# Pressures on the Critical Isochore of He<sup>4</sup><sup>†</sup>

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Measurements are reported of  $(\partial P/\partial T)_{\rho_c}$  on the critical isochore of He<sup>4</sup> very close to the critical temperature. The measurements are well represented by an equation of the form  $(\partial P/\partial T)_{\rho_c} = D + B^*t + A^*t \ln(t)$ , where  $t = (T - T_c)/T_c$  in the interval -0.016 < t < 0.013. They are used with Moldover's heat-capacity data to calculate  $(\partial \mu/\partial T)_{\rho_c}$ , which is found to be a linear function of temperature in the same temperature interval and to be analytic at the critical point. A comparison of the 1958 He<sup>4</sup> vapor-pressure temperature scale  $(T_{58})$  with the NBS Provisional Scale 2-20 K (1965) indicates that  $T_{58}$  is a very unsuitable temperature scale for He<sup>4</sup> critical-point work.

#### INTRODUCTION

The demonstration by Moldover and Little<sup>1</sup> that the constant-volume heat capacity of He<sup>4</sup> is singular at the critical point, has raised the question of what other thermodynamic properties are singular.<sup>2</sup> In particular, since the heat capacity  $C_v$  is related to the pressure *P* and the chemical potential  $\mu$  by the equation

$$\frac{\rho C_{v}}{T} = \left(\frac{\partial^{2} P}{\partial T^{2}}\right)_{\rho} - \rho \left(\frac{\partial^{2} \mu}{\partial T^{2}}\right)_{\rho} \quad , \tag{1}$$

P and  $\mu$  cannot both be analytic at the critical point. Several attractive schemes<sup>3-6</sup> for representing the thermodynamic properties of a fluid as homogeneous functions of the reduced density and temperature depend on the assumption that the chemical potential is analytic in temperature on the critical isochore. Hence, it is important to investigate the validity of that assumption. Since the chemical potential cannot be measured directly, it is necessary to calculate it from measurements of some other property. Moldover<sup>1,7</sup> has used the variation of the heat capacity with density, using the equation

$$\left(\frac{\partial(\rho C_{v})}{\partial\rho}\right)_{T} = -T\left(\frac{\partial^{2}\mu}{\partial T^{2}}\right)_{\rho} , \qquad (2)$$

which can be derived from (1). This procedure works well in the two-phase region below the critical temperature, where  $\rho C_v$  is linear in the density (since  $\mu$  and P are independent of density). However, Eq. (2) is difficult to apply in the one-phase region, where  $\mu$  is nonlinear in the density. A more direct approach is to combine pressure and heat-capacity measurements by means of Eq. (1). Since the second derivative of the pressure is needed, very high resolution is essential.

#### EXPERIMENTAL

The apparatus was designed to achieve the highest possible resolution in pressure and temperature,

minimize gravitational effects, and maintain a reasonably short thermal time constant. The lowtemperature part of the apparatus is shown in Fig. 1.

The sample space (K), 5.2027 cm<sup>3</sup> in volume, consisted of 192 slits, 0.25 mm wide and 1.0 mm deep, milled in a solid oxygen-free high-conductivity copper cell (L). It was surrounded on all sides by at least 1 cm of copper. The 0.5-mmo.d. ×0.25-mm-i.d. 30% copper-nickel pressuresensing capillary (E) was connected at the midplane of the 1-mm-high sample space and was horizontal for 2.0 cm before turning upwards. At the top of the vacuum can (D) it was connected to a vacuumjacketed 2.1-mm-o.d. copper tube (A) which led out of the cryostat to the pressure gauge and filling manifold. The thermal conductivities of the two tubes were such that, when the cell was at the critical temperature, the bottom of the copper tube was within 10 K of room temperature and the high-temperature end of the horizontal part of the capillary was at 8 K. The total mass of helium in the capillary when the cell was at the critical point was calculated to be 55  $\mu$ g, and the hydrostatic head was 0.035 Torr. The measured densities and pressures were corrected accordingly. At the point where the capillary entered the cell a 9 cm length of No. 30 copper wire was used to shunt most of the heat leak to the bath. The upper part of the capillary was surrounded by a copper radiation shield (not shown) to prevent it from radiating to the cell.

The temperature of the cell was controlled by means of a constantan wire electric heater (J) wound uniformly on the cylindrical surface of the cell and by a variable heat switch (B) inserted into one of the stainless-steel supporting tubes (H). The heat switch consisted of a copper rod which fitted snugly into H and partially shunted it. It could be moved vertically by means of a small stainless-steel tube which led to an O-ring seal at the top of the cryostat. When the heat switch was all the way in, the cell was held at about 4.23 K. When it was with-

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FIG. 1. The critical point cell shown in half-section. (A) 0. 8-mm-i. d.  $\times 2.1$ -mm-o. d. Cu vacuum-jacketed pressure-sensing tube; (B) heat-switch rod, OFHC Cu: (C) liquid-He bath; (D) brass vacuum can; (E) 0. 3-mmi.d.  $\times 0.5$ -mm-o.d. 30% Cu-Ni capillary; (F) and (H) 3.2-mm-o.d.  $\times 0.25$ -mm-wall stainless-steel support tubes; (G) brass fitting for pressure-sensing capillary at midplane of sample space; (I) germanium resistance thermometer; (J) manganin wire heater, 2 000  $\Omega$ ; (K) sample space 1.0 mm high, 5.2027 cm<sup>3</sup> volume at 5 K; (L) OFHC Cu cell 10.2 cm o.d.  $\times 2.9$  cm high.

drawn all the way, the cell temperature rose to 5.36 K because of the residual heat leak from the capillary. It was normally inserted just far enough so that a small current in the heater could be used for fine temperature control.

Temperatures were measured by a Cryocal, Inc. germanium resistance thermometer (I) inserted into a close-fitting hole in the copper cell. Apiezon N grease was used to make good thermal contact. Its resistance was measured by an ac potentiometric method using a Gertsch model 1011R ratio transformer as the balancing element and a Princeton Applied Research Corporation model CR-4A preamplifier and model JB-4 lock-in amplifier as null detector. The detector output was displayed on a strip-chart recorder. The heater voltage was controlled by a retransmitting potentiometer mounted on the shaft of the recorder. With this simple control mechanism and occasional manual adjustment, the cell temperature could be maintained within a few microkelvin for many hours. As a check on the temperature scale, a second thermometer was mounted on the cell. At the end of the experiment the two thermometers were compared with each other and with the vapor pressure of helium. Then the apparatus was warmed to room temperature and both thermometers were sent to the National Bureau of Standards for calibration on the NBS Provisional Scale 2-20 K (1965)<sup>8</sup> (the acoustical thermometer scale). Except where noted below, all temperatures in this paper refer to that scale, which we will refer to as  $T_{\rm NBS}$ . The two thermometers agreed with each other to better than 0.2 mdeg K.

Pressures were measured with Texas Instruments, Inc. fused-quartz Bourdon gauges. In order to achieve high resolution in  $(\partial P/\partial T)_{\rho}$ , pressure changes were measured on a differential gauge of 300-Torr range and 10<sup>-3</sup>-Torr resolution. Its reference capsule was connected to a 1449-cm<sup>3</sup> reservoir of helium gas in an ice bath. A 2500-Torr gauge with a resolution of  $10^{-2}$  Torr and a vacuum reference was used to measure the reference pressure. The reference pressure was kept constant to 10<sup>-3</sup> Torr by small manual adjustments of the reference volume, using the null indicator of the 2500-Torr gauge as a pressure monitor. The sensitivity of the null indicator and the stability of the gauge at a constant dial setting were sufficient for this purpose, although the resolution of the counter dial was only  $10^{-2}$  Torr and the absolute accuracy was about 0.1 Torr.

Both gauges were calibrated against a Ruska airpiston dead-weight tester at over 100 different pressures. Particular attention was paid to periodic errors caused by defects in the worm gear. The high-pressure gauge had only a small error  $(\pm 0.03 \text{ Torr})$ , which was satisfactorily corrected by a sawtooth correction. The differential gauge had an error of  $\pm 0.006$  Torr which was not exactly periodic. Since it did not seem feasible to calibrate at every possible gauge setting, measurements were always made at the same position of the worm gear. This restriction set a lower limit on the measurement interval of about 3 Torr, which corresponds to about 2 mdeg K. The accuracy of the differential pressure measurements, considering the resolution of the Ruska gauge, irregularities in the main gear of the Bourdon gauge, and calibration errors, was about  $\pm 0.006$  Torr.

