<sup>21</sup>H. S. Green, J. Chem. Phys. <u>19</u>, 955 (1951). <sup>22</sup> $\lambda^3 G(\mathbf{\vec{r}}, \mathbf{\vec{r}}; \beta)$  (to first order in  $\lambda$ ) has previously been calculated by Nilsen (Ref. 16) and (to first order in  $\beta \epsilon$ ) Edwards (Ref. 18). However their results are expressed in a form which is not very suitable for our purposes. <sup>23</sup> $\alpha$  D. Which is not very suitable for our purposes.

<sup>23</sup>G. E. Uhlenbeck and E. Beth, Physica <u>3</u>, 729 (1936); R. A. Handelsman and J. B. Keller, Phys. Rev. <u>148</u>,

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## Low-Frequency Electric Microfield Distributions in a Plasma Containing Multiply Charged Ions\*†

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A theory for calculating low-frequency component electric microfield distributions for a plasma containing more than a single ion species is developed. Calculations at a charged point are made for a plasma containing  $N^*$  singly charged ions and  $N^{**}$  doubly charged ions together with a charge neutralizing number of electrons,  $N_e(N_e = N^* + 2N^{**})$ . Three different ion ratios  $(R \equiv N^{**}/N^*)$  are treated:  $R = 0.0, 1.0, \infty$ . It is shown that the calculations allow for all ion-ion correlations to a high degree of accuracy. Numerical results are shown both graphically and in tabulated form.

## I. INTRODUCTION

In recent years considerable effort has been devoted to the problem of spectral line broadening in plasmas.<sup>1-3</sup> In relation to this problem various theories of the static electric microfield distributions have been formulated.<sup>4,5</sup> However, all of these theories and subsequent calculations have only been concerned with plasmas containing a single positiveion species. The purpose of this paper is to extend the theory developed by one of us to treat plasmas containing more than a single species of positive ion. Calculations for a plasma containing two positive-ion components have been made; the procedure for extending the calculations to situations with more than two species is indicated.

In this paper, calculations are made for a plasma that contains  $N^*$  singly charged ions and  $N^{**}$  doubly charged ions  $(N = N^* + N^{**})$  together with a charge neutralizing number of electrons  $N_e(N_e = N^* + 2N^{**})$ . It is assumed that ions interact with each other through an effective potential which includes electron-ion shielding. This model is the two-component analog of the single-component low-frequency model previously developed.<sup>4,5</sup> Since helium plasmas may have both singly and doubly charged species present, the model proposed here is appropriate for discussing the effect of a helium plasma on a radiating He<sup>\*</sup> ion (He<sup>\*</sup> = He II) or He atom. As in the papers dealing with singly charged perturbing ions, the calculation of the electric-microfield distribution at a neutral point (e.g., at a He atom) is just a special case of the charged-point development obtained by setting the charge at the origin equal to zero.

94 (1966); P. C. Hemmer and K. J. Mork, ibid. 158,

<sup>24</sup>Reference 7. This method is also used in Refs. 5

<sup>25</sup>The  $\delta$ -function expansion is given by H. Messel and

H. S. Green, Phys. Rev. 87, 738 (1952).

To make the mathematical development more general, we make the assumption that it is valid to consider a two-temperature plasma, one temperature for the ions,  $T_i$  and one for the electrons  $T_e$ . This procedure implies that while the ions may be considered to be in equilibrium with each other, and the electrons with each other, that the ions are not necessarily in equilibrium with the electrons. In the event that a true equilibrium situation prevails,  $T_e = T_i$ .

All numerical results presented here assume an equilibrium situation. The actual distribution functions are expressed in reduced field units which are a function of electron density only. The calculational programs that we have developed are quite general; they allow for the possibility of a twotemperature plasma, for the possibility that there may be any number of charged-ion perturber species (i.e., singly, doubly, etc.), and for the possibility that the radiator may have any degree of ionization.

Section II of this paper deals with the formal calculations. The asymptotic expressions for the microfield distribution function are presented in Sec. III. Numerical results and conclusions are given in Sec. IV. An appendix is devoted to the detailed evaluation of various integral expressions by collective coordinate techniques.

## **II. FORMALISM**

Define  $Q(\vec{\epsilon})d\vec{\epsilon}$  as the probability of finding an electric field  $\vec{\epsilon}$  at the origin of our reference system due to a collection of N ions  $(N^* + N^{**} + \cdots)$  assumed to interact with each other through shielded Coulomb potentials. The plasma is contained in a volume V and is macroscopically neutral. The origin is assigned a charge q defined by

$$q \equiv \xi e, \quad \xi = 0, 1, 2, \dots$$
 (1)

where e is the magnitude of the electronic charge. By choosing the appropriate value of  $\xi$ , expressions for microfield distributions at neutral or variously charged radiators are obtained.

The definition of the microfield distribution function,  $Q(\vec{\epsilon})$  is given by

$$Q(\vec{\epsilon}) = Z^{-1} \int \cdots \int \exp[-\beta V(\vec{r}_1 \cdots \vec{r}_N)]$$
$$\times \delta(\vec{\epsilon} - \sum_j \vec{\epsilon}_j) \prod_{j=1}^N d\vec{r}_j, \quad \beta = \frac{1}{\theta_i} = \frac{1}{kT_i} \quad (2)$$

where Z is the configurational partition function for the two- (or multi-) component system, and  $V(\vec{\mathbf{r}}_1 \cdots \vec{\mathbf{r}}_N)$  is the total potential of interaction between ions.  $\vec{\boldsymbol{\epsilon}}_i$  is the field at the origin due to the *i*th ion that is located at  $\vec{\mathbf{r}}_i$ :

$$\vec{\epsilon}_i = q^{-1} \nabla_{\vec{r}_i} V(\vec{r}_1 \cdots \vec{r}_N) .$$
(3)

Note that because the field point is at the origin and the source at  $\vec{r}_i$ , the sign of the gradient in this last expression differs from that in the usual relation. The sum  $\sum_i \vec{\epsilon}_i$  is given by

$$\sum_{j=1}^{N} \overleftarrow{\epsilon}_{i} = \sum_{j=1}^{N^{+}} \overleftarrow{\epsilon}_{j} + \sum_{m=1}^{N^{++}} \overleftarrow{\epsilon}_{m} .$$
(4)

The integrations in Eq. (2) are over the coordinates of all the ions.

By representing the  $\delta$  function as an integral

$$\delta(\mathbf{x}) = (2\pi)^{-3} \int \int \int \exp[i\mathbf{\hat{1}}\cdot\mathbf{x}] d\mathbf{\hat{1}}, \qquad (5)$$

we may write

$$Q(\vec{\epsilon}) = Z^{-1} \int \cdots \int (2\pi)^{-3} \\ \times \exp\left[-\beta V + i\vec{1} \cdot (\vec{\epsilon} - \sum_i \vec{\epsilon}_i)\right] d\vec{1} \prod_j d\vec{r}_j . (6)$$

Since  $\sum_{j} \vec{1} \cdot \vec{\epsilon}_{j}$  is independent of the direction of  $\vec{1}$ , the angular integrations can be done immediately. The result is the commonly occurring expression for  $P(\epsilon)$  for an isotropic system<sup>4,5</sup>:

$$P(\epsilon) = 4\pi\epsilon^2 Q(\epsilon) = 2\epsilon(\pi)^{-1} \int_0^\infty T(l) \sin(\epsilon l) l \, dl \,, \quad (7)$$

where T(l) is defined by

$$T(l) = Z^{-1} \int \cdots \int \exp[-\beta V - i \sum_j \vec{1} \cdot \vec{\epsilon}_j] \prod_j d\vec{r}_j . \quad (8)$$

The potential energy in the present calculation is

$$V = \sum_{i < j}^{N} \frac{e^2}{r_{ij}} e^{-r_{ij}/\lambda} + \sum_{m < n} \frac{(2e)^2}{r_{mn}} e^{-r_{mn}/\lambda} + \sum_{j,m} \frac{2e^2}{r_{jm}} e^{-r_{jm}/\lambda}, \quad (9)$$

where

$$\lambda = [(kT_e/4\pi n_e e^2)]^{1/2}$$

The subscripts *i*, *j* are reserved for the  $N^*$  ions and the subscripts *m*, *n* are reserved for the  $N^{**}$ ions. It is convenient at this point to define the new quantities  $w_{j0}$ ,  $w_{m0}$ , and  $V_0$ :

$$w_{j0} = q(e/r_{j0}) e^{-\alpha r_{j0}/\lambda} , \qquad (10a)$$

$$w_{m0} = q(2e/r_{m0}) e^{-\alpha r_{m0}/\lambda}$$
, (10b)

$$V \equiv V_0 + \sum_{j=1}^{N^+} w_{j0} + \sum_{m=1}^{N^{++}} w_{m0}$$
 (11)

The w's will take into account the short-range central interactions.  $V_0$  includes all noncentral and long-range interactions.  $\alpha$  is an effective range parameter, the choice of which will be considered later. In terms of the form for the potential energy given in Eq. (11), T(l) can be written

$$T(l) = Z^{-1} \int \cdots \int e^{\tilde{v}_0} \prod_{j}^{N^*} \exp[-\beta w_{j0} - iq^{-1}\vec{1} \cdot \vec{\nabla}_0 w_{j0}] d\vec{r}_j$$
$$\times \prod_{m}^{N^{*+}} \exp[-\beta w_{m0} - iq^{-1}\vec{1} \cdot \vec{\nabla}_0 w_{m0}] d\vec{r}_m, \quad (12)$$

where

$$\vec{V}_0 = -\beta V_0 - iq^{-1}\vec{1} \cdot \vec{\nabla}_0 V_0 .$$
 (12a)

The following definitions can also be made and then substituted into the expression for T(l):

$$\chi^{*}(l,j) \equiv \exp[-\beta w_{j0} - iq^{-1}\vec{1} \cdot \vec{\nabla}_{0} w_{j0}] - 1 , \qquad (13a)$$

$$\chi^{**}(l,m) \equiv \exp[-\beta w_{m0} - i q^{-1} \vec{1} \cdot \vec{\nabla}_0 w_{m0}] - 1 .$$
(13b)

Hence,

$$T(l) = Z^{-1} \int \cdots \int e^{\tilde{\mathbf{v}}_0} \prod_{j}^{N^*} [1 + \chi^*(l, j)] d\mathbf{\dot{r}}_j$$
$$\times \prod_{m}^{N^{**}} [1 + \chi^{**}(l, m)] d\mathbf{\dot{r}}_m . \qquad (14)$$

If the factors in T(l) containing the  $\chi$ 's are multiplied out, the following expression is obtained:

$$T(l) = Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \left( 1 + \sum_{j}^{N^{*}} \chi^{*}(l,j) + \sum_{m}^{M^{*}} \chi^{**}(l,m) + \sum_{i < j} \chi^{*}(l,j) \chi^{*}(l,i) + \sum_{m < j} \chi^{*}(l,m) \chi^{*}(l,m) \right) + \sum_{j < m} \sum_{m} \chi^{*}(l,j) \chi^{*}(l,j) \chi^{**}(l,m) + \cdots \right) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad (15a)$$

$$= Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} + N^{*} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} dr_{j}$$

$$+ N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{*}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m}$$

$$+ \frac{1}{2} N^{*} (N^{*} - 1) Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{*}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m}$$

$$+ \frac{1}{2} N^{**} (N^{*+} - 1) Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{**}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{**} Z^{-1} \int \cdots \int e^{\tilde{v}_{0}} \chi^{*}(l,1) \chi^{**}(l,2) \prod_{j} d\tilde{\mathbf{r}}_{j} \prod_{m} d\tilde{\mathbf{r}}_{m} \quad M^{*} N^{*} N^{*}$$

Now make the following two definitions:

$$T_{jm}(l) \equiv \int \cdots \int e^{\vec{v}_0} \prod_{i=j+1}^{N^*} d\vec{r}_i \prod_{n=m+1}^{N^{*+}} d\vec{r}_n ,$$

$$Q_{jm}(l) \equiv T_{jm}(l) / T_0(l) ,$$
(16)

where  $T_0(l) \equiv T_{00}(l)$ . In terms of these new quantities T(l) can be written

 $T(l) = T_0(l)Z^{-1} \left[ 1 + N^+ \int Q_{10}(l)\chi^*(l, 1)d\vec{\mathbf{r}}_1 + N^{**} \int Q_{01}(l)\chi^{**}(l, 1)d\vec{\mathbf{r}}_1 + (1/2!)N^*(N^* - 1) \right]$ 

 $\times \int \int Q_{20}(l)\chi^{*}(l,1)\chi^{*}(l,2)d\mathbf{\tilde{r}_{1}}d\mathbf{\tilde{r}_{2}} + (1/2!)N^{**}(N^{**}-1) \int \int Q_{02}(l)\chi^{**}(l,1)\chi^{**}(l,2)d\mathbf{\tilde{r}_{1}} d\mathbf{\tilde{r}_{2}}$ 

$$+ N^* N^{**} \int \int Q_{11}(l) \chi^*(l, 1) \chi^{**}(l, 2) d\vec{\mathbf{r}}_1 d\vec{\mathbf{r}}_2 + \cdots ] . \quad (17)$$

Each of the Q's can be expanded in an Ursell expansion according to the following prescription:

$$\begin{split} & \forall \ Q_{10}(l\,;\,1) = g_{10}(l\,;\,1) \ , \\ & \forall \ Q_{01}(l\,;\,1) = g_{01}(l\,;\,1) \ , \\ & \forall^2 \ Q_{20}(l\,;\,1,\,2) = g_{10}(l\,;\,1)g_{10}(l\,;\,2) + g_{20}(l\,;\,1,\,2), \end{split}$$

 $\mathcal{U}^2 Q_{02}(l; 1, 2) = g_{01}(l; 1)g_{01}(l; 2) + g_{02}(l; 1, 2)$ ,

 $\mathcal{U}^2 Q_{11}(l; 1, 2) = g_{10}(l; 1)g_{01}(l; 2) + g_{11}(l; 1, 2)$ . (18)

In terms of these g's and in the thermodynamic limit  $(N \rightarrow \infty, \mathfrak{V} \rightarrow \infty$  so that the density  $n = N/\mathfrak{V}$  remains constant, T(l) is given by

 $T(l) = T_0(l)Z^{-1} \{ 1 + n^* \int g_{10}(l; 1)\chi^*(l; 1)d\vec{r}_1 + n^{**} \int g_{01}(l; 1)\chi^{**}(l; 1)d\vec{r}_1 \}$ 

+ 
$$[(n^{+})^{2}/2!] [\int \int g_{20}(l; 1, 2)\chi^{+}(l, 2)\chi^{+}(l; 2)d\vec{r}_{1}d\vec{r}_{2} + (\int g_{10}(l, 1)\chi^{+}(l, 1)d\vec{r}_{1})^{2}]$$

+ [ $(n^*)^2/2!$ ][ $\int \int g_{02}(l; 1, 2)\chi^{**}(l, 2)d\vec{r_1}d\vec{r_2} + (\int g_{01}(l, 1)\chi^{**}(l, 1)d\vec{r_1})^2$ ]

$$+n^{*}n^{**}\left[\int\int g_{11}(l;1,2)\chi^{*}(l,1)\chi^{**}(l,2)\,d\vec{\mathbf{r}}_{1}d\vec{\mathbf{r}}_{2}+\left(\int g_{10}(l,1)\chi^{*}(l,1)\,d\vec{\mathbf{r}}_{1}\right)\times\left(\int g_{01}(l,2)\chi^{**}(l,2)\,d\vec{\mathbf{r}}_{2}\right)\right]+\cdots\}.$$
 (19)

If  $h_{jm}$  is defined by

$$h_{jm}(l) \equiv \int \cdots \int g_{jm}(l) \chi^{*}(l, 1) \cdots \chi^{*}(l, j) \chi^{**}(l, 1)$$
$$\times \dots \chi(l, m) \prod_{i=1}^{j} d\vec{\mathbf{r}}_{i} \prod_{n=1}^{m} d\vec{\mathbf{r}}_{n}, \quad (20)$$

T(l) can be written in terms of these h's as

$$T(l) = T_{0}(l)Z^{-1} \left\{ 1 + n^{+}h_{10}(l) + n^{++}h_{01}(l) + \left[ (n^{+})^{2}/2! \right] \left[ h_{20}(l) + \left[ h_{10}(l) \right]^{2} \right] + \left[ (n^{++})^{2}/2! \right] \left[ h_{02}(l) + \left[ h_{01}(l) \right]^{2} \right] + n^{+}n^{++} \left[ h_{11}(l) + h_{10}(l)h_{01}(l) \right] + \cdots \right\}.$$
 (21)

These terms can be regrouped and written in the form

$$T(l) = T_0(l)Z^{-1} \exp\left(\sum_{j}^{N^+} \sum_{m}^{N^{++}} \frac{(n^+)^j}{j!} \frac{(n^{++})^m}{m!} h_{jm}(l)\right),$$
(22)

which is a systematic Ursell cluster expansion.

