Quantum engines with interacting Bose-Einstein condensates

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We consider a quantum Otto cycle with an interacting Bose-Einstein condensate at finite temperature. We present a procedure to evolve this system in time in three spatial dimensions, in which closed (adiabatic) strokes are described by the Gross-Pitaevskii equation and open (isochoric) strokes are modeled using a stochastic Ginzburg-Landau equation. We analyze the effect on the thermodynamic efficiency of the strength of interactions, the frequency of the harmonic trap, and the temperatures of the reservoirs. The efficiency has little sensitivity to changes in the temperatures but decreases as interactions increase. However, stronger interactions allow for faster cycles and for substantial increases in power.

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I. INTRODUCTION

Quantum thermodynamics [1,2] has emerged as a captivating field of research that bridges the fundamental principles of quantum mechanics and the laws of thermodynamics. In recent years, there has been growing interest in the study of quantum thermal machines [3–6], which are devices that utilize quantum systems to convert heat into work and vice versa. In this context, how genuine quantum effects, such as quantum coherence [7,8], correlations [9], and measurements [10–12], can be exploited to improve the performance of these machines has been the subject of intense study. In addition to these theoretical studies, several experimental implementations of different quantum thermodynamic cycles have also been carried out using single quantum systems, such as trapped ions and atoms [13–15].

Quantum many-body systems have also been proposed as the working medium for engines and refrigerators [16].

In this context, Bose-Einstein condensates (BECs) have emerged as a prominent candidate due to their remarkable macroscopically observable quantum properties and controllability. BECs are formed by cooling a gas of bosonic particles to extremely low temperatures and are characterized by a high degree of coherence, in which a significant fraction of the particles occupy the same quantum state. The precise control achieved over BECs through techniques such as laser cooling and magnetic trapping allows for the manipulation of their properties and opens up exciting possibilities for exploring quantum thermodynamics. Recent works designed various engines that utilize BECs to extract work. For instance, Ref. [17] considered an endoreversible Otto cycle with a noninteracting Bose gas, showing that the power output can be enhanced in a regime when the working medium is in the BEC phase. In [18], an interacting BEC engine was explored, and its performance was addressed through the experimental determination of the equation of state, while in [19] an experimental realization of a quantum Otto cycle was performed. Interacting BECs were also considered in [20,21] for a cycle working with a particle reservoir at zero temperature and where the interaction strength between atoms is controlled by Feshbach resonances. Reference [22] outlined a strategy for using a mixture of two atomic gases as a quantum refrigerator. Additionally, Ref. [23] proposed building quantum engines using one-dimensional ultracold gases and illustrated their use in the cooling process. BEC engines with spin-orbit coupling have also been proposed [24].

In this paper, we study a quantum Otto cycle using a three-dimensional interacting Bose-Einstein condensate as a working medium. To do so we perform direct numerical simulations in which the closed (adiabatic) strokes are described by the Gross-Pitaevskii equation (GPE), and the open (isochoric) strokes, which occur at finite temperature, are modeled using a stochastic Ginzburg-Landau equation. This approach allows us to obtain the complete dynamics of the BEC during the whole cycle and provides a highly detailed description of the quantum many-body engine. Therefore, we not only obtain the whole thermodynamic description of the system but also are able to track the evolution of the different contributions to the energy, as well as the state of the BEC, consistently. We aim to uncover the underlying principles governing the efficiency, power output, and other relevant features of these machines. By employing advanced theoretical models and

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numerical simulations, we systematically analyze how various parameters, such as the interaction strength, frequency of the harmonic trap, and reservoir temperatures, affect the performance of a quantum Otto cycle. This work presents a different approach for studying quantum thermal machines with interacting BECs since we adopt a methodology developed for the problem of quantum turbulence that allows us to describe the working medium of the engine with a great level of detail and to obtain both thermodynamic magnitudes as well as information regarding the microscopic degrees of freedom. In this way, we can obtain a complete description even in situations far from equilibrium.

II. METHODS

A. Thermodynamic cycle

We consider a finite-time Otto cycle using an interacting Bose-Einstein condensate as a working medium. The thermodynamic cycle starts with the gas at temperature T_h in a spherical trap with frequency ω_h . The first stroke is an adiabatic expansion that changes ω_h to ω_c , with $\omega_h > \omega_c$, thus expanding the condensate. During the second stroke the system is put in contact with an external cold source, and the gas cools down to reach a thermalized state at temperature $T_c < T_h$ in an isochoric process. The third stroke is an adiabatic compression, changing the trap potential from ω_c to ω_h . Finally, in the last stroke the system undergoes an isochoric process in contact with a hot source at temperature T_h . Thus, the cycle is completely described by prescribing the time taken during each of the strokes, τ_e (for the expansion), τ_{cold} , τ_c (for the compression), and τ_{hot} , respectively, together with the time dependence of the trap potential during the adiabatic strokes. In the following, we will use the same expansion and contraction times so that $\tau_{e,c} = \tau_e = \tau_c$.

