

# Grating-coupled excitation of multiple surface plasmon-polariton waves

Muhammad Faryad\* and Akhlesh Lakhtakia

*Nanoengineered Metamaterials Group (NanoMM), Department of Engineering Science and Mechanics, Pennsylvania State University, University Park, Pennsylvania 16802-6812, USA*

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The excitation of multiple surface plasmon-polariton (SPP) waves of different linear polarization states and phase speeds by a surface-relief grating formed by a metal and a rugate filter, both of finite thickness, was studied theoretically, using rigorous coupled-wave analysis. The incident plane wave can be either  $p$  or  $s$  polarized. The excitation of SPP waves is indicated by the presence of those peaks in the plots of absorptance vs the incidence angle that are independent of the thickness of the rugate filter. The absorptance peaks representing the excitation of  $s$ -polarized SPP waves are narrower than those representing  $p$ -polarized SPP waves. Two incident plane waves propagating in different directions may excite the same SPP wave. A line source could excite several SPP waves simultaneously.

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## I. INTRODUCTION

Surface plasmon-polariton (SPP) waves are surface waves guided by a planar interface of a metal and a dielectric material. SPP waves find applications for sensing, imaging, and communication [1,2]. If the dielectric partnering material is isotropic and homogeneous, only one SPP wave—that too, of the  $p$ -polarization state—can be guided by the metal-dielectric interface at a given frequency [3,4]. If a periodic nonhomogeneity normal to the wave-guiding interface is introduced in the dielectric partnering material, multiple SPP waves with different polarization states, phase speeds, and spatial profiles can be guided by the metal-dielectric interface. This has recently been shown both theoretically [5–7] and experimentally [8–10]. In all of these studies, the dielectric partnering material is also locally orthorhombic.

Very recently, we have solved a canonical boundary-value problem [11] to show that multiple SPP waves can be guided even if the dielectric partnering material is isotropic—provided that material is also periodically nonhomogeneous normal to the interface. This is a very attractive result, because both partnering materials are isotropic and because the dielectric partnering material can be fabricated as a rugate filter [12–16].

The canonical boundary-value problem does not possess direct practical significance, because both partnering materials are assumed to be semi-infinite normal to the planar interface. Therefore, we set out to investigate the excitation of multiple SPP waves by the periodically corrugated interface of a metal and a rugate filter. This grating-coupled configuration [2, pp. 35–41] is popular, when the dielectric partnering material is homogeneous, because it allows the excitation of an SPP wave by a nonspecular Floquet harmonic. The interplay of the periodic nonhomogeneity of the dielectric partnering material and a periodically corrugated interface is phenomenologically rich [17,18], and should lead to the excitation of multiple SPP waves as different Floquet harmonics.

The relevant boundary-value problem was formulated using the rigorous coupled-wave analysis (RCWA) [19,20]. In this numerical technique, the constitutive parameters are expanded

in terms of Fourier series with known expansion coefficients, and the electromagnetic field phasors are expanded in terms of Floquet harmonics whose coefficients are determined by substitution in the frequency-domain Maxwell curl postulates. The accuracy of the solution is conventionally held to depend only on the number of Floquet harmonics actually used in the computations [21]. The RCWA has been used to solve for scattering by a variety of surface-relief gratings [20–23], generally with both partnering materials being homogeneous.

The theoretical formulation of the boundary-value problem is provided in Sec. II and the numerical results are discussed in Sec. III. Concluding remarks are presented in Sec. IV. An  $\exp(-i\omega t)$  time dependence is implicit, with  $\omega$  denoting the angular frequency. The free-space wave number, the free-space wavelength, and the intrinsic impedance of free space are denoted by  $k_0 = \omega\sqrt{\epsilon_0\mu_0}$ ,  $\lambda_0 = 2\pi/k_0$ , and  $\eta_0 = \sqrt{\mu_0/\epsilon_0}$ , respectively, with  $\mu_0$  and  $\epsilon_0$  being the permeability and permittivity of free space. Vectors are in boldface, column vectors are in boldface and enclosed within square brackets, and matrices are underlined twice and square-bracketed. The asterisk denotes the complex conjugate, the superscript  $T$  denotes the transpose, and the Cartesian unit vectors are identified as  $\hat{\mathbf{u}}_x$ ,  $\hat{\mathbf{u}}_y$ , and  $\hat{\mathbf{u}}_z$ . The real part of a complex number  $\zeta$  is denoted by  $\text{Re}(\zeta)$ .

## II. BOUNDARY-VALUE PROBLEM

### A. Description

Let us consider the boundary-value problem shown schematically in Fig. 1. The regions  $z < 0$  and  $z > d_3$  are vacuum, the region  $0 \leq z \leq d_1$  is occupied by the dielectric partnering material with relative permittivity  $\epsilon_d(z)$ , and the region  $d_2 \leq z \leq d_3$  by the metallic partnering material with spatially uniform relative permittivity  $\epsilon_m$ . The region  $d_1 < z < d_2$  contains a surface-relief grating of period  $L$  along the  $x$  axis. The relative permittivity  $\epsilon_g(x, z) = \epsilon_g(x \pm L, z)$  in this region is taken to be as

$$\epsilon_g(x, z) = \begin{cases} \epsilon_m - [\epsilon_m - \epsilon_d(z)]\mathcal{U}(d_2 - z - g(x)), & x \in (0, L_1), \\ \epsilon_d(z), & x \in (L_1, L), \end{cases} \quad (1)$$

\*faryad@psu.edu

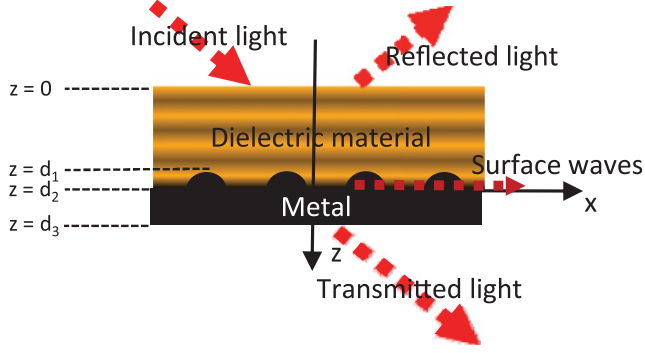


FIG. 1. (Color online) Schematic of the boundary-value problem solved using the RCWA.

for  $z \in (d_1, d_2)$ , with

$$g(x) = (d_2 - d_1) \sin\left(\frac{\pi x}{L_1}\right), \quad L_1 \in (0, L), \quad (2)$$

and

$$U(\zeta) = \begin{cases} 1, & \zeta \geq 0, \\ 0, & \zeta < 0. \end{cases} \quad (3)$$

The depth of the surface-relief grating defined by Eq. (2) is  $d_2 - d_1$ . This particular grating shape is chosen for the ease of fabrication; however, the theoretical formulation given in the remainder of this section is independent of the shape of the surface-relief grating.

In the vacuous half-space  $z \leq 0$ , let a plane wave propagating in the  $xz$  plane at an angle  $\theta$  to the  $z$  axis be incident on the structure. Hence, the incident, reflected, and transmitted

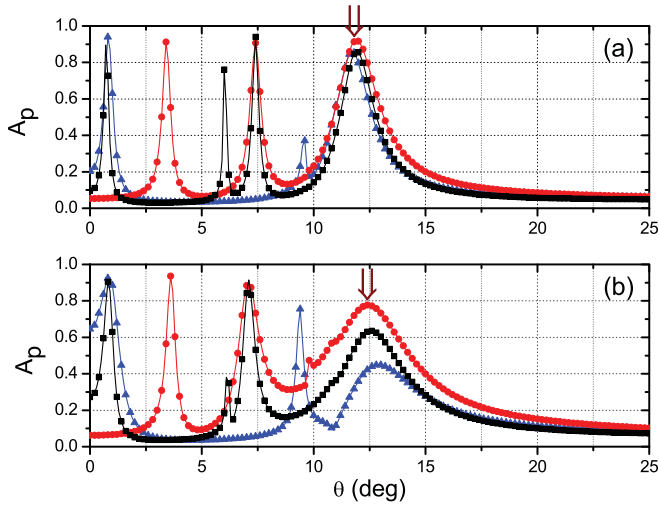


FIG. 2. (Color online) Absorptance  $A_p$  as a function of the incidence angle  $\theta$  when the surface-relief grating is defined by either (a) Eq. (53) or (b) Eq. (2). Black squares represent  $d_1 = 1500$  nm, red circles  $d_1 = 1000$  nm, and blue triangles  $d_1 = 800$  nm. The grating depth ( $d_2 - d_1 = 50$  nm) and the thickness of the metallic layer ( $d_3 - d_2 = 30$  nm) are the same for all cases. The vertical arrows identify SPP waves.

TABLE I. Relative wave numbers  $k_x^{(n)}/k_0$  of Floquet harmonics at the  $\theta$  value of the peak identified in Fig. 2 by a vertical arrow. A boldface entry signifies an SPP wave.

