

Reference-frame-independent model of a collective-excitation atom interferometerB. J. Mommers^{1,2,*} and M. W. J. Bromley^{3,2}¹*Centre for Engineered Quantum Systems, The University of Queensland, St Lucia 4072, Australia*²*School of Mathematics and Physics, The University of Queensland, St Lucia 4072, Australia*³*School of Sciences, University of Southern Queensland, Toowoomba 4350, Australia*

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We theoretically analyze the operating principles of a proposed matter-wave Sagnac interferometer utilizing Bose-Einstein-condensate (BEC) phonon modes as an interference medium. Previous work found that the orbital angular momentum phonon modes of a ring-trapped BEC are split in frequency by rotations, leading to a measurable rotation signal. We develop an alternate description in which an imbalance in the counterpropagating modes' amplitudes (populations) is induced by the rotation of the system during condensation. This description gives analytic forms for the interferometric phase shift in one dimension and is readily generalized to include mean-field interactions. To validate our findings, we simulate a ring-trapped BEC Sagnac interferometer in one dimension and demonstrate that measurement of an unknown rotation rate can be performed using a modified analysis. Our simulation data show strong agreement with our analytic results, and we further employ simulations to explore and clarify the role of superfluidity in this matter-wave Sagnac interferometer.

DOI: [10.1103/PhysRevA.107.023314](https://doi.org/10.1103/PhysRevA.107.023314)**I. INTRODUCTION**

The Sagnac effect links the phase shift between waves counterpropagating within an enclosed loop with the external rotation of such a system [1]. This has been exploited to allow high-precision interferometric measurement of rotations, useful in inertial sensing and navigation (for examples see Ref. [2]). Current state-of-the-art Sagnac interferometers utilize counterpropagating light, with a large enclosed area to boost sensitivity [3]. Matter-wave systems appear to have a sensitivity advantage when considering the energy difference between optical and atomic systems [4]. Despite this, matter-wave Sagnac interferometers are yet to surpass their optical counterparts in terms of precision.

Recent proposals have made use of advances in Bose-Einstein-condensate (BEC) research and experimental techniques, providing an alternative medium to atomic-beam-based and guided matter-wave interferometry schemes [5–23]. In particular, proposals to measure the Sagnac phase shift of an interference pattern produced by counterpropagating orbital angular momentum (OAM) modes in a trapped BEC offer a way to utilize the high levels of control and coherence available in modern experimental systems [23–25]. This can be achieved through imparting optical OAM onto the condensate [24] or by exciting standing-wave collective excitations [25]—the latter is the focus of this work.

The use of collective-excitation modes is expected to ameliorate technical difficulties often associated with BEC interferometric protocols that require condensate splitting or spin-dependent transitions [7,11,13,15,26–29]. A protocol for collective-excitation Sagnac interferometry in a ring-trapped

BEC has been proposed and tested for rotation sensing [25]. This protocol imprints a standing-wave excitation on ring-trapped atoms through a weak azimuthally modulated optical potential while cooling through the BEC transition. By imposing this potential during condensate formation then releasing the BEC to freely evolve in the ring, rotation of the standing-wave pattern is observable in the rotating laboratory frame, as illustrated in Fig. 1.

Reference [25] analyzed the standing-wave rotation in terms of a frequency splitting between the standing wave's constituent counterpropagating traveling-wave components in a three-mode model. However, the frequency-splitting effect requires observation in an inertial frame, something that cannot be achieved when attempting to experimentally measure unknown rotations.

This work is an alternate analysis of the theory in Ref. [25], in which we develop a frame-independent theory of operation for this protocol. By analyzing the dynamics in the context of mode amplitudes we reveal multiple features of the interferometric design that were not previously apparent. The splitting of counterpropagating modes in a rotating waveguide via the Sagnac effect has been exploited in optical systems to produce nonreciprocal propagation of light, analyzed in terms of both mode amplitude [30] and frequency splitting [31,32]. For the purposes of matter-wave Sagnac interferometry for precision rotation sensing, we show that a mode amplitude-splitting analysis provides further insight into achieving high precision.

In Sec. II we describe the three-mode model and use it to derive the relationship between the rotation rate and standing-wave mode amplitudes, showing that rotation induces a splitting in the amplitudes of counterpropagating modes. Section III details our numerical simulations of the interferometer, which show that rotation measurements can be performed by examining the evolution of the Fourier phase of

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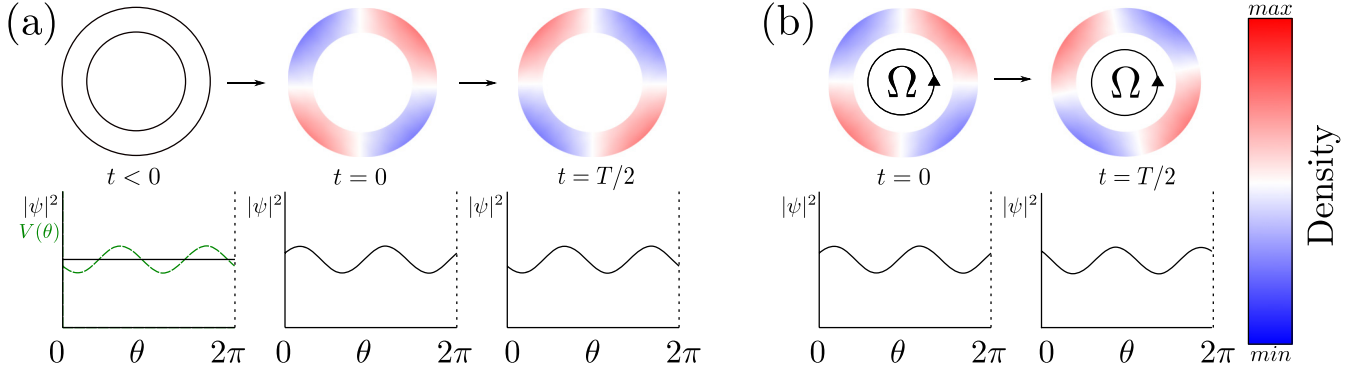


FIG. 1. Marti *et al.*'s [25] proposed schematic illustration, with a 2D top-down view (top) and 1D representation (bottom). (a) Begin with atoms confined to a ring with constant density and impose an optical potential with azimuthally dependent modulations $V(\theta)$ while condensing to form a BEC with density modulations. At $t = 0$, remove the optical potential, and allow the density modulations to undergo standing-wave oscillation, where at each half cycle, the density modulation pattern is inverted. (b) In the presence of rotation, the modulation peaks shift position with each half cycle.

the imprinted density modes. In Sec. IV we show numerically that the imbalanced state is the ground state of the ring system in the presence of both rotation and an imprinting potential. In Sec. V we extend our analysis to low-temperature BECs described by the Gross-Pitaevskii equation (GPE) and examine practical considerations of our results.

