## Convection in <sup>3</sup>He-superfluid-<sup>4</sup>He mixtures: Measurement of the superfluid effects

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Dilute superfluid mixtures bridge the Prandtl-number range between liquid metals and water:  $0.04 < N_{Pr} < 2$ . The convective equations of motion for superfluid mixtures are the equations for Rayleigh-Bénard convection in a normal single-component fluid plus additional superfluid terms. We have measured the latter through their effect on the critical Rayleigh number  $R_c$ . The corrections can be only a few percent for 1.0 < T < 2.0 K, implying an accessible Prandtl-number range near onset of at least  $0.04 < N_{Pr} < 1.5$ .

Rayleigh-Bénard convection (RBC) has been the subject of much recent study.<sup>1</sup> An interesting variation is convection in <sup>3</sup>He-superfluid-<sup>4</sup>He mixtures. Of interest here is the fact that the equations of motion for superfluid mixture convection (SMC) resemble those for ordinary RBC but with additional terms representing superfluid corrections. To the extent that the latter are small, SMC should behave like standard RBC but with a remarkable Prandtl-number range ( $\mathcal{N}_{Pr}$  defined below), one which is unattainable with any other fluid:  $0.04 < N_{Pr} < 2$ . The instabilities of the convective state, which strongly affect the transition to turbulence, change significantly over this Prandtl-number range.<sup>2</sup> SMC has the potential to be an extremely valuable tool for understanding convective flows, but the extent of the superfluid corrections must be determined first.

Previously, the size of the superfluid corrections was not well known; we have made the first direct determination. The experiments were carried out on a mixture of <sup>3</sup>He molar concentration X=0.014 (mass concentration c=0.011) and over a temperature range 1.0 < T < 1.9 K.

Experiments on SMC were pioneered by Wheatley and co-workers,<sup>3,4</sup> and have been pursued more recently by Mainieri, Sullivan, and Ecke.<sup>5</sup> Theoretical work has been carried out by Steinberg,<sup>6,7</sup> Fetter,<sup>8,9</sup> and Steinberg and Brand.<sup>10</sup>

The primary dimensionless parameters for SMC are the Rayleigh number  $R = |\alpha_{p,\mu_4}| gd^3 \Delta T/v\chi_{eff}$  and the Prandtl number  $\mathcal{N}_{Pr} = v_n/\chi_{eff}$ . Here,  $\Delta T$  is the temperature difference across a fluid layer of height *d*. The fluid parameters,  $\alpha_{p,\mu_4}$ ,  $\chi_{eff}$ , and *v* are, respectively, the expansion coefficient at constant pressure and <sup>4</sup>He chemical potential  $\mu_4$ , an effective thermal diffusivity, and the kinematic viscosity; *g* is the acceleration of gravity. Also,  $v_n = (\rho/\rho_n)v$ , where  $\rho$  and  $\rho_n$  are, respectively, the total and normal fluid densities.

The superfluid corrections can be obtained in terms of three parameters,  $\epsilon_1$ ,  $\epsilon_2$ , and  $\epsilon_3$  in Fetter's notation.<sup>8</sup> The first two are proportional to  $\Delta T$ , which, in turn, at the onset of convection is proportional to  $1/d^3$  (see the definition of R). The third parameter is proportional to d, independent of  $\Delta T$ , and a function of several thermohydrodynamic quantities, including the normal viscosity and the second viscosities.<sup>11</sup>

In this paper, we will focus on the effect which these

corrections have on the onset of convection. Fetter has shown for a horizontally infinite layer that up to second order in the  $\epsilon_i$ , the critical Rayleigh number has the form

$$R_c \approx R_{c0} + 24.6\epsilon_1\epsilon_2 + 10.2(\epsilon_1 - \epsilon_2)^2 - 19.9\epsilon_2(\epsilon_1\rho/\rho_s - \epsilon_3), \qquad (1)$$

where  $R_c$  is the Rayleigh number at the onset of convection and  $R_{c0} = 1707...$  is the critical Rayleigh number for classical RBC.

Equation (1) implies that  $R_c \rightarrow R_{c0}$  as  $d^{-2} \rightarrow 0$ ; thus, the correction terms can be determined by measuring the variation of  $R_c$  with d. From this viewpoint,  $R_c$  is obtained as a series in inverse powers of d:

$$R_{c} = R_{c0} + A(\lambda_{0}/d)^{2} + B(\lambda_{0}/d)^{4} + O(d^{-6}).$$
 (2)

The first term comes from Eq. (1), as calculated by Fetter (specifically from the product  $\epsilon_2\epsilon_3$ ). An extension of Fetter's perturbation analysis to include terms in  $(\epsilon_2\epsilon_3)^2$ shows the  $O(d^{-4})$  perturbation to be negligible. The sixth-order term includes products of the  $\epsilon_i$  of the form  $\epsilon_1^2$ ,  $\epsilon_2^2$ , and  $\epsilon_1\epsilon_2$ , as well as  $(\epsilon_2\epsilon_3)^3$ . The constants A and B of Eq. (2) are numerical (specifically, A = 19.9...); however,  $\lambda_0$  is a function of c and T:

$$\lambda_0^2 = \frac{\beta_c \chi_{\text{eff}}(\zeta_1 - \rho \zeta_3) (\partial c / \partial T)_{p,\mu_4}}{c \mid \alpha_{p,\mu_4} (\partial \mu_4 / \partial c)_{T,P} \mid}, \qquad (3)$$

where  $\beta_c = -(1/\rho)\partial\rho/\partial c$ . Both the effective thermal diffusion coefficient  $\chi_{eff}$  and the second viscosity coefficients  $\zeta_i$  are poorly determined in the superfluid phase. Particularly the latter are poorly characterized, since they are measured by first- and second-sound attenuation where they appear only in combination with other considerably uncertain coefficients.

