq. (5). The force uncertainty arises from the uncertainty of the mechanical system prepared by light. Such an approximate description of the dynamics is appropriate on the time scale $t \gg m_P/\gamma$, where m_P is the mass of the piston.

C. The ideal gas

The third part of our model is the cylinder (container sealed by the piston) containing a certain amount (N particles) of the classical ideal gas. The walls of the cylinder are kept at the constant temperature T. Throughout the paper, we assume the particle number N to be sufficiently low and the heat bath temperature T high. Under these assumptions, the state of the gas is well described by the equation of state $PV = Nk_BT$, with P, V = SX being the pressure and volume of the gas, respectively, with S the piston cross section and X the piston position with respect to the bottom of the container. Thus, this equation can be readily recast into the form

$$PS = \frac{Nk_BT}{X}.$$
(4)

The left-hand side of Eq. (4) represents the pressure force that the gas exerts on the piston, while the right-hand side, strongly nonlinear in piston position X, defines the piston position dependence of that force. Further, we assume that the medium surrounding the gas container exerts a pressure force, $-F_0$, on the piston as well, allowing for the establishment of mechanical equilibrium of the piston.

III. EVOLUTION OF THE PISTON TOWARDS THERMAL EQUILIBRIUM

In this section, we describe the piston dynamics and characterize its equilibrium position distribution. To begin with, we specify the form of the force F(X,t) in Eq. (3),

$$F(X,t) = -\kappa X_M - F_0 + \frac{Nk_BT}{X}.$$
(5)

The first right-hand side (RHS) term comes from the Hamiltonian (2). We assume throughout the paper that X_M changes at such time scale that it can be considered *constant* on the time scale of equilibration of the piston. Thus, we can consider an ensemble of equilibrating pistons whereas, for each member of this ensemble, the value of X_M on the RHS of Eq. (5) is constant and sampled from some probability density function (PDF). In other words, X_M is an *uncertain* (random) but not fluctuating variable, throughout the paper.

The second and third terms in Eq. (5) come from Eq. (4) and the discussion below it. These terms describe the possibility that the gas equilibrates mechanically with its surroundings. The Langevin equation for the piston position, given by Eq. (3), using Eq. (5) as the RHS, gets its final form,

$$\gamma \dot{X} = -\kappa X_M - F_0 + \frac{Nk_BT}{X} + \sqrt{2\gamma k_BT} \,\xi(t). \tag{6}$$

Equation (6) is a stochastic differential equation describing the time dependence of the stochastic process X(t). It simultaneously takes into account both the uncertainty of the membrane and the fluctuations of the piston. This equation is equivalent to the Fokker-Planck (FP) equation for the PDF ρ of the piston position, X(t), $\rho \equiv \rho(X,t)$. The FP equation equivalent to Eq. (6) has the form

$$\frac{\partial \rho}{\partial t} = -\frac{1}{\gamma} \frac{\partial}{\partial X} \left[\left(-\kappa X_M - F_0 + \frac{Nk_B T}{X} \right) \rho \right] + \frac{k_B T}{\gamma} \frac{\partial^2 \rho}{\partial X^2}.$$
(7)

The deterministic forces on the RHS of Eq. (6) acting on the piston can be derived from the potential

$$V(X) = (\kappa X_M + F_0)X - Nk_B T \ln (X/L),$$
 (8)

where X_M represents the membrane position and L is the integration constant making the argument of the $\ln(x)$ function dimensionless. We choose the value of L such that it corresponds to the position of the potential minimum for $\kappa = 0$, defining the length unit as

$$L \equiv Nk_B T / F_0. \tag{9}$$

With this definition, we can introduce dimensionless variable $x \equiv X/L$ and rewrite Eq. (8) into the form

$$V(x) = Nk_B T(\alpha x - \ln x), \quad \alpha \equiv 1 + \frac{\kappa X_M}{F_0}.$$
 (10)