	$n = -2$	$n = -1$	$n = 0$	$n = 1$	$n = 2$
$\theta = 12.5^\circ$	-2.1645	-0.9740	0.2164	<b>1.4069</b>	2.5974

field phasors may be written in terms of Floquet harmonics as follows:

$$\mathbf{E}_{\text{inc}}(\mathbf{r}) = \sum_{n \in \mathbb{Z}} (\mathbf{s}_n a_s^{(n)} + \mathbf{p}_n^+ a_p^{(n)}) \exp[i(k_x^{(n)}x + k_z^{(n)}z)], \quad (4)$$

$$z \leq 0,$$

$$\mathbf{H}_{\text{inc}}(\mathbf{r}) = \eta_0^{-1} \sum_{n \in \mathbb{Z}} (\mathbf{p}_n^+ a_s^{(n)} - \mathbf{s}_n a_p^{(n)}) \exp[i(k_x^{(n)}x + k_z^{(n)}z)], \quad (5)$$

$$z \leq 0,$$

$$\mathbf{E}_{\text{ref}}(\mathbf{r}) = \sum_{n \in \mathbb{Z}} (\mathbf{s}_n r_s^{(n)} + \mathbf{p}_n^- r_p^{(n)}) \exp[i(k_x^{(n)}x - k_z^{(n)}z)], \quad (6)$$

$$z \leq 0,$$

$$\mathbf{H}_{\text{ref}}(\mathbf{r}) = \eta_0^{-1} \sum_{n \in \mathbb{Z}} (\mathbf{p}_n^- r_s^{(n)} - \mathbf{s}_n r_p^{(n)}) \exp[i(k_x^{(n)}x - k_z^{(n)}z)], \quad (7)$$

$$z \leq 0,$$

$$\mathbf{E}_{\text{tr}}(\mathbf{r}) = \sum_{n \in \mathbb{Z}} (\mathbf{s}_n t_s^{(n)} + \mathbf{p}_n^+ t t_p^{(n)}) \exp\{i[k_x^{(n)}x + k_z^{(n)}(z - d_3)]\}, \quad (8)$$

$$z \geq d_3,$$

$$\mathbf{H}_{\text{tr}}(\mathbf{r}) = \eta_0^{-1} \sum_{n \in \mathbb{Z}} (\mathbf{p}_n^+ t t_s^{(n)} - \mathbf{s}_n t_p^{(n)}) \times \exp\{i[k_x^{(n)}x + k_z^{(n)}(z - d_3)]\}, \quad z \geq d_3, \quad (9)$$

where  $k_x^{(n)} = k_0 \sin \theta + n\kappa_x$ ,  $\kappa_x = 2\pi/L$ , and

$$k_z^{(n)} = \begin{cases} +\sqrt{k_0^2 - (k_x^{(n)})^2}, & k_0^2 > (k_x^{(n)})^2 \\ +i\sqrt{(k_x^{(n)})^2 - k_0^2}, & k_0^2 < (k_x^{(n)})^2 \end{cases}. \quad (10)$$

The unit vectors

$$\mathbf{s}_n = \hat{\mathbf{u}}_y \quad (11)$$

and

$$p_n^\pm = \mp \frac{k_z^{(n)}}{k_0} \hat{\mathbf{u}}_x + \frac{k_x^{(n)}}{k_0} \hat{\mathbf{u}}_z \quad (12)$$

represent the  $s$ - and  $p$ -polarization states, respectively.

### B. Coupled ordinary differential equations

The relative permittivity in the region  $0 \leq z \leq d_3$  can be expanded as a Fourier series with respect to  $x$ , viz.,

$$\epsilon(x, z) = \sum_{n \in \mathbb{Z}} \epsilon^{(n)}(z) \exp(in\kappa_x x), \quad z \in [0, d_3], \quad (13)$$

where

$$\epsilon^{(0)}(z) = \begin{cases} \epsilon_d(z), & z \in [0, d_1], \\ \frac{1}{L} \int_0^L \epsilon_g(x, z) dx, & z \in (d_1, d_2), \\ \epsilon_m, & z \in [d_2, d_3], \end{cases} \quad (14)$$

and

$$\epsilon^{(n)}(z) = \begin{cases} \frac{1}{L} \int_0^L \epsilon_g(x, z) \exp(-in\kappa_x x) dx, & z \in [d_1, d_2] \\ 0, & \text{otherwise} \end{cases}; \quad \forall n \neq 0. \quad (15)$$

The field phasors may be written in the region  $0 \leq z \leq d_3$  in terms of Floquet harmonics as

$$\begin{aligned} \mathbf{E}(\mathbf{r}) &= \sum_{n \in \mathbb{Z}} \mathbf{E}^{(n)}(z) \exp(ik_x^{(n)} x), \\ \mathbf{H}(\mathbf{r}) &= \sum_{n \in \mathbb{Z}} \mathbf{H}^{(n)}(z) \exp(ik_x^{(n)} x), \quad z \in [0, d_3], \end{aligned} \quad (16)$$

with unknown functions  $\mathbf{E}^{(n)}(z) = E_x^{(n)}(z)\hat{\mathbf{u}}_x + E_y^{(n)}(z)\hat{\mathbf{u}}_y + E_z^{(n)}(z)\hat{\mathbf{u}}_z$  and  $\mathbf{H}^{(n)}(z) = H_x^{(n)}(z)\hat{\mathbf{u}}_x + H_y^{(n)}(z)\hat{\mathbf{u}}_y + H_z^{(n)}(z)\hat{\mathbf{u}}_z$ .

Substitution of Eqs. (13) and (16) in the frequency-domain Maxwell curl postulates results in a system of four ordinary differential equations and two algebraic equations as follows:

$$\frac{d}{dz} E_x^{(n)}(z) - ik_x^{(n)} E_z^{(n)}(z) = ik_0 \eta_0 H_y^{(n)}(z), \quad (17)$$

$$\frac{d}{dz} E_y^{(n)}(z) = -ik_0 \eta_0 H_x^{(n)}(z), \quad (18)$$

$$k_x^{(n)} E_y^{(n)}(z) = k_0 \eta_0 H_z^{(n)}(z), \quad (19)$$

$$\frac{d}{dz} H_x^{(n)}(z) - ik_x^{(n)} H_z^{(n)}(z) = -\frac{ik_0}{\eta_0} \sum_{m \in \mathbb{Z}} \epsilon^{(n-m)}(z) E_y^{(m)}(z), \quad (20)$$

$$\frac{d}{dz} H_y^{(n)}(z) = \frac{ik_0}{\eta_0} \sum_{m \in \mathbb{Z}} \epsilon^{(n-m)}(z) E_x^{(m)}(z), \quad (21)$$

$$k_x^{(n)} H_y^{(n)}(z) = -\frac{k_0}{\eta_0} \sum_{m \in \mathbb{Z}} \epsilon^{(n-m)}(z) E_z^{(m)}(z). \quad (22)$$

Equations (17)–(22) hold  $\forall z \in (0, d_3)$  and  $\forall n \in \mathbb{Z}$ . These equations can be recast into an infinite system of coupled first-order ordinary differential equations. This system can not be implemented on a digital computer. Therefore, we restrict  $|n| \leq N_t$  and then define the column  $(2N_t + 1)$  vectors

$$\begin{aligned} [\mathbf{X}_\sigma(z)] &= [X_\sigma^{(-N_t)}(z), X_\sigma^{(-N_t+1)}(z), \dots, X_\sigma^{(0)}(z), \dots, X_\sigma^{(N_t-1)}(z), \\ &\quad X_\sigma^{(N_t)}(z)]^T, \end{aligned} \quad (23)$$

for  $X \in \{E, H\}$  and  $\sigma \in \{x, y, z\}$ . Similarly, we define  $(2N_t + 1) \times (2N_t + 1)$ -matrices

$$[\underline{\mathbf{K}}_x] = \text{diag}[k_x^{(n)}], \quad [\underline{\epsilon}(z)] = [\epsilon^{(n-m)}(z)], \quad (24)$$

where  $\text{diag}[k_x^{(n)}]$  is a diagonal matrix.

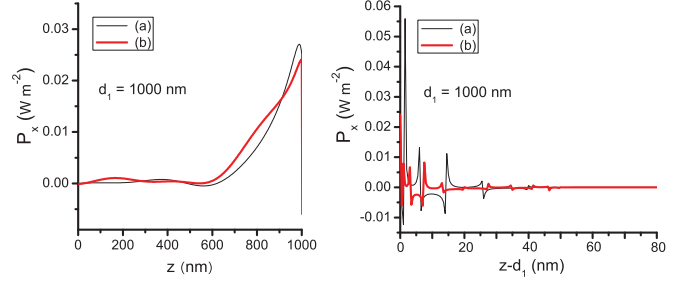


FIG. 3. (Color online) Variation of the  $x$  component of the time-averaged Poynting vector  $\mathbf{P}(x, z)$  along the  $z$  axis in the regions (left)  $0 < z < d_1$  and (right)  $d_1 < z < d_3$  at  $x = 0.75L$  for  $\theta = 12.5^\circ$ , when the surface-relief grating is defined by either (a) Eq. (53) or (b) Eq. (2) and the incident plane wave is  $p$  polarized. Other parameters are the same as for Fig. 2.