We can define W_c and W_e as the work extracted in the compression and the expansion, respectively, and Q_h as the heat absorbed in the isochoric hot process,

$$W_{c,e} = E_{c,e}^{(i)} - E_{c,e}^{(f)},$$
(1)

$$Q_h = E_e^{(f)} - E_c^{(i)}.$$
 (2)

Here *E* is the system total energy, the subindices *e* and *c* denote, respectively, the expansion and contraction strokes, and the superindices *i* and *f* denote, respectively, the initial and final states of these strokes. The efficiency of a heat engine is defined as the net yielded work ($W = W_c + W_e$) divided by the absorbed heat.

In practice, extended systems display heat fluctuations and variations in the work as the cycle is repeated. The efficiency of the cycle is defined as

$$\eta = \frac{W}{Q_h}.$$
(3)

This efficiency will fluctuate in different realizations of the cycle, so one usually is concerned with the mean efficiency.

For noninteracting condensates in the adiabatic regime, the efficiency reduces to the Otto efficiency [17]

$$\eta_O = 1 - \frac{\omega_c}{\omega_h}.\tag{4}$$

B. Adiabatic evolution

We will describe the state of the Bose-Einstein condensate in terms of a single wave function $\psi(\mathbf{r}, t)$. For the expansion and contraction strokes we numerically solve the GPE with a time-dependent harmonic trapping potential $V(\mathbf{r}, t)$,

$$i\hbar\frac{\partial\psi(\mathbf{r},t)}{\partial t} = \left[-\frac{\hbar^2\nabla^2}{2m} + g|\psi(\mathbf{r},t)|^2 + V(\mathbf{r},t)\right]\psi(\mathbf{r},t).$$
(5)

Here *m* is the atomic mass, the interaction is controlled by $g = 4\pi a\hbar^2/m$, and *a* is the *s*-wave scattering length. The spherical potential is given by $V(\mathbf{r}, t) = m\omega^2(t)(x^2 + y^2 + z^2)/2$, and the frequency $\omega(t)$ during the adiabatic strokes changes linearly in time from the initial to the final value. In order to evaluate the total energy of the condensate we consider the Hamiltonian associated with Eq. (5):

$$\mathcal{H}[\psi,\psi^*] = \int d^3r' \left[\frac{\hbar^2}{2m} |\nabla\psi|^2 + \frac{g}{2} |\psi|^4 + V(\mathbf{r},t) |\psi|^2 \right],$$
(6)

where the asterisk denotes the complex conjugate.

C. Thermal baths

During the isochoric strokes the system is coupled to a thermal bath, and in principle, it can exchange both particles and energy. Under these conditions the possible equilibria will be characterized by a volume \mathcal{V} , a chemical potential μ , and a temperature *T*. The probability of these equilibrium states is then given by the grand-canonical ensemble,

$$\mathbb{P} = \frac{e^{-\beta(\mathcal{H}-\mu\mathcal{N})}}{\mathcal{Z}},\tag{7}$$

where $\beta = 1/(k_B T)$, k_B is the Boltzmann constant, \mathcal{Z} is the grand-canonical partition function, and \mathcal{N} is the number of particles in the system.

The evolution of the system towards these equilibria, while in contact with a thermal bath at temperature T, can be done in terms of the approach described in [25,26]. Thus, by adding white noise to Eq. (5) we solve the following stochastic Ginzburg-Landau equation:

$$\frac{\partial \psi}{\partial t} = \left[\frac{\hbar}{2m}\nabla^2 - \frac{g}{\hbar}|\psi|^2 - V(\mathbf{r}) + \frac{\mu}{\hbar}\right]\psi + \sqrt{\frac{2}{\mathcal{V}\hbar\beta}}\zeta(\mathbf{r},t).$$
(8)