It is not possible to solve for time-dependent $\rho(X,t)$ from Eq. (7) analytically, but one can obtain the equilibrium position PDF of the piston $\rho(X) \equiv \lim_{t\to\infty} \rho(X,t)$ as the equilibrium Gibbs distribution,

$$\rho(X) = \frac{1}{Z} \exp\left[-\frac{V(X)}{k_B T}\right],$$
$$Z \equiv \int_{-\infty}^{\infty} \exp\left[-\frac{V(X)}{k_B T}\right] dX.$$
(11)

Note that the equilibrium solution appears as the result of the diffusion process. If the diffusion can be neglected, we obtain the case of the piston drifting to minimum of the potential under an external force with uncertainty of the mechanical membrane. We will go back to this simplification later.

A. The membrane without uncertainty

In this section, we consider X_M to be constant and derive the equilibrium PDF for the position of the piston in two cases. The first one is comprised of the membrane coupled to the piston, i.e., $\kappa \neq 0$, while the second one describes the situation with the two subsystems uncoupled, $\kappa = 0$.

The nonlinear potential V(x), given by Eq. (10), allows for the piston equilibration only if it possesses a local minimum with respect to x. This is equivalent to the constraint on the value of the membrane position, yielding $\alpha > 0$. Taking the potential for $\alpha = 1$ as a reference, we can deduce the following. For $X_M > 0$ ($\alpha > 1$), the membrane compresses the piston (the potential is tighter). If $-F_0/\kappa < X_M < 0$ ($0 < \alpha < 1$), the piston is expanded (the potential is more open). In the case $X_M \leq -F_0/\kappa$ ($\alpha \leq 0$), the potential has no local minimum, and thus no equilibrium piston position distribution $\rho(x)$ exists; cf. Fig. 2.



FIG. 2. An example of the behavior of the potential $V(x)/Nk_BT = \alpha x - \ln x$, for $\alpha = \{-1,0,0.5,1,1.5\}$. For $\alpha \leq 0$, no local minimum exists. For increasing α , the potential is tighter and the position of its minimum shifts towards 0.

Further, we always assume that the equilibrium PDF, given by Eq. (11), for the piston position exists ($\alpha > 0$). In the dimensionless variables, it is given by the gamma distribution,

$$\rho(x) = \frac{1}{Z} x^N \exp[-\alpha N x], \quad x \ge 0, \tag{12}$$

$$Z = \frac{\Gamma(N+1)}{(\alpha N)^{(N+1)}}.$$
 (13)

The mean \overline{x} and the variance $\sigma^2 = \overline{x^2} - \overline{x}^2$ of this distribution are given by

$$\overline{x} = \frac{N+1}{\alpha N}, \quad \sigma^2 = \frac{N+1}{(\alpha N)^2}.$$
(14)

The description of the time sequence of one experimental run can be the following. Initially, the piston is coupled to the membrane, $\kappa \neq 0$, which is determining the value of $\alpha > 0$, in the potential (10) during the whole equilibration process. After the waiting time long enough for the equilibration, the piston approaches the initial equilibrium position distribution, denoted $\rho(x_i)$, where the subscript "*i*" stands for "initial." It is defined by the initial set of parameters N and α . From this initial distribution, we perform a sufficiently slow (quasistatic) and isothermal transformation of the piston state into the "final" state, labeled by the subscript "f," of the piston position distribution, denoted $\rho(x_f)$, by slowly decreasing $\kappa \to 0$, corresponding to $\alpha \to 1$. Thus, changing the value of κ (α) allows us to tighten or open the potential and therefore compress or expand the piston with respect to the reference state $\alpha = 1$. The position PDF, $\rho(x)$, is illustrated in Fig. 3 for different values of α .