The He<sup>4</sup> was taken from a cylinder of 99.999% pure helium, passed through a trap cooled in liquid helium, and stored in the 1449-cm<sup>3</sup> reservoir where its pressure was measured with the high-pressure gauge. Then it was condensed into the evacuated cell. The mass of helium was calculated using 4.0023 for the atomic weight and the second virial coefficient given by Keesom.<sup>9</sup> Corrections were made for the volume of gas remaining in the part of the system at room temperature and in the cell capillary and for the measured diffusion rate of helium through the quartz Bourdon tubes. The volume of the reservoir was measured by weighing it filled with water after the experiment. The cell volume and all other volumes in the system were measured by displacing gas from a volumetric micrometer, with a capacity of 14 cm<sup>3</sup> and a resolution of  $2 \times 10^{-4}$  cm<sup>3</sup>, which was also used for making small changes in the density of the sample. The true density in the cell decreased slightly with increasing pressure because the amount of helium gas in the dead volumes increased with pressure. The measured pressures were all corrected to the critical density using the scaling-law equation of state of Missoni, Sengers, and Green.<sup>6</sup> The correction was nowhere greater than 0.02 Torr. We believe the density measurements to be accurate to 0.02%.

With a constant amount of He<sup>4</sup> in the system and a constant reference pressure, measurements were made with the differential pressure gauge at a series of temperatures, and  $(\partial P/\partial T)_{\rho}$  was calculated from the pressure and temperature increments. No curvature correction was made since it can be shown to be negligible. At each point the temperature was held constant until the system was in equilibrium. In the two-phase region the time constant was about 5 min. In the one-phase region the system came to equilibrium as fast as the temperature could be adjusted, but it was held at constant temperature for at least 5 min before readings were taken.

## **GRAVITY CORRECTION**

Missoni, Sengers, and Green<sup>6</sup> have shown that for He<sup>4</sup>,  $\mu(\rho, T) - \mu(\rho_c, T)$  is an antisymmetric function of  $\rho - \rho_c$  for  $|\rho - \rho_c| \le 0.5\rho_c$ . In this case, in a cell of uniform cross section filled to a mean density equal to the critical density, the material at the midplane is at the critical density and its pressure is the pressure of the critical isochore. In the cell used in this work, the pressure was measured at the midplane so no gravitational correction was needed. In fact, the whole pressure difference in the cell was only  $5 \times 10^{-3}$  Torr ( $3 \times 10^{-6}$ times the critical pressure).

Later we will have to use Moldover's<sup>1,7</sup> heatcapacity measurements, so we will consider the gravitational corrections in his cell. Because of a deformation of the cell caused by the force required to close the O-ring seal,  $\frac{1}{3}$  of the cell volume was not in the main 3-mm-high sample space, but may have been asmuch as 10 mm below it. An approximate calculation indicates that the heat capacities and entropies may be seriously in error at temperatures within 2 mdeg K of the critical temperature, but they should be substantially correct outside that region.

#### CRITICAL CONSTANTS

The critical isochore was picked as the one for which there is no discontinuity in  $(\partial P/\partial T)_{\rho}$  on passing from the two-phase to the one-phase region. Assuming that the size of the discontinuity is antisymmetric in  $\rho - \rho_c$ , at least near  $\rho_c$ , a study of the three isochores in Fig. 2, which differ by 1.0% in density, indicates that the central one is within 0.1% of the critical density. Therefore, the critical density is given by

$$\rho_c = 69.64 \pm 0.07 \text{ mg cm}^{-3}$$
, (3)

which is in good agreement with the values given by Moldover<sup>1,7</sup> (69.58±0.07) and El Hadi<sup>10</sup> (69.76 ±0.20), but is higher than those of Edwards<sup>11</sup> (69.323±0.003) and of Roach<sup>12</sup> (68.5-69.0).

The critical temperature was determined by the following two methods:

(i) The thermal-equilibrium time was observed to be more than ten times greater when two phases were present in the cell than when there was only one phase present, presumably because of the time required for equilibrium between the two phases. This phenomenon provided a sensitive test of when the sample passed out of the two-phase region of the phase diagram. When the cell was filled to the critical density, the temperature at which this abrupt change in thermal behavior occurred was taken to be the critical temperature. It was found to be  $5.19828 \pm 0.00001$  K on the temperature scale defined by our resistance thermometers.

(ii) In the two-phase region  $(\partial P/\partial T)_{\rho}$  is, of course, independent of density, but this is not the case in the one-phase region. On an expanded plot of Fig. 2 the temperature at which the three isochores diverge from each other was determined to be 5.1983 ± 0.0005 K. Calculations using the equation for the coexistence curve given, for example, by Missoni, Sengers, and Green<sup>6</sup> showed that all three isochores pass through the coexistence curve within  $\mu$ deg K of the critical temperature.

Both methods are based on the classical definition of the critical temperature as the temperature at which the two-phase region disappears. Method (i) is more precise, and  $T_c = 5.19828$  was used in the reduction of our data, but it depends on the use of a nonthermodynamic concept. Method (ii) uses only established thermodynamic principles applied to the data. Fortunately, it gives the same result but with less precision. In any event there is a  $\pm 2$  medg K uncertainty in the Bureau of Standards calibration of our thermometers. Therefore

$$T_c = 5.1983 \pm 0.0021 \text{ K}(T_{\text{NBS}})$$
 . (4)

In the same experiment we determined the critical pressure to be



FIG. 2.  $(\partial P/\partial T)_{\rho}$  in units of  $P_c/T_c$ , relative to its value at  $T_c$ , for three isochores close to  $\rho_c = 69.64 \text{ mg/cm}^3$ . The curve for the critical isochore was calculated using Eq. (9). For the other two isochores an asymptotic expansion of the scaling-law equation of state of Missoni, Sengers, and Green (Ref. 6) was used.

$$P_c = 1706.12 \pm 0.10 \text{ Torr}$$
, (5)

where the uncertainty is due to the calibration of the Bourdon gauge. The corresponding temperature on the 1958 vapor-pressure-temperature scale scale<sup>13</sup> is

$$T_c = 5.18992 \pm 0.00010 \text{ K}(T_{58})$$
, (6)

in excellent agreement with the value 5.18988  $\pm$  0.00002 K reported by Edwards.<sup>11</sup>

These results are summarized in Table I, along with recent determinations by other workers.

In discussing critical phenomena it is customary to express the thermodynamic functions in reduced or dimensionless form by dividing by the appropriate combination of the critical temperature, pressure, and density. From the above measurements we find that the unit of dP/dT, entropy per unit volume, and heat capacity per unit volume  $(P_c/T_c)$  is 328.209 Torr/K or 0.0437 577 J/cm<sup>3</sup>K. The unit of chemical potential  $(P_c/\rho_c)$  is 3.266 030 J/g. In the following we will also use the reduced temperature

$$t = (T - T_c) / T_c \tag{7}$$

and reduced density

$$\Delta \rho = (\rho - \rho_c) / \rho_c \quad . \tag{8}$$

### SLOPE OF CRITICAL ISOCHORE

The slope  $(\partial P/\partial T)_{\rho_c}$  of the critical isochore is plotted against temperature in Fig. 2, along with the isochores for  $\rho = 68.926 \text{ mg/cm}^2$  ( $\Delta \rho = -0.01025$ ) and 70.373 mg/cm<sup>2</sup> ( $\Delta \rho = +0.01052$ ). The measurements are tabulated in Table III. The data for the critical isochore were fitted by the method of least squares (unweighted) to the equation, suggested by Moldover and Little's<sup>1</sup> equation for  $C_v$ :

$$\left(\frac{\partial P}{\partial T}\right)_{\rho_{c}} = D + B^{*}t + A^{*}t\ln|t| \quad , \quad -0.016 < t < 0.013$$
(9)

where

TABLE I.	The critical co	onstants.	Except for the
first entry,	all temperatur	es are on i	the $T_{58}$ scale. <sup>a</sup>

	Temperature (K)	Pressure (Torr)	Density (mg/cm <sup>3</sup> )
This work (T <sub>NBS</sub> )	$5.1983 \pm 0.0020$	1706.12 ± 0.10	69.64±0.07
This work (T <sub>58</sub> )	5.18992±0.00010		
Edwards <sup>b</sup>	$5.18988 \pm 0.00002$	$1706.07 \pm 0.02$	$69.323 \pm 0.003$
Edwards <sup>c</sup>	$5.1897 \pm 0.0007$	1705.84±0.86	
Moldover <sup>d</sup>	$5.1891 \pm 0.0007$	$1705.04 \pm 0.9$	$69.58 \pm 0.07$
el Hadi <sup>e</sup>			$69.76 \pm 0.20$
Roach <sup>f</sup>	$5.191 \pm 0.002$	1707.5 ±2.5	$68.75 \pm 0.25$
van Dijk <i>et al</i> .ª	5.1994	1718	

<sup>a</sup>Reference 13.