Here $\zeta(\mathbf{r}, t)$ is a δ -correlated random process such that $\langle \zeta(\mathbf{r}, t) \zeta^*(\mathbf{r}', t') \rangle = \delta(\mathbf{r} - \mathbf{r}')\delta(t - t')$, and the factor $\sqrt{2/(\nu\hbar\beta)}$ controls the amplitude of the fluctuations through the temperature *T*. This equation can be obtained by performing a Wick rotation $t \rightarrow it$ on Eq. (5) and by adding both the chemical potential and the δ -correlated random forcing term. In the absence of forcing this equation evolves into solutions that are stationary solutions of the GPE [27]. Note that the Ginzburg-Landau equation is also used to study nonisolated dissipative dynamics, e.g., in superconductivity [28]. The random forcing in the stochastic case accounts for the random nature of the system coupled to a thermal reservoir. This

equation and other descriptions using the stochastic truncated Gross-Pitaevskii equation provide a classical description of thermal fluctuations that approximate the quantum field of highly occupied modes by a classical field (see, e.g., [29,30]).

We can explicitly verify that the solutions of Eq. (8) result in equilibria compatible with Eq. (7). Defining the free energy $F = \mathcal{H} - \mu \mathcal{N}$, Eq. (8) can be written as a Langevin equation for the evolution of each Fourier mode of ψ [25],

$$\frac{\partial \hat{\psi}(\boldsymbol{k},t)}{\partial t} = -\frac{1}{\mathcal{V}\hbar} \frac{\partial F}{\partial \hat{\psi}^*(\boldsymbol{k},t)} + \sqrt{\frac{2}{\mathcal{V}\hbar\beta}} \hat{\xi}(\boldsymbol{k},t), \qquad (9)$$

where $F = F[\{\hat{\psi}(\mathbf{k}, t), \hat{\psi}^*(\mathbf{k}, t)\}]$ (i.e., it is a functional of the set of Fourier amplitudes of ψ , where a Galerkin truncation up to a maximum wave number is applied to the set of Fourier modes such that $|\mathbf{k}| < k_{\text{max}}$). The resulting stochastic process has a total state probability $\mathbb{P}[\{\hat{\psi}(\mathbf{k}, t), \hat{\psi}^*(\mathbf{k}, t)\}]$ whose evolution is described by a corresponding multivariate Fokker-Planck equation [31],

$$\frac{\partial \mathbb{P}}{\partial t} = \sum_{|\mathbf{k}| < \mathbf{k}_{\text{max}}} \frac{\partial}{\partial \hat{\psi}_{\mathbf{k}}} \left[\frac{1}{\mathcal{V}\hbar} \frac{\partial F}{\partial \hat{\psi}_{\mathbf{k}}^*} \mathbb{P} + \frac{1}{\mathcal{V}\hbar\beta} \frac{\partial \mathbb{P}}{\partial \hat{\psi}_{\mathbf{k}}^*} \right] + \text{ c.c., } (10)$$

where $\hat{\psi}_{k}$ is shorthand for $\hat{\psi}(k, t)$ and c.c. denotes the complex conjugate. This equation evolves into the grand-canonical distribution in Eq. (7) provided that βF is positively defined. Thus, by numerically integrating Eq. (8) we can evolve the system towards states with different temperatures T under the grand-canonical constraints.

For the isochoric strokes, the system evolves at constant volume \mathcal{V} and fixed number of particles \mathcal{N} (or, equivalently, at fixed mean density $\bar{\rho}$ in the total volume that contains the gas). This corresponds to working on the canonical ensemble and can be achieved by solving Eq. (8) coupled with [25,26]

$$\frac{\partial \mu}{\partial t} = -\gamma (\bar{\rho} - \rho_m). \tag{11}$$

This equation adjusts the chemical potential such that the mean density $\bar{\rho}$ remains close to the target mean density in the trap ρ_m ; γ is a parameter that controls how fast convergence to the desired mean density takes place.

It is worth noting that other formulations to describe condensates at finite temperature exist, such as the stochastic Gross-Pitaevskii equation [32,33] and coupled kinetic equations [34]. While the method used here generates the correct thermal states and has long been used to study the dynamics of dissipative systems at finite temperature [35], a stochastic Gross-Pitaevskii or kinetic formulation could better describe nonequilibrium dynamics, although at a larger computational cost. For a comparison between these methods see [36].