II. THREE-MODE MODEL

In this section we introduce the three-mode model and use it to derive the Sagnac phase shift for the ring geometry in both inertial and rotating frames. In the rotating frame we directly relate the mode imbalance to the rotation rate.

Our initial analysis considers a simple model of the proposed phonon-mode interferometer: a noninteracting system confined to a one-dimensional ring. This ideal phonon-mode interferometer with wave function $\psi(\theta)$ populates only three angular momentum eigenstates,

$$\psi(\theta) = \phi_0 + \phi_{+l} + \phi_{-l}, \quad (1)$$

$$\phi_0 = a_0, \quad (2)$$

$$\phi_l = (a + \Delta) e^{il\theta}, \quad (3)$$

$$\phi_{-l} = (a - \Delta) e^{-il\theta}. \quad (4)$$

Here ϕ_k is an angular momentum eigenstate with quantized circulation $k \in \{0, l, -l\}$, a is the mean amplitude of the $k = \pm l$ modes, Δ is the mode splitting, and θ is the positional parameter (angle) around the one-dimensional (1D) ring. The wave function is normalized such that $\int |\psi|^2 dr = 1$. Therefore, ϕ_0 is the constant background on which the angular momentum modes (i.e., phonon modes) with OAM quantum number $\pm l$ are imprinted. Nonzero values of Δ result in an imbalance between counterpropagating mode amplitudes.

A. In the inertial frame

To begin, we first note that Ref. [25] assumes an equal superposition of counterpropagating modes, i.e., $\Delta = 0$. Our analysis proceeds without this assumption. For each mode [Eqs. (2) to (4)], the time evolution operator $U_t = e^{-i\hat{H}t/\hbar}$ is

given by

$$U_t \phi_0 = a_0 e^{-iE_0 t/\hbar}, \quad (5)$$

$$U_t \phi_l = (a + \Delta) e^{i(l\theta - Et/\hbar)}, \quad (6)$$

$$U_t \phi_{-l} = (a - \Delta) e^{-i(l\theta + Et/\hbar)}, \quad (7)$$

where E_0 is the energy of the background mode and $E = E_l = l^2 \hbar^2 / 2mr^2$ is the degenerate energy of the counterpropagating modes, with m representing particle mass and r being the ring's radius, both of which we set to 1 without loss of generality.

The time-dependent density profile can be decomposed into the sum of a standing wave and a traveling wave oscillating on a time-independent background,

$$\begin{aligned} |\psi(t)|^2 = & a_0^2 + (a + \Delta)^2 + (a - \Delta)^2 \\ & + 2(a + \Delta)(a - \Delta) \cos(2l\theta) \\ & + 4a_0 \Delta \cos[l\theta - (E - E_0)t/\hbar] \\ & + 2a_0(a - \Delta) \{ \cos[l\theta - (E - E_0)t/\hbar] \\ & + \cos[l\theta + (E - E_0)t/\hbar] \}. \end{aligned} \quad (8)$$

Note that when $\Delta = 0$, the traveling-wave component of Eq. (8), $4a_0 \Delta \cos[l\theta - (E - E_0)t/\hbar]$, is zero, consistent with a nonrotating standing-wave state. The rotation rate is determined through the evolution of the complex phase shift in the single-frequency Fourier transform of the density profile,

$$\varphi(t) = \arctan \left[\int |\psi(t)|^2 e^{-il\theta} d\theta \right], \quad (9)$$

for a single mode l .

From Eqs. (8) and (9), the phase shift in the inertial frame takes the form

$$\varphi(t) = \arctan \left[-\frac{\Delta}{a} \tan[(E - E_0)t/\hbar] \right]. \quad (10)$$

In the limit $\frac{\Delta}{a} \rightarrow 1$, Eq. (10) gives a constant phase gradient—a linear phase accumulation consistent with a pure traveling wave. Conversely, taking the limit $\Delta \rightarrow 0$ results in a constant zero phase gradient, as expected for a pure standing wave.

Considering Eq. (10) at stroboscopic measurement times,

$$\tau_s = \frac{n\pi\hbar}{E - E_0}, \quad (11)$$

where n is a natural number encoding the number of oscillations since $t = 0$, the phase shift is always zero. The rotation of the density profile relative to the measurement frame (in this case the inertial frame) is given by the time derivative of the phase shift at stroboscopic times—when the standing-wave component is at its maximum amplitude,

$$\frac{d\varphi}{dt} = -\frac{\Delta(E - E_0)}{\hbar a}. \quad (12)$$

In the inertial frame this depends only on the mode imbalance and choice of excited mode number. In a sensing application, the measurement frame is expected to rotate with the system at an unknown rate. By analyzing the phase shift $\varphi(t)$ in the

$$\varphi(t) = \arctan \left[\frac{-\Delta \sin[(E - E_0)t/\hbar] \cos(l\Omega t) + a \cos[(E - E_0)t/\hbar] \sin(l\Omega t)}{\Delta \sin[(E - E_0)t/\hbar] \sin(l\Omega t) + a \cos[(E - E_0)t/\hbar] \cos(l\Omega t)} \right]. \quad (15)$$

For $\Omega = 0$, this reduces to Eq. (10). At stroboscopic times τ_s [Eq. (11)] we find explicit dependence of the phase shift on the rotation rate,

$$\varphi(\tau_s) = \frac{n\pi\hbar l \Omega}{E - E_0}. \quad (16)$$

This phase shift increases with each oscillation due to the n dependence of Eq. (16). At exactly $t = \tau_s$, the rotation of the density profile is zero relative to the rotating frame. At other times, it follows the general form of the phase-shift time derivative in the rotating frame,

$$\frac{d\varphi}{dt} = l\Omega - \frac{\Delta(E - E_0)}{\hbar a}. \quad (17)$$

As $\frac{d\varphi}{dt} = 0$ at stroboscopic measurement times, we can directly relate the mode imbalance Δ to the rotation rate Ω using Eq. (17),

$$\frac{\Delta}{a}(E - E_0) = l\hbar\Omega. \quad (18)$$

This result demonstrates that a rotating system develops an imbalance in the amplitudes of imprinted counterpropagating OAM modes which is intrinsically linked to the rate of rotation—with nonzero rotation there is always a nonzero imbalance.