It can be noted here that the definition of Z would be the same as T(l), if l were set equal to zero. Therefore Z can be written as

$$Z = T_0(0) \exp\left(\sum_{j=m}^{N^*} \sum_{m=m}^{N^{**}} \frac{(n^*)^j (n^{**})^m}{j! m!} h_{jm}(0)\right), \quad (23)$$

This allows T(l) to be written as

$$T(l) = \left(\frac{T_0(l)}{T_0(0)}\right) \times \exp\left(\sum_{j}^{N^*} \sum_{m}^{N^{**}} \frac{(n^*)^j (n^{**})^m}{j! m!} \left[h_{jm}(l) - h_{jm}(0)\right]\right) . (24)$$

If more than two species of perturbing ions are to be considered, Eq. (24) can be generalized:

$$T(l) = \left(\frac{T_0(l)}{T_0(0)}\right) \exp\left(\sum_j \cdots \sum_k \cdots \sum_m \frac{(n)! \dots (n)! \dots (n)!}{j! \dots k! \dots m!} \left[h_{j..k..m}(l) - h_{j..k..m.}(0)\right]\right) .$$
(25)

This allows for any number of perturbing species. The procedure for the evaluation of these terms would be similar to that presented in the Appendix.

Since the calculation of  $P(\epsilon)$  considered in this paper always involves a computer calculation, it should be pointed out that the cost of evaluating these terms is considerable.

Consider the individual terms appearing in Eq. (24). By the method developed in the Appendix, the first factor,  $T_0(l)/T_0(0)$ , becomes

$$T_0(l)/T_0(0) = e^{-\gamma L^2} .$$
 (26)

In Eq. (26),

$$\gamma = \frac{1}{4} \alpha (\theta_{i} / \theta_{e}) \left[ \alpha^{2} - (1+u) \right]^{2} \left\{ \right\}, \qquad (26a)$$

$$\left\{ \right\} = \left\{ \alpha^{5} u + 2 \left[ 1 - (1+u)^{3/2} \right] \alpha^{4} + \left[ 2u + u^{2} \right] \alpha^{3} - 4(1+u) \left[ 1 - (1+u)^{1/2} \right] \alpha^{2} - 3(u+u^{2}) \alpha + 2 \left[ (1+u)^{2} - (1+u)^{3/2} \right] \right\},$$

$$u = \frac{\theta_e}{\theta_i} \left(\frac{1+4R}{1+2R}\right) , \quad R \equiv \frac{n^{**}}{n^*} ,$$
  

$$\theta_e \equiv k T_e , \quad \theta_i \equiv k T_i ,$$
  

$$L \equiv \epsilon_0 l , \quad a \equiv r_0 / \lambda , \quad \epsilon_0 \equiv e / r_0^2 ,$$
(26b)

where  $r_0$  is the ion-sphere radius defined by the expression

$$\frac{4}{3}\pi r_0^3 n_e = 1 . (26c)$$

Now we consider the factors resulting from the series exponent. There are two first-order terms, one for j = 1 and m = 0 and one for j = 0 and m = 1. In general, if there are r different species of perturbing ions, there will be r such first-order terms:

$$I_{10} = n^{+} [h_{10}(l) - h_{10}(0)] = n^{+} \mathcal{O} \int \left( \frac{\int \cdots \int e^{-\beta V_{0} \cdot i q^{-1} l \cdot \vec{\nabla}_{0} V_{0}} (e^{-\beta w_{10} - i q^{-1} l \cdot \vec{\nabla}_{0} w_{10} - 1)}{\int \cdots \int \exp(-\beta V_{0} - i q^{-1} l \cdot \vec{\nabla}_{0} V_{0}) \prod_{1}^{n^{+}} d\vec{r}_{i} \prod_{1}^{n^{++}} d\vec{r}_{n}} - \frac{\int \cdots \int e^{-\beta V_{0} \cdot i q^{-1} l \cdot \vec{\nabla}_{0} V_{0}}{\int \cdots \int e^{-\beta V_{0} \cdot i q^{-1} l \cdot \vec{\nabla}_{0} V_{0}} (e^{-\beta i w_{10} - 1)} \prod_{1}^{n^{+}} d\vec{r}_{j} \prod_{1}^{n^{++}} d\vec{r}_{n}}{\int \cdots \int e^{-\beta V_{0}} \prod_{1}^{n^{+}} d\vec{r}_{j} \prod_{1}^{n^{++}} d\vec{r}_{n}} \right)} d\vec{r}_{1} , \quad (27)$$

and similarly,

$$I_{01} = n^{**} \left[ h_{01}(l) - h_{01}(0) \right]$$

$$= n^{**} \upsilon \int \left( \frac{\int \cdots \int e^{-\beta v_0 - iq^{-1} \vec{1} \cdot \vec{\nabla}_0 v_0} (e^{-\beta w_{10} - iq^{-1} \vec{1} \cdot \vec{\nabla}_0 w_{10} - 1) \prod_{1}^{N^+} d\vec{r}_j \prod_{2}^{N^{*+}} d\vec{r}_m}{\int \cdots \int e^{-\beta v_0} \prod_{1}^{N^+} d\vec{r}_j \prod_{1}^{N^{*+}} d\vec{r}_m} - \frac{\int \cdots \int e^{-\beta v_0 - iq^{-1} \vec{1} \cdot \vec{\nabla}_0 v_0} (e^{-\beta i w_{10} - 1) \prod_{1}^{N^+} d\vec{r}_j \prod_{1}^{N^{*+}} d\vec{r}_m}{\int \cdots \int e^{-\beta v_0} \prod_{1}^{N^+} d\vec{r}_j \prod_{1}^{N^{*+}} d\vec{r}_m} \right) d\vec{r}_1 . \quad (28)$$

Although these integrals appear formidable, they may be readily reduced through the use of collective coordinates to approximate expressions involving only one-dimensional integrals. The accuracy of this approximation is briefly discussed later and has been extensively discussed elsewhere.<sup>5</sup> Collective coordinates are defined and the nature of the evaluation indicated in the Appendix. The final results are merely stated here:

$$I_{10}(l) = n^{*} [h_{10}(l) - h_{10}(0)]$$
  
=  $\frac{3}{1 + 2R} \int_{0}^{\infty} x^{2} dx e^{s(x)} \left[ e^{-\beta w_{10}} \left( \frac{\sin(LG(x))}{(LG(x))} - 1 \right) - \left( \frac{\sin(Lq(x))}{(Lq(x))} - 1 \right) \right]$  (29)

and

 $I_{01} = n^{**} [h_{01}(l) - h_{01}(0)]$ =  $\frac{3R}{1+2R} \int_0^\infty x^2 dx e^{2s(x)} \left[ e^{-2\beta w_{10}} \left( \frac{\sin(2LG(x))}{(2LG(x))} \right) \right]$ 

$$x = r/r_0, \quad \beta w_{10} = \xi \left(\frac{\theta_c}{\theta_i}\right) \left(\frac{a^2}{3x}\right) e^{-\alpha ax},$$
$$s(x) = \xi \frac{ua^2}{3x} \left(\frac{1+2R}{1+4R}\right) \left(\frac{\alpha^2-1}{\alpha^2-(1+u)}\right)$$

$$\times (e^{-\alpha ax} - e^{(1+u)^{1/2}ax}),$$
(30a)
$$q(x) = -\left(\frac{\alpha^2 - 1}{\alpha^2 - (1+u)}\right) \left(\frac{1}{x^2} (e^{-\alpha ax} - e^{-(1+u)^{1/2}ax}) + \frac{a}{x} (\alpha e^{-\alpha ax} - (1+u)^{1/2} e^{-(1+u)^{1/2}ax})\right),$$

 $-\left(\frac{\sin(2Lq(x))}{(2Lq(x))}-1\right)\right], \quad (30)$ 

 $G(x) = q(x) + (e^{-\alpha ax}/x^2)(1 + \alpha ax)$ .

The second-order terms appearing in the series exponent are now given explicitly:

 $I_{20}(l) = \left[ (n^{+})^{2}/2! \right] \left[ h_{20}(l) - h_{30}(0) \right]$ 

 $= \left[ (n^*)^2 / 2! \right] \left\{ \mathcal{V}^2 \int \int \left[ Q_{20}(l, 1, 2) - Q_{10}(l, 1) Q_{10}(l, 2) \right] \chi^*(l, 1) \chi^*(l, 2) d\vec{\mathbf{r}}_1 d\vec{\mathbf{r}}_2 \right\}$ 

$$-\upsilon^{2} \int \int \left[ Q_{20}(0,1,2) - Q_{10}(0,1) Q_{10}(0,2) \right] \chi^{\dagger}(0,1) \chi^{\dagger}(0,2) \, d\vec{\mathbf{r}}_{1} \, d\vec{\mathbf{r}}_{2} \right\} \,. \tag{31}$$

When the  $Q_{20}(l)$  and  $Q_{20}(0)$  functions are evaluated by the methods presented in the Appendix, they have a very interesting form. Equation (A52) gives for  $Q_{20}(l)$ 

$$Q_{20}(l,1,2) = Q_{10}(l,1)Q_{10}(l,2) \exp\left(-\frac{\theta_e}{\theta_i} \frac{a^2}{3x_{12}} e^{-(1+u)^{1/2}ax_2}\right) .$$
(32)

The expression appearing in large parentheses is the Debye-Hückel pair-correlation function (see Ref. 5) for a discussion of this point). Performing the complete collective-coordinate evaluation, as indicated in the Appendix, we find

$$I_{20} = \frac{\theta_{e}}{\theta_{i}} \left(\frac{1}{1+2R}\right)^{2} 3a^{2} \sum_{k} (-1)^{k} (2k+1) \left\{20\right\},$$

$$\left\{20\right\} = \left(\int_{0}^{\infty} x_{2}^{3/2} I_{k+1/2} \left(a'x_{2}\right) e^{s(x_{2})} \left[e^{-\beta_{i}w(x_{2})} j_{k}(LG(x_{2})) - j_{k}(Lq(x_{2}))\right]\right)$$

$$\times \int_{x_{2}}^{\infty} x_{1}^{3/2} K_{k+1/2} \left(a'x_{1}\right) e^{s(x)} \left[e^{-\beta_{i}w(x_{1})} j_{k}(LG(x_{1})) - j_{k}(Lq(x_{1}))\right] dx_{1} dx_{2}$$

$$- \delta_{ko} \int_{0}^{\infty} x_{2}^{3/2} I_{1/2} (a'x_{2}) e^{s(x_{2})} \left[e^{-\beta_{i}w(x_{2})} - 1\right] \int_{x_{2}}^{\infty} x_{1}^{3/2} K_{1/2} (a'x_{1}) e^{s(x_{1})} \left[e^{-\beta_{i}w(x_{1})} - 1\right] dx_{1} dx_{2}\right).$$

$$(33)$$

Similarly an expression for  $I_{02}$  is given by

$$I_{02} = 4 \frac{\theta_{e}}{\theta_{i}} \left(\frac{R}{1+2R}\right)^{2} 3a^{2} \sum_{k} (-1)^{k} (2k+1) \{02\}, \qquad (34)$$

$$\{02\} = \int_{0}^{\infty} x_{2}^{3/2} I_{k+1/2} (a' x_{2}) e^{2s(x_{2})} [e^{-2\beta_{W}(x_{2})} j_{k} (2LG(x_{2})) - j_{k} (Lq(x_{2}))]$$

$$\times \int_{x_{2}}^{\infty} x_{1}^{3/2} K_{k+1/2} (a' x_{1}) e^{2s(x_{1})} [e^{-2\beta_{i} w(x_{1})} j_{k} (2LG(x_{1})) - j_{k} (2Lq(x_{1}))] dx_{1} dx_{2}$$

$$- \delta_{ko} \int_{0}^{\infty} x_{2}^{3/2} I_{1/2} (a' x_{2}) e^{2s(x_{2})} [e^{-2\beta_{i} w(x_{2})} - 1] \int_{x_{2}}^{\infty} x_{1}^{3/2} K_{1/2} (a' x_{1}) e^{2s(x_{1})} [e^{-2\beta_{w}(x_{1})} - 1] dx_{1} dx_{2}.$$

There is yet another second-order term, viz.,  $I_{11}$ ; it is given by

$$I_{11} = 2 \frac{\theta_{q}}{\theta_{t}} \left( \frac{1}{1+2R} \right) \left( \frac{R}{1+2R} \right) 3d^{2} \sum_{k} (-1)^{k} (2k+1) \{ 11 \},$$

$$\{11\} = \left( \int_{0}^{\infty} x_{2}^{3/2} I_{k+1/2} (a'x_{2}) e^{2s(x_{2})} \left[ e^{-2\beta_{W}(x_{2})} j_{k} (2LG(x_{2})) - j_{k} (2Lq(x_{2})) \right] \right)$$

$$\times \int_{x_{2}}^{\infty} x_{1}^{3/2} K_{k+1/2} (a'x_{1}) e^{s(x_{1})} \left[ e^{-\beta_{W}(x_{1})} j_{k} (LG(x_{1})) - j_{k} (Lq(x_{1})) \right] dx_{1} dx_{2}$$

$$+ \int_{0}^{\infty} x_{2}^{3/2} K_{k+1/2} (a'x_{2}) e^{2s(x_{2})} \left[ e^{-2\beta_{W}(x_{2})} j_{k} (2LG(x_{2})) - j_{k} (2Lq(x_{2})) \right]$$

$$\times \int_{0}^{x_{2}} x_{1}^{3/2} I_{k+1/2} (a'x_{1}) e^{s(x_{1})} \left[ e^{-s(x_{1})} j_{k} (LG(x_{1})) - j_{k} (Lq(x_{1})) \right] dx_{1} dx_{2}$$

$$- \delta_{ko} \int_{0}^{\infty} x_{2}^{3/2} K_{1/2} (a'x_{2}) e^{2s(x_{2})} \left[ e^{-2\beta_{W}(x_{2})} - 1 \right] \int_{x_{2}}^{x_{2}} x_{1}^{3/2} K_{1/2} (a'x_{1}) e^{s(x_{1})} \left[ e^{-\beta_{W}(x_{1})} - 1 \right] dx_{1} dx_{2}$$

$$- \delta_{ko} \int_{0}^{\infty} x_{2}^{3/2} K_{1/2} (a'x_{2}) e^{2s(x_{2})} \left[ e^{-2\beta_{W}(x_{2})} - 1 \right] \int_{0}^{x_{2}} x_{1}^{3/2} I_{1/2} (a'x_{1}) e^{s(x_{1})} \left[ e^{-\beta_{W}(x_{1})} - 1 \right] dx_{1} dx_{2}$$

$$- \delta_{ko} \int_{0}^{\infty} x_{2}^{3/2} K_{1/2} (a'x_{2}) e^{2s(x_{2})} \left[ e^{-2\beta_{W}(x_{2})} - 1 \right] \int_{0}^{x_{2}} x_{1}^{3/2} I_{1/2} (a'x_{1}) e^{s(x_{1})} \left[ e^{-\beta_{W}(x_{1})} - 1 \right] dx_{1} dx_{2}$$

*I* and *K* refer to modified Bessel functions of the first and third kind, respectively, while  $j_k(-)$  specifies a spherical Bessel function of order k.<sup>6</sup> The sums over k in these expressions for the second-order terms converge very rapidly and hence only three terms must be evaluated.