Equations (19) and (22) yield

$$[\mathbf{E}_z(z)] = -\frac{\eta_0}{k_0} [\underline{\epsilon}(z)]^{-1} \cdot [\underline{\mathbf{K}}_x] \cdot [\mathbf{H}_y(z)] \quad (25)$$

and

$$[\mathbf{H}_z(z)] = \frac{1}{\eta_0 k_0} [\underline{\mathbf{K}}_x] \cdot [\mathbf{E}_y(z)], \quad (26)$$

the use of which in Eqs. (17), (18), (20), and (21) eliminates  $E_z^{(n)}$  and  $H_z^{(n)} \forall n \in \mathbb{Z}$ , and gives the matrix ordinary differential equation

$$\frac{d}{dz} [\mathbf{f}(z)] = i [\underline{\mathbf{P}}(z)] \cdot [\mathbf{f}(z)], \quad z \in (0, d_3), \quad (27)$$

where the column vector  $[\mathbf{f}(z)]$  with  $4(2N_t + 1)$  components is defined as

$$[\mathbf{f}(z)] = [[\mathbf{E}_x(z)]^T, [\mathbf{E}_y(z)]^T, \eta_0 [\mathbf{H}_x(z)]^T, \eta_0 [\mathbf{H}_y(z)]^T]^T \quad (28)$$

and the  $4(2N_t + 1) \times 4(2N_t + 1)$ -matrix  $[\underline{\mathbf{P}}(z)]$  is given by

$$[\underline{\mathbf{P}}(z)] = \begin{bmatrix} [\underline{\mathbf{0}}] & [\underline{\mathbf{0}}] & [\underline{\mathbf{0}}] & [\underline{\mathbf{P}}_{14}(z)] \\ [\underline{\mathbf{0}}] & [\underline{\mathbf{0}}] & -k_0 [\underline{\mathbf{I}}] & [\underline{\mathbf{0}}] \\ [\underline{\mathbf{0}}] & [\underline{\mathbf{P}}_{32}(z)] & [\underline{\mathbf{0}}] & [\underline{\mathbf{0}}] \\ [\underline{\mathbf{P}}_{41}(z)] & [\underline{\mathbf{0}}] & [\underline{\mathbf{0}}] & [\underline{\mathbf{0}}] \end{bmatrix}. \quad (29)$$

Whereas  $[\underline{\mathbf{0}}]$  is the  $(2N_t + 1) \times (2N_t + 1)$  null matrix and  $[\underline{\mathbf{I}}]$  is the  $(2N_t + 1) \times (2N_t + 1)$  identity matrix, the three non-null submatrices on the right side of Eq. (29) are as follows:

$$[\underline{\mathbf{P}}_{14}(z)] = k_0 [\underline{\mathbf{I}}] - \frac{1}{k_0} [\underline{\mathbf{K}}_x] \cdot [\underline{\epsilon}(z)]^{-1} \cdot [\underline{\mathbf{K}}_x], \quad (30)$$

$$[\underline{\mathbf{P}}_{32}(z)] = \frac{1}{k_0} [\underline{\mathbf{K}}_x]^2 - k_0 [\underline{\epsilon}(z)], \quad (31)$$

$$[\underline{\mathbf{P}}_{41}(z)] = k_0 [\underline{\epsilon}(z)]. \quad (32)$$

### C. Solution algorithm

The column vectors  $[\mathbf{f}(0)]$  and  $[\mathbf{f}(d_3)]$  can be written using Eqs. (4)–(9) as

$$[\mathbf{f}(0)] = \begin{bmatrix} [\underline{\mathbf{Y}}_e^+] & [\underline{\mathbf{Y}}_e^-] \\ [\underline{\mathbf{Y}}_h^+] & [\underline{\mathbf{Y}}_h^-] \end{bmatrix} \cdot [\underline{\mathbf{A}}], \quad [\mathbf{f}(d_3)] = \begin{bmatrix} [\underline{\mathbf{Y}}_e^+] \\ [\underline{\mathbf{Y}}_h^+] \end{bmatrix} \cdot [\underline{\mathbf{T}}], \quad (33)$$

TABLE II. Relative wave numbers  $\kappa/k_0$  of possible SPP waves obtained by the solution of the canonical boundary-value problem [11] for  $\Omega = \lambda_0$ . Other parameters are provided in the beginning of Sec. III B. If  $\kappa$  represents an SPP wave propagating in the  $\hat{\mathbf{u}}_x$  direction,  $-\kappa$  represents an SPP wave propagating in the  $-\hat{\mathbf{u}}_x$  direction.

Polarization	Relative wave numbers				
$s$	$1.48639 + 0.00132i$	$1.7324 + 0.0014i^a$			
$p$	$1.36479 + 0.00169i$	$1.61782 + 0.00548i$	$1.87437 + 0.00998i$	$2.06995 + 0.01526i$	$2.21456 + 0.00246i$

<sup>a</sup>This solution had been missed when solutions for Fig. 1 of Ref. [11] were numerically searched.

where

$$[\mathbf{A}] = [a_s^{(-N_t)}, a_s^{(-N_t+1)}, \dots, a_s^{(0)}, \dots, a_s^{(N_t-1)}, a_s^{(N_t)}, a_p^{(-N_t)}, a_p^{(-N_t+1)}, \dots, a_p^{(0)}, \dots, a_p^{(N_t-1)}, a_p^{(N_t)}]^T, \quad (34)$$

$$[\mathbf{R}] = [r_s^{(-N_t)}, r_s^{(-N_t+1)}, \dots, r_s^{(0)}, \dots, r_s^{(N_t-1)}, r_s^{(N_t)}, r_p^{(-N_t)}, r_p^{(-N_t+1)}, \dots, r_p^{(0)}, \dots, r_p^{(N_t-1)}, r_p^{(N_t)}]^T, \quad (35)$$

$$[\mathbf{T}] = [t_s^{(-N_t)}, t_s^{(-N_t+1)}, \dots, t_s^{(0)}, \dots, t_s^{(N_t-1)}, t_s^{(N_t)}, t_p^{(-N_t)}, t_p^{(-N_t+1)}, \dots, t_p^{(0)}, \dots, t_p^{(N_t-1)}, t_p^{(N_t)}]^T, \quad (36)$$

and the nonzero entries of  $(4N_t + 2) \times (4N_t + 2)$ -matrices  $[Y_{e,h}^\pm]$  are as follows:

$$(Y_e^\pm)_{nm} = 1, \quad n = m + 2N_t + 1, \quad (37)$$

$$(Y_e^\pm)_{nm} = \mp \frac{k_z^{(n)}}{k_0}, \quad n = m - 2N_t - 1, \quad (38)$$

$$(Y_h^\pm)_{nm} = \mp \frac{k_z^{(n)}}{k_0}, \quad n = m \in [1, 2N_t + 1], \quad (39)$$

$$(Y_h^\pm)_{nm} = -1, \quad n = m \in [2N_t + 2, 4N_t + 2]. \quad (40)$$

In order to devise a stable algorithm [20,21,23,24], the region  $0 \leq z \leq d_1$  is divided into  $N_d$  slices and the region  $d_1 < z < d_2$  into  $N_g$  slices, but the region  $d_2 \leq z \leq d_3$  is kept as just one slice. So, there are  $N_d + N_g + 1$  slices and  $N_d + N_g + 2$  interfaces. In the  $j$ th slice,  $j \in [1, N_d + N_g + 1]$ , bounded by the planes  $z = z_{j-1}$  and  $z = z_j$ , we approximate

$$[\underline{P}(z)] = [\underline{P}]_j = \left[ \underline{P} \left( \frac{z_j + z_{j-1}}{2} \right) \right], \quad z \in (z_j, z_{j-1}), \quad (41)$$

so that Eq. (27) yields

$$[\mathbf{f}(z_{j-1})] = [\underline{G}]_j \cdot \exp\{-i\Delta_j[\underline{D}]_j\} \cdot [\underline{G}]_j^{-1} \cdot [\mathbf{f}(z_j)], \quad (42)$$

$$[\underline{Z}]_{j-1} = [\underline{G}]_j \cdot \left[ \exp\{-i\Delta_j[\underline{D}]_j^l\} \cdot [\underline{W}]_j^l \cdot \{[\underline{W}]_j^u\}^{-1} \cdot \exp\{i\Delta_j[\underline{D}]_j^u\} \right], \quad j \in [1, N_d + N_g + 1]. \quad (48)$$

From Eqs. (47) and (48), we find  $[\underline{Z}]_0$  in terms of  $[\underline{Z}]_{N_d+N_g+1}$ . After partitioning

$$[\underline{Z}]_0 = \begin{bmatrix} [\underline{Z}]_0^u \\ [\underline{Z}]_0^l \end{bmatrix}, \quad (49)$$

where  $\Delta_j = z_j - z_{j-1}$ ,  $[\underline{G}]_j$  is a square matrix comprising the eigenvectors of  $[\underline{P}]_j$  as its columns, and the diagonal matrix  $[\underline{D}]_j$  contains the eigenvalues of  $[\underline{P}]_j$  in the same order.

Let us define auxiliary column vectors  $[\mathbf{T}]_j$  and auxiliary transmission matrices  $[\underline{Z}]_j$  by the relation [23]

$$[\mathbf{f}(z_j)] = [\underline{Z}]_j \cdot [\mathbf{T}]_j, \quad j \in [0, N_d + N_g + 1], \quad (43)$$

where  $z_0 = 0$ ,

$$[\mathbf{T}]_{N_d+N_g+1} = [\mathbf{T}], \quad \text{and} \quad [\underline{Z}]_{N_d+N_g+1} = \begin{bmatrix} [\underline{Y}_e^+] \\ [\underline{Y}_h^+] \end{bmatrix}. \quad (44)$$

To find  $[\mathbf{T}]_j$  and  $[\underline{Z}]_j$  for  $j \in [0, N_d + N_g]$ , we substitute Eq. (43) in Eq. (42), which results in the relation

$$[\underline{Z}]_{j-1} \cdot [\mathbf{T}]_{j-1} = [\underline{G}]_j \cdot \begin{bmatrix} e^{-i\Delta_j[\underline{D}]_j^u} & 0 \\ 0 & e^{-i\Delta_j[\underline{D}]_j^l} \end{bmatrix} \cdot [\underline{G}]_j^{-1} \cdot [\underline{Z}]_j \cdot [\mathbf{T}]_j, \quad j \in [1, N_d + N_g + 1], \quad (45)$$

where  $[\underline{D}]_j^u$  and  $[\underline{D}]_j^l$  are the upper and lower diagonal submatrices of  $[\underline{D}]_j$ , respectively, when the eigenvalues are arranged in decreasing order of the imaginary part.