<sup>b</sup>Reference 11. From least-squares fit to the coexistence curve.

<sup>c</sup>Reference 11. Direct determination (meniscus disappearance). <sup>d</sup>Reference 7.

<sup>e</sup>Reference 10.

<sup>f</sup>Reference 12.

 $D = 1289.18 \pm 0.30 \text{ Torr/K}$ = 3.92793 ± 0.00100 (reduced), (10)  $A^* = -664 \pm 20 \text{ Torr/K}$ 

$$= -2.022 \pm 0.060$$
; (11)

for t < 0,

$$B^* = B^*_{\pm} = 1764 \pm 100 \text{ Torr/K}$$
  
= 5.376 \pm 0.300 , (12)

and for t > 0,

$$B^* = B^*_{\star} = -1496 \pm 100 \text{ Torr/K}$$
$$= 04.560 \pm 0.300 . \tag{13}$$

The root-mean-square deviation of the measured points from the curve was 0.85 Torr/K. The large error limits on  $A^*$  and  $B^*$  result from correlation between the constants (98% between  $A^*$  and each  $B^*$ , 95% between  $B^*_*$  and  $B^*_*$ ). D is very little correlated with the other constants, and its error results mainly from the error of the pressure measurements. The logarithmic term in (9) corresponds to a critical exponent<sup>14</sup>  $\alpha^*$  of zero in the equation

$$\left(\frac{\partial P}{\partial T}\right)_{\rho_{c}} = D + B^{*}t + A^{*}_{\alpha}t \left| t \right|^{-\alpha}$$
 (14)

Since in the accessible temperature range the constant and linear terms dominate, the data are not very sensitive to  $\alpha^*$  and acceptable fits are obtained with values of  $\alpha^*$  in the range -0.2 to +0.2. We have preferred to use the form (9), which has fewer adjustable constants.

# CHEMICAL POTENTIAL

Integration of Eq. (1) at constant density yields

$$\rho\left(\frac{\partial\mu}{\partial T}\right)_{\rho} = \left(\frac{\partial P}{\partial T}\right)_{\rho} - \rho S \quad , \tag{15}$$

where S, the entropy, can be obtained by integrating the heat capacity

$$S = S_c + \int_{T_c}^{T} \frac{C_v}{T} dT \quad . \tag{16}$$

We have calculated  $(\partial \mu / \partial T)_{\rho_c}$  from our  $(\partial P / \partial T)_{\rho_c}$ measurements and a table of entropies obtained by integrating Moldover's<sup>7</sup> heat-capacity data. For this integration we used the equation given by Moldover,<sup>7</sup> which fits his data quite well except within 2 mK of the critical temperature, where the effect of gravity is quite pronounced. At the critical isochore his equation reduces to

$$C_{v} = A_{\alpha} \left| t \right|^{-\alpha} + B_{\alpha} + Et \quad , \tag{17}$$

with different values of  $A_{\alpha}$ ,  $B_{\alpha}$ , and  $\alpha$  above and below  $T_c$ . Where the equation does not fit Moldover's data we used graphical integration of the data.

. . . . .

Below  $T_c$  Moldover used the  $T_{58}$  temperature scale, and above  $T_c$  he used an arbitrary scale based on an extrapolation of his carbon thermometer. We could have corrected his temperature scale below  $T_c$ , but there is no way to do it above  $T_c$ . Since the absolute temperature is only of secondary importance, we have used Moldover's value of  $T_c$ (5.1891 K) in reducing his data to dimensionless form. However, in a calculation like this one in which data from two different experiments are used, it is crucially important that the data points to be subtracted from one another correspond to the same temperature. This would be a simple matter if the critical temperature could be used as a fixed point to tie the two scales together as is commonly done, for example, at the  $\lambda$  point. But in these two experiments the critical temperatures were determined by very different methods. Our critical temperature was determined by a thermodynamic criterion (the disappearance of the twophase region), while Moldover's was based on a least-squares fit of his data to an assumed equation of state. Fortunately, the calculated values of  $(\partial \mu / \partial T)_{\rho_c}$  themselves afford a means of relating the two temperature scales, as will be seen below.

In Fig. 3 are plotted values of  $(\partial \mu / \partial T)_{\rho_c}$  calculated using Moldover's  $T_c$  with his data and our  $T_c$  with ours. Points within 2 mK of  $T_c$  are not plotted because they are affected by gravity. The points appear to fall within experimental error on two



FIG. 3.  $(\partial \mu / \partial T)_{\rho_c}$  in units of  $P_c/(\rho_c T_c)$ , relative to its value at  $T_c$ , calculated using the critical temperature reported by Moldover (Ref. 7).

straight lines which do not meet at the critical point. The points above and below  $T_c$  were fitted separately to straight lines by the method of least squares. These lines are shown in Fig. 3. Their slopes are  $-2.677 \pm 0.093$  above  $T_c$  and -3.013± 0.061 below  $T_c$ ;  $(\partial \mu / \partial T)_{\rho_c}$  has a discontinuity at  $T_c$  of  $(4.81 \pm 0.57) \times 10^{-3}$ . This displacement of the high-temperature points relative to the low-temperature ones cannot be correct, since it would imply that a phase with  $\rho = \rho_c$  would be stable below  $T_c$ . Therefore we repeated the calculation, displacing Moldover's  $T_c$  downward in steps of 0.52 mdeg K (increasing the value of t for all his points in steps of  $1 \times 10^{-4}$ ). As  $T_c$  decreased the discontinuity decreased and the slopes became more nearly equal. When Moldover's  $T_c$  was decreased by 2.1 mdeg K (to 5.187 K), the discontinuity was reduced to (0.38  $\,$  $\pm$  0.57)×10<sup>-3</sup> and the slopes were - 2.799 ± 0.091 and  $-2.848 \pm 0.061$ . In fact, the data were equally well fitted by a single line of slope  $-2.801 \pm 0.033$ . which is shown in Fig. 4. A further reduction of 0.52 mK in Moldover's  $T_c$  caused both discontinu-

ities to reappear with opposite signs. The fact that the discontinuities in  $(\partial \mu / \partial T)_{\rho_c}$  and  $(\partial^2 \mu / \partial T^2)_{\rho_c}$  disappeared for the same decrease in Moldover's  $T_c$ is a strong indication that both derivatives are in fact continuous and that either Moldover's  $T_c$  or ours is in error by 2.1±0.5 mdeg K, and we will assume this to be the case. The standard deviations given in this paragraph are based solely on the fitting errors and are cited only for comparative purposes. When we allow for systematic errors in the heatcapacity and pressure measurements and uncertainty in the critical temperature correction, we have

$$\left(\frac{\partial^2 \mu}{\partial T^2}\right)_{\rho_c} = -2.80 \pm 0.25, -0.016 < t < 0.013 .$$
 (18)

Hill and Lounasmaa<sup>15</sup> tabulated the entropy of He<sup>4</sup> at 5.25 K and at  $\rho_c$ . Their value was combined with Moldover's heat-capacity data to calculate the entropy at  $T_c$ . A small correction was made because Hill and Lounasmaa's assumed critical density was smaller than ours. We find



FIG. 4.  $(\partial \mu / \partial T)_{\rho_c}$  in units of  $P_c/(\rho_c T_c)$ , relative to its value at  $T_c$ , calculated with Moldover's critical temperature decreased by 2.1 mdeg K.

$$\rho_c S_c = 8.977 \pm 0.08 \quad . \tag{19}$$

Combining this value with our value for  $(\partial P/\partial T)_{\rho_c}$  (Eq. 10), and with Eq. (18), we find

$$\left(\frac{\partial \mu}{\partial T}\right)_{\rho_{c}} = D_{\mu} + B_{\mu}t$$
, -0.016 < t < 0.013 (20)

TABLE II. Coefficients of equations for  $(\partial P/\partial T)_{\rho_c}$ [Eq. (9)],  $(\partial \mu/\partial T)_{\rho_c}$  [Eq. (25)], and  $T_{\rm NBS} - T_{58}$ [Eq. (28)].