Notice that for high values of *N*, higher statistical moments of $\rho(x)$ tend to be negligible, as evident from Fig. 3. In the limit $N \gg 1$, the variances vanish as well [cf. Eq. (14)] and the distributions approach

$$\lim_{N \to \infty} \rho(x_i) = \delta(x_i - 1/\alpha),$$

$$\lim_{N \to \infty} \rho(x_f) = \delta(x_f - 1), \tag{15}$$



FIG. 3. The equilibrium position distribution, given by Eq. (12), for $\alpha = \{0.5, 1, 1.5\}$ and N = 500. For $\alpha = 1$, the state is equivalent to the final $\rho(x_f)$ distribution. Note that due to the high value of N, the expected distribution skewness is not well distinguishable.

where $\delta(x)$ represents the delta function. The piston then always reaches the minimum of the potential without any fluctuations. The same result can be obtained if the diffusion in Eq. (7) can be neglected. These deterministic results are valid in the thermodynamic limit and describe the standard textbook situation of the piston with a precise, nonfluctuating position. The limit $N \rightarrow \infty$ is rather straightforward in the dimensionless coordinates. In physical units, all three quantities N, κX_M , F_0 become large and the latter two are proportional to N.

Using Eq. (14), we can determine, as well, the value of the mechanical signal-to-noise ratio (SNR) of the state $\rho(x_i)$ as

$$SNR = \frac{\overline{x}_i}{\sigma_i} = \sqrt{N+1},$$
 (16)

which is independent of α for fixed *N*. The interpretation of this result is such that for fixed *N*, the change (increase or decrease) in the mean value \overline{x}_i is always accompanied by the same change (increase or decrease) in the standard deviation σ_i .

B. The membrane with uncertainty

In this section, we assume X_M to take random values sampled from its PDF, corresponding to the fluctuations of α in Eqs. (10)–(14). These α fluctuations have to have the time scale separated with respect to the piston equilibration time scale, in the sense discussed below Eq. (5). Hence, the potential felt by the piston during each equilibration, given by Eq. (10), remains constant, as well as the form of the piston position distribution $\rho(x_i)$, given by Eq. (12). Thus, the final form of the PDF $\rho(x_i)$ for the initial piston position will be the result of the averaging over the random values of α ,

$$\rho(x_i) = \frac{\int_0^\infty p(\alpha) Z_i^{-1} x_i^N \exp[-\alpha N x_i] d\alpha}{\int_0^\infty p(\alpha) d\alpha}.$$
 (17)

The presence of the denominator in Eq. (17) ensures the correct normalization of the $\rho(x_i)$. This factor reflects the cutoff (neglection) of $p(\alpha)$ for $\alpha \leq 0$ because for these values no stationary piston state exists. It is because the piston position can be unstable and therefore we have the probability

$$p_s \equiv \int_0^\infty p(\alpha) d\alpha \tag{18}$$

of a successful experimental run less than unity. It is common for many conditional experiments with unstable systems. We can rectify the membrane position to be sure that the equilibrium piston position will exist. All results from now on will therefore be conditioned by such rectifier. Note that the rectification and subsequently the success probability depends on F_0 . It can be optimized to reach an optimal regime of the transfer from mechanical uncertainty to thermodynamic average work.

Now, we can proceed to discuss the specific choice of $p(\alpha)$ in Eq. (17). The most natural family of states of the membrane is the Gaussian states, characterized by the mean value X_0 and the variance $\overline{\epsilon}^2$. They characterize, e.g., the thermal as well as the coherently displaced squeezed ground



FIG. 4. The example of the probability distributions $\rho(x_i)$ and $\rho(x_f)$, N = 500, for different values of ϵ [cf. Eq. (19)] if Gaussian with $\alpha_0 = 1$ is assumed (thermal state). The success probabilities p_s , given by Eq. (18), are shown. We see that the increasing variance ϵ of $p(\alpha)$ distribution increases the variance of $\rho(x_i)$, positively skews the $\rho(x_i)$ distribution, and causes the shift of the mean value of $\rho(x_i)$ towards 0. As the integration in Eq. (17) suggests, the resulting $\rho(x_i)$ is a weighted sum of γ distributions with different parameter α . Distributions with small α have large mean value and variance creating fat tails of $\rho(x_i)$, whereas large α implies very narrow $p(\alpha)$ distributions with small mean values, causing the peaks of $\rho(x_i)$ moving to the origin.

