# Excitability in semiconductor microring lasers: Experimental and theoretical pulse characterization

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(Received 28 July 2010; published 30 December 2010)

We characterize the operation of semiconductor microring lasers in an excitable regime. Our experiments reveal a statistical distribution of the characteristics of noise-triggered optical pulses that is not observed in other excitable systems. In particular, an inverse correlation exists between the pulse amplitude and duration. Numerical simulations and an interpretation in an asymptotic phase space confirm and explain these experimentally observed pulse characteristics.

DOI: 10.1103/PhysRevA.82.063841

PACS number(s): 42.65.Pc, 42.55.Px, 42.60.Mi

### I. INTRODUCTION

Excitability, the ability of nonlinear systems to fire large, well-defined output pulses when a threshold is crossed, has been investigated in a broad range of scientific areas, including physics, chemistry, biology, and neuroscience [1-7]. The strong interdisciplinarity of excitable systems has attracted the attention of theoreticians interested in their universal properties. These theoretical studies disclosed that excitability takes place when a *separatrix* is crossed in the phase space of the system, which led to a comprehensive classification of excitable systems based on bifurcations taking place in their phase space [3,6]. Considerable theoretical insight was further gained into the role played by networks of excitable units in neuroscience [8]. Moreover, the investigation of excitable units is of high practical relevance as networks of spiking neurons have proved to be computationally superior to other neural networks [4].

In the field of photonics, excitability is widely studied both theoretically and experimentally [9-17], and a broad search was started for optical excitable units that could be deployed in optical neural networks. In the last decade, lasers with saturable absorber [9,10], optically injected lasers [11,16], lasers with optical feedback [15], and vertical-cavity surface-emitting lasers with optoelectronic feedback [17] have all been proposed as optical excitable units.

Most often, excitable behavior in optical systems has been shown to occur close to a fold bifurcation and a homoclinic bifurcation of a *stable* limit cycle [9–12,16]. In these systems, the response to noise is governed by the presence of an *accessible* saddle point *S* embedded in the separatrix. Pulses are activated by noise-induced fluctuations that connect the resting state to *S*, and the large deterministic excursion takes place along the *unstable* manifold of *S*. In this scenario, excitability is therefore possible in the limit of vanishing noise intensity.

In a recent paper [18], we proposed that excitability can take place in systems with weakly broken  $Z_2$  symmetry, which includes optical units such as semiconductor microring lasers [19,20] and microdisk lasers [21]. It can be shown that in this class of systems the accessible saddle is not embedded in the separatrix for excitability. Therefore, the unstable manifold of *S* does not participate in excitability, and the generation of pulses cannot be initiated in the vanishing noise limit. Clear evidence of such excitability was shown in semiconductor

ring lasers with weakly broken  $Z_2$  symmetry in the presence of a nonvanishing, finite intensity of spontaneous emission noise [18].

In this paper, we address the fact that microring lasers (MRLs) in the excitable regime show a notable degree of variation in the amplitude and width of the excited pulses. We characterize, both theoretically and experimentally, the particular pulse properties when the triggering occurs through optical noise in the system. The main result is that a clear inverse correlation is observed between the amplitude and width of the excited pulses. In Sec. II, we experimentally investigate the excitable behavior of a MRL in the time domain. A characterization of the stochastic properties of excitability is carried out to reveal an interspike-interval (ISI) distribution that is exponential for large waiting times but diverges from the Kramers form for intervals below approximately 50 ns. In Secs. III and IV, we use a general rate-equation model and an asymptotic model for excitability in MRLs as introduced in Refs. [18,22] to explain the experimentally observed features. Finally, in Sec. V, we discuss the main results presented and their generality.

# II. EXPERIMENTS

### A. Device and setup

The experiments have been performed on an InP-based multi-quantum-well MRL with a racetrack geometry [see Fig. 1(a)]. The optical power is coupled out of the ring cavity by directional coupling to bus waveguides that are integrated on the same optical chip. The use of two bus waveguides in the microring design allows for four independent input-output ports A–D that can be accessed with optical fibers. The device is mounted on a copper mount and is thermally controlled by a Peltier element that is stabilized with an accuracy of 0.01°C.

The MRL chip is deployed in a setup as shown in Fig. 1. In our experiments only port A is used for collecting output power from the MRL as well as injecting optical noise in the microring cavity. We use a directly biased semiconductor optical amplifier [SOA in Fig. 1(b)] operating in the *C* band to generate a controllable amount of noise through amplified spontaneous emission, which is injected in the ring through a lensed optical fiber coupled to port A of the MRL. The use of a circulator [C in Fig. 1(b)] allows us to read output from port A with the same lensed fiber.

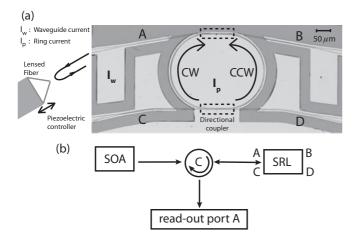


FIG. 1. Experimental MRL setup. (a) The actual MRL device with its contacting. The ring itself is pumped with a current  $I_p$ . Four waveguide contacts are depicted, of which only port A is biased with  $I_w$ . (b) The overall setup where the readout and the SOA are separated from each other by a circulator C.