Experimentally, the rotation rate is measured by imaging the atomic density at one or more stroboscopic measurement times and determining the Fourier phase shift. The linear gradient between stroboscopic phase shifts according to Eq. (16) is proportional to $l\Omega$; therefore, an unknown rotation rate can be measured in a frame where the laboratory is also rotating.

III. NUMERICAL SIMULATIONS

To test and extend our analytic results, we simulate the dynamics of a one-dimensional ring-trapped condensate in

rotating frame, we can determine the relationship between the rotation rate Ω and mode imbalance Δ .

B. In the rotating frame

In the rotating frame, we can perform an analysis similar to that above with the inclusion of a time-dependent coordinate transform,

$$\theta \rightarrow \theta' + \Omega t. \quad (13)$$

Repeating the calculation of the time-dependent density, the Fourier-transform result for a rotating system is given by

$$\int |\psi(\theta', t)|^2 e^{-il\theta'} d\theta' = a_0(a + \Delta)e^{-i(E - E_0)t/\hbar + i\Omega t} + a_0(a - \Delta)e^{i(E - E_0)t/\hbar + i\Omega t}. \quad (14)$$

The phase angle subsequently depends on the rotation rate,

two parameter regimes: the phonon regime and the mean-field regime. In the phonon regime, excitations are of sufficiently small amplitude that inter-particle interactions are negligible, allowing simulation of dynamics using the Schrödinger equation for wave function $\psi(\theta, t)$,

$$-i\hbar \frac{\partial \psi(\theta, t)}{\partial t} = \left(\frac{-\hbar^2}{2mr^2} \frac{\partial^2}{\partial \theta^2} + V(\theta, t) \right) \psi(\theta, t). \quad (19)$$

In the mean-field regime, interactions are non-negligible and are described by the GPE,

$$-i\hbar \frac{\partial \psi(\theta, t)}{\partial t} = \left(\frac{-\hbar^2}{2mr^2} \frac{\partial^2}{\partial \theta^2} + V(\theta, t) + g|\psi(\theta, t)|^2 \right) \psi(\theta, t), \quad (20)$$

where g is the interaction strength parameter, r is the radius of the ring, $V(\theta, t)$ is the time-dependent imprinting potential, and in the GPE $\psi(\theta, t)$ is the 1D order parameter for the bosonic field. Simulation is performed using a three-point Crank-Nicolson method on a grid of 105 points. We simulate the full protocol: condensation (via imaginary-time evolution) in an $|l| = 5$ imprinting potential and removal of the imprinting potential at $t = 0$ for free evolution of the system. The Fourier components at select frequencies corresponding to OAM modes $l = [-15, 15]$ are calculated at each time step, including the phase shift extracted from the density profile. Rotation of the system was independently set for the imaginary-time and real-time portions of the simulation via the rotation parameters Ω_I and Ω_R , respectively. Density plots and extracted phase shifts for the noninteracting system are presented in Fig. 2.

Several features of our numerical results support our analytic solution from Sec. II. In the inertial frame