Coefficient	Value	Units	Reduced
D	$1289.18 \pm 0.30$	Torr/K	3.92793 ± 0.00100
A*	$-664 \pm 20$	Torr/K	$-2.022 \pm 0.060$
<u>B*</u>	$1764 \pm 100$	Torr/K	5.376±0.300
B*	$-1496 \pm 100$	Torr/K	$-4.560\pm0.300$
$D_{\mu}$	$-0.2209 \pm 0.004$	J/cm <sup>3</sup> K	$-5.049 \pm 0.09$
$B_{\mu}$	$-0.123 \pm 0.008$	J/cm <sup>3</sup> K	$-2.80\pm0.20$
$c_1$	8.45745	mK	
$c_2$	61.7795	mK	
$c_3$	122.121	mK	
$c_4$	34.0113	mK	

 $D_{\mu} = 5.049 \pm 0.09 = -0.2209 \pm 0.004 \text{ J/cm}^3 \text{ K}$ 

(21)

$$B_{\mu} = -2.80 \pm 0.20 = 0.123 \pm 0.008 \text{ J/cm}^3 \text{ K}$$
 .  
(22)

Our value for  $B_{\mu}$  is substantially less in magnitude than Moldover's<sup>7</sup> (-3.47). However, it is a relatively small correction in his analysis, and it has to be determined by comparing data from different isochores. Since Moldover had difficulties with thermometer stability and had to adjust the temperature scales for the different isochores empirically, we feel that his value may be in error by this much. Missoni, Sengers, and Green<sup>6</sup> give an even higher value (-3.9) calculated from Hill and Lounasmaa's<sup>15</sup>  $C_{\nu}$  measurements. However, those data were taken so far from critical, in both temperature and density, that they can hardly be considered to represent the critical region. Equation (20) implies that the third and all higher derivatives of  $\mu$  are negligible at  $T_c$  and, therefore, that  $\mu$  is analytic at  $T_c$  within the experimental error.

# 1958 He<sup>4</sup> TEMPERATURE SCALE

The 1958 He<sup>4</sup> temperature scale<sup>12</sup> ( $T_{58}$ ), based on He<sup>4</sup> vapor pressures, is used almost universally by workers studying the properties of He<sup>4</sup>, but it has two serious drawbacks for work at the critical point. In the first place, it does not exist above the critical temperature so that measurements above  $T_c$  are based on the individual experimenter's idea of what is a "suitable" extrapolation of  $T_{58}$ . Such scales will differ from laboratory to laboratory, especially since all secondary thermometers sufficiently sensitive for critical-point work are notoriously nonlinear. The second drawback is that  $T_{58}$ behaves anomalously, compared to the thermodynamic temperature, as the critical temperature is approached. This happens because  $T_{58}$  is defined by a vapor-pressure table in which  $d^2P/dT^2$  approaches zero as T approaches  $T_c$ , whereas, in fact,  $d^2P/dT^2$  approaches infinity as T approaches  $T_c$ . For these reasons we have used the NBS Provisional Scale 2-20 K (1965)<sup>8</sup> in spite of the obvious disadvantages of having to send thermometers to

another laboratory for calibration. The two scales differ by as much as 12 mK, and in order to compare measurements on different scales it is necessary to have a correction curve. No such curve is available for the range 4.2–5.2 K, aside from two points published by Cataland and Plumb.<sup>16</sup> Therefore, we have calculated  $T_{\rm NBS} - T_{58}$  from some of our vapor-pressure measurements and plotted them in Fig. 5. The rapid decrease of  $T_{\rm NBS} - T_{58}$  near  $T_c$  should be noted. The curve in Fig. 4 is plotted from the empirical equation

$$T_{\rm NBS} - T_{58} = c_1 + c_2 t + c_3 t^2 + c_4 t \ln(-t) \quad , \tag{23}$$

with coefficients  $c_n$  given in Table II.

It should be noted that unfortunately the Bureau of Standards provides no calibration points between 4.2 and 5.0 K. However, the eight-parameter interpolation equation is fitted to 20 calibration points in the range 2.3–20 K, so the interpolation should be reasonably smooth. Our measurements of  $T_{\rm NBS}$  –  $T_{56}$  at 4.2 and 5.0 K (11.9 and 10.5 mK, respectively) do not agree very well with those published by Cataland and Plumb<sup>16</sup> (10 and 12 mdeg K, respectively). We know of no reason for this, except that the NBS calibration of our thermometers is only guaranteed to  $\pm 2$  mdeg K. Cetas and Swenson<sup>17</sup> have



FIG. 5. Difference between the NBS Provisional Scale 2-20 K (1965) and the 1958 He<sup>4</sup> vapor-pressure temperature scales. The curve was calculated using Eq. (28).

also compared  $T_{58}$  with  $T_{NBS}$  by means of germanium thermometers calibrated by the NBS. They find  $T_{NBS} - T_{58}$  to be 11 and 10 mK, respectively, at the

same two temperatures.

CONCLUSION

Experimental evidence that the chemical potential

TABLE III. Isochores of He <sup>4</sup> .						
Temp	$(\partial P/\partial T)_{\rho}$	Temp	$(\partial P/\partial T)_{o}$	Temp	(∂P/∂T) <sub>p</sub>	
(K)	(Torr/K)	(K)	(Torr/K)	(K)	(Torr/K)	
		Density=6	$8.93 \text{ mg/cm}^3$			
5, 113 56	1215.7	5, 191 87	1280.9	5,21292	1287.8	
5.11357	1215.1	5,19230	1281.3	5.21349	1286.9	
5.11357	1217.4	5.19248	1281.5	5.21407	1288.6	
5,12887	1226.7	5.19303	1283.5	5.21526	1288.5	
5,12888	1226.9	5.19359	1283.1	5,21583	1288.0	
5.12888	1226.8	5,19464	1284.1	5.21640	1287.0	
5.14433	1239.2	5,19478	1284.4	5,217 59	1288.4	
5,14433	1240.3	5,19482	1283.5	5.21873	1289.2	
5.14434	1239.6	5.19537	1286.8	5,21933	1288.7	
5.14434	1239.1	5.19594	1286.5	5,21992	128 <b>9.1</b>	
5.14434	1239.7	5.19656	1286.0	5.22107	1288.6	
5.14434	1239.2	5.19698	1287.2	5.22115	1289.2	
5.14442	1239.0	5.19716	1287.8	5.22118	1289.3	
5.14460	1239.6	5,198 27	1288.7	5.22225	1289.3	
5.14744	1242.7	5.19890	1283.6	5.22229	1290.4	
5.15679	1248.0	5.19932	1285.3	5.22340	1289.2	
5.15680	1249.4	5.19940	1285.8	5.22399	1288.7	
5.15680	1248.4	5.19947	1285.5	5.22472	1289.6	
5.15994	1250.7	5.19950	1284.0	5.22689	1289.6	
5.15995	1251.6	5.200 05	1285.2	5.22785	1289.9	
5.15995	1252.7	5.20061	1284.7	5.228 08	1289.7	
5.16070	1253.1	5.20124	1284.9	5.22902	1289.1	
5.16217	1255.5	5.20166	1286.5	5.22904	1290.4	
5.16426	1256.5	5.20181	1284.6	5.23098	1290.7	
5.16622	1256.6	5.20184	1286.2	5.23134	1290.2	
5.16873	1259.4	5.20237	1287.3	5.23135	1291.0	
5.17174	1262.0	5.20295	1285.0	5.23179	1291.7	
5.17411	1266.2	5.20633	1285.7	5.23370	1291.3	
5.17412	1264.5	5.20648	1286.7	5.23371	1291.0	
5.17568	1266.0	5.20652	1285.5	5.23372	1291.0	
5.17571	1265.9	5.20706	1284.1	5.23388	1291.1	
5.17571	1266.0	5.20762	1287.0	5.23739	1292.3	
5.17624	1266.5	5.20769	1287.1	5.23880	1292.2	
5.17825	1268.4	5.20769	1287.6	5.23880	1292.3	
5.17887	1270.4	5.20825	1287.4	5.24029	1292.4	
5.17888	1267.9	5.20358	1285.0	5.24142	1292.4	
5.18124	1270.3	5.20399	1287.0	5.24318	1293.4	
5.18244	1270.8	5.20414	1286.2	5.24359	1294.0	
5.18418	1273.3	5.20418	1288.0	5.24359	1294.0	
5.18480	1275.4	5.20473	1286.3	5.24669	1293.2	
5.18598	1276.3	5.20529	1286.9	5.24959	1293.4	
5.18654	1276.0	5.20592	1287.1	5.25247	1294.2	
5.18659	1276.5	5.20607	1286.6	5.25352	1293.4	
5.18716	1276.1	5.20882	1285.0	5.25352	1294.3	
5.188 03	1277.8	5,20939	1287.6	5.25598	1294.9	
5.18840	1277.7	5.20996	1287.0	5.25888	1294.5	
5.18890	1277.0	5.21059	1287.7	5.26176	1295.5	
5.18951	1279.1	5.21090	1288.2	5.26350	1296.0	
5.18952	1277.4	5.21116	1285.5	5.26351	1295.9	
5.19125	1281.8	5.21150	1287.6	5.26352	1295.7	
5.19160	1281.3	5.21151	1287.9	5.26526	1295.8	
5.19162	1281.2	5,21173	1286.7	5,26584	1294.6	
5.19162	1281.2	5.21187	1287.6			