Electrical contacts have been applied to the bus waveguides that can be independently pumped. They allow us to amplify on the chip the signal emitted by the ring. More interestingly, the presence of a contact allows us to continuously break the symmetry of the device in a controlled way by making both the strength and the phase of the linear coupling between the clockwise (CW) and the counterclockwise (CCW) modes asymmetric. Using the fiber's facet as a mirror, we are able to reflect power from one mode (e.g., CCW) back into the waveguide and finally to the counterpropagating mode in the ring. The application of a direct bias current  $I_w$  on the waveguide's electrode has two main effects. First, it controls the power that is coupled to the CW mode; second, it affects the optical length of the waveguide via carrier-induced refractive index changes. Therefore, the phase of the reflected signal can be controlled by tuning the bias current on the waveguide and changing the position of the fiber facet which is piezocontrolled. We have previously demonstrated in Refs. [18,22] that such a breaking of the  $Z_2$  symmetry of the microring leads to excitable behavior when the optical noise intensity is large enough to make one of the states metastable. We analyze the output power of the CCW mode (port A) using a fast photodiode (with a bandwidth of 2.4 GHz) connected to an oscilloscope (with a maximum sampling rate of 20 Gs  $s^{-1}$ ).

### **B.** Excitability

In the temperature range of operation, the transparency current density of our semiconductor material is  $\sim 1.0$  kA cm<sup>-2</sup>, which leads to a transparency current of  $\sim 24$  mA for the MRL and  $\sim 4$  mA for the waveguide. The MRL device reaches threshold at 35 mA, and excitability is observed between 42 and 48 mA. A typical time series revealing the excitable behavior of the microring is shown in Fig. 2(a). The device operates most of the time in the CW unidirectional mode. However, pulses in the CCW direction can be regularly observed. An example of an excited pulse with a pulse duration of  $\sim 7$  ns is shown in Fig. 2(b).

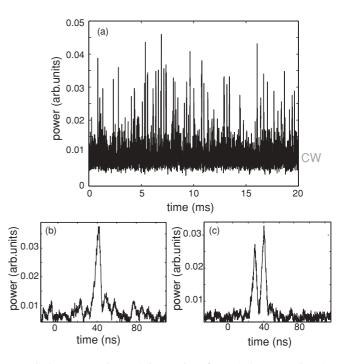


FIG. 2. (a) Experimental time series of port A demonstrating the excitable behavior of the MRL operating at  $I_p = 47.45$  mA. The current on the waveguide of port A is  $I_w = 13$  mA, and the current in the external SOA is  $I_{SOA} = 700$  mA. Examples of (b) a single and (c) a double excited pulse taken from the same time series.

In contrast to what is expected for a typical excitable system, not all excited pulses have the same amplitude and duration; see, e.g., Fig. 2(a). We clearly observe a degree of variation in the amplitude of the pulses (which is not a consequence of undersampling since it persists for higher sampling rates). In the same way, a distribution of pulse durations is observed in the experimental time series, and the pulse durations seem to be spread between a minimum of 7 ns and a maximum of 20 ns. Such a spread is significantly larger than the sampling time.

#### C. Interspike-interval distribution

In order to quantitatively describe the ISI, we have constructed the ISI distribution from the experimental time series. A threshold is put at 60% of the maximum pulse height recorded in the time series. Only pulses above this threshold are taken into account in the calculation of the ISI distribution. We have verified that calculating the ISI distribution for other values of the threshold gives the same qualitative results as long as it is not chosen too low as one will then start to measure noisy excursions instead of actual excited pulses. An example of such an ISI distribution is shown in Fig. 3(a) for the MRL operating at a current of 47.45 mA. The tail of the distribution is well fitted by a typical Kramers exponential distribution  $P(\tau) \propto \exp[-\tau/T_1]$ , which indicates that the excited pulses are activated by noise-induced crossing of a potential barrier. The time constant  $T_1$  obtained from the fitting of Fig. 3(a) is  $T_1 = 0.63 \ \mu s.$ 

A significant deviation from the Kramers law is, however, observed for ISIs shorter than 50 ns, as shown in Fig. 3(b). The distribution of such "short" ISI is strongly peaked

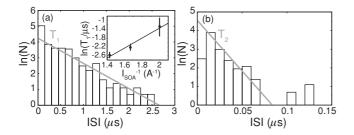


FIG. 3. ISI distribution for pulses emitted by the symmetrybroken MRL for device parameters as given in Fig. 2. The logarithm of the number of events N in each ISI bin is shown. (a) The distribution of long ISIs is well fitted by an exponential curve (see gray solid line). The gradient  $1/T_1 = 1.6 \,\mu s^{-1}$  indicates a characteristic time scale of ~0.63  $\mu s$ . (b) The distribution of short ISIs reveals a different time constant  $T_2 \sim 18.4$  ns. The inset in (a) shows the dependence of the long ISI time scale  $T_1$  (with error bars given by the standard deviation from the mean value  $T_1$ ) on the current on the external SOA ( $I_{SOA}$ ), which is used as noise source.

around approximately 20 ns and decreases abruptly with a characteristic time  $T_2 = 18.4$  ns. A similar deviation from the Kramers law was previously reported in the residence-time distribution of MRLs [23] and in other optical excitable systems, such as lasers with optical feedback close to the low-frequency fluctuations regime [24,25].