D. Energetics

The total energy of the system can be decomposed into several components that provide information on excited ordered and disordered modes in the gas, such as potential and internal energies, or a compressible kinetic energy that can be associated with sound waves and phonons. To this end we use the Madelung transformation,

$$\psi(\mathbf{r},t) = \sqrt{\rho(\mathbf{r},t)/m} e^{iS(\mathbf{r},t)}, \qquad (12)$$

which maps the GPE to the Euler equation for an isentropic, compressible, and irrotational gas with an extra term that accounts for quantum pressure [27]. This allows for a continuum medium description of the system. In Eq. (12) the transformation $\rho(\mathbf{r}, t)$ is the fluid mass density, and $S(\mathbf{r}, t)$ is the phase of the order parameter. Using the momentum density

$$\boldsymbol{j}(\mathbf{r},t) = -\frac{i\hbar}{2}(\psi^* \nabla \psi - \psi \nabla \psi^*), \qquad (13)$$

the gas velocity can then be defined as $\mathbf{v}(\mathbf{r}, t) = j(\mathbf{r}, t)/\rho(\mathbf{r}, t) = (\hbar/m)\nabla S(\mathbf{r}, t)$.

Thus, in terms of the fluid mass density, the total energy of the system per unit volume [see Eq. (6)] can be decomposed as

$$E = E_{\rm k} + E_{\rm q} + E_{\rm int} + E_{\rm V}, \qquad (14)$$

where the kinetic energy is $E_{\rm k} = \langle \rho v^2 \rangle / 2$, the quantum energy is $E_{\rm q} = \hbar^2 / (2m^2) \langle (\nabla \sqrt{\rho})^2 \rangle$, the gas internal (or interaction) energy is $E_{\rm i} = g/(2m^2) \langle \rho^2 \rangle$, and the trap potential energy is $E_{\rm V} = \langle \rho V \rangle$. In all cases the angle brackets denote the volume average. Using the Helmholtz decomposition $(\sqrt{\rho}\mathbf{v}) = (\sqrt{\rho}\mathbf{v})^{\rm (c)} + (\sqrt{\rho}\mathbf{v})^{\rm (i)}$ [27], where the superindices c and i denote, respectively, the compressible and incompressible components [i.e., such that $\nabla \cdot (\sqrt{\rho}\mathbf{v})^{\rm (i)} = 0$], the kinetic energy can be further decomposed into the compressible, $E_{\rm k}^{\rm (c)}$, and incompressible, $E_{\rm k}^{\rm (i)}$, kinetic-energy components. This decomposition is used to study classical compressible gases [37], as well as quantum fluids [26,38,39], and thus provides information that can be compared with the classical picture of thermal engines.

E. Numerical methods

We numerically solve Eqs. (5) and (8) to simulate the adiabatic and isochoric strokes of the cycle, respectively. In order to do so we use a pseudospectral Fourier-based method in a spatial grid of $N^3 = 64^3$ points, with the 2/3 rule for dealiasing, a fourth-order Runge-Kutta method for the time evolution of GPE, and a Euler time-stepping method for the stochastic Ginzburg-Landau equation. In all cases we use the parallel code GHOST, which is publicly available [40], in a cubic domain of dimensions $[-\pi, \pi]L \times [-\pi, \pi]L \times [-\pi, \pi]L$, so that the domain has length $2\pi L$ (with *L* being a unit length). To deal with the nonperiodic trapping potential in the Fourier representation while avoiding the Gibbs phenomenon, we use the continuation method described in [39,41].

Results are shown in units of a characteristic speed U (the speed of sound), the unit length L (proportional to the condensate mean radius), and a unit mean density ρ_0 . Temperatures are written in units of T_{λ} , the condensate critical temperature (see the Appendix for its estimation and for the range of temperatures considered in this study). Except when explicitly stated (e.g., when we study the effect of varying T_h), we consider $T_h \approx 0.012T_{\lambda}$ and $T_c \approx 0.003T_{\lambda}$. Thus, the simulations have $T \ll T_{\lambda}$. The speed of sound is $\varepsilon = (g\rho_0/m)^{1/2} = 1U$, and the condensate healing length is $\xi = \hbar/(2m\rho_0g)^{1/2} = 0.0707L$, except in simulations in which we artificially decrease the interaction strength. In most simulations we use trapping frequencies $\omega_c \approx 0.334638 U/L$ and $\omega_h = 0.337613 U/L$. These frequencies are chosen to be close enough to reduce the computational cost of performing the slow expansions and contractions, and we indicate explicitly when other values of ω_c and ω_h are used. Quantities can be scaled using dimensional values for U, L, and M. In experiments typical dimensional values are $L \approx 10^{-4}$ m and $c = U \approx 2 \times 10^{-3}$ m/s [42]. This results in $\xi \approx 1.12 \times 10^{-6}$ m and a mean trap frequency $\omega \approx 6.7$ Hz. For the typical mass of a gas of ⁸⁷Rb atoms in a BEC, peak densities of $\approx 10^{13}$ cm⁻³ atoms are also compatible with our simulations and with experiments [43]. As a reference, the adiabatic time in the quantum Otto cycle for noninteracting particles with these parameters is $1/\omega_c \sim 0.15$ s.