We have carried out extensive measurements to determine  $R_c(d)$  using an apparatus which allowed the *in situ* variation of *d*. The horizontal geometry of the layer was rectangular with a length of 2.28 cm and a width of 1.01 cm. A similar arrangement was used by Gao and coworkers<sup>12</sup> to study convection in normal liquid <sup>4</sup>He. The present apparatus differs from that used by Gao *et al.* since the present experiment requires the use of a <sup>3</sup>He refrigerator, and since with SMC the expansion coefficient  $\alpha_{p,\mu_4}$  is negative (i.e., convection is driven by heating from

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above), necessitating additional complexity in the design of a variable height apparatus.

The experiments were made by fixing the temperature at the bottom boundary of the fluid layer and applying a succession of closely spaced steady heat currents Q to the top plate fluid boundary. We then determined the steady state  $\Delta T$  for each Q. For each bottom plate temperature, we carried out measurements on Q and  $\Delta T$  for a number of heights. Temperatures were measured using bridge circuits and germanium resistance thermometry with a temperature resolution of  $0.3 \,\mu$ K. The height of the layer was determined by a capacitative technique<sup>12</sup> and indepen-



FIG. 1. Data for N-1 vs  $r = (R-R_c)/R_c$  for five temperatures spanning most of the temperature range covered by the present experiments. These data were obtained for essentially the same height (d=0.1633 cm, within 0.0083 cm).



FIG. 2. Data for  $R_c/R_{c0}$  vs  $d^{-2}$ , the inverse square of the layer height. The mean temperature and Prandtl number of each data set is indicated.



FIG. 3. Data for  $\lambda_0$  vs temperature, as obtained from the slope of the data in Fig. 2

dently by measuring the thermal conductance of the layer.

The experimental data for a given temperature and height are conveniently summarized by plots of the Nusselt number N vs r ( $r \equiv R/R_c - 1$ ), and several examples are shown in Fig. 1. N is defined as the total heat flux across the layer normalized by the effective conductive heat flux; thus, N=1 in the preconvective state ( $R < R_c$ ) and rises rapidly above 1 when convection begins.<sup>13</sup> (Note that the preconvecting state of a superfluid layer has nonzero vertical velocity due to the one-dimensional counterflow.)

Several corrections must be made to the directly measured quantities in order to obtain a good measure of dand the combination  $d^3\Delta T_c$ . (Here,  $\Delta T_c$  is the value of  $\Delta T$  at  $R_c$ .) These corrections arise from the self-heating of the top plate resistance thermometer by the bridge driving voltage and from the fact that at onset the average temperature across the layer,  $T = T_{\text{bottom}} + \frac{1}{2}\Delta T_c$ , increases somewhat as  $\Delta T_c$  increases. All corrections have been determined by direct precise measurement, and in no case is the resulting correction to  $d^3\Delta T_c$  more than 10%.

In Fig. 2 we present data for  $R_c$  vs  $d^{-2}$  for six values of the average temperature. We show the data in a normalized form,  $R_c(d)/R_{c0}$ . The normalization is made by fitting the data for  $d^3\Delta T_c$  at each temperature to a polynomial in  $d^{-2}$ :

$$d^{3}\Delta T_{c} = A^{*}(T) + B^{*}(T)d^{-2} + C^{*}(T)d^{-4} + \cdots$$
 (4)

The zeroth-order term of the fit  $A^*$  is then used as a divisor for the original data for  $d^3\Delta T_c$ , in order to experimentally obtain  $R_c/R_{c0}$ . This procedure was chosen because, of the elements comprising  $R_c$ , only d and  $\Delta T_c$  are well known; the fluid properties, such as v, are not so well known. But with this normalization, the effect of uncertainties in the thermohydrodynamic parameters is re-



FIG. 4. Values of the critical temperature differences for each of the temperatures represented in Fig. 1.

moved. The solid lines in Fig. 2 are fits using only up to the  $O(d^{-2})$  term of Eq. (4). The quality of the fits is generally good. Fits including higher-order terms of Eq. (2) were not significantly better. For the lowest temperature, there is a significant increase in  $R_c/R_{c0}$  as  $d^{-2}$  becomes small, which we attribute to a small aspect ratio effect.<sup>14</sup>

From the above fits we obtain  $\lambda_0$  as  $(B^*/AA^*)^{1/2}$ , which is shown versus T in Fig. 3. It is this quantity in particular which has not been well characterized in the past. Note that  $\lambda_0$  actually decreases slightly with increasing temperature. This result is surprising, since it was anticipated that the superfluid corrections would become more important as T was increased towards  $T_{\lambda}$ . However, it is noteworthy that although  $\lambda_0$  decreases with increasing T, the values of  $\Delta T_c$  (at fixed d) decrease very rapidly as T increases. This is borne out by Fig. 4, which shows, for the five temperatures of Fig. 1, the corresponding values of  $\Delta T_c$ . From the experimental point of view, we see that it becomes rapidly more difficult to resolve the temperature differences near the onset as  $T_{\lambda}$  is approached without compensating by making d very small. Nevertheless, the data imply that with the highestresolution thermometry now available, <sup>15</sup> it would be possible to work in a regime much closer to  $T_{\lambda}$  without incurring significant superfluid effects. Prandtl numbers in the range  $0.04 < N_{Pr} < 1.5$  are accessible with minimal corrections, although at present, this conclusion applies only to the regime close to the onset of convection. Additional experimental and theoretical work is required to understand the effect of the superfluid correction terms on the convective flows well above  $R_c$ .

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