In order to confirm and quantify the noise-activated origin of excitability, we have investigated the dependence of the average interspike-interval  $T_1$  as function of the bias current on the ring  $I_p$  and the external noise. The external noise source is the external semiconductor optical amplifier [see Fig. 1(b)], and it is biased at different DC currents. We assume a linear relationship between the SOA current and the noise intensity coupled into the MRL. In the inset of Fig. 3(a) the dependence of  $T_1$  versus the SOA current is shown. The linear relation between  $\ln(T_1)$  and the inverse of the SOA current is consistent with a Kramers rate across a potential barrier [26].

We have also verified that  $T_1$  increases with the bias current  $I_p$  on the ring, which is consistent with the theoretical result that the activation energy of the MRL increases with the bias current [27].

In contrast, we have checked that the short ISI has a much smaller dependence on the noise strength and remains approximately constant when changing the  $I_{SOA}$  and  $I_p$ . The origin of the non-Arrhenius distribution for these short ISIs is instead related to deterministic dynamics. This will be discussed in more detail in Secs. III and IV.

### D. Amplitude-width distribution

In order to further characterize the properties of the excited pulses, we build the distribution of the pulse duration, defined as the full width at half maximum (FWHM) and the distribution of pulse amplitudes. Typical examples of the amplitude and width distributions are shown in Fig. 4.

A distribution of pulse amplitudes is evident in Fig. 4(a), which is consistent with the pulse amplitude modulation present in Fig. 2. Such a distribution of amplitudes was not observed in other optical excitable systems (see, for instance, [9,14,28]) and is not consistent with a standard excitability

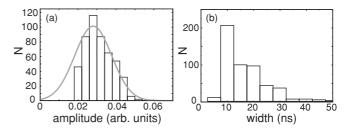


FIG. 4. Distribution of (a) the pulse amplitude and (b) the pulse width for  $I_p = 47.45$  mA,  $I_{SOA} = 700$  mA, and  $I_w = 13.0$  mA. The number of events N in each bin is plotted. The gray solid line shows the corresponding Gaussian distribution as predicted by the theory presented in Sec. IV.

scenario where the system performs a large phase-space excursion following the unstable manifold of a saddle structure [6,7] for which a much sharper distribution is expected. The width of the excited pulses is distributed asymmetrically around an average value of 18 ns and reveals a nonzero probability for pulses as long as 40 ns.

In order to shed light on the dynamical origin of such distributions, we have measured the correlation between pulse amplitude and width for different values of the bias current on the ring. We minimize the noise contributions to the pulse amplitude by performing this measurement without the external SOA. The results are shown in Fig. 5 and are quantified using a correlation coefficient C:

$$C = \frac{\sum (w_i - \bar{w})(h_i - h)}{N_{\text{tot}}\sigma_h \sigma_w},$$
(1)

$$\sigma_h = \sqrt{\frac{\sum (h_i - \bar{h})^2}{N_{\text{tot}}}}; \quad \sigma_w = \sqrt{\frac{\sum (w_i - \bar{w})^2}{N_{\text{tot}}}}.$$
 (2)

For all used bias currents there is a clear correlation between the width and amplitude of the pulses. The experiments reveal that pulses with a higher peak power are narrower, whereas pulses with a lower peak power are wider. For  $I_{SOA} = 0$  mA and  $I_w = 13.0$  mA, we have measured a correlation C of about 0.7. The slope of the linear fit between the amplitude and width becomes steeper as the bias current on the ring  $I_p$  increases (see the gray solid line in Fig. 5). We note that the correlation shown in Fig. 5 has been obtained by defining the pulse width by its FWHM; we have verified that other ways to quantify the pulse duration (not shown) lead to consistent results.

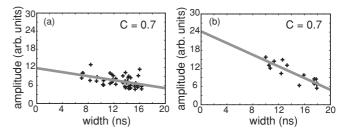


FIG. 5. Measured width and amplitude of the excited pulses for two different values of the bias current  $I_p$  on the ring.  $I_{SOA} = 0$  mA and  $I_w = 13.0$  mA. (a)  $I_p = 42.82$  mA and (b)  $I_p = 44.49$  mA. A linear fit of the data points is shown by the gray solid line. The correlation coefficient *C* is approximately 0.7 in both cases.

To understand the origin of this amplitude-width correlation of the excited pulses, we will numerically analyze the pulse properties in Sec. IV. To allow for a clear presentation of the results, in Sec. III, we briefly review our approach toward modeling the time evolution of a single-longitudinal, single-transverse mode in a microring cavity using a general rate-equation model for MRLs and an asymptotically reduced model. In particular, we explain the excitability scenario for MRLs in the asymptotic phase space. For more information on the rate-equation model, we refer to Refs. [22,29,30].