TABLE III. (continued)						
Temp	(ðP/ðT) <sub>p</sub>	Temp	$(\partial P/\partial T)_{\rho}$	Temp	$(\partial P/\partial T)_{\rho}$	
(K)	(Torr/K)	(K)	(Torr/K)	(K)	(Torr/K)	
		Density = 69	.64 mg/cm <sup>3</sup>			
5.14819	1243.0	5.19706	1287.7	5.21164	1296.3	
5,16510	1256.8	5.19764	1288.7	5.21218	1296.9	
5,16577	1257.7	5.19766	1287.5	5.21275	1297.2	
5,16770	1259.5	5.198 24	1280.0	5,21277	1297.5	
5,16809	1259.8	5,19882	1288.7	5.21278	1296.5	
5,171 25	1262.4	5,19883	1288.7	5.21334	1296.5	
5.17465	1265.2	5,19883	1289.9	5.21394	1298.2	
5,17531	1265.7	5.19939	1289.1	5,21 <b>39</b> 6	1297.5	
5,17643	1267.9	5,19997	1288.8	5,21450	1297.0	
5.17644	1267.0	5,200 00	1289.8	5.21509	1296.5	
5,17646	1266.8	5,200 02	1289.6	5,21510	1296.5	
5, 180 59	1269.8	5,200 57	1290.7	5.21565	1297.6	
5, 181 18	1272.0	5.20115	1290.5	5.21626	1296.7	
5 181 21	1271.3	5,20116	1291.2	5.21627	1297.2	
5, 181 25	1270.2	5,20116	1291.0	5.21682	1298.0	
5,18238	1271.9	5.20172	1292.5	5.21742	1298.2	
5,18296	1272.5	5,20230	1291.2	5.21857	1298.0	
5, 183 54	1270.7	5,20233	1291.7	5.218 59	1299.0	
5,18357	1274.7	5.20235	1293.1	5,21913	1297.9	
5.18474	1275.1	5.20290	1293.2	5.21973	1297.3	
5 185 32	1975 3	5 203 48	1292.9	5,220 89	1296.3	
5 185 91	1275.0	5 203 49	1292.5	5, 220 90	1297.2	
5 185 91	1273.9	5 203 49	1291.3	5,221 45	1297.8	
5 185 93	1275.3	5, 204 05	1292.0	5,22205	1298.3	
5 185 97	1275.8	5, 204 63	1292.8	5,223 21	1299.0	
5,18710	1276.5	5, 204 65	1292.9	5,223 22	1299.8	
5,187.68	1279.2	5,20468	1295.1	5,22376	1298.9	
5,188 26	1278.7	5,205 22	1293.7	5,22668	1299.2	
5,188 29	1279.2	5,20580	1292.8	5,22669	1299.3	
5.18832	1278.5	5,20581	1292.8	5,22783	1299.4	
5,18945	1278.5	5,20581	1294.4	5.22954	1300.3	
5,19003	1279.9	5.20637	1294.3	5.23061	1300.3	
5,190 62	1280.4	5,20695	1295.3	5,23235	1300.7	
5.190 64	1280.6	5,20698	1292.0	5.23237	1300.9	
5,19067	1281.1	5.20700	1294.3	5.23361	1301.7	
5.19179	1282.1	5.20754	1295.1	5.23362	1301.3	
5,191 80	1281.9	5.20812	1293.7	5.23466	1301.2	
5.19238	1280.9	5.20813	1295.0	5.23707	1302.7	
5.19296	1283.7	5.20813	1294.3	5.23878	1302.8	
5,19298	1283.5	5.20814	1291,9	5.24283	1303.6	
5,19302	1283.7	5,208 69	1292.9	5,24285	1303.6	
5, 194 14	1283.6	5,20927	1296.1	5,246 29	1304.3	
5, 194 15	1282.2	5,20930	1295.6	5.24800	1304.4	
5, 19472	1285.1	5,20932	1294,9	5.25205	1305.0	
5, 195 30	1286.3	5,20986	1294.7	5.252 07	1305.0	
5,19533	1284.3	5,21045	1295.3	5,25551	1306.3	
5,19536	1285.4	5,210 46	1294.9	5.257 21	1306.2	
5,19590	1286.0	5.21046	1293.5	5,261 26	1306.7	
5.19648	1285.7	5.21102	1295.1	5.261 27	1306.6	
5.19649	1285.0	5.21162	1295.9	5.26471	1306.9	

TABLE III. (continued)

is an analytic function of temperature on the critical isochore clears up, at least for He<sup>4</sup>, a previously unanswered question which affects the validity of scaling-law formulations of the equation of state near the critical point, since these theories always assume the analyticity of  $\mu(\rho_c, t)$ . On the other hand, observation of the logarithmic anomaly in the pressure serves to emphasize the need for a revision of the 1958 He<sup>4</sup> temperature scale.

