## Energy loss and straggling of ions with any velocity in dense plasma at any temperature

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The exact random-phase-approximation dielectric function is used to compute the energy raggling of nonrelativistic charged particles in very den at any degeneracy and for any velocity ratio  $V/V_F$ . Relevance to ion-driven inertial f is stressed.

With the growing attractiveness of ion beams as an inertial confinement fusion (ICP) driver, we are currently witnessing a new and enlarged interest in energy losses and straggling of nonrelativistic charges in dense and hot matter. In contradistine tion to the highly nonlinear<sup>1</sup> coupling encountered in the laser-dense-plasma interaction, at the critical density, the ion-beam target is expected to display a mostly "classical" behavior<sup>2</sup> monitored by weak but numerous Coulomb collisions between a projectile ion and the electrons, free or bound in the dense medium.

This rather pedestrian approach to the beampellet coupling brings in the possibility of accurate tion profile<sup>3</sup> in a given target. Moreover, integrating these elementary events on a pellet radi ing a compression time of the order of a few nsec  $(10^{-9} \text{ sec})$  allows, through appropriate hydro dynamical codes,<sup>4</sup> to optimize the beam characteristics; emittance, density, energy, pulse shape, etc., in order to achieve a given compression.

In this area, the present emphasis lies mostly on stopping characteristics of a dense and hot plasma with an electron temperature comparable or smaller than the Fermi one. This new situation raises the obvious question of how to extrapolate the usual low-temperature  $(k_B T \ll E_F)$  estimates.

To fulfill these goals, we give a complete and numerically exact solution for the energy loss and straggling of swift nonrelativistic ions in a very dense electron fluid of arbitrary degeneracy and for any ion-velocity — Fermi-velocity ratio problem has already recently received considerable attention.<sup>2,5,6</sup>

Usually, the free-electron fluid provides the overwhelming contribution to the stopping process $es<sup>3</sup>$  as soon as

$$
r_s = (\frac{4}{3}\pi n)^{-1/3}a_0^{-1} \leq 1
$$

As a consequence, the previous work<sup>2,5,6</sup> was mostly devoted to a small  $V/V_F$  approximation where the partial degeneracy effect may be worked out through a simplified<sup>4</sup> low-frequency form of the random-phase-approximation (RPA) dynamic electric function  $\epsilon(k,\omega)$ .



FIG. 1.  $(\pi X^2/6)L$  [Eq. (2)] and its large  $V_F/V$  approximants (factorized with  $\pi X^2/6$ ); ---represents  $\ln(2mV^2/$  $\hbar \omega_p$ );  $\triangle$  represents  $\ln(2mV^2/\hbar \omega_p)$   $-T_e[F_{3/2}(\alpha)/\rho]$  $F_{1/2}(\alpha)|V_F^2/V^2$ ;  $\circ$  represents Eq. (8) at  $T_e=1$ . *V* is measured by the mean thermal-electron velocity<sup>9</sup>  $V_F a_0(T)$ .

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The purpose of this paper is to take advantage of an exact<sup>8</sup> RPA  $\epsilon(k,\omega)$  to remove this velocity constraint by considering any  $V/V_F$  ratios, which allows for a much more realistic modeling of the ion-beam-target coupling. Using the notations of Ref. 5, the stopping power reads

$$
\frac{dE}{dx} = \frac{4\pi Z^2 e^4}{mV^2} nL \t\t(1)
$$

where  $Z$  is the projectile charge and  $n$  and  $m$ denote, respectively, the free-electron density and the electron mass. The stopping number  $L$  is given  $by<sup>9,10</sup>$ 

$$
L = \frac{6}{\pi X^2} \int_0^{V/V_F} du \, u \int_0^{\infty} dz \frac{z^3 X^2 f_2(u,z)}{[z^2 + X^2 f_1(u,z)]^2 + [X^2 f_2(u,z)]^2}
$$
(2)

in terms of the standard dimensionless units  

$$
z = \frac{k}{2k_F}, \ \ u = \frac{\omega}{kV_F}, \ \ X^2 = \frac{\alpha r_s}{\pi}, \ \ \alpha = 0.5211 \ .
$$

It should be noticed that Eq. (2) was considered previously<sup>10</sup> by Lindhard and Winther for the case  $T=0$ . The purpose of the present work is to generalize these RPA calculations to any temperature (degeneracy).