Thus to second order, we may write

$$T(l) = \exp\left[-\gamma L^2 + I_{10}(l) + I_{01}(l) + I_{02}(l) + I_{11}(l)\right] .$$
(36)

This result is used in Eq. (7) to calculate  $P(\epsilon)$  at

a charged point. It may also be shown that this result goes to the Holtsmark limit as  $T \rightarrow \infty$ .<sup>7</sup> If there were *r* different species of ion, there would be *r* second-order terms such as  $I_{20}$ , and r!/2!(r-2)!second-order cross-term such as  $I_{11}$ .

In the event that  $P(\epsilon)$  is desired at a neutral point,  $\xi$  is set equal to zero which excludes central interactions. Because of the cost of evaluating the terms, it is useful to obtain separate analytic expressions for the neutral case. The expression for  $T_0(l)/T_0(0)$  remains unaltered, but the first-

and second-order terms in the series exponent are changed owing to the fact that w(x), s(x), and  $h_{ij}(0)$ are zero. Hence

 $I_{10}(l)_{\text{neutral}} = n^* h_{10}(l)_{\text{neutral}}$  $= \frac{3}{1+2R} \int_{\gamma}^{\infty} dx \, x^2 \left( \frac{\sin(LG(x))}{LG(x)} - \frac{\sin(Lq(x))}{Lq(x)} \right),$ (37)

$$I_{01}(l)_{\text{neutral}} = n^{**} h_{01}(l)_{\text{neutral}}$$

$$=\frac{3R}{1+2R}\int_{0}^{\infty}dx\,x^{2}\left(\frac{\sin(2LG(x))}{2LG(x)}-\frac{\sin(2Lq(x))}{2Lq(x)}\right).$$
(38)

The second-order terms for the neutral case are found by again setting w(x), s(x), and  $h_{ij}(0)$  equal to zero (or, what is equivalent, by setting  $\xi = 0$ ) and, in addition, the  $\delta_{ko}$  terms for all k. Hence,

$$I_{20}(l)_{\text{neutral}} = \frac{1}{2} (n^*)^2 h_{20}(l)_{\text{neutral}} = \frac{\theta_e}{\theta_i} \left(\frac{1}{1+2R}\right)^2 3a^2 \sum_k (-1)^k (2k+1) \{20\}_{\text{neutral}},$$

$$\{20\}_{\text{neutral}} = \{\int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) [j_k(LG(x_2)) - j_k(Lq(x_2))] \int_{x_2}^\infty x_1^{3/2} K_{k+1/2}(a'x_1) [j_k(LG(x_1)) - j_k(Lq(x_1))] dx_1 dx_2\};$$

$$(39)$$

$$I_{02}(l)_{neutral} = \frac{1}{2} (n^{**})^2 h_{02}(l)_{neutral} = 4 \frac{\theta_e}{\theta_i} \left[ \frac{R}{1+2R} \right] 3a^2 \sum_{k} (-1)^k (2k+1) \{02\}_{neutral},$$

$$\{02\}_{neutral} = \int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) \left[ j_k (2LG(x_2)) - j_k (2Lq(x_2)) \right] \int_{x_2}^\infty x_1^{3/2} K_{k+1/2}(a'x_1) \left[ j_k (2LG(x_1)) - j_k (2Lq(x_1)) \right] dx_1 dx_2;$$

$$\{02\}_{neutral} = \int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) \left[ j_k (2LG(x_2)) - j_k (2Lq(x_2)) \right] \int_{x_2}^\infty x_1^{3/2} K_{k+1/2}(a'x_1) \left[ j_k (2LG(x_1)) - j_k (2Lq(x_1)) \right] dx_1 dx_2;$$

$$\{02\}_{neutral} = \int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) \left[ j_k (2LG(x_2)) - j_k (2Lq(x_2)) \right] \int_{x_2}^\infty x_1^{3/2} K_{k+1/2}(a'x_1) \left[ j_k (2LG(x_1)) - j_k (2Lq(x_1)) \right] dx_1 dx_2;$$

$$I_{11}(l)_{\text{neutral}} = n^* n^{**} h_{11}(l)_{\text{neutral}} = 2 \frac{\theta_e}{\theta_i} \left(\frac{1}{1+2R}\right) \left(\frac{R}{1+2R}\right) 3a^2 \sum_{k} (-1)^k (2k+1) \{11\}_{\text{neutral}},$$
(41)

J<sub>×2</sub>

$$\{11\}_{neutral} = \left\{ \int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) \left[ j_k(2LG(x_2)) - j_k(2Lq(x_2)) \right] \int_{x_2}^\infty x_1^{3/2} K_{k+1/2}(a'x_1) \left[ j_k(LG(x_1)) - j_k(Lq(x_1)) \right] dx_1 dx_2 \right\}$$

$$+ \int_{0}^{\infty} x_{2}^{3/2} K_{k+1/2}(a'x_{2}) \left[ j_{k}(2LG(x_{2}) - j_{k}(2Lq(x_{2}))) \right] \int_{x_{2}}^{\infty} x_{2}^{3/2} I_{k+1/2}(a'x_{1}) \left[ j_{k}(LG(x_{1})) - j_{k}(Lq(x_{1})) \right] dx_{1} dx_{2} \\ + \int_{0}^{\infty} x_{2}^{3/2} K_{k+1/2}(a'x_{2}) \left[ j_{k}(2LG(x_{2})) - j_{k}(2Lq(x_{2})) \right] \int_{x_{2}}^{\infty} x_{1}^{3/2} I_{k+1/2}(a'x_{1}) \left[ j_{k}(LG(x_{1})) - j_{k}(Lq(x_{1})) \right] dx_{1} dx_{2} \right\}.$$

Two approximations have been made thus far. First, we have terminated the series appearing in the exponential with the second-order terms. This may be justified, by consideration of the analytic form of the terms appearing in the series, and by direct numerical calculations.<sup>5</sup> The second approximation concerns the use of collective coordinates in the evaluation of the many-dimensional integrals occurring in this theory.<sup>5,8</sup>

As indicated earlier in this section, the evaluation of the many-dimensional integrals appearing in the expressions for  $I_{jm}(l)$  can be transformed into integrals over collective coordinates which have a rather simple form. As is shown in the Appendix, these collective-coordinate integrals may be evaluated as<sup>8</sup>

$$I = \int \cdots \int \exp[-\frac{1}{2} \sum_{k} (A_{k} X_{k}^{2} + 2b_{k} X_{k})] J \prod_{k} dX_{k}$$
  
= (const)  $\exp[\frac{1}{2} \sum_{k} b_{k}^{2} / (1 + A_{k})] (1 - a_{3} + a_{4} - \cdots) .$   
(42)

The  $A_k$  and  $b_k$  are specific functions of k, the  $X_k$ 's represent collective coordinates, and J is the

Jacobian of the  $\vec{r} \rightarrow \vec{X}$  transformation. The series of terms in brackets represents the possible higherorder correction to the first Jacobian approximation. In the calculations made in this paper,  $a_3$  and all other correction terms have been neglected.

Following the procedure previously developed, <sup>5, 8</sup> we have shown that the neglect of corrections to the first Jacobian approximation is valid for the temperatures and densities considered in this paper.

## **III. ASYMPTOTIC MICROFIELD DISTRIBUTION** FUNCTION

In this section we deal with the determination of asymptotic microfield distribution functions. Generating the microfield distribution functions for values of  $\epsilon > 20$  becomes increasingly expensive because the sine transform routine that is required to evaluate Eq. 7 requires an increasingly finer mesh. For values of  $P(\epsilon)$  in this asymptotic region it is more convenient to calculate  $P(\epsilon)$  from one of two approximate formulations: the nearest-neighbor approximation (NNA)<sup>8</sup> or the Holtsmark limit.<sup>7</sup>

This problem has been previously considered for the case of singly charged ion perturbers.<sup>5</sup> Hence we are here extending the method to the situation where more than one perturbing ion species is present. Specifically we will examine the situation where both singly and doubly charged perturbers are present. First we will consider the charged-point case, and then the neutral-point problem.

## A. Charged-Point Case

For the charged-point case, the additional correlations arising from the presence of a charged particle at the origin make the Holtsmark limit an invalid approximation for the field strengths that we consider. Hence we use the nearest-neighbor approximation which we have shown to be in very close agreement with the near-exact function.

The nearest-neighbor model assumes that for high fields the bulk of the contribution to the total field is due only to the nearest neighbor. This neighbor may be either a singly or a doubly charged ion. The probability of two or more ions producing this high field is very small and is assumed to be zero. If this probability were not small, it would mean that the asymptotic region had not yet been reached and the near-exact microfield calculation would have to be extended. The assumption that the probability of two ions being near the origin is small, has been validated by comparisons between calculated nearexact microfield distributions and the asymptotic results in the region where they join. The asymptotic value is always slightly less than the calculated microfield distribution but the difference decreases as  $\epsilon$  increases. At the point where the asymptotic form is assumed to be valid, the difference is less than 1%.

The probability of a singly or a doubly charged ion being close to the origin is related to the probability of this same ion producing an electric field, by the following expressions:

$$P_{1}(\epsilon_{1}) d\epsilon_{1} = 4\pi r_{1}^{2} n^{*} g^{*}(r_{1}) dr_{1} = \frac{1}{1+2R} x_{1}^{2} g^{*}(x_{1}) dx_{1} ,$$
(43a)
$$P_{2}(\epsilon_{2}) d\epsilon_{2} = 4\pi r_{2}^{2} n^{**} g^{**}(r_{2}) dr_{2} = \frac{3R}{1+2R} x_{2}^{2} g^{**}(x_{2}) dx_{2} ,$$

(43b)

where the last expressions on the right are in terms of the reduced quantities already defined.  $g^*(r_1)$ and  $g^{**}(r_2)$  are pair correlation functions between a singly charged particle and a particle of charge  $\xi$ , and between a doubly charged particle and a particle of charge  $\xi$ , respectively. They can be found using Eqs. (A48), (A50), and (A52) by allowing for the variable charge  $\xi$ :

$$g^{*}(x_{1}) = \exp\left(-\xi \frac{a^{2}}{3x_{1}} \frac{\theta_{e}}{\theta_{i}} e^{-(1+u)^{1/2}ax_{1}}\right)$$
, (44a)

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$$g^{++}(x_2) = \exp\left[-2\xi \frac{a^2}{3x_2} \frac{\theta_e}{\theta_i} e^{-(1+u)^{1/2}ax_2}\right]$$
 (44b)

The fields produced by these ions, in units of the reduced field strength  $\epsilon_0$  and reduced distance  $r_0$  [defined in Eq. (26b)] are

$$\epsilon_1 = (2/x_1^2)(1 + ax_1)e^{-ax_1}$$
, (45a)

$$\epsilon_2 = (2/x_2^2)(1 + ax_2)e^{-ax_2}$$
 (45b)

If these field expressions are differentiated, the expressions for  $d\epsilon_1$  and  $d\epsilon_2$  can be used in Eqs. (43) to obtain  $P_1(\epsilon)$  and  $P_2(\epsilon)$ :

$$P_1(\epsilon_1)$$

 $P_2(\epsilon_2)$ 

$$= \left(\frac{1}{1+2R}\right) \frac{3x_1^4 \exp\left[-\xi(a^2/x_1)\left(\frac{\theta_e}{\theta_i}\right)e^{-(1+u)^{1/2}ax_1}\right]}{a \exp(-ax_1)(2+2/ax_1+ax_1)},$$
(46a)

$$= \left(\frac{R}{1+2R}\right) \frac{3x_2^4 \exp\left[-2\xi \left(a^2/3x_2\right)\left(\theta_e/\theta_i\right) e^{-(1+u)^{1/2}}ax_2\right]}{2a \exp\left(-ax_2\right)\left(2+2/ax_2+ax_2\right)}$$
(46b)

The total asymptotic probability is the sum of the probabilities of the two independent events:

$$P(\epsilon)_{asym} = P_1(\epsilon) + P_2(\epsilon)$$
 (47)

#### B. Neutral-Point Case

The Holtsmark distribution function is the proper high-temperature limit of the nearly exact microfield distribution functions. As such it represents the situation when the perturbing ions are totally uncorrelated: The ions move independently of one another. For increasingly large values of the field strength  $\epsilon$ , it can be shown that the neutral-point near-exact distribution function goes over to the Holtsmark result. The Holtsmark result for a twocomponent plasma is

$$P(\epsilon)_{\text{Holtsmark}} = 1.500 \frac{1+2\sqrt{2}R}{1+2R} \epsilon^{-5/2} + 7.680 \frac{1+2\sqrt{2}R}{1+2R} \epsilon^{4} + 21.77 \frac{1+2\sqrt{2}R}{1+2R} \epsilon^{-11/2} + \cdots$$
 (48)

It can also be shown that for the range of  $\epsilon$  values considered in this paper, the near-exact distribution function is also well approximated by the NNA which implies equivalence of the two approximation methods in the asymptotic region. The reason for this equivalence can be seen by taking the  $T \rightarrow \infty$  limit of the NNA and noting that the result is equal to the leading term in the Holtsmark series. For field strengths  $\epsilon < 20$ , the two approximations may differ from each other and from the near-exact value. However, the differences decrease as the field strength increases and in the high-field region where the shielded potential is numerically almost identical to the Coulomb potential, the NNA reduces to the first term of the Holtsmark series which is overwhelmingly the most important term. This is not too surprising since for large fields one would intuitively expect that nearest-neighbor contributions to the Holtsmark expression would be the largest. For the numerical results presented in this paper, the NNA was used.

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## IV. NUMERICAL RESULTS AND ANALYSIS

Following the procedure discussed in detail in Ref. 5, we have generated  $P(\epsilon)$  values in both tabular and graphical form for a macroscopically neutral plasma containing  $N^*$  singly charged shielded ions and  $N^{**}$  doubly charged shielded ions which interact with each other through an effective potential which includes the effect of ion-electron interaction. This model has been and is currently used when dealing with effects of ions on radiating atoms and/ or ions immersed in a plasma.<sup>1-3</sup> The form of the effective potential is assumed to be Debye-Hückel.

Values of  $P(\epsilon)$  have been calculated for four values of a; for each a value three different ion ratios  $(R \equiv n^{**}/n^*)$  have been considered. Figure 1 shows the three curves for a = 0.2; notice that the three curves corresponding to values of R = 0.0 (all perturbers singly charged), R = 1.0 ( $50\% n^*$  and  $50\% n^{**}$ ), and  $R = \infty$  (all perturbers doubly charged) are well separated. Examined in order, Figs. 2, 3, and 4 indicate that as a increases the three R-value curves seem to coalesce. Recall that for a fixed value of temperature an increase in a implies an increase in density. Also note that as a goes from 0.2 to 0.8 the peaks of the three R curves are shifted toward smaller field values and the height of the peaks is



FIG. 1. Electric microfield distribution function  $P(\epsilon)$  at a charged point for a=0.2,  $R=0, 1, \infty$ ;  $\epsilon$  is in units of  $\epsilon_{0}$ .



FIG. 2. Electric microfield distribution function  $P(\epsilon)$  at a charged point for a=0.4,  $R=0, 1, \infty$ ;  $\epsilon$  is in units of  $\epsilon_0$ .

raised.

The behavior of these R curves as a is varied can be interpreted physically. First, the shift and elevation of the peaks is testimony to the effect of increased interion correlations as a is increased. As these correlations increase, the ions have an increased tendency to "stay away" from one another and hence the probability distribution function is shifted to smaller values of  $\epsilon$  with increased probability.

Next, consider the fact that as *a* increases, the relative separation of the curves corresponding to different *R* values decreases. For all *a* values discussed in this paper, the curves for  $R = \infty$  favor larger field strengths than do those corresponding to R = 0. For a given value of  $N_e$ , the requirement that  $R = \infty$  means that the plasma being treated contains one-half the number of ions than one would for which R = 0; but each of these ions is doubly charged.



FIG. 3. Electric microfield distribution function  $P(\epsilon)$  at a charged point for a=0.6,  $R=0, 1, \infty$ ;  $\epsilon$  is in units of  $\epsilon_0$ .

TABLE I. Probability distribution  $P(\epsilon)$  at a charged point for several values of a, with R=1.0. The electric field strength  $\epsilon$  is in units of  $\epsilon_0$ . The lines in the columns indicate the point at which asymptotic expressions were used in the calculations.