states of the mechanical membrane. For the above-mentioned Gaussian state, we obtain from the original membrane position distribution $\rho(X_M)$ the induced $p(\alpha)$ distribution,

$$\rho(X_M) = \frac{1}{\sqrt{2\pi\epsilon}} \exp\left[-\frac{(X_M - X_0)^2}{2\epsilon^2}\right]$$

$$\Rightarrow p(\alpha) = \frac{1}{\sqrt{2\pi\epsilon}} \exp\left[-\frac{(\alpha - \alpha_0)^2}{2\epsilon^2}\right],$$

$$\epsilon = \frac{\kappa\overline{\epsilon}}{F_0}, \quad \alpha_0 = \left(1 + \frac{\kappa X_0}{F_0}\right). \quad (19)$$

Below, we will recognize two cases for $p(\alpha)$. For the membrane coherent state, ϵ is fixed to the standard position deviation of the mechanical ground state $\epsilon_0 = \sqrt{\hbar/(2m\omega)}$ and α_0 is a free parameter, representing the "coherent" shift of the mean value. In contrast, the thermal state is characterized by $\alpha_0 = 1$ kept constant and ϵ changed as a free parameter, reflecting the increase in fluctuations of the thermal state corresponding to $p(\alpha)$.

The effect of changing $\epsilon > 0$, keeping $\alpha_0 = 1$ (thermal state), can be seen in Fig. 4. The distribution $\rho(x_i)$, given by Eq. (17), is a weighted sum of the gamma distributions, given by Eq. (12), with $p(\alpha)$ as the weights. The shapes of the resulting $\rho(x_i)$ on Fig. 4 result from their composition of the type of functions seen in Fig. 3. The gamma distributions with small α_i sum up to the thick distribution tails, while large α_i create the positively skewed maxima closer to x = 0.

One may naively tend to expect that while the modes (maxima positions) of the distributions $\rho(x_i)$, given by Eq. (17), tend to decrease monotonically (Fig. 4), so do their mean values.



FIG. 5. The dependence of the mean value \overline{x}_i from Eq. (17), on the parameter ϵ , given by Eq. (19), for fixed $\alpha_0 = 1$ and N = 500.

Figure 5 shows that this is not the case. Dependent on the parameter ϵ , the mean value \overline{x}_i increases initially above $\overline{x}_i = 1$ (the mean value for the *final* distribution as well) and then falls back below this value. One may interpret such behavior as an increase or decrease of the average piston position with respect to the final position distribution and its \overline{x}_f . The behavior, nontrivial as well, of the standard deviation, σ_i , is plotted in Fig. 6. The SNR, given by Eq. (16), for the piston states (17), using different $p(\alpha)$ distributions of the type (19), are shown in Fig. 7.

It shows that for intuitive understanding of the piston mechanics, it is better to keep in mind that the thermal energy of the membrane is transformed into the shift of the piston distribution maximum. Simultaneously, the local convexity around the maximum increases as well. It is therefore not easy to predict how much average work can be obtained.

IV. WORK OF THE GAS AND PISTON

This section examines the thermodynamic consequences of the results of nonlinear stochastic mechanics, derived in



FIG. 6. The dependence of the standard deviation σ_i from Eq. (17), on the parameter ϵ , given by Eq. (19), for fixed $\alpha_0 = 1$ and N = 500.



FIG. 7. The mechanical SNR plotted for different states (17), compared to the result (16). The $p(\alpha)$ distributions correspond to the coherent and thermal states, given by Eq. (19), with different values of the parameter \overline{n} ; see Sec. IV C.

Sec. III, first in the limit of large N (with suppressed position fluctuations) and second with these fluctuations taken into account.