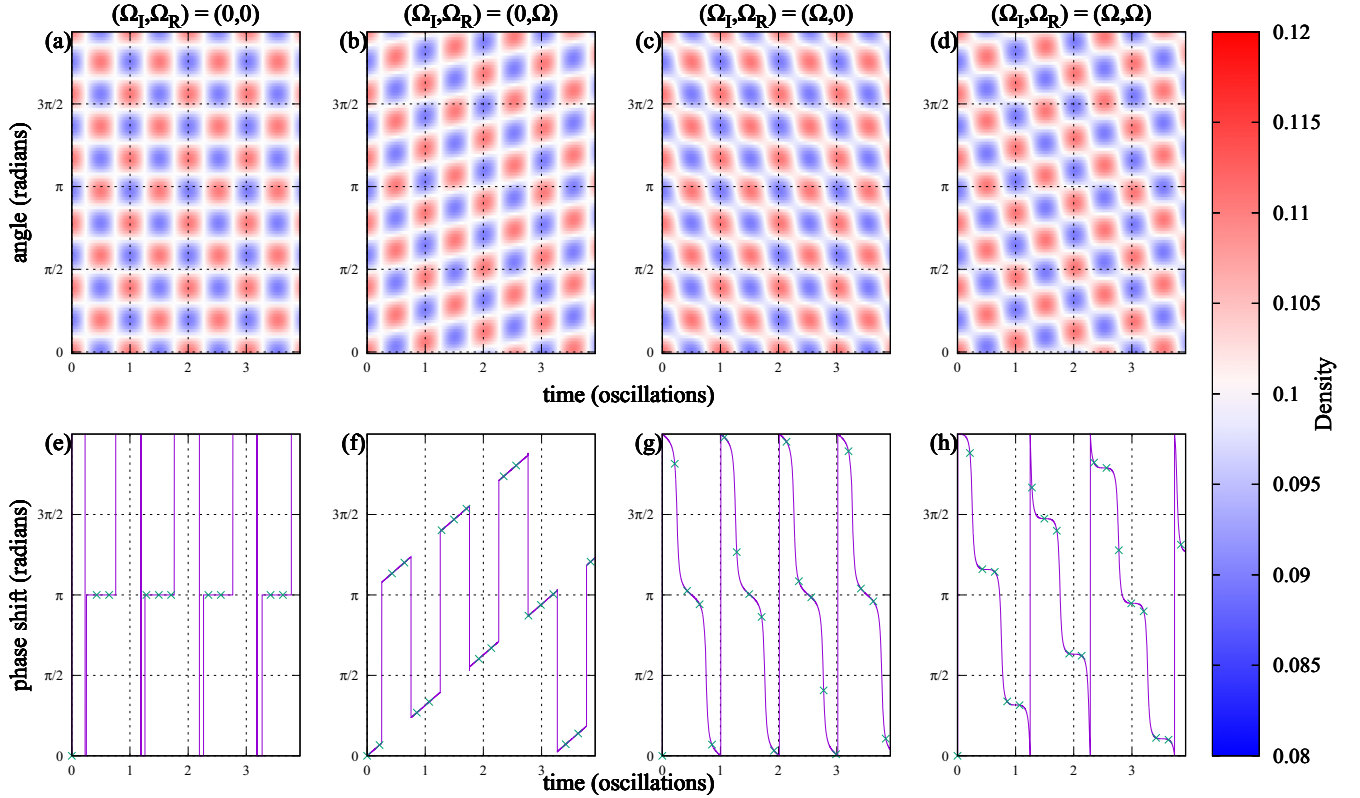


FIG. 2. Space-time density profiles and extracted phase for different rotating-reference-frame configurations from simulations without interactions. (a)–(d) Space-time density profiles for the ideal 1D ring system. Each case is labeled with the rotation rate of the system during imaginary-time evolution Ω_I , which corresponds to condensate formation, and the real-time rotation rate Ω_R , which corresponds to the free evolution of the system once the imprinting potential is removed. Dashed vertical lines indicate full oscillations of the standing-wave component from $t = 0$, while dashed horizontal lines indicate angular positions around the ring to guide the eye. (e)–(h) Plots of the extracted phase for each of the simulation conditions matching the density-profile plot immediately above. The purple curve is from simulations using the ground state found via imaginary time, while the green points are from simulations that numerically optimize Eq. (22). The numerics in Ref. [25] correspond to (b) and (f), while a physical experiment necessarily corresponds to (d) and (h).

($\Omega_I = \Omega_R = 0$) the phase shift at stroboscopic times is zero, as shown in Fig. 2(e). Similarly, Fig. 2 shows the time derivative of the phase shift in the rotating frame ($\Omega_I = \Omega_R = \Omega$) is zero, and the phase shift accumulates by a fixed amount proportional to $l\Omega$ for each oscillation, as predicted by Eq. (16).

Figure 2 highlights the differences in both phase shift and density oscillations under different rotation conditions. The rotating-frame analysis in Sec. II corresponding to Figs. 2(d) and 2(h) matches the conditions of an experimental measurement of an unknown rotation—the condensate is prepared under rotation and freely evolves in the ring trap under rotation.

IV. NUMERICAL CALCULATION OF THE GROUND STATE

The protocol in Ref. [25] requires an imprinting potential during condensation to form the initial state. According to the three-mode model, the ground state in the imprinting potential will depend on model parameters a_0 , a , and Δ . In this section, we calculate the expectation value of the imprinting Hamiltonian using a three-mode state and compare its numerically calculated minimum value to the ground state found using imaginary-time evolution.

We simulate the 1D particle-in-a-ring Hamiltonian with imprinting potential in a rotating frame,

$$\hat{H} = -\frac{\hbar^2}{2mR^2} \frac{\partial^2}{\partial \theta^2} + [V_0 - \alpha \cos(l\theta)] + i\hbar\Omega \frac{\partial}{\partial \theta}. \quad (21)$$

Here m is the particle mass, R is the ring radius, Ω is the rotation rate, and $V = [1 - \alpha \cos(l\theta)]$ is the imprinting potential with modulation amplitude α . We choose as our ansatz ψ from Eq. (1), with normalization factor $\mathcal{N} = [2\pi(a_0^2 + 2a^2 + 2\Delta^2)]^{-1/2}$. We then calculate the expectation value of the Hamiltonian $\langle \hat{H} \rangle$,

$$\langle \hat{H} \rangle = \frac{\hbar^2 l^2 (2a^2 + 2\Delta^2) + 4l\Omega a \Delta - 2\alpha a_0 a}{a_0^2 + 2a^2 + 2\Delta^2}. \quad (22)$$

Full details of the calculation are available in Appendix A. The ground state of the system is defined by the values of a_0 , a , and Δ that minimize this expectation value for given values of the ring radius, rotation rate, and imprinting potential amplitude. Note that for nonzero rotation $|\Omega| > 0$, there is an explicit coupling of a and Δ ; therefore, the ground state of a nonrotating system will have a different value for a than that of an identical system that is rotating. This can be seen by careful examination of Fig. 3. As the normalization factor