	E	A = 0.2	A = 0.4	A = 0.6	A = 0.8
0.2 $0.193 53E-01$ $0.38871E-01$ $0.76721E-01$ $0.1151500$ $0.3$ $0.434 54E-01$ $0.136 80E 00$ $0.243 88E 00$ $0.49721E 00$ $0.5$ $0.1120E 00$ $0.25164E 00$ $0.23564E 00$ $0.4553E 00$ $0.6$ $0.14857E 00$ $0.23164E 00$ $0.32258E 00$ $0.5643E 00$ $0.7$ $0.1752E 00$ $0.3764E 00$ $0.44041E 00$ $0.5572E 00$ $0.8$ $0.22513E 00$ $0.3764E 00$ $0.4473E 00$ $0.5772E 00$ $1.0$ $0.2866E 00$ $0.39801E 00$ $0.4473E 00$ $0.47746E 00$ $0.47746E 00$ $1.1$ $0.31416E 00$ $0.440909E 00$ $0.444473E 00$ $0.38663E 00$ $1.4$ $0.3571E 00$ $0.3379961E 00$ $0.3365200$ $0.32753E 00$ $1.4$ $0.3545E 00$ $0.33115E 00$ $0.33756E 00$ $0.32753E 00$ $1.5$ $0.3345E 00$ $0.33119E 00$ $0.33165E 00$ $0.264382E 00$ $1.7$ $0.4338E 00$ $0.33056E 00$ $0.28482E 00$ $0.31056E 00$ $0.28482E 00$ $1.6$ $0.35455E 00$ $0.32755600$ $0.32754500$ <td>0.1</td> <td>0.42203E-02</td> <td>0.10043E-01</td> <td>0.20326E-01</td> <td>0.42245E-01</td>	0.1	0.42203E-02	0.10043E-01	0.20326E-01	0.42245E-01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.2	0.19353E-01	0.38871E-01	0.76721E-01	0.15115E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.3	0.43454E-01	0.82859E-01	0.15830E 00	0.28553E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.4	0.74448E-01	0.13680E 00	0.243 88E 00	0.40721E 00
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0.5	0.11020E 00	0.19490E 00	0.32569E 00	0.49529E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.6	0.14857E 00	0.25168E 00	0.39258E 00	0.545 85E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.7	0.18752E 00	0.30271E 00	0.44041E 00	0.56435E 00
0.9 $0.25972E$ $00$ $0.37624E$ $00$ $0.46021E$ $00$ $0.53792E$ $00$ $1.0$ $0.2866E$ $00$ $0.39801E$ $00$ $0.47766E$ $00$ $0.50716E$ $00$ $1.2$ $0.33287E$ $00$ $0.41128E$ $00$ $0.44462E$ $00$ $0.43388E$ $00$ $1.3$ $0.34565E$ $00$ $0.40128E$ $00$ $0.44462E$ $00$ $0.338297E$ $00$ $0.36094E$ $00$ $1.4$ $0.35271E$ $00$ $0.33915E$ $00$ $0.36656E$ $00$ $0.32738E$ $00$ $1.6$ $0.35185E$ $00$ $0.33168E$ $00$ $0.36662E$ $00$ $0.22674E$ $00$ $1.7$ $0.34530E$ $00$ $0.32119E$ $00$ $0.28118E$ $00$ $0.226468E$ $00$ $1.8$ $0.33622E$ $00$ $0.29914E$ $00$ $0.28118E$ $00$ $0.22042E$ $00$ $2.0$ $0.30972E$ $00$ $0.2996E$ $00$ $0.2394E$ $00$ $0.12990E$ $00$ $2.5$ $0.2315E$ $00$ $0.12918E$ $00$ $0.12858E$ $00$ $0.12836E$ $00$ $0.2394E$ $00$ $0.2986E$ $00$ $3.5$ $0.1507E$ $00$ $0.8556E-01$ $0.7082F-01$ $0.38966E-01$ $0.71738-01$ $0.22070E-01$ $4.5$ $0.59935E-01$ $0.75798E-02$ $0.78738E-02$ $0.6248E-01$ $0.29268E-01$ $4.5$ $0.59935E-01$ $0.35564E-01$ $0.312428E-01$ $0.322470E-01$ $4.5$ $0.5993$	0.8	0.22513E 00	0.34496E 00	0.46890E 00	0.55909E 00
	0.9	0.25972E 00	0.37684E 00	0.48021E 00	0.53792E 00
1.1       0.314 16E 00       0.409 09E 00       0.444 62E 00       0.471 42E 00         1.2       0.332 67E 00       0.416 128E 00       0.444 62E 00       0.438 88E 00         1.4       0.356 71E 00       0.396 15E 00       0.326 97E 00       0.366 63E 00         1.4       0.356 71E 00       0.379 96E 00       0.365 65E 00       0.237 53E 00         1.6       0.351 83E 00       0.379 96E 00       0.365 65E 00       0.226 73E 00         1.7       0.436 30E 00       0.314 16E 00       0.310 56E 00       0.248 68E 00         1.8       0.335 62E 00       0.321 19E 00       0.285 18E 00       0.226 42E 00         2.0       0.309 72E 00       0.296 61E 00       0.239 48E 00       0.199 90E 00         2.5       0.231 55E 00       0.194 48E 00       0.164 87E 00       0.215 37E 00         3.5       0.115 07E 00       0.895 56E -01       0.708 02E -01       0.661 61E -01         4.5       0.599 35E -01       0.470 49E -01       0.571 73E -01       0.329 48E         4.5       0.599 35E -01       0.470 49E -01       0.371 73E -01       0.389 66E -01         4.5       0.599 35E -01       0.470 49E -01       0.371 73E -01       0.389 66E -01         5.6       0.176 35E -01       0.22	1.0	0.28968E 00	0.39801E 00	0.47766E 00	0.50716E 00
1.2       0.332 27E 00       0.41128E 00       0.44201E 00       0.4386E 00         1.3       0.346 65E 00       0.4001E 00       0.386 03E 00       1.43 0.354 55E 00       0.327 93E 00       0.366 03E 00         1.4       0.354 55E 00       0.379 96E 00       0.365 05E 00       0.327 53E 00         1.6       0.351 63E 00       0.341 96E 00       0.337 34E 00       0.226 74E 00         1.7       0.435 30E 00       0.321 19E 00       0.225 18E 00       0.226 42E 00         1.8       0.336 52E 00       0.327 93E 00       0.261 45E 00       0.220 42E 00         2.0       0.309 72E 00       0.279 61E 00       0.228 48E 00       0.198 90E 00         2.5       0.318 55E 00       0.128 18E 00       0.102 85E 00       0.125 37E 00         3.0       0.163 92E 00       0.129 18E 00       0.102 85E 00       0.221 42E 01         3.5       0.118 07E 00       0.855 66E-01       0.760 452E-01       0.898 86E-01         4.5       0.599 35E-01       0.470 48E-01       0.371 73E-01       0.222 070E-01         4.5       0.599 35E-01       0.470 48E-01       0.371 73E-01       0.222 070E-01         5.0       0.448 16E-01       0.371 73E-01       0.222 070E-01       0.428 28E-02         7.0 </td <td>1.1</td> <td>0.31416E 00</td> <td>0.40909E 00</td> <td>0.46473E 00</td> <td>0.47142E 00</td>	1.1	0.31416E 00	0.40909E 00	0.46473E 00	0.47142E 00
1.3       0.345 65E       00       0.406 102 00       0.426 201E 00       0.366 63E 00         1.4       0.352 71E 00       0.351 55E 00       0.379 96E 00       0.365 05E 00       0.327 53E 00         1.6       0.351 53E 00       0.361 55E 00       0.379 96E 00       0.310 56E 00       0.2267 45E 00         1.7       0.345 30E 00       0.321 19E 00       0.326 51E 00       0.226 42E 00       0.226 42E 00         1.8       0.335 52E 00       0.327 351E 00       0.236 48E 00       0.220 42E 00       0.220 42E 00         2.0       0.307 325 1E 00       0.300 23E 00       0.246 48E 00       0.1225 37E 00       0.223 94 8E 00       0.125 37E 00         3.5       0.163 92E 00       0.129 18E 00       0.154 87E 00       0.828 136E 01       0.561 61E -01         4.0       0.820 51E -01       0.639 56E -01       0.768 02E -01       0.586 68E -01       0.371 78E -01       0.928 68E -01         5.0       0.150 97E -01       0.479 48E -01       0.311 340E -01       0.526 68E -01       0.220 70E -01         6.0       0.217 067E -01       0.317 78E -01       0.282 68E -01       0.317 178E -01       0.292 68E -02         7.0       0.458 98E -02       0.737 38E -02       0.662 48E -02       0.426 44E -02       0.322 48E -02 <td>1.2</td> <td>0.332 87E 00</td> <td>0.41128E 00</td> <td>0.44462E 00</td> <td>0.433 88E 00</td>	1.2	0.332 87E 00	0.41128E 00	0.44462E 00	0.433 88E 00
1.4       0.35271E       00       0.39515E       00       0.36505E       00       0.36694E       00         1.5       0.35455E       00       0.36185E       00       0.36505E       00       0.32753E       00         1.7       0.34530E       00       0.34196E       00       0.3165E       00       0.28618E       00       0.28618E       00       0.28618E       00       0.28628E       00       0.22042E       00       0.22042E       00       0.22351E       00       0.22042E       00       0.22357E       00       0.22042E       00       0.2237E	1.3	0.34565E 00	0.40610E 00	0.42001E 00	0.39663E 00
1.50.364 55E000.379 66E000.363 734E000.327 35E001.60.351 83E000.361 85E000.337 34E000.296 74E001.70.345 30E000.341 96E000.310 56E000.266 68E001.80.335 52E000.321 19E000.261 45E000.220 42E002.00.307 72E000.279 61E000.239 48E000.125 37E002.50.231 85E000.190 48E000.154 87E000.125 37E003.00.163 92E000.128 18E000.128 5E000.821 36E-010.368 64E-014.00.820 51E-010.639 56E-010.778 60E-010.371 73E-010.292 68E-014.50.599 35E-010.470 49E-010.371 73E-010.222 70E-015.00.176 63E-010.217 72E-010.173 38E-010.134 29E-017.00.176 63E-010.217 72E-010.173 38E-020.602 49E-029.00.828 98E-020.725 79E-020.570 36E-020.432 29E-029.00.882 98E-020.725 79E-020.570 36E-020.126 68E-0210.00.662 54E-020.220 97E-020.163 96E-030.432 29E-0212.00.403 84E-020.153 30E-030.446 70E-030.321 77E-0312.00.438 88E-020.153 36E-030.464 70E-030.321 77E-0314.00.266 66E-020.280 97E-030.186 68E-020.126 68E-02	1.4	0.35271E 00	0.39515E 00	0.39297E 00	0.36094E 00
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1.5	0.35455E 00	0.37996E 00	0.36505E 00	0.32753E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.6	0.35183E 00	0.36185E 00	0.33734E 00	0.29674E 00
1.80.335 62E 000.321 19E 000.285 18E 000.243 28E 001.90.323 51E 000.300 23E 000.261 45E 000.220 42E 002.00.309 72E 000.279 61E 000.239 48E 000.159 90E 002.50.231 55E 000.190 48E 000.164 87E 000.152 37E 003.00.163 92E 000.129 18E 000.102 85E 000.821 36E-013.50.115 07E 000.895 56E-010.708 02E-010.564 61E-014.00.820 51E-010.639 54E-010.549 55E-010.281 92E-015.00.449 16E-010.355 64E-010.281 28E-010.222 070E-016.00.706 7E-010.217 72E-010.173 82E-010.875 71E-027.00.176 35E-010.989 25E-020.573 738E-020.622 48E-029.00.882 98E-020.725 79E-020.570 36E-020.322 48E-0210.00.662 54E-020.725 79E-020.613 96E-020.322 48E-0212.00.438 45E-020.132 96E-030.132 65E-030.429 95E-0314.00.269 69E-020.220 97E-020.613 64E-020.836 88E-0314.00.269 69E-020.123 65E-030.424 95E-030.429 95E-0322.00.138 45E-030.633 55E-030.290 85E-030.429 95E-0324.00.424 50E-030.633 55E-030.290 85E-030.429 95E-0324.00.426 45E-020.132 66E-030.232 177E-030.122 65E-0324.00.426 45E-030.232 177E-030.122 36E-030.242 92E-0330.00.354 60E-	1.7	0.34530E 00	0.34196E 00	0.31056E 00	0.26868E 00
1.9 $0.32351E00$ $0.30023E00$ $0.26145E00$ $0.22042E00$ 2.0 $0.30972E00$ $0.27661E00$ $0.23948E00$ $0.19990E00$ 2.5 $0.23185E00$ $0.19048E00$ $0.123948E00$ $0.12337E00$ 3.0 $0.61392E00$ $0.12218E00$ $0.10228E00$ $0.823136E01$ 3.5 $0.11507E00$ $0.89556E-01$ $0.70802E-01$ $0.56161E-01$ 4.0 $0.82051E-01$ $0.63954E-01$ $0.5945E-01$ $0.28128E-01$ 5.0 $0.44916E-01$ $0.37173E-01$ $0.22070E-01$ 6.0 $0.270767E-01$ $0.21772E-01$ $0.71238E-01$ $0.13429E-01$ 7.0 $0.17630E-01$ $0.98925E-02$ $0.78738E-02$ $0.60249E-02$ 8.0 $0.12192E-01$ $0.99825E-02$ $0.73738E-02$ $0.60249E-02$ 9.0 $0.86254E-02$ $0.54584E-02$ $0.4264E-02$ $0.32248E-01$ 10.0 $0.66254E-02$ $0.54584E-02$ $0.133760E-02$ $0.32248E-02$ 12.0 $0.40384E-02$ $0.33174E-02$ $0.24931E-02$ $0.32248E-02$ 12.0 $0.40384E-02$ $0.33174E-02$ $0.1386E-02$ $0.132368E-02$ 12.0 $0.13875E-02$ $0.15390E-02$ $0.11364E-02$ $0.8206E-03$ 24.0 $0.64775E-03$ $0.63357E-03$ $0.63357E-03$ $0.4298E-03$ 25.0 $0.13875E-02$ $0.13174E-03$ $0.4298E-03$ $0.23917E-03$ 26.0 $0.13875E-02$ $0.13162E-02$ $0.83006E-03$ $0.59008E-03$ 27.0 $0.13875E-03$ $0.1226E-03$ $0.23917E-03$ $0.12236E-03$ <td>1.8</td> <td>0.33562E 00</td> <td>0.32119E 00</td> <td>0.28518E 00</td> <td>0.24328E 00</td>	1.8	0.33562E 00	0.32119E 00	0.28518E 00	0.24328E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.9	0.32351E 00	0.30023E 00	0.26145E 00	0.22042E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.0	0.30972E 00	0.27961E 00	0.23948E 00	0.19990E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.5	0.231 85E 00	0.19048E 00	0.154 87E 00	0.12537E 00
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.0	0.16392E 00	0.12918E 00	0.10285E 00	0.82136E-01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.5	0.11507E 00	0.89556E-01	0.70802E-01	0.56161E-01
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4.0	0.82051E-01	0.63954E-01	0.50495E-01	0.39896E-01
5.0 $0.44916E-01$ $0.35564E-01$ $0.28128E-01$ $0.22070E-01$ $6.0$ $0.27067E-01$ $0.21772E-01$ $0.17238E-01$ $0.13429E-01$ $7.0$ $0.17630E-01$ $0.14339E-01$ $0.11340E-01$ $0.87571E-02$ $8.0$ $0.12192E-01$ $0.9825E-02$ $0.78738E-02$ $0.60249E-02$ $9.0$ $0.88298E-02$ $0.72579E-02$ $0.57036E-02$ $0.60249E-02$ $10.0$ $0.66254E-02$ $0.54584E-02$ $0.42644E-02$ $0.32248E-02$ $12.0$ $0.40384E-02$ $0.33174E-02$ $0.24931E-02$ $0.12365E-02$ $14.0$ $0.26969E-02$ $0.22097E-02$ $0.16396E-02$ $0.12365E-02$ $16.0$ $0.1888E-02$ $0.15390E-02$ $0.13164E-02$ $0.83683E-03$ $18.0$ $0.13875E-02$ $0.11216E-02$ $0.8206E-03$ $0.59008E-03$ $20.0$ $0.10443E-02$ $0.83760E-03$ $0.61108E-03$ $0.42995E-03$ $22.0$ $0.81788E-03$ $0.62335E-03$ $0.661470E-03$ $0.32177E-03$ $24.0$ $0.64775E-03$ $0.50292E-03$ $0.36534E-03$ $0.24625E-03$ $26.0$ $0.51023E-03$ $0.33365E-03$ $0.23517E-03$ $0.15221E-03$ $30.0$ $0.35460E-03$ $0.27745E-03$ $0.19275E-03$ $0.12236E-03$ $30.0$ $0.35460E-03$ $0.27745E-03$ $0.13209E-03$ $0.74588E-04$ $40.0$ $0.17034E-03$ $0.12788E-04$ $0.86504E-04$ $0.22792E-04$ $40.0$ $0.734E-03$ $0.12788E-04$ $0.38079E-04$ $0.28504E-04$ $0.22792E-04$	4.5	0.59935E-01	0.47049E-01	0.37173E-01	0.29268E-01
	5.0	0.44916E-01	0.35564E-01	0.28128E-01	0.22070E-01
7.00.176 30 E-010.143 39 E-010.113 40 E-010.875 71 E-028.00.121 92 E-010.998 25 E-020.787 38 E-02 $0.602 49 E-02$ 9.00.882 98 E-020.725 79 E-020.570 36 E-02 $0.432 29 E-02$ 10.00.662 54 E-020.545 84 E-02 $0.426 44 E-02$ $0.322 48 E-02$ 12.00.403 84 E-020.331 74 E-02 $0.249 31 E-02$ $0.192 68 E-02$ 14.00.266 69 E-020.220 97 E-02 $0.163 96 E-02$ $0.132 65 E-02$ 16.00.188 88 E-02 $0.133 90 E-02$ $0.113 64 E-02$ $0.836 83 E-03$ 18.00.138 75 E-02 $0.112 16 E-02$ $0.820 06 E-03$ $0.590 08 E-03$ 20.00.517 88 E-03 $0.633 35 E-03$ $0.611 08 E-03$ $0.429 95 E-03$ 24.0 $0.647 75 E-03$ $0.502 92 E-03$ $0.365 34 E-03$ $0.246 25 E-03$ 24.0 $0.510 23 E-03$ $0.406 53 E-03$ $0.290 83 E-03$ $0.152 21 E-03$ 30.0 $0.354 60 E-03$ $0.277 45 E-03$ $0.123 09 E-03$ $0.152 21 E-03$ 30.0 $0.354 60 E-03$ $0.277 45 E-03$ $0.123 09 E-04$ $0.481 82 E-04$ 40.0 $0.170 34 E-03$ $0.127 88 E-03$ $0.830 79 E-04$ $0.481 82 E-04$ 40.0 $0.120 88 E-04$ $0.928 70 E-04$ $0.585 04 E-04$ $0.227 92 E-04$ 60.0 $0.962 96 E-04$ $0.696 63 E-04$ $0.224 48 E-04$ $0.121 43 E-04$ 70.0 $0.466 25 E-04$ $0.277 36 E-04$ $0.244 48 E-04$ $0.121 43 E-04$ 70.0 $0.466 20 E-04$ $0.277 36 E-04$ $0.$	6.0	0.27067E-01	0.21772E-01	0.17238E-01	0.13429E-01
8.00.121 92 E-010.998 25 E-020.787 38 E-02 $0.602 49E-02$ 9.00.882 98E-020.725 79E-020.570 36E-02 $0.432 29E-02$ 10.00.662 54E-020.545 84E-02 $0.257 9E-02$ $0.570 36E-02$ $0.322 48E-02$ 12.00.403 84E-020.331 74E-02 $0.249 31E-02$ $0.192 68E-02$ 14.00.269 69E-020.220 97E-02 $0.163 96E-02$ $0.123 65E-02$ 16.00.188 88E-02 $0.153 90E-02$ $0.113 64E-02$ $0.836 83E-03$ 18.00.138 75E-02 $0.112 16E-02$ $0.820 06E-03$ $0.590 08E-03$ 20.00.817 88E-03 $0.633 35E-03$ $0.464 70E-03$ $0.321 77E-03$ 24.0 $0.647 75E-03$ $0.502 92E-03$ $0.365 34E-03$ $0.249 25E-03$ 24.0 $0.647 75E-03$ $0.502 92E-03$ $0.235 17E-03$ $0.122 36E-03$ 36.0 $0.354 60E-03$ $0.277 45E-03$ $0.235 17E-03$ $0.122 36E-03$ 30.0 $0.354 60E-03$ $0.277 45E-03$ $0.123 09E-03$ $0.745 88E-04$ 40.0 $0.170 34E-03$ $0.127 88E-03$ $0.830 79E-04$ $0.325 49E-04$ 50.0 $0.962 96E-04$ $0.696 63E-04$ $0.286 18E-04$ $0.227 92E-04$ 60.0 $0.603 55E-04$ $0.422 12E-04$ $0.244 48E-04$ $0.121 43E-04$ 70.0 $0.288 15E-04$ $0.227 36E-04$ $0.189 74E-04$ $0.996 60E-05$ $0.434 01E-05$ 90.0 $0.212 74E-04$ $0.136 31E-04$ $0.996 60E-05$ $0.434 01E-05$ 90.0 $0.212 74E-04$ $0.136 31E-04$ $0.486 80E-05$ </td <td>7.0</td> <td>0.17630E-01</td> <td>0.14339E-01</td> <td>0.11340E-01</td> <td>0.87571E-02</td>	7.0	0.17630E-01	0.14339E-01	0.11340E-01	0.87571E-02
9.0 $0.88298E-02$ $0.72579E-02$ $0.57036E-02$ $0.43229E-02$ 10.0 $0.66254E-02$ $0.54584E-02$ $0.42644E-02$ $0.32248E-02$ 12.0 $0.40384E-02$ $0.33174E-02$ $0.24931E-02$ $0.19268E-02$ 14.0 $0.26969E-02$ $0.22097E-02$ $0.16396E-02$ $0.12365E-02$ 16.0 $0.18888E-02$ $0.15390E-02$ $0.11364E-02$ $0.83688E-03$ 18.0 $0.13875E-02$ $0.11216E-02$ $0.8206E-03$ $0.59008E-03$ 20.0 $0.10443E-02$ $0.83760E-03$ $0.61108E-03$ $0.32177E-03$ 22.0 $0.81788E-03$ $0.63335E-03$ $0.46470E-03$ $0.32177E-03$ 24.0 $0.64775E-03$ $0.50292E-03$ $0.36534E-03$ $0.24625E-03$ 26.0 $0.51023E-03$ $0.40653E-03$ $0.23517E-03$ $0.15221E-03$ 30.0 $0.42262E-03$ $0.33365E-03$ $0.19275E-03$ $0.12236E-03$ 35.0 $0.23946E-03$ $0.12778E-03$ $0.12309E-03$ $0.7458E-04$ 40.0 $0.17034E-03$ $0.92870E-04$ $0.58504E-04$ $0.32549E-04$ 50.0 $0.96296E-04$ $0.69663E-04$ $0.42618E-04$ $0.22792E-04$ 60.0 $0.60355E-04$ $0.27536E-04$ $0.99660E-05$ $0.12143E-04$ 70.0 $0.40620E-04$ $0.27536E-04$ $0.99660E-05$ $0.28123E-05$ 90.0 $0.21274E-04$ $0.18631E-04$ $0.99660E-05$ $0.28123E-05$ 100.0 $0.6195E-04$ $0.10108E-04$ $0.48680E-05$ $0.18868E-05$	8.0	0.12192E-01	0.99825E-02	0.78738E-02	0.60249E-02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.0	0.88298E-02	0.72579E-02	0.57036E-02	0.43229E-02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.0	0.66254E-02	0.54584E-02	0.42644E-02	0.32248E-02
14. 0 $0.26969E-02$ $0.22097E-02$ $0.16396E-02$ $0.12365E-02$ 16. 0 $0.18888E-02$ $0.15390E-02$ $0.11364E-02$ $0.83683E-03$ 18. 0 $0.13875E-02$ $0.11216E-02$ $0.82006E-03$ $0.59008E-03$ 20. 0 $0.10443E-02$ $0.83760E-03$ $0.61108E-03$ $0.42995E-03$ 22. 0 $0.81788E-03$ $0.63335E-03$ $0.64670E-03$ $0.32177E-03$ 24. 0 $0.64775E-03$ $0.50292E-03$ $0.36534E-03$ $0.24625E-03$ 26. 0 $0.51023E-03$ $0.40653E-03$ $0.29083E-03$ $0.19204E-03$ 28. 0 $0.42262E-03$ $0.33365E-03$ $0.23517E-03$ $0.15221E-03$ 30. 0 $0.35460E-03$ $0.27745E-03$ $0.12309E-03$ $0.74588E-04$ 40. 0 $0.17034E-03$ $0.12788E-03$ $0.83079E-04$ $0.48182E-04$ 45. 0 $0.12608E-03$ $0.92870E-04$ $0.58504E-04$ $0.22792E-04$ 60. 0 $0.60355E-04$ $0.42212E-04$ $0.24448E-04$ $0.12143E-04$ 70. 0 $0.40620E-04$ $0.27536E-04$ $0.42618E-04$ $0.70335E-05$ 80. 0 $0.28815E-04$ $0.18974E-04$ $0.99660E-05$ $0.43401E-05$ 90. 0 $0.21274E-04$ $0.13631E-04$ $0.48680E-05$ $0.18868E-05$	12.0	0.40384E-02	0.33174E-02	0.24931E-02	0.19268E-02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	14.0	0.26969E-02	0.22097E-02	0.16396E-02	0.12365E-02
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16.0	0.18888E-02	0.15390E-02	0.11364E-02	0.83683E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	18.0	0.13875E-02	0.11216E-02	0.82006E-03	0.59008E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.0	0.10443E-02	0.83760E-03	0.61108E-03	0.42995E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22.0	0.81788E-03	0.63335 E - 03	0.46470E-03	0.32177E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24.0	0.64775E-03	0.50292E-03	0.36534E-03	0.24625E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	26.0	0.51023E-03	0.40653 E - 03	0.29083E-03	0.19204E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	28.0	0.42262E-03	0.33365E-03	0.23517E-03	0.15221E-03
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	30.0	0.35460E-03	0.27745E-03	0.19275E-03	0.12236E-03
	35.0	0.23946E-03	$0.18341 \mathrm{E-}03$	0.12309E-03	0.74588E-04
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	40.0	0.17034E-03	0.12788E-03	0.83079E-04	0.48182E-04
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	45.0	0.12608E-03	0.92870E-04	0.58504E-04	0.32549E-04
60.0         0.603 55E-04         0.422 12E-04         0.244 48E-04         0.121 43E-04           70.0         0.406 20E-04         0.275 36E-04         0.151 61E-04         0.703 35E-05           80.0         0.288 15E-04         0.189 74E-04         0.996 60E-05         0.434 01E-05           90.0         0.212 74E-04         0.136 31E-04         0.685 10E-05         0.281 23E-05           100.0         0.161 95E-04         0.101 08E-04         0.486 80E-05         0.188 68E-05	50.0	0.96296E-04	0.69663E-04	0.42618E-04	0.22792E-04
70.0         0.40620E-04         0.27536E-04         0.15161E-04         0.70335E-05           80.0         0.28815E-04         0.18974E-04         0.99660E-05         0.43401E-05           90.0         0.21274E-04         0.13631E-04         0.68510E-05         0.28123E-05           100.0         0.16195E-04         0.10108E-04         0.48680E-05         0.18868E-05	60.0	0.60355E-04	0.42212E-04	0.24448E-04	0.12143E-04
80.0         0.28815E-04         0.18974E-04         0.99660E-05         0.43401E-05           90.0         0.21274E-04         0.13631E-04         0.68510E-05         0.28123E-05           100.0         0.16195E-04         0.10108E-04         0.48680E-05         0.18868E-05	70.0	0.40620E-04	0.27536E-04	0.15161E-04	0.70335E-05
90.0         0.21274E-04         0.13631E-04         0.68510E-05         0.28123E-05           100.0         0.16195E-04         0.10108E-04         0.48680E-05         0.18868E-05	80.0	0.28815E-04	$0.18974 \pm 04$	0.99660E-05	0.43401E-05
100.0         0.16195E-04         0.10108E-04         0.48680E-05         0.18868E-05	90.0	0.21274E-04	0.13631E-04	0.68510E-05	0.28123E-05
	100.0	0.16195E-04	0.10108E-04	0.486 80E-05	0.18868E-05