Since  $[\mathbf{T}]_j$  and  $[\underline{Z}]_j$  cannot be determined simultaneously from Eq. (45), let us define [23]

$$[\mathbf{T}]_{j-1} = \exp\{-i\Delta_j[\underline{D}]_j^u\} \cdot [\underline{W}]_j^u \cdot [\mathbf{T}]_j, \quad (46)$$

where the square matrix  $[\underline{W}]_j^u$  and its counterpart  $[\underline{W}]_j^l$  are defined via

$$\begin{bmatrix} [\underline{W}]_j^u \\ [\underline{W}]_j^l \end{bmatrix} = [\underline{G}]_j^{-1} \cdot [\underline{Z}]_j. \quad (47)$$

Substitution of Eq. (46) in Eq. (45) results in the relation

and using Eqs. (33) and (43),  $[\mathbf{R}]$  and  $[\mathbf{T}]_0$  are found as follows:

$$\begin{bmatrix} [\mathbf{T}]_0 \\ [\mathbf{R}] \end{bmatrix} = \begin{bmatrix} [\underline{Z}]_0^u & -[\underline{Y}_e^-] \\ [\underline{Z}]_0^l & -[\underline{Y}_h^-] \end{bmatrix}^{-1} \cdot \begin{bmatrix} [\underline{Y}_e^+] \\ [\underline{Y}_h^+] \end{bmatrix} \cdot [\mathbf{A}]. \quad (50)$$

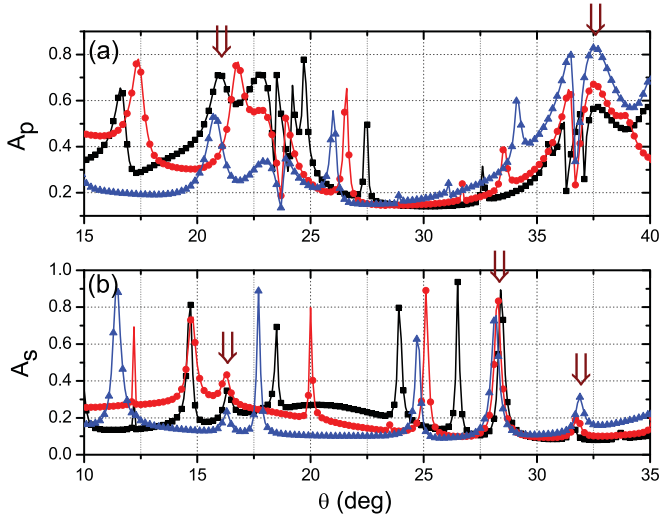


FIG. 4. (Color online) Absorptances (a)  $A_p$  and (b)  $A_s$  as functions of the incidence angle  $\theta$ , when the surface-relief grating is defined by Eq. (2) with  $L_1 = 0.5L$ ,  $\lambda_0 = 633$  nm,  $\Omega = \lambda_0$ , and  $L = \lambda_0$ . Black squares are for  $d_1 = 6\Omega$ , red circles for  $d_1 = 5\Omega$ , and blue triangles for  $d_1 = 4\Omega$ . The grating depth ( $d_2 - d_1 = 50$  nm) and the thickness of the metallic layer ( $d_3 - d_2 = 30$  nm) are the same for all plots. Each vertical arrow identifies an SPP wave.

Equation (50) is obtained by enforcing the usual boundary conditions across the plane  $z = 0$ . After  $[\mathbf{T}]_0$  is known,  $[\mathbf{T}] = [\mathbf{T}]_{N_d+N_g+1}$  is found by reversing the sense of iterations in Eq. (46).

### III. NUMERICAL RESULTS AND DISCUSSION

#### A. Homogeneous dielectric partnering material

Let us begin with the dielectric partnering material being homogeneous, i.e.,  $\epsilon_d(z)$  is independent of  $z$ . This case has been numerically illustrated by Homola [[2], p. 38] and we adopted the same parameters:  $\lambda_0 = 800$  nm,  $\epsilon_d = 1.766$  (water),  $\epsilon_m = -25 + 1.44i$  (gold), and  $L = 672$  nm. The incident plane wave is  $p$  polarized ( $a_p^{(n)} = \delta_{n0}$  V m $^{-1}$  and  $a_s^{(n)} \equiv 0 \forall n \in \mathbb{Z}$ ), and the quantity of importance is the absorbance

$$A_p = 1 - \sum_{n=-N_t}^{N_t} (|r_s^{(n)}|^2 + |r_p^{(n)}|^2 + |t_s^{(n)}|^2 + |t_p^{(n)}|^2) \times \text{Re}(k_z^{(n)}/k_z^{(0)}), \quad (51)$$

TABLE III. Relative wave numbers  $k_x^{(n)}/k_0$  of Floquet harmonics at the  $\theta$  values of the peaks identified in Fig. 4 by vertical arrows when  $\Omega = \lambda_0$  and  $L = \lambda_0$ . Boldface entries signify SPP waves.

	$n = -2$	$n = -1$	$n = 0$	$n = 1$	$n = 2$
$\theta = 16.3^\circ$	-1.7210	-0.7210	0.2790	1.2790	2.2790
$\theta = 21.0^\circ$	-1.6416	-0.6416	0.3584	<b>1.3584</b>	2.3584
$\theta = 28.4^\circ$	-1.5244	-0.5244	0.4756	<b>1.4756</b>	2.4756
$\theta = 31.6^\circ$	-1.4760	-0.4760	0.5240	1.5240	2.5240
$\theta = 37.7^\circ$	-1.3885	-0.3885	0.6115	<b>1.6115</b>	2.6115

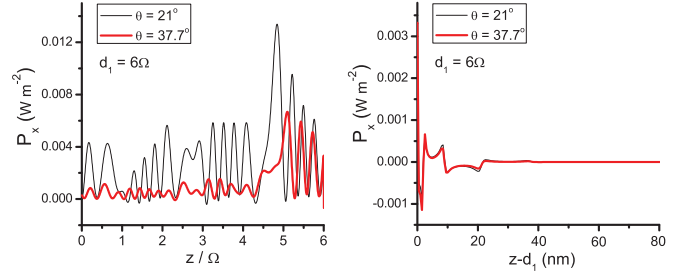


FIG. 5. (Color online) Variation of the  $x$  component of the time-averaged Poynting vector  $\mathbf{P}(x, z)$  along the  $z$  axis in the regions (left)  $0 < z < d_1$  and (right)  $d_1 < z < d_3$  at  $x = 0.75L$ , when the surface-relief grating is defined by Eq. (2). The grating period  $L = \lambda_0$  and the incident plane wave is  $p$  polarized. Other parameters are the same as for Fig. 4.

which simplifies to

$$A_p = 1 - \sum_{n=-N_t}^{N_t} (|r_p^{(n)}|^2 + |t_p^{(n)}|^2) \text{Re}(k_z^{(n)}/k_z^{(0)}), \quad (52)$$

because all materials are isotropic.

Figure 2(a) shows the variation of  $A_p$  vs the incidence angle  $\theta$  for a sinusoidal surface-relief grating defined by [2]

$$g(x) = \frac{1}{2}(d_2 - d_1) \left[ 1 + \sin\left(\frac{2\pi x}{L}\right) \right] \quad (53)$$

instead of Eq. (2), and Fig. 2(b) shows the same for the surface-relief grating defined by Eq. (2) with  $L_1 = 0.5L$ . For computational purposes, we set  $N_d = 1$ ,  $N_g = 50$ , and  $N_t = 10$ , after ascertaining that all nonzero reflectances  $|r_p^{(n)}|^2 \text{Re}(k_z^{(n)}/k_z^{(0)})$  and transmittances  $|t_p^{(n)}|^2 \text{Re}(k_z^{(n)}/k_z^{(0)})$  converged within  $\pm 0.5\%$  for all  $n \in [-N_t, N_t]$ .

Each figure shows plots of  $A_p$  vs  $\theta$  for three different values of the thickness  $d_1$ , in order to distinguish [25] between

- (i) surface waves [11], which must be independent of  $d_1$  for sufficiently large values of that parameter, and
- (ii) waveguide modes [26,27], which must depend on  $d_1$ ,

as has been shown elsewhere [28,29]. In both figures, an absorbance peak at  $\theta \simeq 12.5^\circ$  for all three values of  $d_1$  indicates the excitation of an SPP wave. Parenthetically, let us note here that an SPP wave is a solution of a canonical boundary-value problem involving the planar interface of two semi-infinite half spaces, one of which is occupied by a metal and the other by a dielectric material; but, as the canonical boundary-value problem cannot be implemented practically,

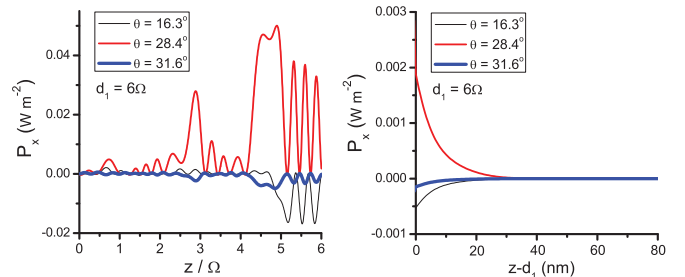


FIG. 6. (Color online) Same as Fig. 5 except that the incident plane wave is  $s$  polarized.

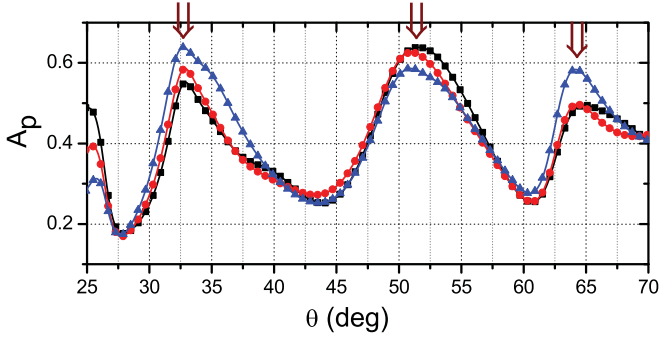


FIG. 7. (Color online) Absorbance  $A_p$  as a function of the incidence angle  $\theta$ , when the surface-relief grating is defined by Eq. (2) with  $L_1 = 0.5L$ ,  $\lambda_0 = 633$  nm,  $\Omega = \lambda_0$ , and  $L = 0.75\lambda_0$ . Black squares are for  $d_1 = 6\Omega$ , red circles for  $d_1 = 5\Omega$ , and blue triangles for  $d_1 = 4\Omega$ . The grating depth ( $d_2 - d_1 = 50$  nm) and the thickness of the metallic layer ( $d_3 - d_2 = 30$  nm) are the same for all plots. Each vertical arrow identifies an SPP wave.

both materials must be present as sufficiently thick layers in a real situation so that the SPP wave decays appreciably through the thickness of each layer.