# III. MODELING AND ORIGIN OF EXCITABILITY IN SEMICONDUCTOR RING LASERS

In order to model the MRL operating in single-longitudinal and single-transverse mode, we use a rate-equation model for the the evolution of the slowly varying amplitudes of the counterpropagating modes  $E_{cw,ccw}$  and the carrier inversion N [22]:

$$\frac{dE_{\rm cw}}{dt} = \kappa (1+i\alpha) \left[g_{\rm cw}N - 1\right] E_{\rm cw} - (k - \Delta k/2)e^{i(\phi_k - \Delta \phi_k/2)} E_{\rm ccw} + \xi_{\rm cw}, \qquad (3)$$

$$\frac{dE_{\rm ccw}}{dt} = \kappa (1+i\alpha) [g_{\rm ccw}N - 1] E_{\rm ccw} - (k + \Delta k/2) e^{i(\phi_k + \Delta \phi_k/2)} E_{\rm cw} + \xi_{\rm ccw}, \quad (4)$$

$$\frac{dN}{dt} = \gamma [\mu - N - g_{\rm cw} N |E_{\rm cw}|^2 - g_{\rm ccw} N |E_{\rm ccw}|^2], \quad (5)$$

where  $g_{cw} = 1 - s|E_{cw}|^2 - c|E_{ccw}|^2$ ,  $g_{ccw} = 1 - s|E_{ccw}|^2 - c|E_{ccw}|^2$  is a differential gain function that includes phenomenological self (s) and cross (c) saturation terms.  $\kappa$  is the field decay rate,  $\gamma$  is the inversion decay rate,  $\alpha$  is the linewidth enhancement factor of the semiconductor material, and  $\mu$  is the renormalized injection current with  $\mu \approx 0$  at transparency and  $\mu \approx 1$  at lasing threshold. For a device such as the one discussed in Sec. II,  $\mu = 0$  corresponds to 25 mA, and  $\mu = 1$  corresponds to 35 mA, yielding the approximate relation  $I_p \approx (10\mu + 25)$  mA.

Asymmetric linear coupling terms are present in Eqs. (3) and (4) between  $E_{cw}$  and  $E_{ccw}$ , which model a backscattering of power from one mode to the other. Such intrinsic backscattering originates from reflections at the directional coupler or at the chip facets and is, in general, asymmetric due to unavoidable imperfections introduced during device fabrication. Moreover, asymmetries in backscattering introduced externally in our setup (see Fig. 1), such as reflections at the fiber tip at one side of the chip, are also lumped into these coupling terms. The parameters k and  $\phi_k$  represent the average coupling amplitude and phase, respectively, and the coupling asymmetry is described by the symmetry-breaking terms  $\Delta k$  and  $\Delta \phi_k$ . Unless mentioned otherwise, throughout this manuscript we will use the parameters shown in Table I.

Noise terms are introduced in Eqs. (3)–(5) as complex, Gaussian, zero-mean stochastic terms  $\xi_{cw,ccw}$  described by the correlation terms  $\langle \xi_i(t+\tau)\xi_j^*(t)\rangle = 2DN\delta_{ij}\delta(\tau)$ , where  $i, j = \{cw, ccw\}$  and D is the noise intensity [31].

All simulations are performed in this rate-equation model (3)–(5). However, we will interpret our results in a twodimensional phase space corresponding to a reduced MRL TABLE I. Summary of the physical meaning of the parameters in the rate equations (3)–(5) and their typical values used throughout this article, unless stated otherwise.

Symbol	Physical meaning	Simulation value
κ	Field decay rate	$100 \text{ ns}^{-1}$
γ	Carrier inversion decay rate	$0.2 \text{ ns}^{-1}$
α	Linewidth enhancement factor	3.5
$\mu$	Renormalized bias current	1.65
s	Self-saturation coefficient	0.005
с	Cross-saturation coefficient	0.01
k	Coupling amplitude	$0.44 \text{ ns}^{-1}$
$\Delta k$	Coupling amplitude asymmetry	$0.044 \text{ ns}^{-1}$
$\phi_k$	Coupling phase	1.5
$\Delta \phi_k$	Coupling phase asymmetry	0

model that has been proven to be a powerful tool for modeling the slow time dynamics in MRLs [18,22,23,32]. This twodimensional model is valid on time scales slower than those of the relaxation oscillations. The variables  $\theta \in [-\pi/2, \pi/2]$ and  $\psi \in [0, 2\pi]$  are defined by

$$\theta \equiv 2 \arctan\left(\frac{|E_{\rm cw}|}{|E_{\rm ccw}|}\right) - \frac{\pi}{2},$$
 (6a)

$$\psi \equiv \angle E_{\rm ccw} - \angle E_{\rm cw},\tag{6b}$$

where  $\theta$  is a measure for the power partitioning between the counterpropagating modes and  $\psi$  is the phase difference between the corresponding electric fields.

To describe the excitability scenario in MRLs, we consider a ring laser operating unidirectionally, whose symmetry has been slightly broken. The corresponding phase space is shown in Fig. 6.

Two counterpropagating unidirectional stable attractors are present in the MRL, the CW and the CCW modes, and are depicted here in the two-dimensional  $(\theta, \psi)$  phase space. The white and gray regions in Fig. 6 indicate the basins of attraction of the CW and the CCW modes. They are separated by the stable manifolds of a saddle state indicated by S.