Numerical constants reported in this paper are

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$							
Tensity = 70.37 mg/cm³Density = 70.37 mg/cm³Density = 70.37 mg/cm³5.137 841236.65.137 841234.65.198 861289.95.212 221305.95.156 061249.35.198 801291.25.212 221305.35.162 041254.25.198 801291.25.212 661305.95.171 691266.75.200 671296.65.214 531306.35.177 611267.45.200 681297.15.214 961305.45.177 651267.35.201 121297.75.216 821307.25.181 901270.15.201 311296.85.216 831307.25.182 351270.35.202 371299.25.217 261307.95.184 261273.65.203 411300.75.219 121308.65.184 721276.05.204 141300.05.219 561307.35.187 6071277.55.204 691300.75.221 421307.65.187 801277.75.205 761301.35.221 661308.75.188 311277.75.205 761301.95.233 181310.85.191331280.05.207 611303.15.236 331331.15.191331280.05.207 621303.85.236 761331.15.193 71284.55.209 011303.85.246 581315.15.194 121283.45.208 061302.75.245 511315.15.196 1285.95.20	 Temp	$(\partial P/\partial T)_{\rho}$	Temp (K)	$(\partial P/\partial T)_{p}$	Temp (K)	$(\partial P/\partial T)_{p}$	
Density = 70.37 mg/cm²5. 137 841234.65. 198 361289.95. 212 221305.95. 156 061249.35. 198 801293.55. 212 261305.95. 162 041254.25. 198 801291.25. 212 661305.95. 177 151266.75. 200 061296.25. 214 521305.65. 177 151266.75. 200 0671296.65. 214 4531306.35. 177 611267.45. 200 681297.15. 216 821306.65. 181 901270.15. 201 131296.85. 217 261307.95. 182 351270.35. 203 701299.45. 219 121308.65. 184 261273.65. 203 441300.75. 219 121307.75. 184 261277.05. 204 411300.05. 214 211307.65. 187 071277.55. 205 741301.35. 227 161307.65. 187 801277.95. 205 741301.45. 227 161300.05. 188 311277.75. 205 741301.45. 227 161300.05. 190 671280.25. 207 001301.95. 233 181310.85. 191 781281.75. 206 661302.75. 245 611313.15. 191 781281.75. 206 661302.75. 245 611315.15. 196 011285.95. 209 901303.85. 266 761313.15. 196 021288.25. 209 911303.85. 266 711317.25. 196 021288.2 <t< th=""><th>(K)</th><th>(1011/K)</th><th>(11)</th><th>(1011/18)</th><th>(11)</th><th>(1011)</th><th></th></t<>	(K)	(1011/K)	(11)	(1011/18)	(11)	(1011)	
5.13784 $1234.6$ $5.19836$ $1289.9$ $5.21222$ $1305.9$ $5.160.66$ $1249.3$ $5.19880$ $1293.5$ $5.21222$ $1305.3$ $5.162.04$ $1254.2$ $5.19880$ $1291.2$ $5.21266$ $1305.9$ $5.17169$ $1262.0$ $5.20006$ $1296.2$ $5.21452$ $1305.6$ $5.17715$ $1266.7$ $5.20067$ $1296.6$ $5.21453$ $1306.3$ $5.17761$ $1267.4$ $5.20068$ $1297.1$ $5.21462$ $1305.4$ $5.17765$ $1267.3$ $5.20112$ $1297.7$ $5.21682$ $1306.6$ $5.18190$ $1270.1$ $5.2013$ $1299.2$ $5.21726$ $1307.9$ $5.18235$ $1270.3$ $5.20237$ $1299.2$ $5.21912$ $1308.6$ $5.18426$ $1273.6$ $5.20344$ $1300.7$ $5.21912$ $1307.7$ $5.18426$ $1277.6$ $5.20344$ $1300.0$ $5.21422$ $1307.6$ $5.18760$ $1277.9$ $5.20531$ $1301.3$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20576$ $1301.0$ $5.22716$ $1310.0$ $5.18831$ $1277.7$ $5.20576$ $1301.0$ $5.22716$ $1309.8$ $5.190.67$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.191.7$ $5.20676$ $1301.0$ $5.22760$ $1309.8$ $5.191.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.199.7$ $5.20576$ $1301.0$ $5.22760$ $130$			Density = 70	.37 mg/cm <sup>°</sup>			
$5.156\ 06$ $1249.3$ $5.198\ 80$ $1293.5$ $5.212\ 22$ $1305.3$ $5.162\ 04$ $1254.2$ $5.198\ 80$ $1291.2$ $5.212\ 66$ $1305.9$ $5.177\ 16$ $1262.0$ $5.200\ 66$ $1296.2$ $5.214\ 52$ $1306.3$ $5.177\ 15$ $1266.7$ $5.200\ 67$ $1296.6$ $5.214\ 52$ $1306.3$ $5.177\ 61$ $1267.3$ $5.201\ 12$ $1297.7$ $5.216\ 82$ $1306.4$ $5.177\ 65$ $1267.3$ $5.201\ 12$ $1297.7$ $5.216\ 82$ $1307.4$ $5.182\ 35$ $1270.3$ $5.202\ 37$ $1299.2$ $5.217\ 26$ $1307.9$ $5.183\ 60$ $1272.8$ $5.203\ 40$ $1300.7$ $5.219\ 12$ $1307.7$ $5.184\ 26$ $1277.6$ $5.204\ 43$ $1300.7$ $5.219\ 12$ $1307.7$ $5.184\ 72$ $1276.0$ $5.204\ 41$ $1300.0$ $5.219\ 12$ $1307.6$ $5.187\ 60$ $1277.0$ $5.204\ 46$ $1300.7$ $5.221\ 42$ $1307.6$ $5.187\ 80$ $1277.9$ $5.205\ 31$ $1301.3$ $5.221\ 42$ $1307.6$ $5.187\ 80$ $1277.7$ $5.205\ 74$ $1301.4$ $5.227\ 60$ $1309.8$ $5.196\ 71$ $1280.2$ $5.207\ 62$ $1301.4$ $5.236\ 76$ $1310.6$ $5.191\ 73$ $1280.2$ $5.207\ 62$ $1303.8$ $5.236\ 76$ $1311.6$ $5.193\ 67$ $1284.5$ $5.208\ 06$ $1302.7$ $5.245\ 48$ $1315.1$ $5.193\ 67$ $1284.5$ $5.208\ 06$ $1302.7$ $5.245\ 48$ $1315.1$ </td <td> 5.13784</td> <td>1234.6</td> <td>5,19836</td> <td>1289.9</td> <td>5.21222</td> <td>1305.9</td> <td></td>	 5.13784	1234.6	5,19836	1289.9	5.21222	1305.9	
5.162.04 $1254.2$ $5.198.80$ $1291.2$ $5.212.66$ $1305.9$ $5.171.69$ $1262.0$ $5.200.067$ $1296.2$ $5.214.52$ $1306.6$ $5.177.15$ $1266.7$ $5.200.687$ $1292.66.6$ $5.214.53$ $1306.3$ $5.177.65$ $1267.3$ $5.201.12$ $1297.1$ $5.216.82$ $1306.6$ $5.181.90$ $1270.1$ $5.202.37$ $1299.2$ $5.217.26$ $1307.9$ $5.182.35$ $1270.3$ $5.202.37$ $1299.4$ $5.219.12$ $1307.9$ $5.183.60$ $1272.8$ $5.203.44$ $1300.7$ $5.219.12$ $1307.7$ $5.184.26$ $1273.6$ $5.203.43$ $1300.7$ $5.219.12$ $1307.7$ $5.184.72$ $1276.0$ $5.203.44$ $1300.0$ $5.219.12$ $1307.6$ $5.187.96$ $1277.7$ $5.204.469$ $1300.7$ $5.221.42$ $1307.6$ $5.187.96$ $1277.7$ $5.205.511$ $1301.3$ $5.221.42$ $1307.6$ $5.187.80$ $1277.7$ $5.205.74$ $1301.4$ $5.227.16$ $1310.0$ $5.188.31$ $1277.7$ $5.205.76$ $1301.0$ $5.227.60$ $1309.8$ $5.190.67$ $1280.2$ $5.207.61$ $1303.1$ $5.236.33$ $1313.1$ $5.191.78$ $1281.7$ $5.208.66$ $1302.7$ $5.245.81$ $1315.1$ $5.194.61$ $1280.2$ $5.209.90$ $1303.3$ $5.246.58$ $1315.1$ $5.196.67$ $1284.5$ $5.209.90$ $1303.3$ $5.245.68$ $1315.2$ $5.196.61$ $1285.9$ <	5.15606	1249.3	5.19880	1293.5	5.21222	1305.3	
5.17169 $1262.0$ $5.20006$ $1296.2$ $5.21452$ $1305.6$ $5.17715$ $1266.7$ $5.20067$ $1296.6$ $5.21453$ $1306.3$ $5.17761$ $1267.4$ $5.20068$ $1297.1$ $5.21682$ $1306.6$ $5.17765$ $1267.3$ $5.20112$ $1297.7$ $5.21682$ $1306.6$ $5.18190$ $1270.1$ $5.2013$ $1299.2$ $5.21726$ $1307.9$ $5.18235$ $1270.3$ $5.20343$ $1300.7$ $5.21912$ $1308.6$ $5.18360$ $1272.8$ $5.20343$ $1300.7$ $5.21912$ $1307.7$ $5.18426$ $1273.6$ $5.20343$ $1300.7$ $5.21926$ $1307.3$ $5.18596$ $1277.0$ $5.204414$ $1300.0$ $5.22142$ $1307.6$ $5.18707$ $1277.5$ $5.20531$ $1301.3$ $5.221686$ $1308.7$ $5.18831$ $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18831$ $1277.7$ $5.20574$ $1301.0$ $5.22716$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20762$ $1303.8$ $5.23676$ $1313.1$ $5.19367$ $1284.5$ $5.20806$ $1304.0$ $5.24658$ $1315.1$ $5.19460$ $1284.5$ $5.20930$ $1303.3$ $5.24658$ $1315.2$ $5.19602$ $1284.5$ $5.20930$ $1303.3$ $5.24658$ $1315.2$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.26574$ $1$	5,16204	1254.2	5.19880	1291.2	5.21266	1305.9	