The implication of Figs. 1, 2, 3, and 4 is that as a increases, the relative importance of correlation between the ions becomes increasingly important so that at a = 0.8, the curves for the several values of

*R* are not too different. Figure 5 shows the electric microfield distribution, at a charged point, for several values of *a*, with R = 1; Fig. 6 shows the same results but for  $R = \infty$ .

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the calculations.

TABLE II. Probability distribution  $P(\epsilon)$  at a charged point for several values of a, with  $R = \infty$ . The electric field strength  $\epsilon$  is in units of  $\epsilon_0$ . The lines in the columns indicate the point at which asymptotic expressions were used in

E	A = 0.2	A = 0.4	A = 0.6	A = 0.8
0.1	0.21470E-02	0.91050E-02	0.19529E-01	0.43009E-01
0.2	0.15170E-01	0.35286E-01	0.73663E-01	0.15308E00
0.3	0.36692E-01	0.75380E-01	0.14987F 00	0.28686E 00
0.4	0.64492E-01	0.12483E 00	0.23358E 00	0.40539E 00
0.5	0.96515E-01	0.17852E 00	0.31175E 00	0.48890E 00
0.6	0.13088E 00	0.23157E 00	0.37587E 00	0.53529E 00
0.7	0.16588E 00	0.27997E 00	0.42220E 00	0.55119E 00
0.8	0.20003E 00	0.32090E 00	0.45051E 00	0.54513E 00
0.9	0.232 03E 00	0.35276E 00	0.462 81E 00	0.52460E 00
1.0	0.26079E 00	0.37506E 00	0.46209E 00	0.49537E 00
1.1	0.28546E00	0.38817E 00	0.45152E 00	0.46160E 00
1.2	0.30532E00	0.39301E 00	0.43401E 00	0.42616E 00
1.3	0.31983E 00	0.39085E 00	0.41198E 00	0.39091E 00
1.4	0.32935E 00	0.38304E 00	0.38737E 00	0.357 03E 00
1.5	0.33417E 00	0.37091E 00	0.36163E 00	0.32517E 00
1.6	0.33474E00	0.35567E 00	0.335 80E 00	0.29569E 00
1.7	0.33162E 00	0.33837E 00	0.31061E 00	0.26870E 00
1.8	0.32528E 00	0.31986E 00	0.28652E 00	0.24416E 00
1.9	0.31631E 00	0.30084E 00	0.263 82E 00	0.22196E 00
2.0	0.30539E 00	0.28182E 00	0.24264E 00	0.20195E 00
2.5	0.23754E 00	0.19675E 00	0.15964E 00	0.12839E 00
3.0	0.17283E 00	0.13576E 00	0.10731F 00	0.84915E-01
3.5	0.12377F 00	0.95232F-01	0.744 88E-01	0.58450E-01
4.0	0.89411E-01	0.68547E-01	0.53426E-01	0.41708E-01
4.5	0.65855E-01	0.50696E-01	0.39477E-01	0.306 80E-01
5.0	0.49609E-01	0.38460E-01	0.29951E-01	0.23181E-01
6.0	0.30046E-01	0.23643E-01	0.18412E-01	0.14136E-01
6.6	0.19599E-01	0.15598E-01	0.12122E-01	0.10911E-01
7.6	0.13555E-01	0.10870E-01	0.84250E-02	0.74565E-02
9.0	0.98140E-02	0.79084E-02	0.61027E-02	0.46858E-02
10.0	0.73617E-02	0.59477E-02	0.45629E-02	0.34916E-02
12.0	0.44841E-02	0.36144 E - 02	0.27041E-02	0.20804E-02
14.0	0.29850E-02	0.24018E-02	0.17747E-02	0.13307E-02
16.0	0.20905E-02	0.16715E-02	<u>0.12247E-02</u>	0.89740E-03
18.0	0.15340E-02	0.12186E-02	0.88366E-03	0.63044E-03
20.0	0.11549E-02	0.90830E-03	0.65698E-03	0.45760E-03
22.0	0.90305E-03	0.68899E-03	0.50136E-03	0.34113E-03
24.0	0.71835E-03	0.54654E-03	0.39099E-03	0.26004E-03
26.0	0.56184E-03	0.44135E-03	0.31055E-03	0.20200E-03
28.0	0.46526E-03	0.36186E-03	0.25055E-03	0.15948E-03
30.0	0.39028E-03	0.30062E-03	0.20490E-03	0.12769E-03
35.0	0.26340E-03	0.19826E-03	0.13014E-03	0.77083E-04
40.0	0.18727E-03	0.13791E-03	0.87372E-04	0.49313E-04
45.0	0.13853E-03	0.99938E-04	0.61212E-04	0.32997E-04
50.0	0.10575E-03	0.74804E-04	0.44367E-04	0.22889E-04
60.0	0.66221E-04	0.45148E-04	0.25207E-04	0.11973E-04
70.0	0.44529E-04	0.29340E-04	0.15488E-04	0.68120E-05
80.0	0.31553E-04	0.21038E-04	0.10087E-04	0.41276E-05
90.0	0.23269E-04	0.14411E-04	0.68690E-05	0.26251E-05
100.0	0.17713E-04	0.10662 E - 04	0.19598E-05	0.17365E-05