The presence of an asymmetry parameter manifests itself in the different stability of the modes, leading to different

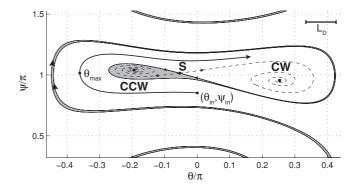


FIG. 6. The phase-space topology of an asymmetric MRL. CW, CCW, and S are two quasiunidirectional states and a saddle state whose stable and unstable manifolds are displayed, respectively. The basin of attraction of the CW (CCW) quasiunidirectional state is white (gray). Parameters are as in Table I.

sizes of their basins of attraction. In particular, the distance between two branches of the stable manifold of S is affected by the symmetry breaking and can be made arbitrarily small by controlling the parameters of the system [22]. When noise is present in the system, a diffusion length scale  $L_D$ appears, which depends on the noise intensity D. The onset of excitability in MRLs is regulated by the interplay between  $L_D$ and the distance between the folds of the stable manifold of S.

Assume that the MRL is operating in a regime such that  $L_D$  is small compared to the size of the basin of attraction of CW and large compared to the distance between the branches of the stable manifold of *S*. The MRL will spend most of the time in the vicinity of the CW stable state; however, a rare large fluctuation may move the system to the boundary of the basin of attraction of CW. When this happens, the system will cross this boundary with an overwhelming probability by crossing *both branches* of the stable manifold of *S* and thereafter will perform a large deterministic excursion leading to the emission of a CCW pulse.

This excitability scenario is different from the one most frequently encountered in optics, where pulses are initiated stochastically by crossing only *one branch* of the stable manifold of a saddle and completed largely deterministically by following a branch of the *unstable* manifold of the same saddle back to the initial quiescent state [9–11,14,16]. Even in the rare situations where the system was shown to be both bistable and excitable at the same time, the excitable excursions were still completed by following the unstable manifold of the saddle point [33]. In MRLs, however, this scenario is forbidden by the residual  $Z_2$  symmetry and the unstable manifold of S, which connects with the metastable CW state [18].

This specific mechanism of excitability is general for all systems with weakly broken Z<sub>2</sub> symmetry and occurs near a homoclinic bifurcation that unfolds from a Takens-Bogdanov point. In that homoclinic bifurcation an unstable cycle is created, which later disappears in a fold of cycles [22]. Such a sequence of bifurcations leads to the folded shape of the stable manifold of the saddle (see Fig. 6), which is necessary for the system to be excitable. The unfolding of the different bifurcations from a Takens-Bogdanov point has been characterized in depth, both in systems with  $Z_2$  symmetry [34,35] and in systems where this symmetry is broken [36]. As an example of other systems that share the same symmetry as the MRL and that can therefore exhibit similar excitable behavior when weakly breaking this symmetry, we mention, e.g., CO<sub>2</sub> lasers [37] and oscillatory convection in binary fluid mixtures [38]. Perhaps the most obvious example with the same circular symmetry as MRLs is semiconductor microdisk lasers [21]. In semiconductor microdisk lasers where the two lasing modes are the whispering gallery modes, the appropriate rate-equation model is identical to the one studied in this work.

# IV. STOCHASTIC ANALYSIS AND COMPARISON TO THE EXPERIMENTS

In this section, we use direct numerical integration of Eqs. (3)–(5) using a stochastic Euler-Heun method to characterize the specific features of excited pulses in MRLs. More specifically, numerical time series are collected, and statistics

of the ISI, the pulse amplitude, and the pulse width are built. A projection of the time series on the reduced phase space  $(\theta, \psi)$  is then performed in order to validate the topological arguments of Sec. III, explaining the spread in amplitude of the pulses and the associated correlated spread in their width, as also observed experimentally (see Figs. 4 and 5).

### A. Pulse amplitude and width

Figure 7 shows the distribution of the phase-space trajectories corresponding to excited pulses. In order to avoid sampling of double pulses, the system is reinitialized to the original CW mode when the tail of the pulse satisfies the condition  $\theta > 0$ . Rare excursions that reside longer than 20 ns around the metastable CCW state are discarded. Figures 7(a) and 7(c) show histograms of the collected trajectories projected on the asymptotically reduced two-dimensional phase space  $(\theta, \psi)$  for two different values of the noise strength *D*. The solid (dashed) white lines indicate the stable (unstable) manifolds of the saddle *S*.

It is clear from Figs. 7(a) and 7(c) that noise-activated trajectories cross the excitability threshold at a finite distance from the saddle *S*. Such saddle avoidance is expected in stochastic systems where  $L_D$  is not the shortest length scale [39], and it is therefore compatible with the mechanism described in Sec. III.

After crossing the stable manifolds of *S*, the trajectories spread in the phase space due to diffusion. A distribution of pulse amplitudes and pulse widths as experimentally observed in Figs. 2 and 4 can therefore be expected in MRLs as the deterministic evolution of the pulse does not take place along a unique trajectory. In the reduced phase space, pulses are a one-parameter family of trajectories that can be parameterized by their initial conditions ( $\theta_{in}$ ,  $\psi_{in}$ ) (see Fig. 6). By fixing

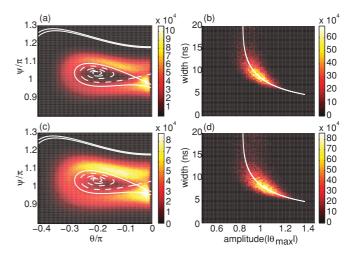


FIG. 7. (Color online) Results of simulations of Eqs. (3)–(5). In (a) and (b)  $D = 1.5 \times 10^{-4} \text{ ns}^{-1}$ ,  $t_{obs} = 100 \text{ ms}$ , and in (c) and (d)  $D = 2.5 \times 10^{-4} \text{ ns}^{-1}$ ,  $t_{obs} = 10 \text{ ms}$ , where D is the noise strength and  $t_{obs}$  is the observation time. (a) and (c) Histogram of the trajectories in asymptotically reduced two-dimensional phase space. The solid (dashed) white lines indicate the stable (unstable) manifolds of the saddle. (b) and (d) Pulse width versus pulse amplitude. The white line indicates the prediction from the deterministic reduced model. Parameters are as in Table I.