For a given set of parameters, each cycle is repeated four times. This results in several values for the energies $E_i^{(j)}$ (with i = c or e and j = i or f) and thus for W and Q_h at the end of each cycle. To compute efficiencies we assume these quantities have a Gaussian distribution and use a Monte Carlo method to generate a random set of W and Q_h values compatible with the fluctuations observed in the four explicitly integrated cycles. From these values, the distribution of the efficiency η and its mean value are finally obtained.

Each realization of the cycle is performed with the following protocol: Given a state at temperature T_h (which can be generated for the first cycle by integrating the stochastic Ginzburg-Landau equation or can be the result of the final state of a previous cycle), we integrate the expansion stroke using the GPE. The frequency of the trap is decreased linearly in time from ω_h to ω_c with a time step $dt = 2.5 \times$ $10^{-3}L/U$; the length of this simulation depends on the speed of the expansion. When the expansion finishes, the system is evolved towards the lower temperature T_c using the stochastic Ginzburg-Landau equation. Time integration is performed until the system reaches a stationary regime. Then, the contraction is integrated using GPE with a linear ramp in the trap frequency from ω_c to ω_h , with the same dt and total time as in the expansion. Finally, the system is again coupled to the hot source at temperature T_h and integrated using the stochastic Ginzburg-Landau equation until a new stationary state is reached.

III. RESULTS

A. Analysis of the system evolution on a cycle

We first analyze the evolution of the system in each stroke and the evolution of the different energy components for the set of parameters introduced in Sec. II E. Then, we evaluate the efficiency of the cycle in terms of the variation of these parameters.

A diagram of several consecutive cycles in the energyfrequency plane and their time evolution (with the time t = 0set arbitrarily at the beginning of each cycle expansion and with the time given in units of the inverse of the frequency difference $\Delta \omega = \omega_h - \omega_c$) is shown in Fig. 1. The numerical simulations agree with the usual picture of an Otto cycle. An abrupt change in energy can be seen as soon as the condensate comes in contact with the thermal sources. The full dynamics allows us to see fluctuations in both the energy after the adiabatic phases and those produced by the thermalization process. These fluctuations also result in slightly different



FIG. 1. Top: Energy as a function of the trap frequency ω for several consecutive cycles. Expansions and contractions are plotted in gray; cooling and heating strokes are in cyan and orange, respectively. Bottom: Time evolution (with time in units of the inverse of $\Delta \omega = \omega_h - \omega_c$) of the total energy in the same cycles, setting time t = 0 for all cycles at the beginning of the expansion. The inset shows the probability density function (PDF) of the condensate mass density in the trap at different times; colors of the lines match the times of the diamond markers in the main plot.

values of the energy along each of the expansions and contractions in the different cycles.

During the isochoric strokes a long integration time is necessary for the system to thermalize at the new temperature. The inset in Fig. 1 shows the tails of the probability density functions (PDFs) of the mass density in the trap at different times after the system is coupled to the cold source. At early times, as the condensate is still hot, the PDF displays strong tails, associated with strong fluctuations in the mass density. Shortly after these regions with strong fluctuations disappear and as the condensate cools down, the PDFs converge to new stationary solutions with weaker tails. Similar results are obtained for the evolution with the hot source. In the next section we vary the strength of the interaction in the BEC and verify that even for weak interactions the system thermalizes. We also ensured that the isochoric branches were integrated long enough to achieve stationary and accurate convergence of the PDFs.

The final states of the isochoric strokes are shown in Fig. 2. The top panels show the mass density in a twodimensional slice in the xy plane at the end of the hot and cold branches solved with the stochastic Ginzburg-Landau equation. At higher temperature the gas displays stronger fluctuations in the mass density at the center of the trap as well as in the borders of the condensate where irregularities can be seen. Density fluctuations are associated with more energy in compressible modes (sound waves or phonons) and with an increase in the quantum energy (caused by gradients in the mass density). The bottom panel shows the compressible kinetic-energy spectrum in both cases. Note that this spectrum measures the energy in sound waves. Two interesting features are worth mentioning. First, the spectra are proportional to a k^2 power law, which corresponds to the equipartition of energy in three-dimensional modes (i.e., thermalization).