The imaginary and real parts<sup>8</sup> of  $\epsilon(k,\omega)$  read

$$
f_2(u,z) = -\frac{\pi T_e}{8z} \ln \left[ \frac{1 + \exp\left(\frac{\gamma - p_+^2}{T_e}\right)}{1 + \exp\left(\frac{\gamma - p_-^2}{T_e}\right)} \right],
$$
\n(3)

$$
f_1(u,z) = \int_0^\infty dk \, n^0(k)
$$
  
 
$$
+ \pi T_e \sum_{n=0}^\infty \left[ \frac{b_n}{r_n} - \frac{1}{4z} \left[ \tan^{-1} \frac{P_+ - a_n}{b_n} + \tan^{-1} \frac{P_+ - a_n}{b_n} - \tan^{-1} \frac{P_- + a_n}{b_n} - \tan^{-1} \frac{P_- - a_n}{b_n} \right] \right],
$$
 (4)

where 
$$
(\epsilon_F = 1.84r_s^{-2})
$$
,  
\n
$$
T_e = \frac{k_B T}{\epsilon_F}, \quad n^0(k) = \left[ \exp\left(\frac{k^2 - \gamma}{T_e}\right) + 1 \right]^{-1}, \quad P_{\pm} = u \pm z,
$$
\n
$$
\gamma = \frac{\mu}{\epsilon_F},
$$

with the coefficients

$$
a_n = \pm \frac{1}{\sqrt{2}} \left\{ \gamma + \left[ \gamma^2 + (2n+1)^2 \pi^2 T_e^2 \right]^{1/2} \right\}^{1/2}.
$$

and

$$
b_n = \pm \frac{1}{\sqrt{2}} \left\{ -\gamma + \left[ \gamma^2 + (2n+1)^2 \pi^2 T_e^2 \right]^{1/2} \right\}^{1/2}.
$$

Similarly, the straggling

$$
\Omega^2 = \frac{4\pi Z^2 e^4}{mV^2} nL'
$$
\n<sup>(5)</sup>

is expressed in terms of a straggling number



FIG. 2. Stopping power  $dE/dx$  (a.u.) at  $n = 10^{25}e$  cm<sup>-3</sup> and various temperature

$$
L' = \frac{24\epsilon_F}{\pi X^2} \int_0^{V/V_F} du \ u^2 \int_0^{\infty} \frac{dz \ z^4 f_2(u,z)}{\left[z^2 + X^2 f_1(u,z)\right]^2 + \left[X^2 f_2(u,z)\right]^2} \left[\frac{2}{\exp\left(\frac{4zu}{T_e}\right) - 1} + 1\right].
$$
 (6)



 $\alpha=\gamma=0$ .

while the large V limit  $\left[\omega_p^2 = (4\pi n e^2/m)\right]$ ,

The small velocity limit<sup>6</sup> is recovered with

 $L = \frac{2}{\pi} \left[ \frac{V}{V} \right]^3 \int_0^{\infty} dz \, z^3 \frac{\partial u}{\partial z^3}$ 

$$
L = \ln \frac{2mV^2}{\hbar \omega_p} - T_e \frac{F_{3/2}(\alpha)}{F_{1/2}(\alpha)} \frac{V_F^2}{V^2} - \frac{T_e^2}{2} \frac{F_{5/2}(\alpha)}{F_{1/2}(\alpha)} \frac{V_F^4}{V^4} ,
$$
\n(8)

 $\pi |V_F|$  Jo<sup>x2</sup>  $[z^2+x^2g(0)]^2$ 

 $\partial f_2(u, z)$ 

(7)

is a novel result, where

$$
F_s(\alpha) = \int_0^\infty \frac{dx x^s}{e^{x-\alpha}+1} \; .
$$

Equation (8) well approximates the complete calculation (see Fig. 1) for  $V/a_0V_F \geq 2$ .

The effect of temperature is especially noticable at low velocity, which allows us to visualize the discrepancies of the present complete calculation with respect to the  $T=0$  calculations.<sup>10</sup> The corre-

sponding  $dE/dx$  displayed in Fig. 2 exhibits *impor*<br>tant temperature effects around  $T_e \sim 1$  for ions with a few MeV per nucleon, an energy range typical of heavy ions used in ICF. As expected,  $dE/dx$  is a decreasing function of T.

The straggling number  $L'$  is given in Fig. 3. Its large  $V$  limit (again a novel result) reads as

$$
L' \sim 2\epsilon_F \left(\frac{V}{V_F}\right)^2 + \frac{4T_e}{3} \frac{F_{3/2}(\alpha)}{F_{1/2}(\alpha)} \ln \frac{V}{V_F} + L'_{\text{res}} ,
$$
\n(9)

where

$$
L'_{\text{res}} = 4\epsilon_F \left[\frac{X^2}{3}\right]^{1/2}
$$

$$
\times \left[\frac{2}{\exp\left[4\left(\frac{X^2}{3}\right)\right]^{1/2} \frac{1}{T_e}}\right] - 1 + 1\left[\frac{L}{2},\right]
$$
(10)

reduces to  $k_BTL$  when  $X/T_e \ll \sqrt{3}/4$ . The above computations for the first time allow us to design accurate pseudoanalytic interpolating  $L$  and  $L'$  formulas valid for any  $V/V_F$  ratios.

The present results thus permit accurate predictons for the stopping properties of hot and dense matter in the weak coupling (RPA) approximation when its kinetic-energy density is larger than its potential one. It remains for us to design appropriate models for the strongly coupled case  $(r_s \ge 1)$ , which is of special relevance at the beginning of the compression. However, preliminary calculations show that the required large-k extension amounts only to a few percent of modifications of the present RPA quantities.

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