In the previous section, we have understood the mechanical motion of the piston with increasing uncertainty. Our main goal in this section is therefore to quantify the average work done by the gas and piston expanding from the positions distributed with $\rho(x_i)$ into the positions distributed with $\rho(x_f)$ during the reversible isothermal expansion of the piston enclosing the ideal gas of N particles and driven by the position of the membrane, X_M , distributed with $\rho(X_M)$, given by Eq. (19). We discuss examples of how this average work depends on the type of the $\rho(X_M)$ distribution and, hence, $p(\alpha)$ distribution; cf. Eq. (19). In this respect, we consider an ensemble of reversible expansion or compression processes of an ideal gas in contact with the heat reservoir of the temperature T (Fig. 1), where the particular realizations of the ensemble are characterized by different values of the membrane position X_M , and thus the parameter α determining the potential, given by Eq. (10). The ensemble average is taken over these α values. We point out that we do not take into account the work used to create the complete chain, i.e., the work necessary to map the state of the light onto the membrane and to establish the membrane-piston interaction. The reversibility condition can be satisfied by adiabatic switching off the piston coupling to the membrane, $\alpha \rightarrow 1$, in Eq. (12).

A. The thermodynamic limit

This section describes the results stemming from the limit of $N \gg 1$. This limit implies for the piston position distributions the form of Eq. (15), represented by the δ functions. Further, we distinguish two regimes: (i) without any uncertainty in X_M , with $\rho(X_M)$ being a δ function, and (ii) with possible uncertainty in X_M .

First, let us analyze the deterministic case, i.e., the membrane being characterized by a sharp value of X_M , and thus α , without any uncertainty. In such case, one can apply the results of macroscopic equilibrium thermodynamics describing the isothermal, reversible expansion (compression) of the ideal gas [8], yielding the mechanical work, with the ideal gas pressure, given by Eq. (4),

$$W \equiv -\int_{x_i}^{x_f} PS \, dx = -Nk_B T \ln \frac{x_f}{x_i},$$
$$w(\alpha) \equiv \frac{W}{Nk_B T} = -\ln\alpha, \quad \alpha = 1 + \frac{\kappa X_M}{F_0}.$$
 (20)

Equation (20) forms an important result of our thermodynamic analysis. It represents the (macroscopic) thermodynamic work done on the ideal gas, i.e., when *W* is positive, the positive amount of work is done by an external agent on the ideal gas. In the thermodynamic limit ($N \gg 1$), the work *W* has a sharp (deterministic) value for given x_f , x_i , α . The normalized work is $w(\alpha) = -\ln \alpha$.

The second case described in this section has logic similar to Sec. III B. In this case, each thermalization of the piston is realized in a different potential, given by Eq. (10), due to the uncertainty in the parameter α , the slope of the thermalization potential. Each member of the ensemble characterized by different value of α , given by Eq. (10), is realized with the probability $p(\alpha)$, given by Eq. (19). For any α -dependent physical quantity, we can observe its values only on this ensemble and represent such quantity by its mean value. This is the case for $w(\alpha)$, given by Eq. (20), as well, leading to

$$\overline{w} = -\overline{\ln \alpha} = -\int_{-\infty}^{\infty} \ln(\alpha)\overline{p}(\alpha)d\alpha,$$
$$\overline{p}(\alpha) \equiv \frac{\theta(\alpha)p(\alpha)}{\int_{-\infty}^{\infty} \theta(\alpha)p(\alpha)d\alpha},$$
(21)

where $\theta(\alpha)$ is the Heaviside step function ensuring the cutoff $\alpha > 0$ necessary for the successful thermalization. The denominator of $\overline{p}(\alpha)$ represents the probability of successful experiment, given by Eq. (18). The average work \bar{w} is therefore defined on a subensemble of successful experimental runs. Equation (21) yields the average work done by the piston during the isothermal reversible transition from $\lim_{N\to\infty} \rho(x_i)$, given by Eq. (17), to $\rho(x_f) = \delta(x_f - 1)$, given by Eq. (15). For each value of α from the ensemble, $w(\alpha)$ yields a certain value of the mechanical work, but these values are sampled randomly from the distribution $p(\alpha)$. Equation (21) is the functional relation $p(\alpha) \mapsto \overline{w}$, yielding \overline{w} for given $p(\alpha)$. Note that if the diffusion process for the piston can be neglected, we arrive at the same formula, given by Eq. (21), for the average work extractable from position distribution of the membrane in our physical chain.