FIG. 2. Top: Two-dimensional slices of the mass density in the *xy* plane, $\rho(x, y, z = 0)$, for temperatures $T_h/T_\lambda \approx 0.012$ and $T_c/T_\lambda \approx 0.003$. Bottom: Spectrum of the compressible kinetic energy in the hot and cold cases. An $\sim k^2$ power law corresponding to equipartition of compressible three-dimensional modes is shown as a reference.

Second, the amplitude of sound waves increases with temperature.

Now we analyze the behavior of the energy components during the adiabatic strokes. Naturally, this depends on whether we consider a compression or an expansion, as well as on the speed of the stroke. For the sake of clarity we here consider shorter strokes than in Fig. 1 (i.e., faster compressions and expansions), as they result in more evident effects. Figure 3 shows the time evolution of the different energy components, averaged over four cycles. The energy variations are normalized by the absolute value of the total energy difference during the stroke. During the expansion, the interaction and trap potential energies decay rapidly as the condensate expands. Both quantities also oscillate with the frequency of the breathing mode of the condensate in the trap and have, due to the nature of each energy, almost opposite phases. Meanwhile, the compressible kinetic energy grows as sound waves are excited during the expansion. The incompressible and quantum energies remain almost constant. During the compression, the interaction and trap potential energies grow as the condensate contracts. In this case the compressible kinetic energy remains almost constant, with a small increase in the quantum energy as density gradients grow due to the contraction.

Finally, we consider the isochoric strokes. Note that our integration method for these strokes does not properly describe the system evolution. Therefore, in order to analyze the changes in the different components of the energy during these strokes, we consider only energy changes between the initial and final states of the strokes, as shown in Fig. 4. In both the hot and cold isochores, the interaction energy is the



FIG. 3. Time evolution of the different energy components, averaged over an ensemble of four cycles, during the adiabatic expansion (left) and contraction (right). The value of each energy component at the beginning of the strokes (here arbitrarily labeled as t = 0) is subtracted from the energies, and the energy variations are then normalized by the absolute value of the total energy difference during the entire stroke.

one responsible for the majority of the energy exchange. This highlights the relevance of interactions in this system.

B. Efficiency

We now analyze the efficiency of the cycle. In particular, we focus on its behavior in terms of the speed of the expansion and compression (i.e., $\tau_{e,c}$), the temperature, and the interaction strength.

Let us first consider the impact of the speed of the adiabatic stroke. To this end, for the set of parameters introduced in Sec. II E, we performed several cycles with adiabatic strokes of different lengths $\tau_{e,c}$ (longer $\tau_{e,c}$ corresponds to slower



FIG. 4. Energy variations for each energy component (E_{int} , E_q , $E_k^{(i)}$, $E_k^{(c)}$, and E_V) during the isochoric strokes when in contact with the hot and cold sources. Each component is normalized by the total change of energy during the stroke, resulting in a fraction of the total change.



FIG. 5. Efficiency of the cycles in units of the ideal Otto efficiency η_O as a function of $\tau_{e,c}$ for the parameters listed in Sec. II E. The shaded areas indicate the PDFs of the efficiencies, and the error bars indicate the minimum and maximum efficiencies obtained. The vertical dashed line indicates the time ω_c^{-1} . In a noninteracting condensate, the expansion and contraction times must be much larger than this value to achieve adiabaticity. As a reference, for a gas of ⁸⁷Rb atoms as discussed in Sec. II E, $\omega_c^{-1} \approx 0.15$ s, and $\tau_{e,c}\Delta\omega \approx 0.03$ corresponds to times of ≈ 0.5 s.

expansions and contractions). In this case, we expect to attain the utmost efficiency for greater values of $\tau_{e,c}$ since the dynamics gets closer to the adiabatic limit. Figure 5 shows the efficiency distribution of the cycles for different values of $\tau_{e,c}$ (in units of $\Delta \omega^{-1}$). As expected, we find that the mean efficiency grows with this time, and for times $\tau_{e,c}$ much longer than the characteristic time associated with the adiabatic limit for noninteracting gases ($\sim \omega_h^{-1}$), the efficiency reaches a value that is independent of $\tau_{e,c}$. In this regime, the efficiency is roughly half that of the ideal Otto efficiency for a noninteracting gas.

On the other hand, when only the temperature of the hot reservoir T_h is varied, we find that the efficiency remains approximately constant (i.e., within error bars; see Fig. 6), as expected for an Otto cycle [17,44]. However, increasing T_h (and therefore the difference between T_h and T_c) results in a reduction in fluctuations. Thus, larger temperature gradients lead to a better determination of the averaged efficiency. Note that this is also what happens with the ideal Otto cycle, where the efficiency is independent of the temperatures.