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## APPENDIX

In order to evaluate the terms used in Eq. (24) for T(l), it is convenient to employ the collective-coordinate techniques of Bohm and Pines as used by

Broyles.<sup>8</sup>

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The definitions for  $V_0$ ,  $w_{j0}$ , and  $w_{m0}$ , and the potential energy V, are given by Eqs. (9)-(11). V can be written in terms of a Fourier series, excluding the k = 0 term to allow for the boundary condition of charge neutrality:

$$V = \frac{4\pi\lambda^2}{\upsilon} \sum_{k}' \left( \frac{1}{2} \sum_{i \neq j} \frac{e^2 e^{-i\vec{k}\cdot\vec{r}_{ij}}}{(k\lambda)^2 + 1} + \frac{1}{2} \sum_{m\neq n} \frac{(2e)^2 e^{-i\vec{k}\cdot\vec{r}_{mn}}}{(k\lambda)^2 + 1} + \sum_{j,m} \frac{2e^2 e^{-i\vec{k}\cdot\vec{r}_{jm}}}{(k\lambda)^2 + 1} \right) .$$
(A1)

The prime indicates that the k = 0 term has been omitted. This will be understood in all subsequent expressions and the prime will be omitted:

$$\vec{k} = 2\pi (\upsilon)^{-1/3} \left[ n_x \hat{i} + n_y \hat{j} + n_z \hat{k} \right], \qquad (A2)$$

i.e., box normalization. The *n*'s are positive or negative integers, not all of which can be simultaneously zero. The first term of Eq. A1 can be written in terms of trigonometric functions:

$$\sum_{\vec{\mathbf{k}}} \frac{e^{-i\vec{\mathbf{k}}\cdot\vec{\mathbf{r}}_{ij}}}{(k\lambda)^2 + 1} = \sum_{\vec{\mathbf{k}}} \left(\frac{1}{(k\lambda)^2 + 1}\right) \left[\cos\left(\vec{\mathbf{k}}\cdot\vec{\mathbf{r}}_{ij}\right) - i\sin\left(\vec{\mathbf{k}}\cdot\vec{\mathbf{r}}_{ij}\right)\right].$$
(A3)

The imaginary part can be shown to sum to zero since the sine is an odd function. Then applying a familiar cosine identity, Eq. (A3) becomes

$$\sum_{\mathbf{k}} \frac{e^{-i\mathbf{k}\cdot\mathbf{\tilde{r}}_{ij}}}{(k\lambda)^{2}+1}$$

$$= \sum_{\mathbf{k}} \left(\frac{1}{(k\lambda)^{2}+1}\right) \left[\cos\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{i}\right)\cos\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{j}\right)\right]$$

$$+ \sin\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{i}\right)\sin\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{j}\right)\right]$$

$$= 2\sum_{k_{Z}\geq0} \frac{\cos\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{i}\right)\cos\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{j}\right)}{(k\lambda)^{2}+1} + 2\sum_{k_{Z}<0} \frac{\sin\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{i}\right)\sin\left(\mathbf{\tilde{k}\cdot\tilde{r}}_{j}\right)}{(k\lambda)^{2}+1}.$$
(A4)



FIG. 4. Electric microfield distribution function  $P(\epsilon)$  at a charged point for a=0.8,  $R=0, 1, \infty$ ;  $\epsilon$  is in units of  $\epsilon_0$ .



FIG. 5. Electric microfield distribution function  $P(\epsilon)$  at a charged point for R=1, a=0.2, 0.4, 0.6, 0.8;  $\epsilon$  is in units of  $\epsilon_0$ .

Next, define

$$S(\vec{k} \cdot \vec{r}) \equiv \begin{cases} \cos(\vec{k} \cdot \vec{r}), & k_z \ge 0\\ \sin(\vec{k} \cdot \vec{r}), & k_z < 0 \end{cases}$$
(A5)

This allows the following equation to be written:

$$\sum_{\vec{k}} \frac{e^{-i\vec{k}\cdot\vec{r}_{ij}}}{(k\lambda)^2+1} = \sum_{\vec{k}} \frac{2S(\vec{k}\cdot\vec{r}_i)S(\vec{k}\cdot\vec{r}_j)}{(k\lambda)^2+1}.$$
 (A6)

If similar definitions are made for the terms involving  $\exp(-i\mathbf{k}\cdot\mathbf{r}_{mn})$  and  $\exp(-i\mathbf{k}\cdot\mathbf{r}_{jm})$ , the potential energy can be written as

$$V = \frac{4\pi\lambda^2}{\upsilon} \frac{\sigma}{2} \sum_{\vec{k}} \left(\frac{1}{(k\lambda)^2 + 1}\right) \left(\sum_{i,j} \frac{2e^2}{\sigma} S_i^* S_j^* + \sum_{m,n} \frac{2(2e)^2}{\sigma} S_m^{**} S_n^{**}\right)$$



FIG. 6. Electric microfield distribution function  $P(\epsilon)$  at a charged point for  $R = \infty$ , a = 0.2, 0.4, 0.6, 0.8;  $\epsilon$  is in units of  $\epsilon_0$ .

$$+ 2 \sum_{j,m} \frac{2(2e^{2})}{\sigma} S_{j}^{*} S_{m}^{**} + 2 \sum_{i} \frac{2eq}{\sigma} S_{i}^{*} S_{0}$$
$$+ 2 \sum_{m} \frac{4eq}{\sigma} S_{m}^{**} S_{0} - \frac{2}{\sigma} e^{2} N^{*} - \frac{2}{\sigma} (2e)^{2} N^{**} \right), \quad (A7)$$

where

 $\sigma = N^{+}e^{2} + N^{++}(2e)^{2} .$ 

The last two terms subtract the self-energy that is added by removing the restrictions i=j and m=nfrom the first two terms. The two terms involving q take into account the charge  $q = \xi e$  placed at the origin. Previously, these terms have not been explicitly written, but were understood to be present for  $\xi = 0$ , 1, and 2 in the general interaction potential, Eq. (9). In subsequent expressions it will be necessary to treat them explicitly. It can be shown that Eq. (A7) is correct for any positive value of  $\xi$ . By defining the generalized coordinates

$$X_{k}^{+} \equiv \sum_{j} (2e^{2}/\sigma)^{1/2} S_{j}^{+} \text{ and } X_{k}^{++} \equiv \sum_{m} [2(2e)^{2}/\sigma]^{1/2} S_{m}^{++}$$

this expression can be written in a more compact form:

$$V = \frac{2\pi\lambda^2\sigma}{\upsilon} \sum_{\vec{k}} \left(\frac{1}{(k\lambda)^2 + 1}\right) \left[ (X_k^+)^2 + (X_k^{++})^2 + 2X_k^+ X_k^{++} + 2(2q^2/\sigma)^{1/2} S_0 (X_k^+ + X_k^{++}) - 2 \right].$$
(A8)

According to the definition [Eq. (A5)],  $S_0 = 1$  if  $k_z \ge 0$ and equals zero if  $k_z < 0$ . By using the expressions

$$\frac{2\pi\lambda^{2}\sigma}{\upsilon} = \frac{\theta_{e}}{2} \left( \frac{1+4R}{1+2R} \right) , \quad R = \frac{n^{**}}{n^{*}} , \quad \theta_{e} = kT_{e} ,$$

$$A_{k} = \frac{1}{(k\lambda)^{2}+1} , \qquad Y_{k} \equiv X_{k}^{*} + X_{k}^{**} ,$$
(A9)

V can be written as

$$V = \frac{\theta_{e}}{2} \left( \frac{1+4R}{1+2R} \right) \\ \times \left[ \sum_{\vec{k}} A_{k} Y_{k}^{2} + 2(2q^{2}/\sigma)^{1/2} \sum_{k_{Z} \ge 0} A_{k} Y_{k} - 2 \sum_{\vec{k}} A_{k} \right],$$
(A10)

where the  $Y_k$  represent a new collective coordinate. Similar transformations can be made on  $w_{j0}$  and  $w_{m0}$ , which result in

$$\sum_{j} w_{j0} = 2 \frac{\theta_{e}}{2} \left( \frac{1+4R}{1+2R} \right) \left( \frac{2q^{2}}{\sigma} \right)^{1/2} \sum_{\substack{k_{Z} \ge 0 \\ k_{Z} \ge 0}} \frac{X_{k}^{*}}{(k\lambda)^{2} + \alpha^{2}} ,$$

$$\sum_{m} w_{m0} = 2 \frac{\theta_{e}}{2} \left( \frac{1+4R}{1+2R} \right) \left( \frac{2q^{2}}{\sigma} \right)^{1/2} \sum_{\substack{k_{Z} \ge 0 \\ k_{Z} \ge 0}} \frac{X_{k}^{*+}}{(k\lambda)^{2} + \alpha^{2}} ,$$

$$\sum_{j} w_{j0} + \sum_{m} w_{m0} = \theta_{e} \left( \frac{1+4R}{1+2R} \right) \left( \frac{2q^{2}}{\sigma} \right)^{1/2} \sum_{k_{Z} \ge 0} \frac{Y_{k}}{(k\lambda)^{2} + \alpha^{2}} .$$
(A11)

Now it is possible to write  $V_0$  in terms of the collective coordinate  $Y_k$ :

$$V_{0} = V - \sum_{j} w_{j0} - \sum_{m} w_{m0}$$

$$= \frac{\theta_{e}}{2} \left( \frac{1+4R}{1+2R} \right) \left( \sum_{\vec{k}} A_{k} Y_{k}^{2} + 2(2q^{2}/\sigma)^{1/2} \right)$$

$$\times \sum_{k \neq 0} f_{k}(\alpha) A_{k} Y_{k} - 2\sum_{\vec{k}} A_{k} , \qquad (A12)$$

$$f_{k}(\alpha) = \frac{\alpha^{2} - 1}{(k\lambda)^{2} + \alpha^{2}}, \quad A_{k} = \frac{1}{(k\lambda)^{2} + 1}.$$

In order to evaluate  $\vec{\nabla}_0 V$ , it is necessary to consider the following relation:

$$\vec{\nabla}_{0}S(\vec{k}\cdot\vec{r}) = \begin{cases} \vec{\nabla}_{0}\cos(\vec{k}\cdot\vec{r}) = -\vec{k}\sin(\vec{k}\cdot\vec{r}), \ k_{Z} \ge 0\\ \vec{\nabla}_{0}\sin(\vec{k}\cdot\vec{r}) = \vec{k}\cos(\vec{k}\cdot\vec{r}), \ k_{Z} < 0 \end{cases}$$
(A13)

Changing  $\vec{k}$  to  $-\vec{k}$  we find that

$$\vec{\nabla}_0 S(\vec{\mathbf{k}} \cdot \vec{\mathbf{r}}) = \begin{cases} -\vec{\mathbf{k}} \cos(\vec{\mathbf{k}} \cdot \vec{\mathbf{r}}), & k_z \ge 0\\ -\vec{\mathbf{k}} \sin(\vec{\mathbf{k}} \cdot \vec{\mathbf{r}}), & k_z < 0 \end{cases}$$
(A14)

Therefore,

$$\vec{\nabla}_0 S(\vec{k} \cdot \vec{r}) = -\vec{k} S(\vec{k} \cdot \vec{r}) , \qquad (A15)$$

which implies that

$$\vec{\nabla}_0 \sum_{k \ge 0} Y_k = -\sum_{k < 0} Y_k \vec{k} , \qquad (A16)$$

since  $Y_k$  is a linear combination of the  $S(\vec{k} \cdot \vec{r})$ . If the gradients of the expressions given by Eqs. (9), (11), and (12) are evaluated, the terms which are summed over all  $k_z$  go to zero. The only terms that contribute are the ones summed only over negative  $k_z$ . The results are

$$\begin{split} \vec{\nabla}_{0} V &= -\theta_{e} \left( \frac{1+4R}{1+2R} \right) \left( \frac{2q^{2}}{\sigma} \right)^{1/2} \sum_{\substack{k_{Z} \geq 0}} A_{k} Y_{k} \vec{k} ,\\ \vec{\nabla}_{0} V_{0} &= -\theta_{e} \left( \frac{1+4R}{1+2R} \right) \left( \frac{2q^{2}}{\sigma} \right)^{1/2} \sum_{\substack{k_{Z} < 0}} f_{k}(\alpha) A_{k} Y_{k}(\vec{k}) ,\\ \vec{\nabla}_{0} (\sum_{j} w_{j0} + \sum_{m} w_{m0}) &= \vec{\nabla}_{0} V - \vec{\nabla}_{0} V_{0} \\ &= \frac{\theta_{e}}{2} \left( \frac{1+4R}{1+2R} \right) \left( \frac{2q^{2}}{\sigma} \right)^{1/2} \sum_{\substack{k_{Z} < 0}} \left[ \frac{1}{(k\lambda)^{2} + \alpha^{2}} \right] Y_{k} \vec{k} . \end{split}$$

Sufficient definitions have now been made so that  $T_0(l)/T_0(0)$ , the first factor in T(l), can be written in terms of collective coordinates

$$\frac{T_0(l)}{T_0(0)} = \frac{\int \dots \int \exp(-\beta_i V_0 - iq^{-1} \vec{l} \cdot \vec{\nabla}_0 V_0) \prod_{j=1}^{N^+} \prod_{m=1}^{N^{++}} d\vec{\mathbf{r}}_j d\vec{\mathbf{r}}}{\int \dots \int \exp(-\beta_i V_0) \prod_{j=1}^{N^+} \prod_{m=1}^{N^{++}} d\vec{\mathbf{r}}_j d\vec{\mathbf{r}}_m}$$

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$$= \frac{\int \cdots \int \exp\{-\beta_i \theta_e/2) [(1+4R)/(1+2R)] \sum_{k} [A_k Y_k^2 + 2b_k(l) Y_k] \} J \prod dY_k}{\int \cdots \int \exp\{-\beta_i \theta_e/2) [(1+4R/(1+2R)] \sum_{k} [A_k Y_k^2 + 2b_k(0) Y_k] \} J \prod dY_k} ,$$

$$b_{k}(l) = \left(\frac{2q^{2}}{\sigma}\right)^{1/2} f_{k}(\alpha) A_{k} \times \begin{cases} 1, & k_{z} \ge 0\\ -i\theta_{i}q^{-1}\vec{l}\cdot\vec{k}, & k_{z} < 0 \end{cases}$$

$$(2q^{2})^{1/2} \qquad (1 \qquad h \ge 0)$$

$$b_k(0) = \left(\frac{2q^2}{\sigma}\right) + f_k(\alpha)A_k \times \begin{cases} 1 & k_Z \leq 0 \\ 0 & k_Z < 0 \end{cases}, \qquad k_Z < 0 .$$