5.17715 $1266.7$ $5.20067$ $1296.6$ $5.21453$ $1306.3$ $5.17761$ $1267.4$ $5.20068$ $1297.1$ $5.21496$ $1305.4$ $5.17765$ $1267.3$ $5.20112$ $1297.7$ $5.21682$ $1307.2$ $5.18190$ $1270.1$ $5.20237$ $1299.2$ $5.21726$ $1307.9$ $5.18235$ $1270.3$ $5.20237$ $1299.2$ $5.21726$ $1307.9$ $5.18426$ $1272.8$ $5.20300$ $1299.4$ $5.21912$ $1308.6$ $5.18426$ $1273.6$ $5.20344$ $1300.0$ $5.21912$ $1307.7$ $5.18472$ $1276.0$ $5.20444$ $1300.0$ $5.21422$ $1307.6$ $5.18790$ $1277.5$ $5.20444$ $1300.0$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.22142$ $1307.6$ $5.18780$ $1277.7$ $5.20576$ $1301.4$ $5.22716$ $1309.8$ $5.19067$ $1280.2$ $5.20761$ $1303.1$ $5.23381$ $1310.6$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19178$ $1281.7$ $5.20805$ $1304.0$ $5.24548$ $1315.6$ $5.19462$ $1302.7$ $5.24548$ $1315.6$ $5.19539$ $1284.5$ $5.20991$ $1303.8$ $5.25664$ $1317.2$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.26574$ $1317.1$ $5.19666$ $1327.7$ $5.19602$ $1288.2$ $5.20992$	5.17169	1262.0	5,20006	1296.2	5.21452	1305.6	
5.17761 $1267.4$ $5.20068$ $1297.1$ $5.21496$ $1305.4$ $5.17765$ $1267.3$ $5.20112$ $1297.7$ $5.21682$ $1306.6$ $5.18190$ $1270.1$ $5.20113$ $1296.8$ $5.21683$ $1307.2$ $5.18235$ $1270.3$ $5.20237$ $1299.2$ $5.21726$ $1307.9$ $5.18360$ $1272.8$ $5.20343$ $1300.7$ $5.21912$ $1307.7$ $5.18426$ $1273.6$ $5.20344$ $1300.0$ $5.21956$ $1307.3$ $5.18596$ $1277.0$ $5.20444$ $1300.0$ $5.221422$ $1307.6$ $5.18790$ $1277.5$ $5.20446$ $1300.7$ $5.221422$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.221422$ $1307.6$ $5.18831$ $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18943$ $1278.7$ $5.20576$ $1301.4$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19178$ $1281.7$ $5.20806$ $1302.7$ $5.24548$ $1315.1$ $5.19412$ $1283.4$ $5.20806$ $1302.7$ $5.24591$ $1315.6$ $5.19601$ $1285.9$ $5.20991$ $1303.8$ $5.25504$ $1317.1$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.26373$ $1318.8$ $5.19666$ $1286.2$ $5.$	5.17715	1266.7	5.200 67	1296.6	5.21453	1306.3	
5.17765 $1267.3$ $5.20112$ $1297.7$ $5.21682$ $1306.6$ $5.18190$ $1270.1$ $5.20113$ $1296.8$ $5.21883$ $1307.2$ $5.18235$ $1270.3$ $5.20237$ $1299.2$ $5.21726$ $1307.9$ $5.18360$ $1272.8$ $5.20300$ $1299.4$ $5.21912$ $1308.6$ $5.18426$ $1273.6$ $5.20343$ $1300.7$ $5.21912$ $1307.7$ $5.18472$ $1276.0$ $5.20344$ $1300.0$ $5.21956$ $1307.3$ $5.18596$ $1277.0$ $5.20444$ $1300.0$ $5.221422$ $1307.6$ $5.18707$ $1277.5$ $5.20469$ $1300.7$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.22161$ $1308.7$ $5.18831$ $1277.7$ $5.20576$ $1301.4$ $5.22716$ $1310.0$ $5.18943$ $1278.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23653$ $1313.1$ $5.19133$ $1280.0$ $5.20966$ $1302.7$ $5.24548$ $1315.1$ $5.19461$ $1283.4$ $5.20805$ $1304.0$ $5.24548$ $1315.1$ $5.19462$ $5.20930$ $1303.3$ $5.24658$ $1315.2$ $5.19602$ $1288.5$ $5.20991$ $1303.8$ $5.25461$ $1317.2$ $5.196602$ $1288.5$ $5.21036$ $1$	5.17761	1267.4	5,20068	1297.1	5.21496	1305.4	
5.18190 $1270.1$ $5.20113$ $1296.8$ $5.21683$ $1307.2$ $5.18235$ $1270.3$ $5.20237$ $1299.2$ $5.21726$ $1307.9$ $5.18360$ $1272.8$ $5.20300$ $1299.4$ $5.21912$ $1308.6$ $5.18426$ $1273.6$ $5.20343$ $1300.7$ $5.21912$ $1307.7$ $5.18472$ $1276.0$ $5.20344$ $1300.0$ $5.21956$ $1307.3$ $5.18596$ $1277.0$ $5.20414$ $1300.0$ $5.22142$ $1307.6$ $5.18707$ $1277.5$ $5.20469$ $1300.7$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20574$ $1301.3$ $5.22186$ $1308.7$ $5.18943$ $1277.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19067$ $1280.2$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19133$ $1280.0$ $5.20805$ $1304.0$ $5.24548$ $1315.1$ $5.19367$ $1284.5$ $5.20806$ $1302.7$ $5.24548$ $1315.1$ $5.19423$ $1288.2$ $5.20930$ $1303.3$ $5.24658$ $1317.2$ $5.19601$ $1285.9$ $5.20991$ $1303.4$ $5.25504$ $1317.1$ $5.19646$ $1286.2$ $5.20992$ $1304.4$ $5.26373$ $1318.8$ $5.19773$ $1288.5$ $5.21161$ $1305.2$ $5.26416$ $1318.7$ $5.19835$ $1291.1$ $1291.1$ $1291.1$ $1291.1$ <td>5.17765</td> <td>1267.3</td> <td>5.20112</td> <td>1297.7</td> <td>5.21682</td> <td>1306.6</td> <td></td>	5.17765	1267.3	5.20112	1297.7	5.21682	1306.6	
5.18235 $1270.3$ $5.20237$ $1299.2$ $5.21726$ $1307.9$ $5.18360$ $1272.8$ $5.20300$ $1299.4$ $5.21912$ $1308.6$ $5.18426$ $1273.6$ $5.20343$ $1300.7$ $5.21912$ $1307.7$ $5.18472$ $1276.0$ $5.20344$ $1300.0$ $5.21956$ $1307.3$ $5.18596$ $1277.0$ $5.20444$ $1300.0$ $5.22142$ $1307.6$ $5.18707$ $1277.5$ $5.20469$ $1300.7$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.22142$ $1307.6$ $5.18780$ $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18831$ $1277.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23676$ $1313.1$ $5.19178$ $1281.7$ $5.20806$ $1302.7$ $5.24591$ $1315.6$ $5.19412$ $1283.4$ $5.20930$ $1303.3$ $5.24658$ $1315.2$ $5.19601$ $1285.9$ $5.20991$ $1303.8$ $5.25604$ $1317.2$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.26373$ $1318.8$ $5.19773$ $1288.5$ $5.21036$ $1303.4$ $5.26373$ $1318.7$ $5.19835$ $1291.1$ $5.21036$ $1303.4$ $5.26373$ $1318.7$	5,181 90	1270.1	5,20113	1296.8	5.21683	1307.2	
5.18360 $1272.8$ $5.20300$ $1299.4$ $5.21912$ $1308.6$ $5.18426$ $1273.6$ $5.20343$ $1300.7$ $5.21912$ $1307.7$ $5.18472$ $1276.0$ $5.20344$ $1300.0$ $5.21956$ $1307.3$ $5.18596$ $1277.0$ $5.20414$ $1300.0$ $5.22142$ $1307.6$ $5.18707$ $1277.5$ $5.20469$ $1300.7$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.22142$ $1307.6$ $5.18780$ $1277.7$ $5.20531$ $1301.3$ $5.22142$ $1307.6$ $5.18831$ $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18943$ $1278.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19178$ $1281.7$ $5.20762$ $1303.8$ $5.23676$ $1313.1$ $5.19367$ $1284.5$ $5.20806$ $1302.7$ $5.24591$ $1315.6$ $5.19601$ $1285.9$ $5.20991$ $1303.8$ $5.25461$ $1317.2$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.25504$ $1317.1$ $5.19646$ $1286.2$ $5.21036$ $1303.4$ $5.26373$ $1318.8$ $5.19773$ $1288.5$ $5.21161$ $1305.2$ $5.26416$ $1318.7$ $5.19835$ $1291.1$ $1291.1$ $1291.1$ $1291.1$ <td>5,18235</td> <td>1270.3</td> <td>5.20237</td> <td>1299.2</td> <td>5,21726</td> <td>1307.9</td> <td></td>	5,18235	1270.3	5.20237	1299.2	5,21726	1307.9	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,18360	1272.8	5,203 00	1299.4	5,21912	1308.6	