The relative wave numbers  $k_x^{(n)}/k_0$  of a few Floquet harmonics at  $\theta = 12.5^\circ$  are given in Table I. The solution of the canonical boundary-value problem [2] (when both partnering materials are semi-infinite along the  $z$  axis and their interface is planar) shows that the relative wave number  $\kappa/k_0$  of the SPP wave that can be guided by the planar gold-water interface is

$$\kappa/k_0 = \sqrt{\epsilon_d \epsilon_m / (\epsilon_d + \epsilon_m)} = 1.3784 + 0.0030i. \quad (54)$$

A comparison of Table I and Eq. (54) confirms that an SPP wave is excited at  $\theta = 12.5^\circ$  as the Floquet harmonic of order  $n = 1$ . The spatial profiles of the  $x$  component of the time-averaged Poynting vector

$$\mathbf{P}(x, z) = \frac{1}{2} \text{Re}[\mathbf{E}(x, z) \times \mathbf{H}^*(x, z)] \quad (55)$$

along the  $z$  axis for  $x = 0.75L$  for the  $p$ -polarized incident plane wave at  $\theta = 12.5^\circ$  (the  $\theta$  value of the peak identified in Fig. 2 by a vertical arrow), presented in Fig. 3, also indicate that  $p$ -polarized SPP waves are indeed excited for both types of the surface-relief grating because  $P_x$  decays quickly away from the interface  $z = d_1$ .

We note that the absorbance peak in Fig. 2(b) is not only wider than in Fig. 2(a), but also of lower magnitude, which points out the critical importance of the shape function  $g(x)$  of the surface-relief grating. The incidence angle  $\theta$  determined by Homola [2, p. 38] is approximately  $11^\circ$ , the small difference between his and our results being (i) due to the different methods of computation and (ii) the fact that, while Homola

TABLE IV. Relative wave numbers  $k_x^{(n)}/k_0$  of Floquet harmonics at the  $\theta$  values of the peaks identified in Fig. 7 by vertical arrows when  $\Omega = \lambda_0$  and  $L = 0.75\lambda_0$ . Boldface entries signify SPP waves.

	$n = -2$	$n = -1$	$n = 0$	$n = 1$	$n = 2$
$\theta = 32.5^\circ$	-2.1294	-0.7960	0.5373	<b>1.8760</b>	3.2040
$\theta = 50.9^\circ$	-1.8906	-0.5573	0.7760	<b>2.1094</b>	3.4427
$\theta = 64.2^\circ$	-1.7664	-0.4330	0.9003	<b>2.2336</b>	3.5670

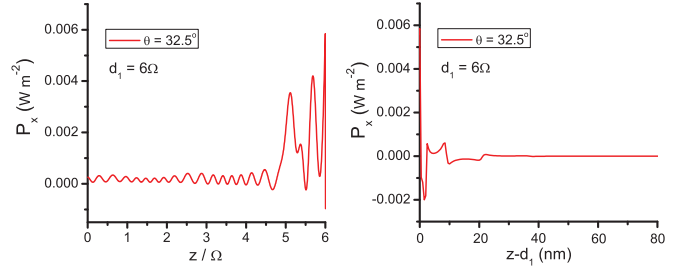


FIG. 8. (Color online) Variation of the  $x$  component of the time-averaged Poynting vector  $\mathbf{P}(x, z)$  along the  $z$  axis in the regions (left)  $0 < z < d_1$  and (right)  $d_1 < z < d_3$  at  $x = 0.75L$ , when the surface-relief grating is defined by Eq. (2) and the incident plane wave is  $p$  polarized. The grating period  $L = 0.75\lambda_0$ ,  $\Omega = \lambda_0$ , and  $d_1 = 6\Omega$ .

had semi-infinite dielectric and metallic partnering materials, we have the two of finite thickness.

## B. Periodically nonhomogeneous dielectric partnering material

Now let us move on to the excitation of *multiple* SPP waves by a surface-relief grating where the dielectric partnering material has a periodic nonhomogeneity normal to the mean metal-dielectric interface:

$$\epsilon_d(z) = \left[ \left( \frac{n_b + n_a}{2} \right) + \left( \frac{n_b - n_a}{2} \right) \sin \left( \pi \frac{d_2 - z}{\Omega} \right) \right]^2, \quad z > 0, \quad (56)$$

where  $2\Omega$  is the period. We chose  $n_a = 1.45$  and  $n_b = 2.32$  from an example provided by Baumeister [30], Sec. 5.3.3.2]. For all calculations reported in the remainder of this paper, we chose the metal to be bulk aluminum ( $\epsilon_{\text{met}} = -56 + 21i$ ) and the free-space wavelength  $\lambda_0 = 633$  nm. The surface-relief grating is defined by Eq. (2) with  $L_1 = 0.5L$ . We fixed  $N_t = 8$  after ascertaining that the absorbances for  $N_t = 8$  converged to within  $\pm 1\%$  of the absorbances calculated with  $N_t = 9$ . The grating depth  $d_2 - d_1 = 50$  nm and the thickness  $d_3 - d_2 = 30$  nm were also fixed, as their variations would not qualitatively affect the excitation of multiple SPP waves. Numerical results for  $\Omega = \lambda_0$  and  $\Omega = 1.5\lambda_0$  are now presented.

### I. $\Omega = \lambda_0$

Let us commence with  $\Omega = \lambda_0$ . The solution of the corresponding canonical boundary-value problem [11,31] (when both the rugate filter and the metal are semi-infinite in thickness and their interface is planar) results in five  $p$ -polarized and two

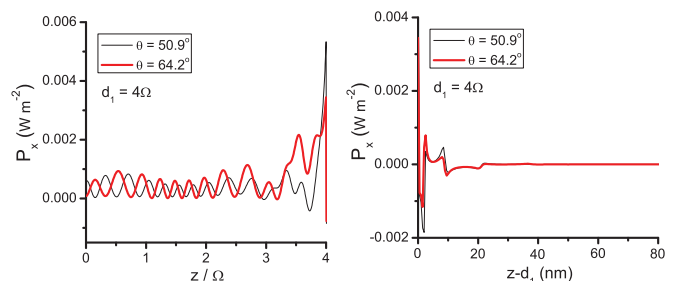


FIG. 9. (Color online) Same as Fig. 8 except that  $d_1 = 4\Omega$ .

TABLE V. Same as Table II except for  $\Omega = 1.5\lambda_0$ .

Polarization	Relative wave numbers			
<i>s</i>	$1.4363 + 0.00025i^a$	$1.61507 + 0.00114i$	$1.78735 + 0.00078i$	$1.9512 + 0.00037i^a$
<i>p</i>	$1.40725 + 0.00052i$	$1.54121 + 0.00374i$	$1.71484 + 0.0049i$	$1.88541 + 0.00739i$
	$2.11513 + 0.0045i$	$2.02159 + 0.01301i$		

<sup>a</sup>These solutions had been missed when solutions for Fig. 1 of Ref. [11] were numerically searched.

*s*-polarized SPP waves, the relative wave numbers  $\kappa/k_0$  being provided in Table II. We used the solution of the canonical boundary-value problem as a guide to choose the grating period  $L$  and as a reference for the relative wave numbers of SPP waves. To analyze the excitation of *s*-polarized SPP waves in the grating-coupled configuration, we calculated the absorptance

$$A_s = 1 - \sum_{n=-N_t}^{n=N_t} (|r_s^{(n)}|^2 + |t_s^{(n)}|^2) \text{Re}(k_z^{(n)}/k_z^{(0)}) \quad (57)$$

for  $a_s^{(n)} = \delta_{n0} \mathbf{V} \text{ m}^{-1}$  and  $a_p^{(n)} \equiv 0 \forall n \in \mathbb{Z}$ . Both  $A_p$  and  $A_s$  were calculated as functions of  $\theta$  for  $d_1 \in \{4\Omega, 5\Omega, 6\Omega\}$ , with  $N_g$  and  $N_d$  selected to have slices of thickness 2 nm in the region  $0 \leq z \leq d_1$  but 1 nm in the region  $d_1 < z < d_2$ .

For all three values of  $d_1$ , a peak is present at  $\theta = 37.7^\circ$  in the plots of  $A_p$  vs  $\theta$  in Fig. 4(a). The relative wave numbers  $k_x^{(n)}/k_0$  of several Floquet harmonics at this incidence angle are given in Table III. At  $\theta = 37.7^\circ$ ,  $k_x^{(1)}/k_0 = 1.6115$  is close to  $\text{Re}(\kappa/k_0) = 1.61782$ , where  $\kappa/k_0$  is the relative wave number of a *p*-polarized SPP wave in the canonical boundary-value problem as provided in Table II. Thus, this  $A_p$  peak represents the excitation of a *p*-polarized SPP wave as a Floquet harmonic of order  $n = 1$ . In order to confirm this conclusion, we plotted the spatial profile of  $P_x(0.75L, z)$  in Fig. 5 for  $\theta = 37.7^\circ$ . Indeed,  $P_x$  decays quickly away from the plane  $z = d_1$  in the region containing metal, and it also decays—periodically, according to the Floquet–Lyapunov theorem [32]—inside the rugate filter away from the same interface, thereby providing confirmation.