FIG. 6. Efficiency (in units of the ideal Otto efficiency) as a function of the hot temperature T_h using the same parameters as in Sec. II E. Labels for the markers are the same as in Fig. 5.



FIG. 7. Efficiency of the cycle η as a function of $\eta_0 = 1 - \omega_c/\omega_h$ as we vary ω_c/ω_h (symbols with the same color). For an ideal Otto cycle we expect $\eta = \eta_0$. Different colors of the symbols correspond to different interaction strengths: gray for $\alpha = 1$ ($g = g_0$) and purple for $\alpha = 0.064$ ($g = 0.064g_0$). Two slopes are indicated as references.

We will now analyze the efficiency in terms of the interaction strength. In this case, we expect that in the limit of a noninteracting gas the efficiency should approach η_O , as defined in Eq. (4) [17]. However, our method can attain this limit only asymptotically. This is due to the fact that when the interaction is removed, g = 0, the thermalization time extends to infinity (as illustrated in Fig. 1). Therefore, we evaluate the efficiency as the interaction strength is reduced. Reducing the interaction strength leads to a decrease in the speed of sound and an increase in the healing length (i.e., a more dilute gas). In the following, we express the results with respect to a coefficient α , defined as

$$g = \alpha g_0, \tag{15}$$

where $0 < \alpha \leq 1$ and g_0 corresponds to setting the speed of sound $c = (g_0 \rho_0 / m)^{1/2} = 1U$ and $\xi = \hbar / (2m\rho_0 g_0)^{1/2} = 0.0707L$ (i.e., the value used so far in this work).

First, we performed several cycles with different values of ω_c/ω_h , varying ω_c for two interaction strengths, $\alpha = 1$ and $\alpha = 0.064$ (the other parameters are the same as in Sec. II E). Figure 7 shows the efficiency as a function of the ideal Otto efficiency $\eta_O = 1 - \omega_c/\omega_h$. We can see that it remains smaller than the Otto efficiency (which is indicated for reference by an orange dashed line). However, it still scales linearly with $1 - \omega_c/\omega_h$ and also gets closer to η_O when α decreases. Interestingly, the behavior in Figs. 6 and 7 indicates that the efficiency is independent of the temperature and the dependence on α can be factorized. This, at least in the regime of parameters that we are exploring, suggests that efficiency for the interacting gas is proportional to the ideal noninteracting Otto efficiency, with a proportionality factor that decreases with the interaction strength.

Then, we fix the value of ω_c/ω_h and vary the interaction strength. Note that the volume of the condensate depends on *g*. In this case, as we consider repulsive interactions, the volume decreases with *g* at a fixed potential. We considered two different situations: one in which the total mass of the condensate is kept constant as the interaction strength is changed and one in which the density in the center of the trap is kept constant.



FIG. 8. Top: Efficiency in units of η_O for different interaction strengths $\alpha = g/g_0$. We compare situations in which the total mass in the condensate is constant (labeled M) and in which the density in the center of the trap is constant (labeled ρ_0). Labels for the markers are the same as in Fig. 5. Bottom: Mean work extracted by the engine as a function of α in units of the work W^* for the fully interacting case with $\alpha = 1$.

We can appreciate from the top panel of Fig. 8 that both cases display similar efficiencies. However, when the mass is constant, the fluctuations are larger than when the density is kept constant. This stems from the fact that as the interaction strength is reduced, the concentration of particles at the center of the trap decreases substantially, thus increasing the number of fluctuations. In general, we observe that the efficiency grows slowly for small α . In both cases, as α decreases, the efficiency increases, attaining a mean value $\approx 65\%$ of η_0 for the minimum α considered in the simulations. As previously stated, we are unable to reduce the value of α any further as calculating isochoric strokes becomes excessively expensive with a progressively increasing thermalization time.

Finally, we analyze the power of this engine. Let us first look at the bottom panel of Fig. 8, where the mean extracted work as a function of the interaction strength α is shown. In this case, we compare the extracted amount of work for a given value of α with the work W^* extracted in the fully interacting case with $\alpha = 1$. Note that W/W^* increases by $\approx 50\%$ for decreasing α and becomes approximately constant for $\alpha < 10^{-1}$. The actual power of the cycle is determined by the ratio of the work to the time required to complete the cycle. As it occurs in both numerical simulations and real gases, we consider that the thermalization times in the isochoric strokes are longer than the times required for the expansion and compression. Thus, we can approximate the length of the cycle as twice the length of the thermalization process. Note that in our simulations we use the stochastic Ginzburg-Landau equation as a multivariate Fokker-Plank equation to obtain the new equilibria (at a given temperature) of the grand-canonical ensemble; therefore, the time in the simulation should not be directly associated with an actual thermalization time. However, in the noninteracting limit the thermalization time effectively goes to infinity, as the time between collisions diverges.