 $\theta_{in} = 0$  and  $\psi_{in}$  beyond the excitability separatrix, a sampling of excited pulses is achieved. The width of each pulse can be quantified by the required time to return to the  $\theta > 0$  condition; in the same way, the extreme value  $\theta_{max}$  can be used to quantify the pulse amplitude.

The correlation between amplitude and width can now be understood due to the different velocity fields at different positions in the reduced phase space. Higher (larger  $|\theta|$ ) pulses move faster in phase space and are thus narrower, while lower pulses are slower and consequently also wider. The correlation curves extracted in such a way are plotted in Figs. 7(b) and 7(d) (see the solid white line). The observed increase in pulse width with the decrease in pulse amplitude confirms the experimental trend reported in Sec. II D (see Fig. 5). A projection of the pulses, obtained by numerically solving the stochastic full-rate equation model, in the amplitude-width space [see point cloud in Figs. 7(b) and 7(d)] provides an extra confirmation of this deterministic prediction.

We observe that the theoretical amplitude-width curve is not evenly sampled by the numerical pulses and that the numerical data cluster around a middle value. For this reason, we argue that the full profile of the amplitude-width curve cannot be observed experimentally in our devices. The position of the point cloud in the amplitude-width space is slightly affected by noise. The correlation relation holds for the two different noise strengths, although it is clear that for lower noise strengths [Fig. 7(b)] the pulses tend to be less high in amplitude and thus wider than in the case of higher noise strengths [Fig. 7(d)]. The fact that the point cloud in Figs. 7(b)and 7(d)) opens up for decreasing pulse amplitudes is related to the nature of these pulses. These relatively long pulses tend to wander around the metastable CW state or the saddle point. Near the saddle point the deterministic trajectory greatly slows down. Hence, in this case, the transit times of the pulses are mainly determined by the noise, giving rise to a larger spread.

A more tangible picture is given by considering the width distribution and the amplitude distribution separately, instead of their mutual projection on the two-dimensional  $(\theta, \psi)$  phase plane. These histograms are shown in Fig. 8. The pulse amplitude distribution can be properly fitted by a Gaussian distribution  $A \exp[-(\theta_{\text{max}} - B)^2/C^2]$ , indicating that the amplitude of the pulse is mainly determined by the magnitude of the perturbation and less by the topology of the flow. The average pulse amplitude also increases with increasing noise intensity, initiating excursions farther away from the stable saddle manifold. In contrast, the pulse width distribution is asymmetric. Some of the pulses tend to erratically wander around the CCW state or the saddle, giving rise to the tail in the pulse width distribution. The average pulse width decreases with increasing noise intensity, indicating that the flow near the stable manifold is slower. This also confirms the pulse amplitude-width trade-off trend of Fig. 7. Similar experimental histograms have been shown in Fig. 4. Figure 4(a) shows that the spread in pulse amplitudes is consistent with a Gaussian distribution, while the spread in the width of the pulses in Fig. 4(b) is distributed asymmetrically.

Finally, in Fig. 9 we show typical pulse shapes as the pulse width varies. Figures 9(a)-9(e) show a random collection of pulses with widths in the following intervals: 5–6, 8–9,

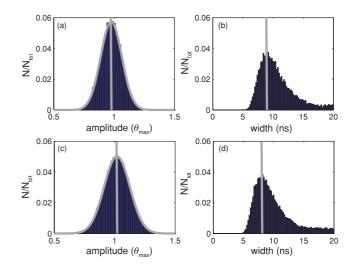


FIG. 8. (Color online) Results of simulations of Eqs. (3)–(5). The histogram of events  $N/N_{\text{tot}}$  is shown (a) and (c) as a function of the pulse amplitudes and (b) and (d) as a function of the pulse widths.  $D = 1.5 \times 10^{-4} \text{ ns}^{-1}$  for (a) and (b), and  $D = 2.5 \times 10^{-4} \text{ ns}^{-1}$  for (c) and (d). The histogram of the pulse amplitudes can be fitted by a Gaussian distribution:  $A \exp\{-[(x - B)/C]^2\}$ . In (a),  $N_{\text{tot}} = 15052$  events, A = 0.0575, B = 0.9762, C = 0.1237. In (c),  $N_{\text{tot}} = 23748$  events, A = 0.0503, B = 1.019, C = 0.1508. The vertical gray lines show the maxima of the histograms: A width of  $\approx 9.20$  ns is found in (b), and a width of  $\approx 7.99$  ns is found in (d). Parameters are as in Table. I.