In order to evaluate \overline{w} , given by Eq. (21), we have to restrict ourselves to numerical results. As an example of the distribution $p(\alpha)$, we take again the Gaussian family of the membrane states, given by Eq. (19).

B. The piston as a Brownian particle

This section describes the thermodynamic consequences for the work done in our scheme by the gas and fluctuating piston for the finite number of particles N. In this case, to correctly determine the average work, one has to naturally take into account the fluctuations of the piston position neglected in Sec. IV A, which we do in a standard manner [69]. The piston equilibrium state $\rho(x; \alpha)$, given by Eq. (12), is characterized by the mean potential energy $V(x; \alpha)$, given by Eq. (10), for the fixed parameter α ,

$$\overline{V}(\alpha) = \int_0^\infty V(x;\alpha)\rho(x;\alpha)dx,$$
$$\overline{v}(\alpha) \equiv \frac{\overline{V}(\alpha)}{Nk_BT},$$
(22)

in the overdamped regime assumed here. The infinitesimal dimensionless work, given by Eq. (20), done by the piston is the infinitesimal change of average energy for the infinitesimal change of the parameter α ,

$$\delta w \equiv \frac{\partial \overline{v}(\alpha)}{\partial \alpha} d\alpha \tag{23}$$

$$= \int_0^\infty \frac{\partial v(x;\alpha)}{\partial \alpha} \bigg|_\rho \rho(x;\alpha) dx d\alpha, \qquad (24)$$

where the last partial derivative $\partial/\partial \alpha$ is taken under constant piston distribution condition. The total work done by the piston during the transition $\rho(x_i) \rightarrow \rho(x_f)$ [see the discussion bellow Eq. (14)] is

$$w(\alpha) = \int_{\alpha}^{1} \delta w = -\frac{N+1}{N} \ln \alpha, \qquad (25)$$

yielding

$$\overline{w} = -\frac{N+1}{N}\overline{\ln\alpha} = -\frac{N+1}{N}\int_{-\infty}^{\infty}\ln(\alpha)\overline{p}(\alpha)d\alpha, \quad (26)$$

resembling the results (20) and (21) in the limit $N \gg 1$. The summand 1 in the nominator of (25) reflects the fact that the piston itself, treated microscopically as a Brownian particle, performs average work on its surroundings.

In the general case for \overline{w} , given by Eq. (21), i.e., the case when α is uncertain and distributed with $p(\alpha)$, the results in Figs. 8 and 9 describe the behavior of \overline{w} with high precision, even in the case of non-negligible piston fluctuations, e.g., for $N \approx 10^3$.

Equation (21) also implies that for the states of the membrane with similar $p(\alpha)$, namely its statistical moments, the value of the mean work \overline{w} "extractable" from $p(\alpha)$ is



FIG. 8. Numerically obtained value \overline{w} from Eq. (21). The independent parameter is $\epsilon = \kappa \overline{\epsilon} / F_0$, the standard deviation of the thermal state given by Eq. (19); its mean value $\alpha_0 = 1$ is fixed.



FIG. 9. Numerically obtained value \overline{w} from Eq. (21). The independent parameter is the mean value α_0 of the coherent state in Eq. (19). The different curves are parametrized by the values of variance $\epsilon = \overline{\epsilon}\kappa/F_0 = \{0, 1.5, 3\}$ of this state. The behavior of \overline{w} for $\alpha_0 \approx 1$ is determined by the ϵ dependence of \overline{w} shown in Fig. 8. Note the asymptotic behavior of all curves being the same, $\overline{w} \approx -\ln(\alpha_0)$.

also similar. This is the case, e.g., for the thermal state of the membrane and the Fock state of the membrane, when both states possess the same value of average energy. This fact is demonstrated in the next section for several possible states of the membrane.