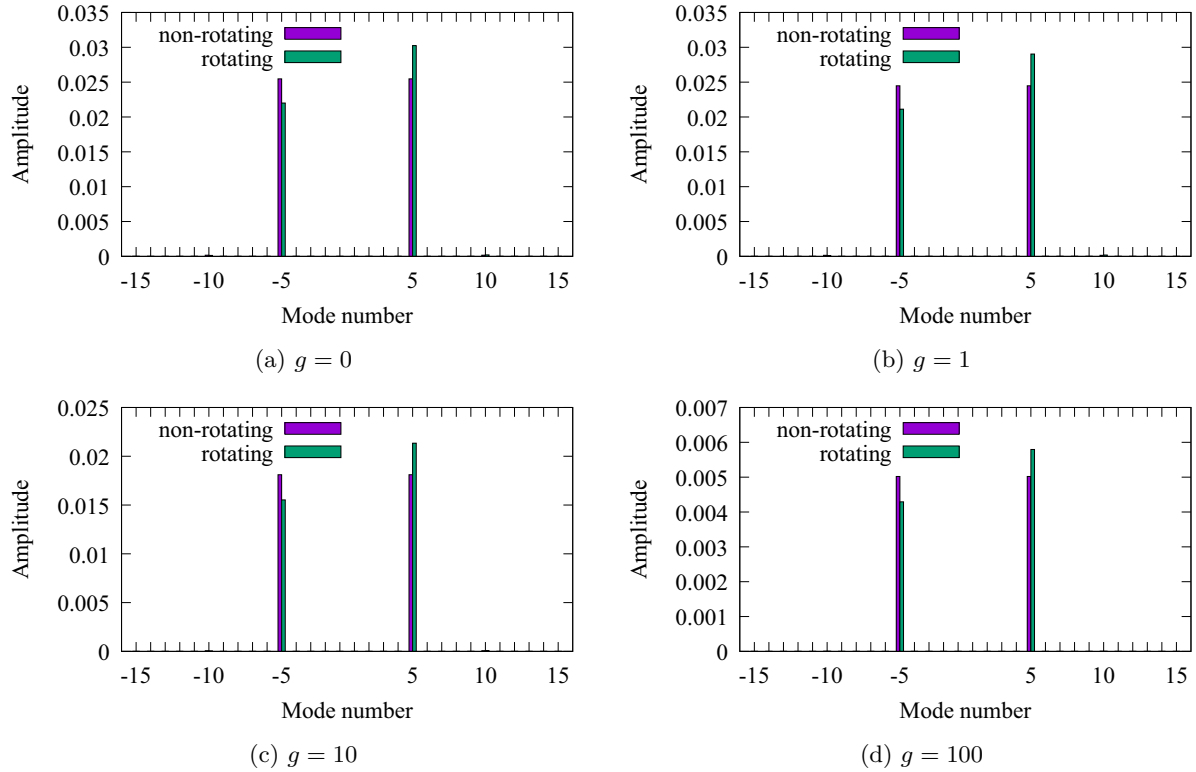


FIG. 3. Mode decomposition of the simulated state following imaginary-time evolution with and without rotation for increasing interaction strength g : (a) $g = 0$, (b) $g = 1$, (c) $g = 10$, and (d) $g = 100$. The mode splitting is clear between the nonrotating and rotating cases. The dominant $l = 0$ mode has been omitted for visual clarity. Note that the amplitude in the nonrotating case is not the mean amplitude for the corresponding rotating case due to coupling between parameters a and Δ in Eqs. (22) and (23). As g is increased, we see a suppression of the imprinted mode.

couples the derivatives with respect to our three main parameters, we use a numerical gradient-descent method to obtain values for a_0 , a , and Δ and compare to the converged ground state obtained by simulating the system in one dimension with imaginary-time evolution. The main result of this comparison is shown in Figs. 2(e)–2(h), where the extracted phase of both the three-mode model and imaginary-time simulations are shown with strong agreement.

V. MEAN-FIELD EXCITATIONS

To investigate the effects of imprinting deeper modulations, we consider the 1D GPE from Eq. (20) to describe mean-field condensate dynamics.

As we increase the interaction parameter $g > 0$, the amplitude of the primary (l) mode Fourier component decreases as the repulsive interactions of the mean-field potential suppress modulations, as shown in Fig. 3.

The ground state for the interacting case is determined by using the GPE Hamiltonian from Eq. (20). This gives an expectation value modified from that in Sec. IV, although it can be numerically minimized in the same way as Eq. (22),

$$\langle \hat{H} \rangle = \frac{1}{a_0^2 + 2a^2 + 2\Delta^2} \left(\frac{\hbar^2 l^2}{2mR^2} (2a^2 + 2\Delta^2) + 4l\Omega a \Delta - 2\alpha a_0 a + g[8a_0^2 a^2 + (a^2 - \Delta^2)^2 a^4] \right). \quad (23)$$

As shown in Fig. 4, the interacting ground-state result provides strong agreement between optimized parameters and those found via imaginary-time evolution in numerical simulations.

An additional feature of Fig. 4 when viewed in comparison to Fig. 2 is the dependence of the density oscillation period on the interaction strength. In Fig. 5 we compare the oscillation periods of simulations with varying interaction strengths and find that in the mean-field approximation the oscillation frequency is dependent on the Bogoliubov mode energy,

$$\epsilon(p) = \sqrt{\left(\frac{p^2}{2m}\right)^2 + \frac{p^2 g n}{m}}, \quad (24)$$

where p is the mode's momentum and n is the atomic density.

A. The Hess-Fairbank effect

The Hess-Fairbank effect describes the formation of a nonrotating superfluid condensate in a container rotating sufficiently slowly [33]. It is in this slowly rotating regime that the three-mode model is obtained exactly, as shown in Fig. 6—higher external rotation rates induce a global circulation in the condensed state, shifting the mode occupation. This corresponds to a global phase factor in the wave function, which does not alter the mode structure of the density nor the evolution of the Fourier phase (except for the expected scaling with rotation rate). This is explored further in Appendix B.