11-12, 14-15, and 17-18 ns, respectively. The corresponding trajectories in the  $(\theta, \psi)$  phase space are shown in gray. The faster, narrower pulses start out at a relatively large distance from the stable manifold and remain distant from it during the whole pulse trajectory. This is clearly visible in the pulses in Figs. 9(a) and 9(b). Conversely, pulses that start out closer to the stable manifold slow down and are less high. For this type of excursion, if the pulse trajectory comes too close to the stable manifold, it can get tangled up in the metastable CCW state or slowed down near the saddle, explaining the formation of possible plateaus in the pulse. In the case where one gets trapped in the CCW state, the pulse would show a plateau at the pulse maximum, while if the pulse slows down near the saddle, it would exhibit a plateau at the trailing edge of the pulse. In Fig. 9(d), many of the pulses come very close to the saddle point, resulting in an even more pronounced slowdown, especially at the trailing edge of the pulse. Several rare pulse events where the system briefly gets stuck in the CCW state are depicted in Fig. 9(e). Also, pulses that do not get close to the CCW state or the saddle point are characterized by an asymmetric pulse shape. Such asymmetry due to a slowing down of the pulse at the trailing edge (higher values of  $\psi$ ) is best visible in Figs. 9(b) and 9(c).

## B. Interspike-interval diagram

We have also determined the ISI distribution by simulating Eqs. (3)–(5) during a time  $t_{obs} = 10$  ms. The distribution of the ISI between all excited pulses is shown in Fig. 10. We have plotted the logarithm of the normalized number of events  $\ln(N/N_{tot})$  as a function of the interspike interval, where N

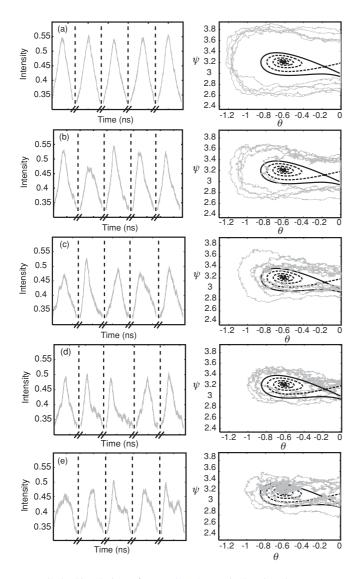


FIG. 9. Simulation of Eqs. (3)–(5). Typical pulse shapes corresponding to different pulse widths are shown. (left) Single pulses are collected from the time traces, and (right) the corresponding trajectory in the  $(\theta, \psi)$  phase space is shown in gray. Stable (solid lines) and unstable (dashed lines) manifolds are in black. From (a) to (e), pulses are shown with widths in the following intervals: 5–6, 8–9, 11–12, 14–15, and 17–18 ns.  $D = 2.5 \times 10^{-4} \text{ ns}^{-1}$ , and the other parameters are as in Table. I.

is the total amount of events in each bin and  $N_{\text{tot}}$  is the total amount of excited pulses.

In Fig. 10(a), we have set  $\mu = 1.65$  and  $D = 2.5 \times 10^{-4}$  ns<sup>-1</sup>, corresponding to the parameter set used in Figs. 7–9. The bin size has been chosen to be 1 ns. It becomes evident from Fig. 10(a) that the total ISI distribution is the combination of two different time scales. The short ISIs and long ISIs are distributed in a different way and together represent a strong Kramers type of behavior.

The slow time scale can be fitted by an exponential curve  $[\propto \exp(-t/T_1)]$ , where the average ISI  $(T_1)$  is the fitting parameter. This slow time scale  $T_1$  is typically of the order of  $\mu$ s and corresponds to the generation of the pulses in a Kramers-type noise-activation process across the

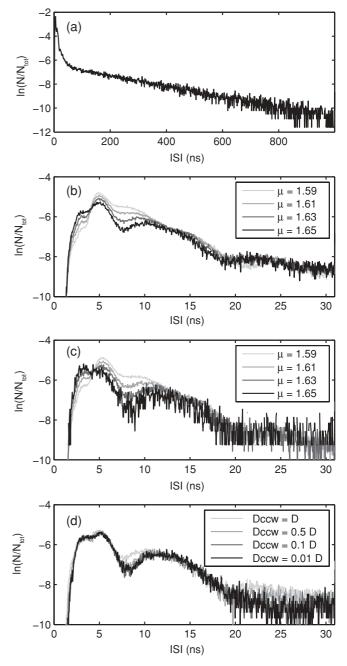


FIG. 10. Simulation of Eqs. (3)–(5) for 10 ms, showing the interspike-interval diagram.  $\ln(N/N_{tot})$  is plotted as a function of the interspike interval. In (a)  $\mu = 1.65$ ,  $D = 2.5 \times 10^{-4} \text{ ns}^{-1}$ , and the bin size is chosen to be 1 ns. In (b)–(d), a zoom of the peak at shorter ISI is shown with a bin size of 0.05 ns. (b) and (c) show the variation of the ISI with  $\mu$  for  $D = 2.5 \times 10^{-4} \text{ ns}^{-1}$  and  $D = 1.5 \times 10^{-4} \text{ ns}^{-1}$ , respectively. (d) demonstrates the change in ISI for asymmetric noise contributions to the CW ( $D_{cw} = D$ ) and the CCW ( $D_{ccw}$ ) modes for  $\mu = 1.65$ . The other parameters are as in Table. I.

excitability threshold [26]. The short ISI times, however, are a signature of multiple consecutive excited pulses due to noise clustering. The possible excitation of double pulses such as those experimentally shown in Fig. 2(c) depends on the closeness of the stable and unstable manifolds of the saddle S. When these are close enough, noise can excite a second pulse before the system can relax to the quiescent state. The presence of such excited multipulses will show up in the ISI distribution as a sharp peak around the average pulse width. The numerical results in Fig. 10(a) confirm the experimental observation of both time scales in the experimental ISI distribution presented in Sec. II (see Fig. 3).