C. Work performed by different membrane states

In this section, we discuss the average work performance \overline{w} of different mechanical membrane states. We examine the Gaussian family of states as an example, plus two representatives of non-Gaussian states. The reader may have intuition about the results already, stemming from Figs. 8 and 9. The coherent and thermal states used here are examples of the classical states of the mechanical membrane. Can the quantum mechanical coherence and nonclassicality of the membrane state play any role in the work performance? As an example of the nonclassical state, we examine the harmonic-oscillator eigenstate, the Fock state, the coherent-squeezed state, and the phase-randomized coherent state [67] as the distribution of the membrane positions. To make a fair comparison of the work performance, we parametrize all assumed states by the same mean number of photons \overline{n} they have. The mean photon number determines the average energy of the state, as well.

The distribution of the *coherent state* is of the form (19), with $\epsilon = 1$ and $\alpha_0 = 1 + 2\sqrt{n}$. The *thermal state* parameters are $\alpha_0 = 1$ and $\epsilon = \sqrt{1 + 2n}$. Although the mean energy of each state mentioned is the same, the way that these states sample the value of $w(\alpha) = -\ln(\alpha)$, given by Eq. (21), through distribution $p(\alpha)$ is different.

The coherent state can be typically envisaged like a peaked Gaussian distribution, $p(\alpha)$, with large mean value relative to its standard deviation. Thus, the coherent state samples the function $w(\alpha) = -\ln(\alpha)$ in a relatively narrow region of α values around α_0 ; cf. Eq. (19). In comparison, the thermal state represents a Gaussian state with the vanishing mean value. Hence, the thermal state samples the function $w(\alpha)$ in a very wide region of α . Because of the cutoff at $\alpha = 0$, $p(\alpha)$



FIG. 10. Numerically obtained value \overline{w} from Eq. (21) for the subensemble of the successful thermalizations. The independent parameter is the photon mean number \overline{n} . The coherent states, number states, and thermal states with the same \overline{n} , i.e., the same average energy, are used at each point.

samples $w(\alpha)$ in a region $\alpha < 1$, where the integral converges to a positive value, whereas in a region $\alpha > 1$, the resulting integral is strictly negative and possibly divergent. These two contributions add, and for a wide enough distribution $p(\alpha)$ the negative part dominates.

A similar situation appears in the case of the Fock state [67]. It has formally the same standard deviation as the thermal state, even though it is an oscillating function with increasing amplitude for an increasing magnitude of the argument, in contrast to the thermal state. Due to this increase, the contribution to the negative part of the integral (21) increases faster in magnitude compared to the thermal state. This effect is resulting in the set of the Fock-state data points located bellow the thermal state data points in Fig. 10.

Figure 11 presents the results for other possible membrane states, namely, the squeezed coherent state and phaserandomized coherent state [67]. The squeezed coherent state belongs to the family of the Gaussian states, given by Eq. (19), with $\epsilon = \exp(-r)$ and $\alpha_0 = 1 + 2\sqrt{n} - \sinh^2(r)$, where r



FIG. 11. Numerically obtained value \overline{w} from Eq. (21) for the subensemble of the successful thermalizations. The same variables as in Fig. 10 are shown for the same oscillator. The squeezing parameter r = 2 for the squeezed state and the phase distribution variance $\tau = \pi/4$.



FIG. 12. Numerically obtained value of the experiment success probability p_s from Eq. (18). The independent parameter is the photon mean number \overline{n} for the states used in Fig. 10.

is the squeezing parameter [67]. The expression for α_0 reflects the fact that squeezing is an active transformation changing the mean number \overline{n} of photons with the squeezing parameter r. This has to be taken into account when comparing different state types with the same \overline{n} . In our example, squeezing reduces fluctuations of position distribution, so one can therefore naively expect that they can produce more average work. We show the dependence of the average work \overline{w} on the mean number \overline{n} for the coherent-squeezed state with r = 2.