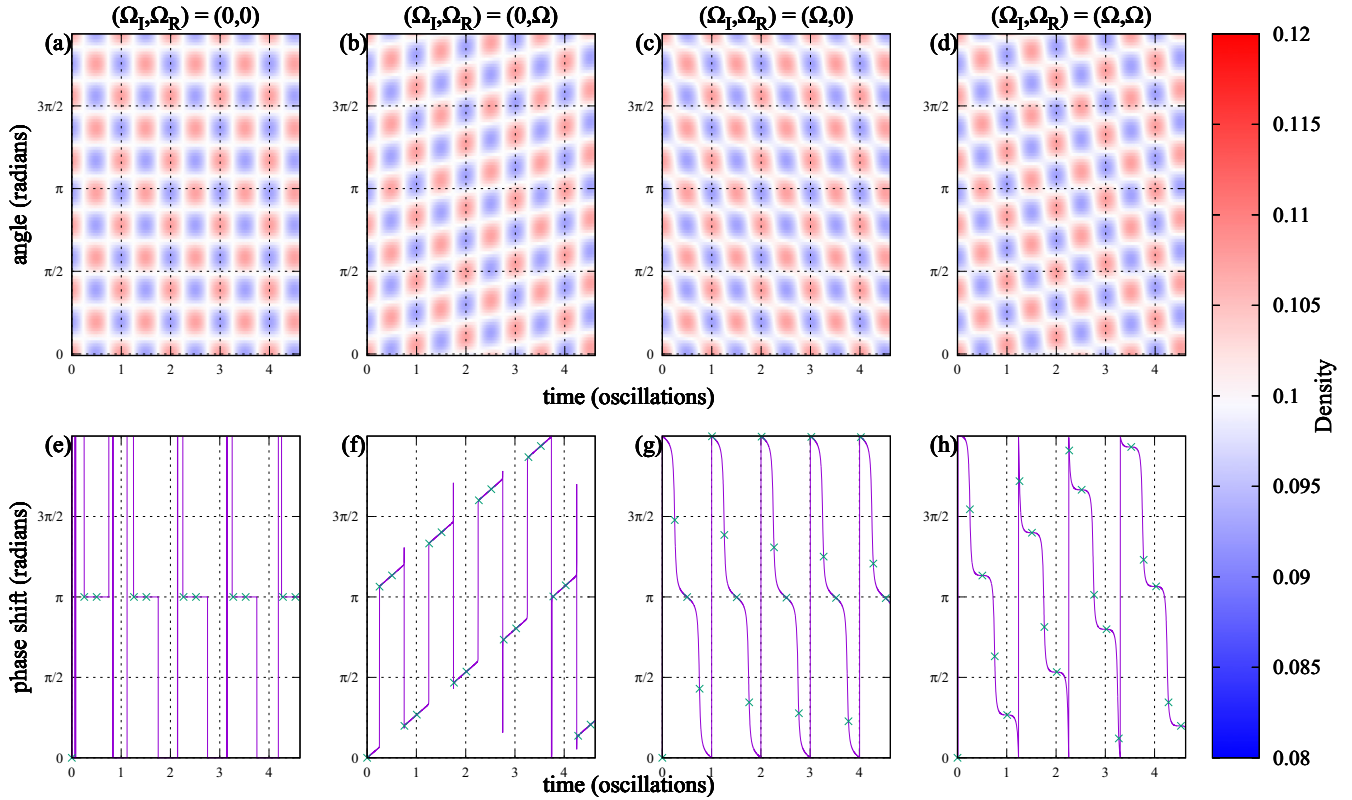


FIG. 4. Same as Fig. 2, but with mean-field interaction strength $g = 10$. Note the lighter color in the density plots in (a)–(d) due to interactions suppressing the imprinted mode amplitudes. The temporal oscillation frequency is also increased due to the extra energy in the system. The Fourier phase evolution of the three-mode model [green crosses in (e)–(h)] agrees with that of the ground state found through imaginary time (purple curve).

A condensate formed in a rotating Sagnac interferometer is not irrotational as described by the Hess-Fairbank effect. In the slowly rotating regime, the rotation of the imprinted density profile indicates flow without global circulation. This is where classical fluid analogies break down, as they cannot describe the superposition state of the condensate. A simple experimental test of the Hess-Fairbank effect in the collective-excitation interferometer can be performed using a rotating imprinting potential to simulate different external

rotation rates as in Fig. 6 without requiring rotation of the entire experimental apparatus.

B. Experimental considerations

The rotating reference frame and mean-field effects described above impact the feasibility of the original interferometric scheme. In a typical inertial sensing application, the time dependence of the phase shift requires stroboscopic

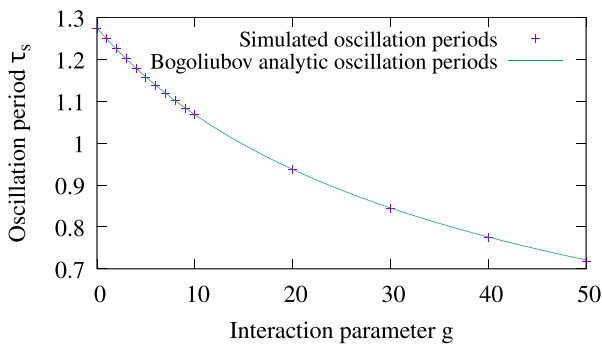


FIG. 5. Dependence of the temporal oscillation period on interaction strength g . Points are the oscillation periods extracted from numerical simulations; the curve corresponds to the analytic Bogoliubov mode energy from Eq. (24). Natural units are set such that $\hbar = m = c = 1$.

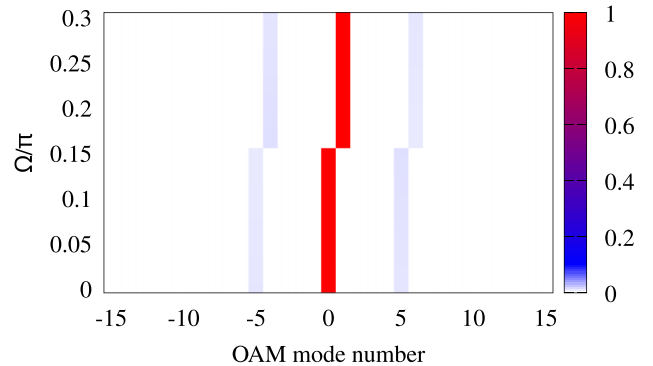


FIG. 6. Heat map of normalized mode amplitudes for quantized angular momentum modes formed under rotation. Imaginary-time evolution of an initial Gaussian state under external rotation at Ω produces the expected three-mode state at low rotation rates and induces a global rotation of the system at higher rates.

measurements to be precisely timed for maximum accuracy. This is complicated by the dependence of the stroboscopic measurement time on the interaction strength, which in an experiment is related to the atom number and cannot be precisely controlled between iterations. Using the Bogoliubov mode energy as a guide to ideal measurement time can mitigate this where interactions are sufficiently weak.

VI. CONCLUSION

In conclusion, the three-mode model with imbalanced mode amplitudes is a frame-independent model for studying the rotation signal in a phonon-mode Sagnac interferometer. We have shown that this model is accurate in describing the one-dimensional behavior of this system and that absolute rotation measurement is possible. The three-mode state is not irrotational per the Hess-Fairbank effect even at low rotation rates, and we have suggested a simple experiment to demonstrate this.

Given the results of this work, the ideal rotation-measurement scheme involves measuring the extracted phase at as close to the first stroboscopic measurement time as possible. We have shown that there are multiple subtleties in the reference frame and interaction effects that must be considered when designing ring-trapped interferometric schemes.

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APPENDIX A: NUMERICAL GROUND-STATE CALCULATION

In order to numerically determine the three-mode model parameters that define the ground state in a rotating ring system, we calculate the expectation value of the Hamiltonian for numerical minimization. The 1D particle-in-a-ring Hamiltonian with imprinting potential is given in a rotating frame by

$$\hat{H} = -\frac{\hbar^2}{2mR^2} \frac{\partial^2}{\partial \theta^2} + [V_0 - \alpha \cos(n\theta)] + i\hbar\Omega \frac{\partial}{\partial \theta}, \quad (\text{A1})$$

where m is the particle mass, R is the ring radius, Ω is the rotation rate, and $V = [1 - \alpha \cos(n\theta)]$ is the imprinting potential with modulation amplitude α . We choose as our ansatz ψ from the three-mode model, with normalization factor $[2\pi(a_0^2 + 2a^2 + 2\Delta^2)]^{-1/2}$. We can then determine the

expectation value of the Hamiltonian $\langle \hat{H} \rangle$:

$$\begin{aligned} \langle \hat{H} \rangle &= \int_0^{2\pi} \psi^* \hat{H} \psi d\theta \\ &= \frac{1}{2\pi(|a_0|^2 + 2|a|^2 + 2|\Delta|^2)} \\ &\quad \times \int_0^{2\pi} [V_0 - \alpha \cos(m\theta)] |a_0|^2 \\ &\quad + \left(\frac{\hbar^2 l^2}{2mR^2} + [V_0 - \alpha \cos(n\theta)] - \hbar l \Omega \right) |a + \Delta|^2 \\ &\quad + \left(\frac{\hbar^2 l^2}{2mR^2} + [V_0 - \alpha \cos(n\theta)] + \hbar l \Omega \right) |a - \Delta|^2 \\ &\quad + \left[\left(\frac{\hbar^2 l^2}{2mR^2} + [V_0 - \alpha \cos(n\theta)] - \hbar l \Omega \right) \right. \\ &\quad \quad \left. \times a_0^*(a + \Delta) e^{il\theta} \right] \\ &\quad + \left[\left(\frac{\hbar^2 l^2}{2mR^2} + [V_0 - \alpha \cos(n\theta)] + \hbar l \Omega \right) \right. \\ &\quad \quad \left. \times a_0^*(a - \Delta) e^{-il\theta} \right] \\ &\quad + [V_0 - \alpha \cos(n\theta)] (a + \Delta)^* a_0 e^{-il\theta} \\ &\quad + [V_0 - \alpha \cos(n\theta)] (a - \Delta)^* a_0 e^{il\theta} \\ &\quad + \left[\left(\frac{\hbar^2 l^2}{2mR^2} + [V_0 - \alpha \cos(n\theta)] - \hbar l \Omega \right) \right. \\ &\quad \quad \left. \times (a - \Delta)^*(a + \Delta) e^{-2il\theta} \right] \\ &\quad + \left[\left(\frac{\hbar^2 l^2}{2mR^2} + [V_0 - \alpha \cos(n\theta)] + \hbar l \Omega \right) \right. \\ &\quad \quad \left. \times (a + \Delta)^*(a - \Delta) e^{-2il\theta} \right] d\theta. \quad (\text{A2}) \end{aligned}$$

This integral is simplified by noting that all terms with a single oscillatory factor integrate to zero, leaving only the nonoscillatory terms and terms with a product of $\cos(n\theta)$ and an exponential. The latter can be calculated as follows.

To determine the contribution of the imprinting potential modulations to the integral in Eq. (A2), we calculate the potential matrix element for generic OAM eigenstates $|k\rangle = \psi_k = (2\pi)^{-1/2} e^{ik\theta}$:

$$\begin{aligned} \langle l | V_m | n \rangle &= \int_0^{2\pi} \psi_l^*(\theta) [V_0 - \alpha \cos(m\theta)] \psi_n(\theta) d\theta \\ &= \int_0^{2\pi} \psi_l^*(\theta) V_0 \psi_n(\theta) d\theta \\ &\quad - \frac{\alpha}{2\pi} \int_0^{2\pi} \psi_l^*(\theta) \cos(m\theta) \psi_n(\theta) d\theta \\ &= V_0 \delta_{l,n} - \frac{\alpha}{2\pi} \int_0^{2\pi} \cos(m\theta) e^{-i(l-n)\theta} d\theta \end{aligned}$$

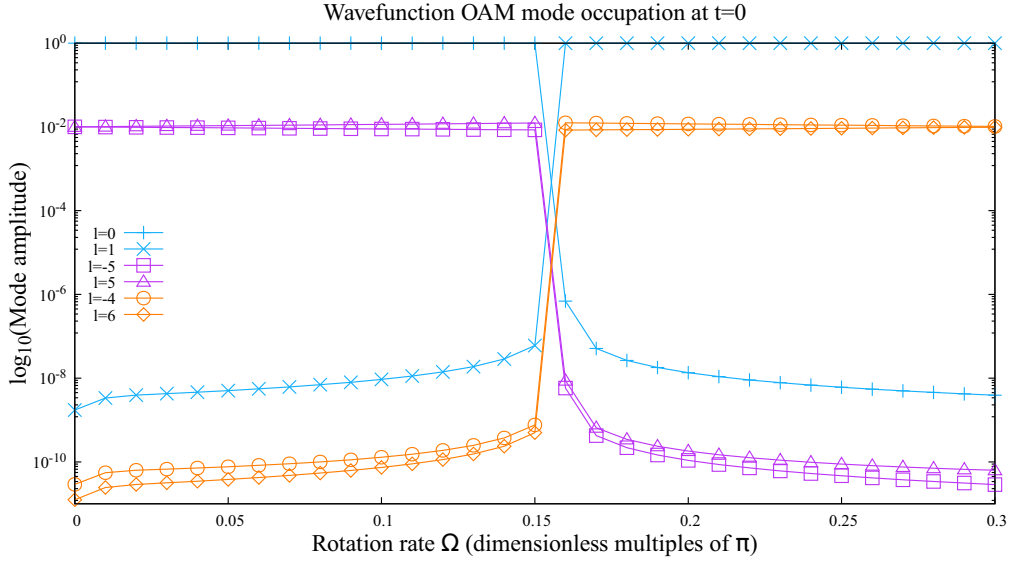


FIG. 7. Occupation of select orbital angular momentum (OAM) modes after condensation into an $l = 5$ imprinting potential for increasing the external rotation rate during condensation. Values below 10^{-6} are equivalent to zero due to a finite convergence threshold.

$$\begin{aligned}
 &= V_0 \delta_{l,n} - \frac{\alpha}{2\pi} \int_0^{2\pi} \frac{1}{2} \{ \cos[(l-n+m)\theta] \\
 &+ \cos[(l-n-m)\theta] \} - \frac{i}{2} \{ \sin[(l-n+m)\theta] \\
 &- \sin[(l-n-m)\theta] \} d\theta. \tag{A3}
 \end{aligned}$$

The integral is nonzero if and only if either $l-n+m=0$ or $l-n-m=0$. In either of these cases, the matrix element reduces to

$$\langle l|V_m|n \rangle = -\frac{\alpha}{2}. \tag{A4}$$

For the three-mode model, there are four such terms, resulting in the $-2\alpha a_0 a$ term in the final expression for the expectation

value of the Hamiltonian:

$$\begin{aligned}
 \langle \hat{H} \rangle &= \frac{1}{a_0^2 + 2a^2 + 2\Delta^2} \\
 &\times \left(\frac{\hbar^2 l^2}{2mR^2} (2a^2 + 2\Delta^2) + 4\hbar l \Omega a \Delta - 2\alpha a_0 a \right). \tag{A5}
 \end{aligned}$$

This process is repeated using the Gross-Pitaevskii equation to obtain the nonlinear expectation value presented in the main text.