For the  $A_p$  peak at  $\theta \simeq 21^\circ$ , the angular location changes slightly with the change in the value of  $d_1$ . However, this peak also represents the excitation of a *p*-polarized SPP wave because (i)  $k_x^{(1)}/k_0 = 1.3584$  (Table III) is close to  $\text{Re}(\kappa/k_0) =$

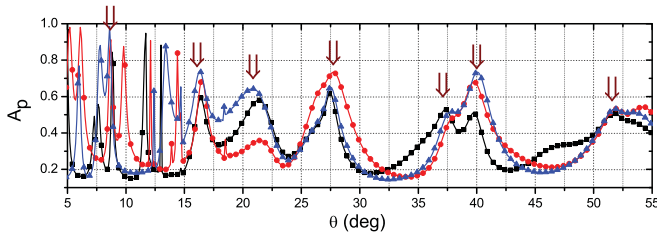


FIG. 10. (Color online) Absorptance  $A_p$  as a function of the incidence angle  $\theta$ , when the surface-relief grating is defined by Eq. (2) with  $L_1 = 0.5L$ ,  $\lambda_0 = 633 \text{ nm}$ ,  $\Omega = 1.5\lambda_0$ , and  $L = 0.8\lambda_0$ . Black squares are for  $d_1 = 6\Omega$ , red circles for  $d_1 = 5\Omega$ , and blue triangles for  $d_1 = 4\Omega$ . The grating depth ( $d_2 - d_1 = 50 \text{ nm}$ ) and the width of the metallic layer ( $d_3 - d_2 = 30 \text{ nm}$ ) are the same for all the plots. Each vertical arrow indicates an SPP wave.

$1.36479$  (Table II), and (ii) the spatial profile of  $P_x(0.75L, z)$  provided in Fig. 5 is also indicative of a surface wave guided by the metal–rugate-filter interface. The reason for the change in the  $\theta$  value of the  $A_p$  peak is the weak localization of this SPP wave in the region  $z < d_1$  (see the left panel in Fig. 5 for  $\theta = 21^\circ$ ). However, for a sufficiently large value of  $d_1$ , the peak should be independent of the value of  $d_1$ .

Three  $A_s$  peaks are present at  $\theta \simeq 16.3^\circ$ ,  $28.4^\circ$ , and  $31.6^\circ$  in the plots of  $A_s$  vs  $\theta$ , for all three values of  $d_1$  in Fig. 4(b). The relative wave numbers of Floquet harmonics at these values of the incidence angle are also provided in Table III. At  $\theta = 16.3^\circ$ , an *s*-polarized SPP wave is excited as a Floquet harmonic of order  $n = -2$  because  $k_x^{(-2)}/k_0 = -1.7210$  (Table III) is close to  $\text{Re}(\kappa/k_0) = -1.7324$  (Table II). The spatial profile of  $P_x(0.75L, z)$  given in Fig. 6 for  $\theta = 16.3^\circ$  also confirms this conclusion. Let us also note that the *s*-polarized SPP wave is propagating in the  $-\hat{\mathbf{u}}_x$  direction because it is excited as a Floquet harmonic of a negative order.

The  $A_s$  peak at  $\theta = 28.4^\circ$  represents the excitation of an *s*-polarized SPP wave, as a Floquet harmonic of order  $n = 1$ , because (i)  $k_x^{(1)}/k_0 = 1.4756$  (Table III) is close to  $\text{Re}(\kappa/k_0) = 1.48639$  (Table II), and (ii) the spatial profile of  $P_x(0.75L, z)$  provided in Fig. 6 shows that an *s*-polarized SPP wave is guided by the interface  $z = d_1$  in the  $+\hat{\mathbf{u}}_x$  direction. Coincidentally, the  $A_s$  peak at  $\theta = 31.6^\circ$  represents the excitation of the same *s*-polarized SPP wave but as a Floquet harmonic of order  $n = -2$  because  $k_x^{(-2)}/k_0 = -1.4760$  (Table III) is close to  $\text{Re}(\kappa/k_0) = -1.48639$  (Table II). This is also evident from the comparison of the spatial profiles given in Fig. 6 for  $\theta = 28.4^\circ$  and  $31.6^\circ$ . Although the two spatial profiles are mirror images of each other, the excitation of the *s*-polarized SPP wave at  $\theta = 31.6^\circ$  is not very efficient because it is excited as a Floquet harmonic of a higher order ( $|n| = 2$ ).

Since not all possible *p*-polarized SPP waves (predicted from the solution of the canonical boundary-value problem)

TABLE VI. Relative wave numbers  $k_x^{(n)}/k_0$  of Floquet harmonics at the  $\theta$  values of the peaks identified in Fig. 10 by vertical arrows when  $\Omega = 1.5\lambda_0$  and  $L = 0.8\lambda_0$ . Boldface entries signify SPP waves.

	$n = -2$	$n = -1$	$n = 0$	$n = 1$	$n = 2$
$\theta = 8.8^\circ$	-2.3470	-1.0970	0.1530	<b>1.4030</b>	2.6530
$\theta = 16.3^\circ$	-2.2193	-0.9693	0.2807	<b>1.5307</b>	2.7807
$\theta = 20.8^\circ$	<b>-2.1416</b>	-0.8916	0.3584	1.6084	2.8584
$\theta = 27.5^\circ$	-2.0382	-0.7882	0.4618	<b>1.7118</b>	2.9618
$\theta = 37.3^\circ$	<b>-1.8940</b>	-0.6440	0.6060	1.8560	3.1060
$\theta = 40^\circ$	-1.8572	-0.6072	0.6428	<b>1.8928</b>	3.1428
$\theta = 51.8^\circ$	-1.7141	-0.4641	0.7859	<b>2.0359</b>	3.2859

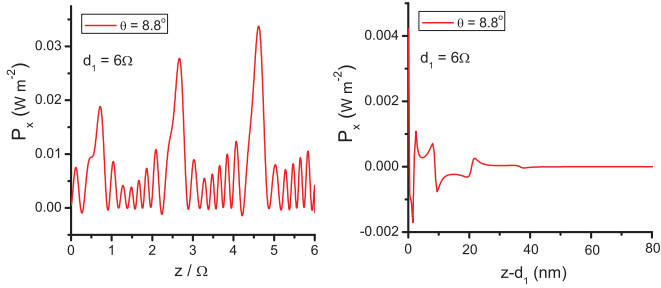


FIG. 11. (Color online) Variation of the  $x$  component of the time-averaged Poynting vector  $\mathbf{P}(x, z)$  along the  $z$  axis in the regions (left)  $0 < z < d_1$  and (right)  $d_1 < z < d_3$  at  $x = 0.75L$ , when the surface-relief grating is defined by Eq. (2) and the incident plane wave is  $p$  polarized. The grating period  $L = 0.8\lambda_0$  and  $d_1 = 6\Omega$ .

can be excited with period  $L = \lambda_0$  of the surface-relief grating, the grating period needs to be changed in order to excite the remaining SPP waves. The plots of  $A_p$  vs  $\theta$  for  $L = 0.75\lambda_0$  are presented in Fig. 7, again for  $d_1 \in \{4\Omega, 5\Omega, 6\Omega\}$ . The figure

shows three  $A_p$  peaks at  $\theta \simeq 32.5^\circ$ ,  $50.9^\circ$ , and  $64.2^\circ$  that are present for all three chosen values of  $d_1$ . The relative wave numbers of several Floquet harmonics at these values of  $\theta$  are given in Table IV. The  $A_p$  peak at  $\theta = 32.5^\circ$  represents the excitation of a  $p$ -polarized SPP wave as a Floquet harmonic of order  $n = 1$  because  $k_x^{(1)}/k_0 = 1.8760$  is close to  $\text{Re}(1.87437 + 0.00998i)$  in Table II. The spatial profile of  $P_x(0.75L, z)$  given in Fig. 8 also supports this conclusion. Similarly, the  $A_p$  peaks at  $\theta = 50.9^\circ$  and  $64.2^\circ$  represent the excitation of two other  $p$ -polarized SPP waves as a Floquet harmonic of the same order ( $n = 1$ ), as is evident from the comparison of Tables III and IV and from the spatial profiles of  $P_x(0.75L, z)$  provided in Fig. 9.