The presence of these time scales was also found in our study of stochastic mode hopping in the bistable regime in Refs. [23,27,32]. Both a mode hop in the bistable regime and an excitation beyond the excitability threshold are described by a noise-activated escape, corresponding to the slow Arrhenius time scale. The fast non-Arrhenius character of the ISI originates in a noise-induced diffusion through both branches of the stable manifold, thus initiating another excursion in phase space before relaxing to the CW state. Such a noise clustering of pulses due to the proximity of the relaxation trajectory of the excited pulse and the excitability threshold has been observed in several other noise-driven excitable systems, such as lasers with optical feedback [24,25], quantum-dot lasers with optical injection [28,40], and neurons of the Hodgkin-Huxley type [41].

In Figs. 10(b)-10(d), we study in more detail the ISI distribution of the faster time scale for different values of the pump current  $\mu$ , the noise strength D, and asymmetric contributions of the noise to both counterpropagating modes. The bin size is taken to be 0.05 ns. Figures 10(b) and 10(c)show the ISI distribution for varying values of the current  $\mu$  at a fixed noise strength  $D = 2.5 \times 10^{-4} \text{ ns}^{-1}$  and D = $1.5 \times 10^{-4}$  ns<sup>-1</sup>, respectively. One can see that in all cases the maximum number of events is located around 5 ns, which corresponds roughly to half of an excitable excursion [42]. For slightly higher ISI (5 - 10 ns) a dip in the ISI distribution is observed. Such a dip is typical for noise clustering [24,41] and is due to the nature of the relaxation trajectory of the excited pulse. In particular, it becomes evident from Figs. 10(b) and 10(c) that the dip becomes less pronounced for decreasing values of the current  $\mu$  because the relaxation to the stable node occurs increasingly slowly for lower values of  $\mu$ . One can also see that the entire ISI curve moves up for decreasing  $\mu$ , which is a logical consequence of the decreasing depth of the potential well. It is interesting to note that the basin of attraction of the metastable CCW state decreases when decreasing  $\mu$ . In fact, similar excited pulses and ISI distribution still hold for  $\mu = 1.59$  when the saddle and the metastable CCW state have disappeared. This can be explained by the fact that such dynamics arise as a scar of the bifurcations nearby [24].

All of the previous theoretical analysis has been done for the stochastic rate-equation system (3)–(5), where for reasons of simplicity the noise terms have been added in a symmetric way to both counterpropagating modes. From the experimental

setup explained in Sec. II, one can wonder whether this symmetric assumption is valid as noise coming from the external SOA is injected mainly in one direction (the stable CW state). In order to check the validity of such an assumption, we have checked our analysis for asymmetric noise contributions, introducing noise with strength  $D_{cw} = D$  in Eq. (3) for the stable CW mode and noise with strength  $D_{ccw} < D$  in Eq. (4) for the metastable CCW mode. Qualitatively similar results are obtained as presented throughout this paper, which is reflected in Fig. 10(d), which shows the ISI distribution for  $\mu = 1.65$ ,  $D_{cw} = D = 2.5 \times 10^{-4}$  ns<sup>-1</sup>, and different values of  $D_{ccw}$ .

# V. DISCUSSION AND CONCLUSION

In conclusion, we have investigated the features of excitability in optical systems that are close to  $Z_2$  symmetry and have elucidated the differences with other, more common, excitability scenarios [9–16,24,28]. The key message of this paper is the experimental and theoretical observation of a spread of the pulse amplitude and width in MRLs in the presence of noise, where a correlation between the amplitude and width of the excited pulses has been observed. Such a correlation between these two quantities is the signature of the deterministic evolution of the system once the separatrix is crossed. Multipulse excitability [24] is also present due to the finiteness of the noise intensity and the relaxation to the quiescent state being slow due to the closeness to a homoclinic bifurcation in parameter space.

For a realization of an all-optical neural network based on MRLs, such a pulse width distribution can present a drawback compared to other excitable systems. However, such a drawback is eventually balanced by the easy integrability of MRLs on an optical chip and the possibility of controlling the coupling between the ring cavity and waveguide [43]. Furthermore, excitability in MRLs does not require feedback from an external cavity or optical injection from a master laser, as in the case of other optical systems.

### ACKNOWLEDGMENTS

This work has been partially funded by the European Union under Project No. IST-2005-34743 (IOLOS). This work was supported by the Belgian Science Policy Office Grant No. IAP-VI10. We acknowledge the Research Foundation-Flanders (FWO) for individual support and project funding. Furthermore, we thank Gabor Mezosi and Marc Sorel for fabricating the semiconductor ring lasers on which the experiments have been performed, and we thank Ingo Fischer for interesting discussions.

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