The last type of state to be compared is the phaserandomized coherent state, belonging to the family of non-Gaussian states [67]. In our example, we use the phaserandomized coherent state with Gaussian phase distribution, namely,

$$p(\alpha)d\alpha = \int_{-\infty}^{\infty} \frac{d\phi}{2\pi\tau} \exp\left(-\frac{\phi^2}{2\tau^2}\right) \\ \times \exp\left\{-\frac{\left[\alpha - (1 + 2\sqrt{n}\cos\phi)\right]^2}{2}\right\} d\alpha, \quad (27)$$

where τ^2 is the variance of the phase ϕ distribution. Phase randomization is broadening the position distribution of the coherent state; it is therefore important to check how sensitive the average work is to phase instability of the coherent state of the membrane. Figure 11 shows the phase-randomized coherent state with $\tau = \pi/4$.

For both squeezed and phase-randomized states, we note that the \overline{w} values, shown in Fig. 11, lie above the date for the coherent state. In the asymptotic regime $\overline{n} \gg 1$, the approximate value of the integral (21) for the coherent states is

$$\overline{w}_{\rm coh} \approx -\ln \alpha_0 = -\ln 2 - \frac{1}{2} \ln \overline{n}, \quad \overline{n} \gg 1,$$

placing the coherent state into the candidate position for the state with the most effective energy transfer through the assumed chain. If one is interested in the work done on the *whole* ensemble, it is necessary to multiply the subensemble work values, shown in Figs. 10 and 11, by the respective



FIG. 13. Numerically obtained value of the experiment success probability p_s from Eq. (18). The independent parameter is the photon mean number \overline{n} for the states used in Fig. 11.

success probabilities p_s , given by Eq. (18), plotted on Figs. 12 and 13. This favors the coherent states again.

Thus, within the limits of our scheme, the nonclassicality of the states does not seem to represent any considerable advantage with respect to the work performance. It is a very interesting and unexpected result, considering the complexity of the nonlinear way to obtain the average work from the position distribution.

V. CONCLUSIONS

We have presented a physical model of a von Neumann one-way chain consisting of the following parts: (i) The quantum state of radiation swapped to (ii) the quantum mechanical membrane (oscillator), linearly coupled to (iii) a one-dimensional piston sealing a certain number of (iv) classical ideal gas particles. The gas can be compressed or expanded as an effect of the membrane pressure exerted through the mutual coupling on the piston. This process is assumed to take place at constant temperature, due to the presence of a heat bath.

The mechanical effect of the membrane on the piston position distribution under the isothermal conditions is studied for different position distributions of the membrane. The result is comprehensively expressed by the formula (26) for rectified distribution of membrane position ensuring existence of the equilibrium state. It can be simply used to operationally determine achievable thermodynamic work corresponding to any position distribution of the membrane or any other mechanical object.

For an ensemble of the membrane positions, we determine the average work done by the gas and piston when the isothermal reversible process of switching off the membranepiston coupling is assumed. The average reversible work done by the gas isothermal transformation from the initial into the final states is compared for different membrane position distributions. Namely, the work is compared for some states from the Gaussian family of the membrane states, for its Fock states, and for the non-Gaussian phase-randomized coherent state. M. KOLÁŘ, A. RYABOV, AND R. FILIP

From our results, we conclude several facts. We observe a nontrivial, strongly nonlinear and nonmonotonic relationship between the quantum and classical uncertainty of light and average work. We observe a clear advantage of Gaussian coherent states of light over thermal states, squeezed states, or even highly nonclassical Fock states of light to transform their energy into average work. We confirm that for large energy of light, we asymptotically reach the classical limit. The coherent states are the candidates for the most efficient mean energy to work transfer among the states assumed in our work. As a goal of our future work, we plan to examine the effect of

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finite-time (irreversible) dynamics of the piston and hence the work distribution and irreversible-work losses.

All of these theoretical results are important for further, more realistic development of the physical interconnection between quantum optics, optomechanics, and classical thermodynamics.

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