2.  $\Omega = 1.5\lambda_0$

The relative wave numbers of possible SPP waves that can be guided by the planar interface of the chosen rugate filter and the metal are given in Table V for  $\Omega = 1.5\lambda_0$ . In this case, the solution of the canonical boundary-value problem

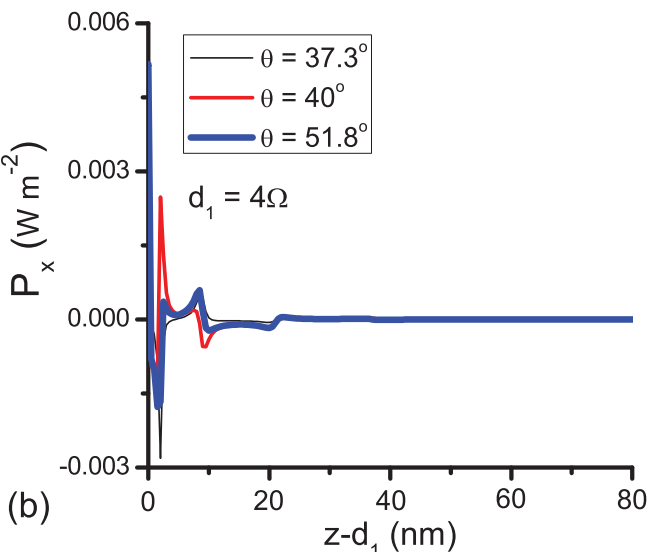
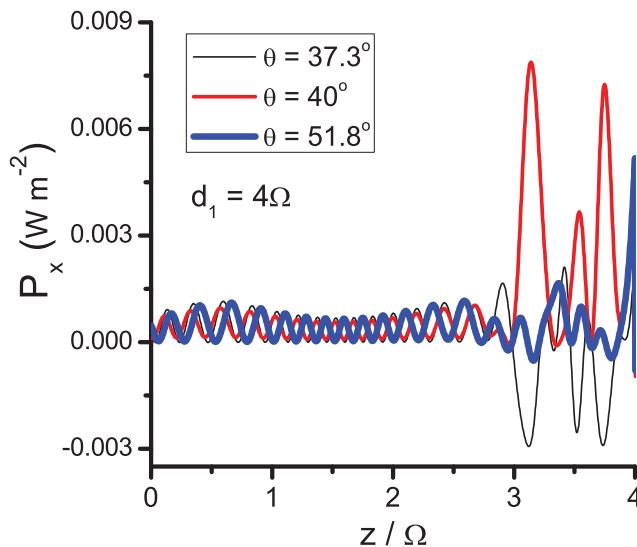
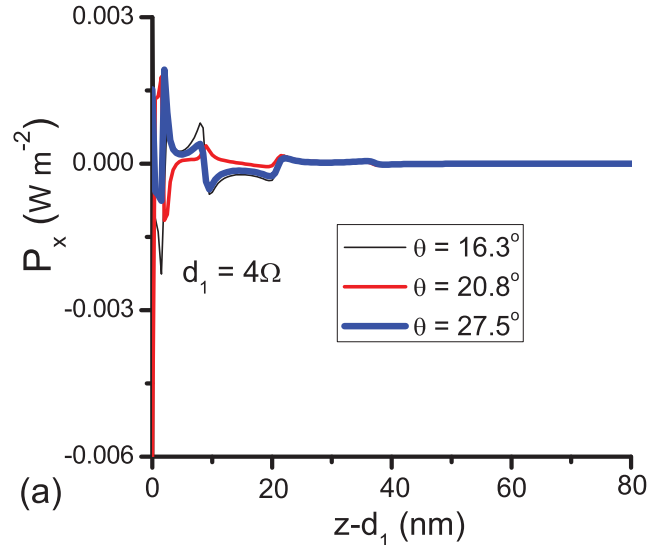
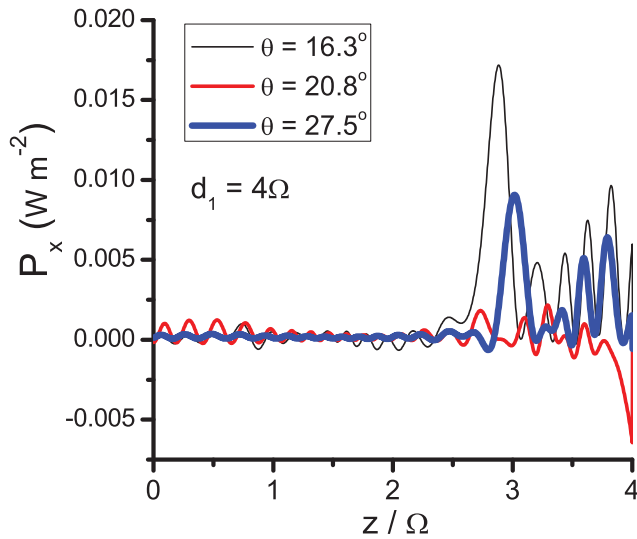


FIG. 12. (Color online) Same as Fig. 11 except that  $d_1 = 4\Omega$ .



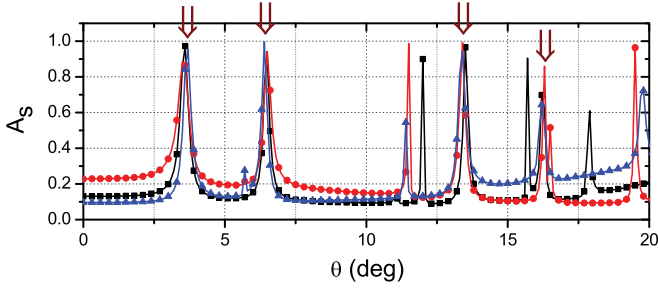


FIG. 13. (Color online) Same as Fig. 10 except that  $A_s$  is plotted instead of  $A_p$ , and  $L = 0.6\lambda_0$ .

[11,31] indicated that four  $s$ -polarized and six  $p$ -polarized SPP waves can be guided by the metal-rugate-filter interface. For computations, the region  $d_1 < z < d_2$  was again divided into 1-nm-thick slices; however, the region  $0 \leq z \leq d_1$  was divided into 3-nm-thick slices to reduce the computation time, after ascertaining that the accuracy of the computed reflectances and transmittances had not been adversely affected.

In the plots of  $A_p$  vs  $\theta$  for  $L = 0.8\lambda_0$ , provided in Fig. 10, the excitation of  $p$ -polarized SPP waves is indicated at seven values of the incidence angle:  $\theta \simeq 8.8^\circ, 16.3^\circ, 20.8^\circ, 27.5^\circ, 37.3^\circ, 40^\circ$ , and  $51.8^\circ$ . The relative wave numbers  $k_x^{(n)}/k_0$  of a few Floquet harmonics at these values of the incidence angle are given in Table VI. The  $A_p$  peak at  $\theta = 8.8^\circ$  represents the excitation of a  $p$ -polarized SPP wave because  $k_x^{(1)}/k_0 = 1.4030$  is close to  $\text{Re}(\kappa/k_0) = 1.40725$  (Table V). The spatial profile of  $P_x(0.75L, z)$  given in Fig. 11 for  $\theta = 8.8^\circ$  confirms the excitation of a  $p$ -polarized SPP wave; however, the SPP wave is very loosely bound to the interface  $z = d_1$  in the region  $0 < z < d_1$ .

The  $A_p$  peak at  $\theta = 16.3^\circ$  represents the excitation of another  $p$ -polarized SPP wave, because  $k_x^{(1)}/k_0 = 1.5307$  is close to  $\text{Re}(\kappa/k_0) = 1.54121$  (Table V). The  $A_p$  peak at  $\theta = 20.8^\circ$  also represents a  $p$ -polarized SPP wave because  $k_x^{(-2)}/k_0 = -2.1416$  is close to  $\text{Re}(\kappa/k_0) = -2.11513$  (Table V). Similarly, the  $A_p$  peak at  $\theta = 27.5^\circ$  is due to the excitation of another  $p$ -polarized SPP wave as a Floquet harmonic of order  $n = 1$ . The spatial profiles of  $P_x(0.75L, z)$  given in Fig. 12(a) for three different  $p$ -polarized plane waves incident at  $\theta = 16.3^\circ, 20.8^\circ$ , and  $27.5^\circ$  also confirm that SPP waves are excited as Floquet harmonic of order  $n = 1, -2$ , and  $1$ , respectively.

A comparison of Tables V and VI shows that the  $A_p$  peaks at  $\theta = 37.3^\circ$  and  $40^\circ$  represent the excitation of the same  $p$ -polarized SPP wave; however, the SPP wave is excited as a Floquet harmonic of order  $n = -2$  at  $\theta = 37.3^\circ$  but of order

TABLE VII. Relative wave numbers  $k_x^{(n)}/k_0$  of Floquet harmonics at the  $\theta$  values of the peaks identified in Fig. 13 by vertical arrows when  $\Omega = 1.5\lambda_0$  and  $L = 0.6\lambda_0$ . Boldface entries signify SPP waves.

	$n = -2$	$n = -1$	$n = 0$	$n = 1$	$n = 2$
$\theta = 3.7^\circ$	-3.2688	<b>-1.6021</b>	0.0645	1.7312	3.3979
$\theta = 6.4^\circ$	-3.2219	-1.5552	0.1115	<b>1.7781</b>	3.4448
$\theta = 13.5^\circ$	-3.0999	<b>-1.4332</b>	0.2334	1.9001	3.5668
$\theta = 16.2^\circ$	-3.0543	-1.3877	0.2790	<b>1.9457</b>	3.6123

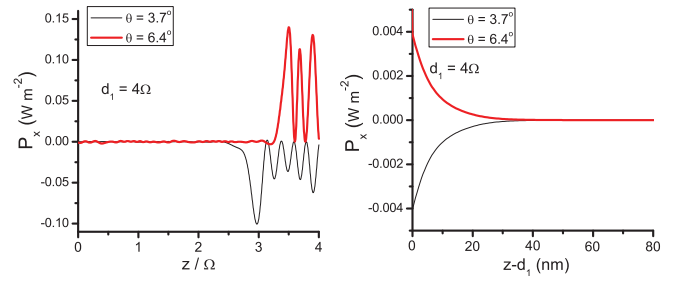


FIG. 14. (Color online) Variation of the  $x$  component of the time-averaged Poynting vector  $\mathbf{P}(x, z)$  along the  $z$  axis in the regions (left)  $0 < z < d_1$  and (right)  $d_1 < z < d_3$  at  $x = 0.75L$  for two  $s$ -polarized incident plane waves, when the surface-relief grating is defined by Eq. (2). The grating period  $L = 0.6\lambda_0$ ,  $d_1 = 4\Omega$ , and  $\Omega = 1.5\lambda_0$ .

$n = 1$  at  $\theta = 40^\circ$ . Similarly, a  $p$ -polarized SPP wave is excited as a Floquet harmonic of order  $n = 1$  at  $\theta = 51.8^\circ$ . The spatial profiles of  $P_x(0.75L, z)$  given in Fig. 12(b) also support these conclusions.