The self-energy portions of  $V_0$ , appearing in both the numerator and the denominator, are independent of the integrations and cancel. J is the Jacobian of the transformation from  $\vec{r}_{ij}$  and  $\vec{r}_{mn}$  to  $\vec{Y}_k$ . If we define

$$A'_{k} \equiv \frac{\theta_{e}}{\theta_{i}} \left( \frac{1+4R}{1+2R} \right) A_{k} \equiv uA_{k} ,$$

$$b'_{k} \equiv \frac{\theta_{e}}{\theta_{i}} \left( \frac{1+4R}{1+2R} \right) b_{k} \equiv ub_{k} ,$$
(A19)

the expression for  $T_0(l)/T_0(0)$  can be put in the form

$$\frac{T_0(l)}{T_0(0)} = \frac{\int \dots \int \exp\left[-\frac{1}{2}\sum_{\mathbf{k}} (A'_k Y^2_{\mathbf{k}} + 2b'_k(l) Y_k)\right] J \prod dY_k}{\int \dots \int \exp\left[-\frac{1}{2}\sum_{\mathbf{k}} (A'_k Y^2_{\mathbf{k}} + 2b'_k(0) Y_k\right] J \prod dY_k}$$
(A20)

This allows for evaluation of the integrals according to the formalism used by Broyles. The multiple integrations are thus evaluated:

$$\frac{T_0(\ell)}{T_0(0)} = \frac{\exp\left\{\frac{1}{2}\sum_{\mathbf{k}} [b_k'(\ell)]^2 / (1+A_k')\right\} [1-a_3(\ell)+a_4(\ell)\cdots]}{\exp\left\{\frac{1}{2}\sum_{\mathbf{k}} [b_k'(0)]^2 / (1+A_k')\right\} [1-a_3(0)+a_4(0)\cdots]}.$$

 $a_3$  and  $a_4$  can be shown to be small and are neglected. The definitions of  $b'_k(l)$  and  $b'_k(0)$  further allow us to write

$$\frac{T_0(l)}{T_0(0)} = \exp\left\{\frac{-\theta_e^2}{\sigma} \left(\frac{1+4R}{1+2R}\right)^2 \sum_{k_Z < 0} \left[\frac{f_k^2(\alpha) A_k^2(\vec{\ell} \cdot \vec{k})^2}{1+A_k'}\right]\right\}.$$
(A22)

The sum over k is now replaced by an integral and evaluated. The result of this integration, in terms of conveniently defined reduced variables, is

$$T_{0}(l)/T_{0}(0) = e^{-\gamma L^{2}},$$
  

$$\gamma = \frac{a}{4} \frac{\theta_{i}}{\theta_{e}} \frac{1}{[\alpha^{2} - (1 + u)]^{2}} \{\alpha^{5}u + 2[1 - (1 + u)^{3/2}]\alpha^{4}$$

$$+ (2u + u^{2}) \alpha^{3} - 4 (1 + u) [(1 - u)^{1/2}] \alpha^{2} - 3 (u + u^{2}) \alpha + 2 [(1 + u)^{2} - (1 + u)^{3/2}] \} ,$$

$$u = \frac{\theta_{e}}{\theta_{i}} \left(\frac{1 + 4R}{1 + 2R}\right), \quad R = \frac{n^{**}}{n^{*}}, \quad \theta_{e} = kT_{e} , \quad \theta_{i} = kT ,$$

$$\frac{4}{3} \pi r_{0}^{3} n_{e} = 1 , \quad a = \frac{\gamma_{0}}{\lambda} , \quad \epsilon_{0} = \frac{e}{r_{0}^{2}} , \quad L = \epsilon_{0} l .$$
(A23)

With this choice of reduced quantities, the unit of electric field strength  $\epsilon_0$  is a function of electron density only.

In order to evaluate the remaining terms in the exponential of Eq. (24), it is necessary to derive an expression for  $Q_{jm}(l)$  in terms of these same reduced quantities. Collective coordinates are used again with the modification indicated below.  $Q_{jm}(l)$  is defined by Eq. (16). In terms of collective coordinates

$$Q_{jm}(l) = \frac{\int \cdots \int \exp\left\{-\frac{1}{2}\sum_{\vec{k}} \left[A'_{k} Y^{2}_{k} + 2b'_{k}(l) Y_{k}\right]\right\} \prod_{j+1}^{N^{*}} \prod_{n+1}^{N^{*+}} d\vec{r}_{i} d\vec{r}_{n}}{\int \cdots \int \exp\left\{-\frac{1}{2}\sum_{\vec{k}} \left[A'_{k} Y^{2}_{k} + 2b'_{k}(l) Y_{k}\right]\right\} \prod_{i=1}^{N^{*}} \prod_{n=1}^{N^{*+}} d\vec{r}_{i} d\vec{r}_{n}}.$$
(A24)

In order to do the  $(N^* - j) + (N^{**} - m)$  integrals, it is convenient to introduce another collective coordinate:

$$Y'_{k} \equiv Y_{k} - y_{k} \equiv (X^{*}_{k} + X^{**}_{k}) - (a^{*}_{k} + a^{**}_{k}), \qquad (A25)$$

where

(A21)

$$a_{k}^{+} \equiv \left(\frac{2e^{2}}{\sigma}\right)^{1/2} \sum_{i=1}^{j} S^{+}(\vec{\mathbf{k}} \cdot \vec{\mathbf{r}}_{i}),$$
$$a_{k}^{++} \equiv \left(\frac{2(2e)^{2}}{\sigma}\right)^{1/2} \sum_{n=1}^{m} S^{++}(\vec{\mathbf{k}} \cdot \vec{\mathbf{r}}_{n}).$$

In terms of this new collective coordinate the exponentials in Eq. (A24) are

$$-\frac{1}{2}\sum_{\vec{k}}(A'_{k}Y_{k}^{2}+2b'_{k}Y_{k})=-\frac{1}{2}\sum_{\vec{k}}[A'_{k}(Y'_{k})^{2}+2(y_{k}A'_{k}+b'_{k})Y'_{k}+Y_{k}^{2}A'_{k}+2y_{k}b'_{k}].$$
 (A26)

This allows factors of  $Q_{jm}(l)$  to be integrated by the collective-coordinate technique as follows:

$$Q_{jm}(l) = \frac{\exp\{-\frac{1}{2}\sum_{\vec{k}}[A'_{k}y^{2}_{k}+2y_{k}b'_{k}]\} \int \dots \int \exp\{-\frac{1}{2}\sum_{\vec{k}}[A'_{k}(Y'_{k})^{2}+2(y_{k}A'_{k}+b'_{k})]\} J dY_{k}}{\int \dots \int \exp\{-\frac{1}{2}\sum_{\vec{k}}[A'_{k}y^{2}_{k}+2y_{k}b'_{k}]\} \int \dots \int \exp\{-\frac{1}{2}\sum_{\vec{k}}[A'_{k}(Y'_{k})^{2}+2(y_{k}A'_{k}+b'_{k})]\} J dY_{k}\prod \prod_{n} m d\vec{r}_{i} d\vec{r}_{n}}$$

$$= \frac{\exp\{\frac{1}{2}\sum_{\vec{k}}[y_{k}A'_{k}+b'_{k})^{2}/(1+A'_{k})-y^{2}_{k}A'_{k}-2y_{k}b'_{k}]\}}{\int \dots \int \exp\{\frac{1}{2}\sum_{\vec{k}}[(y_{k}A'_{k}+b'_{k})^{2}/(1+A'_{k})-y^{2}_{k}A'_{k}-2y_{k}b'_{k}]\}}{\int \dots \int \exp\{\frac{1}{2}\sum_{\vec{k}}[(y_{k}A'_{k}+b'_{k})^{2}/(1+A'_{k})-y^{2}_{k}A'_{k}-2y_{k}b'_{k}]\}}$$
(A27a)

$$=\frac{(\mathfrak{U})^{-j-m}\exp\{-\frac{1}{2}\sum_{\vec{k}}(y_{k}^{2}A_{k}')/(1+A_{k}')-\sum_{\vec{k}}(y_{k}b_{k}')/(1+A_{k}')\}}{(\mathfrak{U})^{-j-m}\int\cdots\int\exp\{-\frac{1}{2}\sum_{\vec{k}}(y_{k}^{2}A_{k}')(1+A_{k}')-\sum_{\vec{k}}(y_{k}b_{k}'(1+A_{k}'))\}}\prod_{j}\prod_{m}d\vec{\mathbf{r}_{j}}d\vec{\mathbf{r}_{m}}}$$
(A27b)

The last equation has been simplified algebraically and the terms in the numerator and denominator that are independent of  $y_k(\mathbf{r})$  have been canceled. For  $Q_{10}$  and  $Q_{01}$ , the sum  $\sum_{\mathbf{k}} \left[ y_k^2 A'_k / (1 + A'_k) \right]$  appearing in the numerator and denominator is independent of the coordinates of integration and will also cancel. In the thermodynamic limit, it can be shown that the denominator of Eq. (A37b) becomes

$$\upsilon \rightarrow \infty \left\{ \frac{1}{\upsilon} \int \exp\left[-\sum_{\vec{k}} \frac{y_k b'_k}{1+A'_k}\right] d\vec{r} \right\} = 1 .$$
 (A28)

It is also necessary to have expressions for  $-\beta_i w_{j0}$  and  $-\beta_i w_{m0}$  and their respective gradients, in terms of the reduced variables defined in Eqs. (A23) and (A31). These are listed below:

$$-\beta_{i}w_{j0} \equiv -\frac{1}{\theta_{i}}\frac{qe}{r_{j0}}e^{-\alpha r_{j0}/\lambda} = -\xi\left(\frac{\theta_{e}}{\theta_{i}}\right)\frac{a^{2}}{3x}e^{-\alpha ax} = -\beta w,$$

$$-\beta_{i}w_{m0} = -\frac{1}{\theta_{i}}q\frac{2e}{r_{m0}}e^{-\alpha r_{m0}/\lambda}$$

$$= -2\xi\left(\frac{\theta_{e}}{\theta_{i}}\right)\frac{a^{2}}{3x}e^{-\alpha ax} = -2\beta w, \qquad (A33)$$

$$-iq^{-1}\ell\cdot\nabla_0 w_{j0} = iL\cos\theta[(e^{-\alpha ax}/x^2)(1+\alpha ax)],$$
  
$$-iq^{-1}\tilde{\ell}\cdot\vec{\nabla}_0 w_{m0} = 2iL\cos\theta(e^{-\alpha ax}/x^2)(1+\alpha ax).$$

By comparing the expressions for T(l) given by Eqs. (19) and (24), we can define  $I_{10}$  and  $I_{01}$ :

$$I_{10} \equiv n^{*}[h_{10}(l) - h_{10}(0)]$$
  
=  $n^{*}[\int g_{10}(l)\chi^{*}(l, 1)d\mathbf{r} - \int g_{10}(0)\chi^{*}(0, 1)d\mathbf{r}],$   
(A34)  
$$I_{01} \equiv n^{**}[h_{01}(l) - h_{01}(0)]$$
  
=  $n^{**}[\int g_{01}(l)\chi^{**}(l, 1)d\mathbf{r} - \int g_{01}(0)\chi^{*}(0, 1)d\mathbf{r}].$ 

The remaining variables can be transformed to the set of dimensionless quantities defined by Eq.(A23):

$$n^{*}d\mathbf{\hat{r}} = n^{*}r^{2}dr \, d\Omega = [3/(1+2R)]x^{2} \, dx \, d\Omega ,$$

$$n^{**}d\mathbf{\hat{r}} = n^{**}r^{2}dr \, d\Omega = [3R/(1+2R)]x^{2} \, dx \, d\Omega .$$
(A35)

The relationship between  $g_{jm}$  and  $Q_{jm}$  [Eq. (18)] together with Eq. (A30) allows  $I_{10}$  to be written as

$$I_{10} = \frac{3}{1+2R} \frac{1}{2} \int_0^\infty \left( \int_0^{\pi} \int_0^{2\pi} \int_0^{2\pi} \int_0^{\pi} \int_0^{2\pi} \int_0^{\pi} \int_0^{\pi} \int_0^{\pi} \int_0^{2\pi} \int_0^{\pi} \int_0$$

(e<sup>-pwj0-i</sup> ×e L(VOW)COS  $(d)^{2} - 1 d\Omega$ 

$$-\int_0^{\pi} \int_0^{2\pi} e^{s(x)} \left( e^{-\beta w_{j0}} - 1 \right) d\Omega \bigg) x^2 dx . \quad (A36)$$

The angular integration can be easily performed to give

$$I_{10} = \frac{3}{1+2R} \int_{0}^{\infty} x^{2} dx \, e^{s(x)} \left[ e^{-\beta w} \left( \frac{\sin(LG(x))}{(LG(x))} - 1 \right) - \left( \frac{\sin(Lq(x))}{(Lq(x))} - 1 \right) \right],$$
(A37)

where

$$G(x) = q(x) + \frac{e^{-\alpha ax}}{x^2} [1 + \alpha ax]$$
 (A38)

In a similar manner  $I_{01}$  can be evaluated as

$$I_{01} = \frac{3R}{1+2R} \int_{0}^{\infty} x^{2} dx e^{2s(x)} \left[ e^{-2\beta w} \left( \frac{\sin(2LG(x))}{2LG(x)} - 1 \right) - \left( \frac{\sin(2Lq(x))}{2Lq(x)} \right) \right].$$
 (A39)

In order to calculate  $I_{20}$ ,  $I_{02}$ , and  $I_{11}$ , it is necessary to have expressions for  $\sum_{\mathbf{k}} \left[ y_k b'_k / (1 + A'_k) \right]$  and  $\sum_{\mathbf{k}} \left[ y_{\mathbf{k}}^{2} A'_{\mathbf{k}} / (1 + A'_{\mathbf{k}}) \right]$  in each case. For convenience we label these cases (a), (b), and (c), respectively. Case (a). As seen in Eq. (A25),  $y_k$  is given by

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$$y_{k} = (2e^{2}/\sigma)^{1/2} \left[ S(\mathbf{k} \cdot \mathbf{r}_{1}) + S(\mathbf{k} \cdot \mathbf{r}_{2}) \right].$$
 (A40)

Therefore

$$-\sum_{k} \frac{y_{k}A'_{k}}{1+A_{k}} = [s(x_{1})+iLq(x_{1})\cos\theta_{1}] + [s(x_{2})+iLq(x_{2})\cos\theta_{2}], \quad (A41)$$

which is a linear combination of the expressions for the first-order term. Similar considerations give the necessary expressions for cases (b) and (c). Case(b):

$$-\sum_{\vec{k}} \frac{y_{k}A'_{k}}{1+A'_{k}} = 2 \left[ s(x_{1}) + iLq(x_{1})\cos\theta_{1} \right] \\ + 2 \left[ s(x_{2}) + iLq(x_{2})\cos\theta_{2} \right].$$
(A42)

Case (c):

$$-\sum_{k} \frac{y_{k}A'_{k}}{1+A'_{k}} = [s(x_{1})+iLq(x_{1})\cos\theta_{1}] + 2[s(x_{2})+iLq(x_{2})\cos\theta_{2}]. \quad (A43)$$

For case (c), particle 2 is assumed to be doubly charged.