5.18472 $1276.0$ $5.20344$ $1300.0$ $5.21956$ $1307.3$ $5.18596$ $1277.0$ $5.20414$ $1300.0$ $5.22142$ $1307.6$ $5.18707$ $1277.5$ $5.20469$ $1300.7$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.22186$ $1308.7$ $5.18831$ $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18943$ $1278.7$ $5.20576$ $1301.0$ $5.23318$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19367$ $1284.5$ $5.20805$ $1304.0$ $5.24548$ $1315.1$ $5.19367$ $1284.5$ $5.20806$ $1302.7$ $5.24591$ $1315.6$ $5.19539$ $1284.5$ $5.20991$ $1303.8$ $5.24561$ $1317.2$ $5.19601$ $1285.9$ $5.20991$ $1303.8$ $5.25641$ $1317.2$ $5.19646$ $1286.2$ $5.21036$ $1303.4$ $5.26373$ $1318.8$ $5.19773$ $1288.5$ $5.21161$ $1305.2$ $5.26416$ $1318.7$ $5.19835$ $1291.1$ $1291.1$ $1291.1$ $1291.1$	5,184 26	1273.6	5.20343	1300.7	5,21912	1307.7	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,18472	1276.0	5.20344	1300.0	5,21956	1307.3	
5.18707 $1277.5$ $5.20469$ $1300.7$ $5.22142$ $1307.6$ $5.18780$ $1277.9$ $5.20531$ $1301.3$ $5.22186$ $1308.7$ $5.18831$ $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18943$ $1278.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19178$ $1281.7$ $5.20762$ $1303.8$ $5.23676$ $1313.1$ $5.19412$ $1284.5$ $5.20805$ $1304.0$ $5.24548$ $1315.1$ $5.19539$ $1284.5$ $5.20930$ $1303.3$ $5.24658$ $1315.2$ $5.19601$ $1285.9$ $5.20991$ $1303.8$ $5.25461$ $1317.2$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.25504$ $1317.1$ $5.19666$ $1286.2$ $5.210.36$ $1303.4$ $5.26373$ $1318.8$ $5.19773$ $1288.5$ $5.211.61$ $1305.2$ $5.26416$ $1318.7$ $5.19835$ $1291.1$ $1291.1$ $1291.1$ $1291.1$	5.18596	1277.0	5.20414	1300.0	5.22142	1307.6	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5,18707	1277.5	5.204 69	1300.7	5.22142	1307.6	
5.18831 $1277.7$ $5.20574$ $1301.4$ $5.22716$ $1310.0$ $5.18943$ $1278.7$ $5.20576$ $1301.0$ $5.22760$ $1309.8$ $5.19067$ $1280.2$ $5.20700$ $1301.9$ $5.23318$ $1310.8$ $5.19133$ $1280.0$ $5.20761$ $1303.1$ $5.23633$ $1313.1$ $5.19178$ $1281.7$ $5.20762$ $1303.8$ $5.23676$ $1313.1$ $5.19367$ $1284.5$ $5.20805$ $1304.0$ $5.24548$ $1315.1$ $5.19412$ $1283.4$ $5.20806$ $1302.7$ $5.24591$ $1315.6$ $5.19539$ $1284.5$ $5.20930$ $1303.3$ $5.24658$ $1315.2$ $5.19601$ $1285.9$ $5.20991$ $1303.8$ $5.25461$ $1317.2$ $5.19602$ $1288.2$ $5.20992$ $1304.4$ $5.25504$ $1317.1$ $5.19646$ $1286.2$ $5.21036$ $1303.4$ $5.26373$ $1318.8$ $5.19773$ $1288.5$ $5.21161$ $1305.2$ $5.26416$ $1318.7$ $5.19835$ $1291.1$ $1291.1$ $1291.1$ $1291.1$ $1291.1$	5.18780	1277.9	5.20531	1301.3	5,22186	1308.7	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.18831	1277.7	5.20574	1301.4	5,22716	1310.0	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5.18943	1278.7	5.20576	1301.0	5,22760	1309.8	
5.191331280.05.207 611303.15.236 331313.15.191781281.75.207 621303.85.236 761313.15.193 671284.55.208 051304.05.245 481315.15.194 121283.45.208 061302.75.245 911315.65.195 391284.55.209 301303.35.246 581317.25.196 011285.95.209 911303.85.254 611317.25.196 021288.25.209 921304.45.255 041317.15.196 461286.25.210 361303.45.263 731318.85.197 731288.55.211 611305.25.264 161318.75.198 351291.15.211 15.211 15.264 161318.7	5,19067	1280.2	5.207 00	1301.9	5,23318	1310.8	
5.191781281.75.207621303.85.236761313.15.193671284.55.208051304.05.245481315.15.194121283.45.208061302.75.245911315.65.195391284.55.209301303.35.246581315.25.196011285.95.209911303.85.254611317.25.196021288.25.209921304.45.255041317.15.196461286.25.210361303.45.263731318.85.197731288.55.211611305.25.264161318.75.198351291.15.201.35.201.35.264165.26416	5.19133	1280.0	5.20761	1303.1	5,23633	1313.1	
5. 193 671284.55. 208 051304.05. 245 481315.15. 194 121283.45. 208 061302.75. 245 911315.65. 195 391284.55. 209 301303.35. 246 581315.25. 196 011285.95. 209 911303.85. 254 611317.25. 196 021288.25. 209 921304.45. 255 041317.15. 196 461286.25. 210 361303.45. 263 731318.85. 197 731288.55. 211 611305.25. 264 161318.75. 198 351291.11291.11111	5.19178	1281.7	5.20762	1303.8	5,23676	1313.1	
5. 194 121283.45. 208 061302.75. 245 911315.65. 195 391284.55. 209 301303.35. 246 581315.25. 196 011285.95. 209 911303.85. 254 611317.25. 196 021288.25. 209 921304.45. 255 041317.15. 196 461286.25. 210 361303.45. 263 731318.85. 197 731288.55. 211 611305.25. 264 161318.75. 198 351291.11201.11201.11201.11201.1	5,19367	1284.5	5,208 05	1304.0	5,24548	1315.1	
5.195 391284.55.209 301303.35.246 581315.25.196 011285.95.209 911303.85.254 611317.25.196 021288.25.209 921304.45.255 041317.15.196 461286.25.210 361303.45.263 731318.85.197 731288.55.211 611305.25.264 161318.75.198 351291.11201.11305.21201.11305.2	5,19412	1283.4	5.20806	1302.7	5,24591	1315.6	
5.196 011285.95.209 911303.85.254 611317.25.196 021288.25.209 921304.45.255 041317.15.196 461286.25.210 361303.45.263 731318.85.197 731288.55.211 611305.25.264 161318.75.198 351291.11291.11305.21291.11305.2	5.19539	1284.5	5.20930	1303.3	5,24658	1315,2	
5.196 021288.25.209 921304.45.255 041317.15.196 461286.25.210 361303.45.263 731318.85.197 731288.55.211 611305.25.264 161318.75.198 351291.11291.11288.51291.11305.2	5.19601	1285.9	5.20991	1303.8	5.25461	1317.2	
5.19646       1286.2       5.21036       1303.4       5.26373       1318.8         5.19773       1288.5       5.21161       1305.2       5.26416       1318.7         5.19835       1291.1	5,19602	1288.2	5.20992	1304.4	5.25504	1317.1	
5.19773         1288.5         5.21161         1305.2         5.26416         1318.7           5.19835         1291.1	5.19646	1286.2	5.21036	1303.4	5,26373	1318.8	
5, 198 35 1291, 1	5.19773	1288.5	5.21161	1305.2	5.26416	1318.7	
	5.19835	1291.1					

TABLE III. (continued)

summarized in Tables I and II, and the experimental data are listed in Table III.

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