In the plots of  $A_s$  vs  $\theta$  for  $L = 0.6\lambda_0$ , provided in Fig. 13, four peaks at  $\theta \simeq 3.7^\circ, 6.4^\circ, 13.5^\circ$ , and  $16.2^\circ$  are present for all values of  $d_1$ . The  $A_s$  peak at  $\theta = 3.7^\circ$  represents the excitation of an  $s$ -polarized SPP wave as a Floquet harmonic of order  $n = -1$  because  $k_x^{(1)}/k_0 = -1.6021$  is close to  $\text{Re}(\kappa/k_0) = -1.61507$  (Table V), which is a solution of the canonical boundary-value problem for an  $s$ -polarized SPP wave, whereas the  $A_s$  peak at  $\theta = 6.4^\circ$  represents the excitation of another  $s$ -polarized SPP wave because  $k_x^{(1)}/k_0 = 1.7781$  is close to  $\text{Re}(\kappa/k_0) = 1.78735$  (Table V). Similarly, two  $s$ -polarized SPP waves are excited as a Floquet harmonic of order  $n = 1$  at  $\theta = 13.5^\circ$  and of order  $n = -1$  at  $\theta = 16.2^\circ$ , respectively, as is evident from the comparison of Tables VI and VII. The spatial profiles of  $P_x(0.75L, z)$  given in Figs. 14 and 15 confirm these conclusions.

### C. General conclusions

In the last two subsections, we have deciphered a host of numerical results and identified those absorptance peaks that indicate the excitation of SPP waves in the grating-coupled configuration, when the dielectric partnering material is periodically nonhomogeneous normal to the mean plane of the surface-relief grating. We found that

- (i) the periodic nonhomogeneity of the dielectric partnering material enables the excitation of multiple SPP waves of both  $p$ - and  $s$ -polarization states;
- (ii) fewer  $s$ -polarized SPP waves are excited than  $p$ -polarized SPP waves;

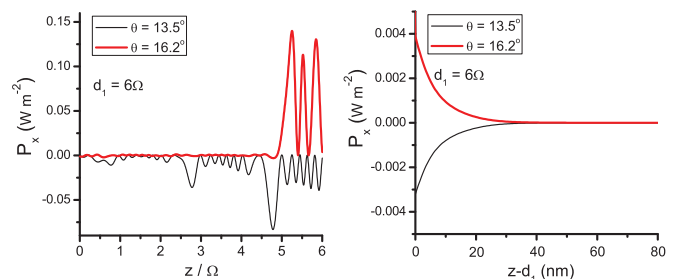


FIG. 15. (Color online) Same as Fig. 14 except that  $d_1 = 6\Omega$ .

(iii) for a given period of the surface-relief grating, it is possible for two plane waves with different angles of incidence to excite the same SPP wave [Figs. 4(b) and 10];

(iv) not all SPP waves predicted by the solution of the canonical problem may be excited in the grating-coupled configuration for a given period of the surface-relief grating;

(v) the absorptance peaks representing the excitation of  $p$ -polarized SPP waves are generally wider than those representing  $s$ -polarized SPP waves;

(vi) the absorptance peak is narrower for an SPP wave of higher phase speed [i.e., smaller  $\text{Re}(\kappa)$ ]; and

(vii) an SPP wave that is excited as a Floquet harmonic of order  $n = +1$  for  $\theta \in [0, \pi/2)$ —or  $n = -1$  for  $\theta \in (-\pi/2, 0)$ , by virtue of symmetry—is the most efficient (Fig. 6).

Let us note that some other combination of the periodic functions  $\epsilon_d(z)$  and  $g(x)$  may allow all solutions of the canonical boundary-value problem to be excited in the grating-coupled configuration with a specific  $\{d_1, d_2, d_3\}$ .

The solution of the canonical boundary-value problem [11] indicates that the period  $2\Omega$  of the rugate filter needs to be greater than a certain value in order for more than one SPP wave to be excited, and the excitation of  $s$ -polarized SPP waves may require an even larger period. However, the number of possible SPP waves increases as the period increases up to a certain value.

#### IV. CONCLUDING REMARKS

The excitation of multiple surface plasmon-polariton (SPP) waves by a surface-relief grating formed by a metal and a dielectric material, both of finite thickness, was studied theoretically using the rigorous coupled-wave analysis for a practically implementable setup. The presence of an SPP

wave was inferred by a peak in the plot of absorptance vs the angle of incidence  $\theta$ , provided that the  $\theta$  location of the peak turned out to be independent of the thickness of the dielectric partnering material. If that material is homogeneous, only one  $p$ -polarized SPP wave, that too of a  $p$ -polarization state, is excited. However, the periodic nonhomogeneity of the partnering dielectric material normal to the mean metal-dielectric interface results in the excitation of multiple SPP waves of different polarization states and phase speeds. In general, the absorptance peak is narrower for an  $s$ -polarized SPP wave than for of a  $p$ -polarized SPP wave, and the absorptance peak is narrower for an SPP wave of higher phase speed.

Since the electromagnetic field radiated by a line source can be considered as a spectrum of plane waves propagating at all angles [ [33], Sec. 2.2], the grating-coupled configuration discussed in this paper can be used to excite multiple SPP waves simultaneously by a line source. The excitation of multiple SPP waves may be significant for practical applications—for example, to increase the absorption of light in solar cells due to the increased possibility of excitation of SPP waves [34]. This application is currently under investigation by the authors.

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- [1] S. A. Maier, *Plasmonics: Fundamentals and Applications* (Springer, New York, 2007).
- [2] *Surface Plasmon Resonance Based Sensors*, edited by J. Homola (Springer, Heidelberg, 2006).
- [3] A. V. Zayats, I. I. Smolyaninov, and A. A. Maradudin, *Phys. Rep.* **408**, 131 (2005).
- [4] M. Dragoman and D. Dragoman, *Prog. Quantum Electron.* **32**, 1 (2008).
- [5] J. A. Polo Jr. and A. Lakhtakia, *Laser Photon. Rev.* **5**, 234 (2011).
- [6] J. A. Polo Jr. and A. Lakhtakia, *Proc. R. Soc. London A* **465**, 87 (2009).
- [7] M. Faryad, J. A. Polo Jr., and A. Lakhtakia, *J. Nanophoton.* **4**, 043505 (2010).
- [8] Devender, D. P. Pulsifer, and A. Lakhtakia, *Electron. Lett.* **45**, 1137 (2009).
- [9] T. H. Gilani, N. Dushkina, W. L. Freeman, M. Z. Numan, D. N. Talwar, and D. P. Pulsifer, *Opt. Eng.* **49**, 120503 (2010).
- [10] A. Lakhtakia, Y.-J. Jen, and C.-F. Lin, *J. Nanophoton.* **3**, 033506 (2009).
- [11] M. Faryad and A. Lakhtakia, *J. Opt. Soc. Am. B* **27**, 2218 (2010).
- [12] B. G. Bovard, *Appl. Opt.* **32**, 5427 (1993).
- [13] R. Overend, D. R. Gibson, R. Marshall, and K. Lewis, *Vacuum* **43**, 51 (1992).
- [14] E. Lorenzo, C. J. Oton, N. E. Capuj, M. Ghulinyan, D. Navarro-Urrios, Z. Gaburro, and L. Pavesi, *Phys. Stat. Sol. C* **2**, 3227 (2005).
- [15] C. C. Lee, C. J. Tang, and J. Y. Wu, *Appl. Opt.* **45**, 1333 (2006).
- [16] A. Lakhtakia, *J. Mod. Opt.* **58**, 562 (2011).
- [17] M. W. McCall and A. Lakhtakia, *Electromagnetics* **23**, 1 (2003).
- [18] J. P. McIlroy, M. W. McCall, A. Lakhtakia, and I. J. Hodgkinson, *Optik* **116**, 311 (2005).
- [19] M. G. Moharam and T. K. Gaylord, *J. Opt. Soc. Am.* **72**, 1385 (1982).
- [20] L. Li, *J. Opt. Soc. Am. A* **12**, 2581 (1993).
- [21] M. G. Moharam, E. B. Grann, and D. A. Pommet, *J. Opt. Soc. Am. A* **12**, 1068 (1995).
- [22] E. N. Glytsis and T. K. Gaylord, *J. Opt. Soc. Am. A* **4**, 2061 (1987).
- [23] F. Wang, M. W. Horn, and A. Lakhtakia, *Microelectron. Eng.* **71**, 34 (2004).

- [24] N. Chateau and J.-P. Hugonin, *J. Opt. Soc. Am. A* **11**, 1321 (1994).
- [25] M. A. Motyka and A. Lakhtakia, *J. Nanophoton.* **2**, 021910 (2008).
- [26] N. S. Kapany and J. J. Burke, *Optical Waveguides* (Academic, New York, 1972).
- [27] D. Marcuse, *Theory of Dielectric Optical Waveguides* (Academic, San Diego, 1991).
- [28] A. Otto and W. Sohler, *Opt. Commun.* **3**, 254 (1971).
- [29] M. Faryad and A. Lakhtakia, *Phys. Rev. A* **83**, 013814 (2011).
- [30] P. W. Baumeister, *Optical Coating Technology* (SPIE, Bellingham, 2004).
- [31] In addition to solutions provided in Fig. 1 of Ref. [11], other solutions were found. These have been identified by <sup>a</sup> in Tables II and V.
- [32] V. A. Yakubovich and V. M. Starzhinskii, *Linear Differential Equations with Periodic Coefficients* (Wiley, New York, 1975).
- [33] W. C. Chew, *Waves and Fields in Inhomogeneous Media* (IEEE Press, Piscataway, 1990).
- [34] V. E. Ferry, A. Sweatlock, D. Pacifici, and H. A. Atwater, *Nano Lett.* **8**, 4391 (2008).