In order to evaluate the second term of these expressions, we also need an expression for  $y_k^2$  in each case.

$$Case (a):$$
  

$$y_{k}^{2} = (2e^{2}/\sigma) \left[ S^{2}(\vec{k} \cdot \vec{r}_{1}) + 2S(\vec{k} \cdot \vec{r}_{1}) S(\vec{k} \cdot \vec{r}_{2}) + S^{2}(\vec{k} \cdot \vec{r}_{2}) \right].$$
(A44)

When summed over k, the  $S^2(\vec{k} \cdot \vec{r})$  terms in the numerator and denominator of (A44) are independent of r and will cancel in the same manner as that seen when  $I_{10}$  was evaluated [see Eq. (A27)]. Hence, the necessary terms are

$$y_{k}^{2} = (4e^{2}/\sigma) S(\vec{k} \cdot \vec{r}_{1}) S(\vec{k} \cdot \vec{r}_{2}) .$$
 (A45)

Case(b):

$$y_k^2 = [4(2e)^2/\sigma] S(\vec{k} \cdot \vec{r}_1) S(\vec{k} \cdot \vec{r}_2)$$
 (A46)

Case(c):

$$y_k^2 = [4(2e^2)/\sigma] S(\vec{k} \cdot \vec{r}_1) S(\vec{k} \cdot \vec{r}_2)$$
 (A47)

If Eqs. (A45)-(A47) are used to evaluate  $-\frac{1}{2}\sum_{\mathbf{k}} \left[ y_k^2 A'_k / (1+A'_k) \right]$ , the results are as follows. *Case* (a):

$$-\frac{1}{2}\sum_{\vec{k}} \frac{y_{\vec{k}}^2 A'_{\vec{k}}}{1+A'_{\vec{k}}} = -\frac{2e^2}{\sigma} \sum_{\vec{k}} \frac{S(\vec{k}\cdot\vec{r}_1)S(\vec{k}\cdot\vec{r}_2)}{1+A'_{\vec{k}}} A'_{\vec{k}}$$
$$= \frac{-2e^2}{\sigma} \sum_{\substack{k_Z \ge 0}} \frac{u\cos\left[\vec{k}\cdot(\vec{r}_1-\vec{r}_2)\right]}{(k\lambda)^2+(1+u)}$$
$$= \frac{-\theta_g}{\theta_i} \frac{a^2}{3x_{12}} \exp\left[-(1+u)^{1/2}ax_{12}\right]. (A48)$$

Case(b):

$$-\frac{1}{2}\sum_{\mathbf{k}}\frac{y_{\mathbf{k}}^{2}A_{\mathbf{k}}'}{1+A_{\mathbf{k}}'} = -4\frac{\theta_{e}}{\theta_{i}}\frac{a^{2}}{3x_{12}}\exp[-(1+u)^{1/2}ax_{12}].$$
(A49)

Case (c):

$$-\frac{1}{2}\sum_{k}\frac{y_{k}^{2}A_{k}^{\prime}}{1+A_{k}^{\prime}} = -2\frac{\theta_{e}}{\theta_{i}}\frac{a^{2}}{3x_{12}}\exp[-(1+u)^{1/2}ax_{12}].$$
(A50)

In Eqs. (A48)-(A50) the summations over k were replaced by integrals which were then evaluated.

The expression for  $I_{20}$ , obtained by comparing the expressions for T(l) in Eqs. (19) and (24) is

$$\begin{split} I_{20} &\equiv \frac{(n^{*})^{2}}{2!} \left[ h_{20}(l) - h_{20}(0) \right] \\ &= \frac{(n^{*})^{2}}{2!} \left\{ \upsilon^{2} \int \int \left[ Q_{20}(l;1,2) - Q_{10}(l,1) Q_{10}(l,2) \right] \right. \\ &\times \chi^{*}(l,1) \chi^{*}(l,2) d\vec{\mathbf{r}}_{1} d\vec{\mathbf{r}}_{2} \\ &- \upsilon^{2} \int \int \left[ Q_{20}(0;1,2) - Q_{10}(0,1) Q_{10}(0,2) \right] \\ &\times \chi^{*}(0,1) \chi^{*}(0,2) d\vec{\mathbf{r}}_{1} d\vec{\mathbf{r}}_{2} \right\} . \end{split}$$
(A51)

If Eqs. (A48)-(A50) are used to evaluate  $Q_{20}(l)$ , as given in Eq. (A27), the result is

$$Q_{20}(l; 1, 2) = Q_{10}(l; 1) \ Q_{10}(l; 2)$$

$$\times \exp\left(\frac{-\theta_e}{\theta_i} \frac{a^2}{3x_{12}} e^{-(1+u)^{1/2}ax_{12}}\right).$$
(A52)

This can be substituted into the definition of  $h_{20}(l)$ :

$$h_{20}(l) = \upsilon^{2}(a\lambda)^{6} \iint Q_{10}(l; 1) Q_{10}(l, 2) \chi^{*}(l; 1) \chi^{*}(l, 2)$$

$$\times \left[ \exp\left(\frac{-\theta_{e}}{\theta_{i}} - \frac{a^{2}}{3x_{12}} e^{-(1+u)^{1/2}ax}\right) - 1 \right] d\bar{\mathbf{x}}_{1} d\bar{\mathbf{x}}_{2} d\bar{\mathbf{x$$

As indicated in the body of this paper, the expression appearing in brackets is the Debye-Hückel pair correlation function which can be simplified by employing the linearized approximation:

$$\left[ \exp\left(\frac{-\theta_e}{\theta_i} \frac{a^2}{3x_{12}} e^{-(1+u)^{1/2}ax}\right) - 1 \right]$$
$$= -\frac{\theta_e}{\theta_i} \frac{a^2}{3x_{12}} e^{-(1+u)^{1/2}ax} = \frac{\theta_e}{\theta_i} V(x_{12}) \quad . \quad (A54)$$

The pair potential  $V(x_{12})$  can be decoupled by the method of Swiatecki<sup>9</sup>:

$$V(x_{12}) \equiv \frac{-a^2}{3x_{12}} \exp\left[-a'x_{12}\right]$$
  
=  $+\sum_{k=0}^{\infty} (2k+1) V_k(x_1, x_2) P_k(\cos\theta_{12}) , (A55)$   
 $V_k(x_1, x_2) = -\frac{1}{2} \int_0^{\pi} \frac{a^2}{3x_{12}} e^{-a'x_{12}} P_k(\cos\theta) \sin\theta d\theta ,$   
(A56)

where  $a' = (1+u)^{1/2}a$ .  $V_k$  has been evaluated by Swiatecki as

$$V_{k}(x_{1}, x_{2}) = \frac{-a^{2}}{3} \frac{K_{k+1/2}(a'x_{1})}{\sqrt{x_{1}}} \frac{I_{k+1/2}(a'x_{2})}{\sqrt{x_{2}}} ,$$

$$x_{1} > x_{2} .$$
(A57)

I and K are modified Bessel functions.<sup>6</sup> The Legendre polynomial  $P_k(\cos\theta_{12})$  can be written as<sup>10</sup>

$$P_{k}(\cos\theta_{12}) = \sum_{m=0}^{k} \epsilon_{m} \left( \frac{(k-m)!}{(k+m)!} \right)$$
$$\times P_{k}^{m}(\cos\theta_{1}) P_{k}^{m}(\cos\theta_{2}) \cos(m(\varphi_{1}-\varphi_{2}))$$

$$\epsilon_m = \begin{cases} 1, & m = 0 \\ 2, & m \neq 0 \end{cases} \quad (A58)$$

Since  $\int_0^{2\pi} \int_0^{2\pi} d\varphi_1 d\varphi_2 \cos(m(\varphi_1 - \varphi_2))$ , used in the evaluation of Eq. (A53), is nonzero only if m = 0, the only contributing term in Eq. (A58) is  $P_k(\cos\theta_1) \times P_k(\cos\theta_2)$ . This form for  $P_k(\cos\theta_{12})$  and the Swiatecki expression [Eq. (A57)] allow  $h_{20}(l)$  and  $h_{20}(0)$  to be written as

$$h_{20}(l) = (a\lambda)^{6} \frac{\theta_{\theta}}{\theta_{i}} \left(\frac{-a^{2}}{3}\right) \sum_{k} (2k+1)$$

$$\times \iint d\vec{\mathbf{x}}_{1} d\vec{\mathbf{x}}_{2} f(x_{1}) g(x_{2}) \quad , \qquad (A59)$$

$$f(x_1) = \exp[s(x_1) + iLq(x_1)\cos\theta_1]$$

$$\times \{\exp\left[-\beta w(x_1) + iL\nabla w(x_1)\cos\theta_1\right] - 1\}$$

$$\times P_b(\cos\theta_1)K_{ba1/2}(a'x_1)/\sqrt{x_1}, \quad (A60)$$

$$1 \ k (cob(1)) \ k + 1 / 2 (a \ x_1) / x_1 ;$$
 (P

$$g(x_2) = \exp[s(x_2) + iLq(x_2)\cos\theta_2]$$

$$\times \{\exp[-\beta w(x_2) + iL\nabla w(x_2)\cos\theta_2] - 1\}$$

$$\times P_k(\cos\theta_2)I_{k+1/2}(a'x_2)/\sqrt{x_2}$$

for 
$$x_1 > x_2$$
, (A61)

$$h_{20}(0) = (a\lambda)^6 \frac{\theta_e}{\theta_i} (4\pi)^2 \left(\frac{-a^2}{3}\right)$$

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$$\times 2\delta_{k0} \int_{0}^{\infty} dx_{2} \int_{x_{2}}^{\infty} dx_{1} f_{0}(x_{1}) g_{0}(x_{2}) , \qquad (A62)$$

$$f_0(x_1) = x_1^{3/2} K_{1/2}(a'x_1) e^{s(x_1)} (e^{-\beta w(x_1)} - 1) , \quad (A63)$$

$$g_0(x_2) = x_2^{3/2} I_{1/2}(a'x_2) e^{s(x_2)} (e^{-\beta w(x_2)} - 1) .$$
 (A64)

By using the integral definition of the spherical **Bessel** function

$$j_k(Z) \equiv \frac{1}{2} (-i)^k \int_0^{\pi} e^{iZ\cos\theta} P_k(\cos\theta) \sin\theta \,d\theta , \quad (A65)$$

the angular portion of Eq. (A59) can be evaluated. If these forms for  $h_{20}(l)$  and  $h_{20}(0)$  are used in Eq. (A51), the final form for  $I_{20}$  becomes

$$I_{20} = \frac{\theta_e}{\theta_t} \left[ \frac{1}{1+2R} \right]^2 3a^2 \sum_k (-1)^k (2k+1) \{20\} ,$$

$$\{20\} = \left\{ \int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) e^{s(x_2)} \left[ e^{-\beta w(x_2)} j_k(LG(x_2)) - j_k(Lq(x_2)) \right] - \delta_{k0} \int_0^\infty x_1^{3/2} K_{k+1/2}(a'x_1) e^{s(x_1)} \right.$$

$$\times \left[ e^{-\beta w(x_1)} j_k(LG(x_1)) - j_k(Lq(x_1)) \right] dx_1 dx_2 x_2^{3/2} I_{1/2}(a'x_2) e^{s(x_2)} \\ \times \left( e^{-\beta w(x_2)} - 1 \right) \int_{x_2}^\infty x_1^{3/2} K_{1/2}(a'x_1) e^{s(x_1)} \left[ e^{-\beta w(x_1)} - 1 \right] dx_1 dx_2 \right\} .$$
(A66)

 $I_{02}$  is relatively simple and can be treated similarly with only appropriate factors of two needing to be considered. The final form is

$$I_{02} = 4 \frac{\theta_e}{\theta_i} \left(\frac{R}{1+2R}\right)^2 3a^2 \sum_k (-1)^k (2k+1) \{02\}, \qquad (A67)$$

$$\{02\} = \left\{ \int_0^\infty x_2^{3/2} I_{k+1/2}(a'x_2) e^{2s(x_2)} \left[ e^{-2\beta w(x_2)} j_k (2LG(x_2)) - j_k(2Lq(x_2)) \right] \right\}$$

$$\times \int_{x_2}^\infty x_1^{3/2} K_{k+1/2}(a'x_1) e^{2s(x_1)} \left[ e^{-2\beta w(x_1)} j_k(2LG(x_1)) - j_k(2Lq(x_1)) \right] dx_1 dx_2$$

$$- \delta_{k0} \int_0^\infty x_2^{3/2} I_{1/2}(a'x_2) e^{2s(x_2)} (e^{-2\beta w(x_2)} - 1) \int_{x_2}^\infty x_1^{3/2} K_{1/2}(a'x_1) e^{2s(x_1)} (e^{-2\beta w(x_1)} - 1) dx_1 dx_2 \right\}.$$

 $I_{11}$  has more subtle differences. First, there is a factor of 2 multiplying  $V(r_{12})$  [compare Eqs. (A48) and (A50)]. Second, as can be seen from the definition of  $I_{11}$ , obtained by comparing Eqs. (22) and (36), there is no 2! dividing the densities.

Third, because the integrand is not symmetric in  $x_1$  and  $x_2$ , the cases  $x_1 > x_2$  and  $x_1 < x_2$  cannot be replaced by one integration which results in another factor of 2. With these differences accounted for, the final expression is

$$\times \int_{0}^{2} x_{1}^{3/2} I_{k*1/2}(a'x_{1}) e^{s(x_{1})} \left[ e^{-\beta w(x_{1})} j_{k}(LG(x_{1})) - j_{k}(Lq(x_{1})) \right] dx_{1} dx_{2} - \delta_{k0} \int_{0}^{\infty} x_{2}^{3/2} I_{1/2}(a'x_{2}) e^{2s(x_{2})} (e^{-2\beta w(x_{2})} - 1) \int_{x_{2}}^{\infty} x_{1}^{3/2} K_{1/2}(a'x_{1}) e^{s(x_{1})} (e^{-\beta w(x_{1})} - 1) dx_{1} dx_{2} - \delta_{k0} \int_{0}^{\infty} x_{2}^{3/2} K_{1/2}(a'x_{2}) e^{2s(x_{2})} (e^{-2\beta w(x_{2})} - 1) \int_{0}^{x_{2}} x_{1}^{3/2} I_{1/2}(a'x_{1}) e^{s(x_{1})} (e^{-\beta w(x_{1})} - 1) dx_{1} dx_{2} - \delta_{k0} \int_{0}^{\infty} x_{2}^{3/2} K_{1/2}(a'x_{2}) e^{2s(x_{2})} (e^{-2\beta w(x_{2})} - 1) \int_{0}^{x_{2}} x_{1}^{3/2} I_{1/2}(a'x_{1}) e^{s(x_{1})} (e^{-\beta w(x_{1})} - 1) dx_{1} dx_{2}$$

With these expressions for  $I_{im}(l)$  up to second order, we can evalute T(l):

$$T(l) = \exp\left[-\gamma L^2 + I_{10}(l) + I_{01}(l) + I_{20}(l) + I_{02}(l) + I_{11}(l)\right].$$
(A69)

If we omit the last three terms in the exponent we

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<sup>1</sup>E. W. Smith, Phys. Rev. <u>166</u>, 102 (1968). References 1-3 are meant only as illustrations of the several line broadening theories and are not intended to be exhaustive.

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<sup>4</sup>M. Baranger and B. Mozer, Phys. Rev. 115, 521

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get

$$T(l) = \exp\left[-\gamma L^2 + I_{10}(l) + I_{01}(l)\right], \qquad (A70)$$

• which is referred to as the first approximation to T(l). Then in this sense the second approximation to T(l) is given by Eq. (A69).

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<sup>5</sup>C. F. Hooper, Jr., Phys. Rev. <u>149</u>, 77 (1966); <u>165</u>, 215 (1968); 169, 193 (1968).

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## Laser with a Transmitting Window\*

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The effect of transmission of radiation through one mirror of a laser is investigated. For a laser oscillator the result is to change the effective resonance frequency and Q of the cavity. Using the same model for the cavity, a signal is injected into the active medium through the transmitting window, and its effect on the system studied. When the external signal is strong enough and sufficiently close to the natural frequency of the laser oscillator, the laser locks its frequency to the input signal. The equations describing the system are solved over the range of input frequencies where the laser is locked, and the resulting gain found. In the high-intensity limit the medium saturates, and the gain tends to that of a lossy cavity. As the input intensity vanishes, the gain approaches infinity and the system tends to a laser oscillator.

#### I. INTRODUCTION

It is the purpose of this paper to investigate the effects on the operation of a laser arising from the fact that to some extent it is in communication with the rest of space outside the resonant cavity; i.e.,

some of its internal energy is escaping through the windows. As a result the effective cavity Q is lowered, and there is a slight change in operating frequency. Furthermore, using the same techniques it is possible to consider the case of an external signal applied to the laser through one of its