FIG. 9. Mean value for different times of the mean density in the center of the trap as a function of the temperature for thermal states. The shaded part shows where all the temperatures mentioned in this work lie, showing that they are far away from the transition, so the noncondensed fraction can be neglected.

We can still estimate the order of the thermalization time for the interacting case from kinetic theory. Note that $g \sim a$; that is, it is linearly proportional to the scattering length, and thus, $g \sim a \sim \sqrt{\sigma}$, where σ is the collision cross section. As $\sigma \sim 1/\tau$, where τ is the time between collisions, for a fixed number of particles the time it takes for the system to thermalize with $\alpha = 1$ compared with the time when $\alpha < 1$ is proportional to the ratio of the times between collisions,

$$\frac{\tau_0}{\tau} \sim \left(\frac{g}{g_0}\right)^2 = \alpha^2,$$
 (16)

where τ_0 is the value of τ when $\alpha = 1$. This indicates (in qualitative agreement with the results from the numerical simulations) that interactions allow for much faster cycles and extraction of significantly more power (e.g., from the cycles in the plateau of *W* for $\alpha < 10^{-1}$ in Fig. 8, even with the reduction in the extracted work of $\approx 50\%$ with respect to $\alpha = 1$). In other words, interacting gases allow us to get higher power in a finite time cycle. Moreover, in principle by adjusting the interaction strength of the condensate, a power enhancement at nearly constant efficiency can be achieved (see Figs. 7 and 8).

IV. CONCLUSIONS

In this work, we performed numerical simulations of quantum Otto engines that have an interacting BEC as the working medium. We were able to recover not only the thermodynamics of the system but also its complete dynamics, which enabled us, in turn, to perform a detailed analysis of the engine, analyzing, for instance, the different contributions to the energy along the adiabatic strokes.

We characterized the efficiency of the engine by performing several simulations in which we independently changed the temperatures, the trap frequencies, and the interaction strength of the gas. We found that the efficiency is independent of the temperature. However, fluctuations in the efficiency and in other observables are reduced as the difference between the temperatures of the reservoirs increases. Also, their dependence on the trap frequencies turns out to be similar to that in the noninteracting case, but with a proportionality factor that depends on the interaction strength.

We also showed that the efficiency and work output of the engine decrease as the interaction strength of the BEC becomes larger. However, the timescale it takes the system to thermalize is inversely proportional to the square of the interaction strength. Thus, for small interactions, we found a regime in which increasing the interaction of the BEC allows for a considerable increase in power, while the efficiency is only slightly reduced. Since the interaction strength of the BEC can be experimentally tuned, our results provide a possible way to improve the power of a quantum engine at a small cost in efficiency.

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APPENDIX: ESTIMATION OF T_{λ}

In order to estimate the critical temperature T_{λ} of the condensate, we performed a series of simulations of the

stochastic Ginzburg-Landau equation with parameters as listed in Sec. **IIE** (i.e., the most interacting case in our paper) at constant frequency of the trap ω_c while varying the temperature T. In mean-field theory, the critical temperature decreases with increasing interaction, a result that has been confirmed experimentally where higher-order corrections were also observed [45,46]. This guarantees that temperatures used in this study, as they are far below T_{λ} of the most interacting case, are sufficiently small that all the simulations are below the critical temperature. This is enhanced by the fact that to determine T_{λ} we use the smallest value of ω for the trap. To obtain the condensed fraction in the gas as a function of the temperature we use an approach similar to that used in experiments [47]. We consider the mean mass density in the vicinity of the center of the trap as the order parameter, $\langle \rho_0 \rangle$, averaged in time once the system reaches equilibrium.

Figure 9 shows the result as a function of the temperature. Temperature is shown in units of the transition temperatures T_{λ} ; that is, it is rescaled in such a way that the transition in the behavior of $\langle \rho_0 \rangle$ happens at $T/T_{\lambda} = 1$. Note that this parameter has an abrupt change in behavior at this temperature as it decreases from 1 monotonically and then remains approximately constant. This is compatible with a second-order phase transition. All the temperatures considered in this study lie in the light-blue shaded region of Fig. 9, i.e., far away from the phase transition.

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