APPENDIX B: THE HESS-FAIRBANK EFFECT

First observed in liquid helium [33], the Hess-Fairbank effect describes the formation of a nonrotating superfluid in

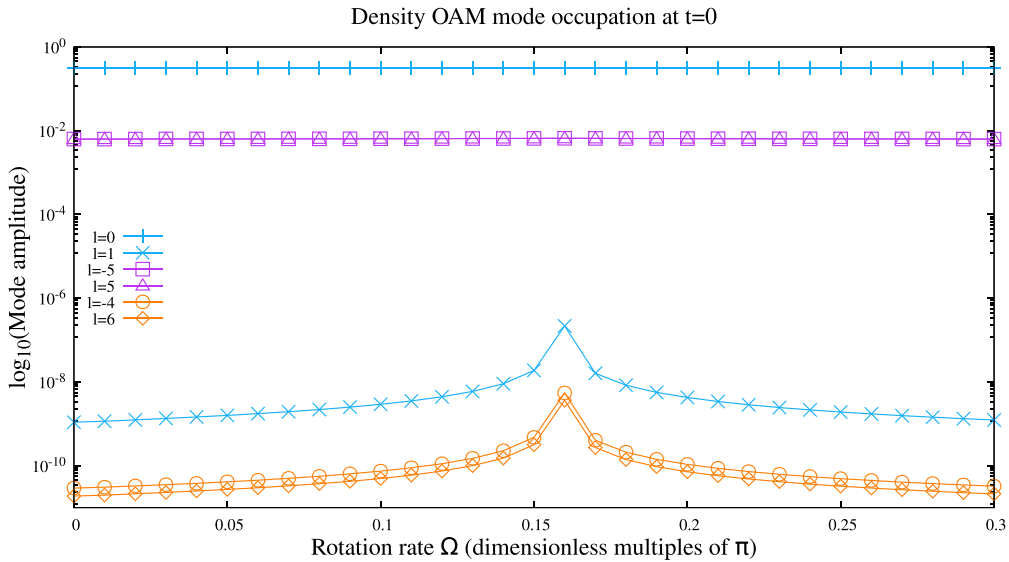


FIG. 8. Amplitudes of select density Fourier modes after condensation into an $l = 5$ imprinting potential for increasing the external rotation rate during condensation. Values below 10^{-6} are equivalent to zero due to a finite convergence threshold.

a container rotating sufficiently slowly during the transition to the superfluid phase. In a simply connected cylindrical container of radius R , rotation proportional to $\frac{n\hbar}{mR^2}$ is sufficient to generate n vortices of quantized circulation. This places an upper limit on the rotation rate of such a container such that the ground state has zero circulation.

In the ring geometry of the phonon-mode interferometer, it is straightforward to calculate the rotation rate at which an energy crossing between two OAM modes (Figs. 7 and 8) occurs for a noninteracting superfluid by equating their eigenenergies:

$$E_l = E_k, \quad (\text{B1})$$

$$\frac{\hbar^2 l^2}{2mR^2} - \hbar l \Omega = \frac{\hbar^2 k^2}{2mR^2} - \hbar k \Omega, \quad (\text{B2})$$

$$\frac{\hbar}{2mR^2}(l^2 - k^2) = \Omega(l - k), \quad (\text{B3})$$

$$\Omega = \frac{\hbar}{mR^2} \frac{l^2 - k^2}{2(l - k)}. \quad (\text{B4})$$

For the l th mode and the mode directly adjacent (in the direction of rotation), the crossing occurs at $\Omega = \frac{\hbar}{mR} \frac{2l+1}{2}$. However, in the three-mode model each mode does not shift to the adjacent mode; instead, there is a patterned shift where

TABLE I. Rotation rates as multiples of $\frac{\hbar}{mR^2}$ that produce energy crossings from OAM mode k to mode l ; determined using Eq. (B4). Bold entries show the mode shifting for the three-mode model studied in the text. Note that the observed shift is not due to adjacent modes coupling for $l = \pm 5$.

$k \backslash l$	-5	-4	-3	-2	-1	0	1	2	3	4	5	6
-5		$-\frac{9}{2}$	-4	$-\frac{7}{2}$	-3	$-\frac{5}{2}$	-2	$-\frac{3}{2}$	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$
-4	$-\frac{9}{2}$		$-\frac{7}{2}$	-3	$-\frac{5}{2}$	-2	$-\frac{3}{2}$	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$	1
-3	-4	$-\frac{7}{2}$		$-\frac{5}{2}$	-2	$-\frac{3}{2}$	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$	1	$\frac{3}{2}$
-2	$-\frac{7}{2}$	-3	$-\frac{5}{2}$		$-\frac{3}{2}$	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$	1	$\frac{3}{2}$	2
-1	-3	$-\frac{5}{2}$	-2	$-\frac{3}{2}$		$-\frac{1}{2}$	0	$\frac{1}{2}$	1	$\frac{3}{2}$	2	$\frac{5}{2}$
0	$-\frac{5}{2}$	-2	$-\frac{3}{2}$	-1	$-\frac{1}{2}$		$\frac{1}{2}$	1	$\frac{3}{2}$	2	$\frac{5}{2}$	3
1	-2	$-\frac{3}{2}$	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$		$\frac{3}{2}$	2	$\frac{5}{2}$	3	$\frac{7}{2}$
2	$-\frac{3}{2}$	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$	1	$\frac{3}{2}$		$\frac{5}{2}$	3	$\frac{7}{2}$	4
3	-1	$-\frac{1}{2}$	0	$\frac{1}{2}$	1	$\frac{3}{2}$	2	$\frac{5}{2}$		$\frac{7}{2}$	4	$\frac{9}{2}$
4	$-\frac{1}{2}$	0	$\frac{1}{2}$	1	$\frac{3}{2}$	2	$\frac{5}{2}$	3	$\frac{7}{2}$		$\frac{9}{2}$	5
5	0	$\frac{1}{2}$	1	$\frac{3}{2}$	2	$\frac{5}{2}$	3	$\frac{7}{2}$	4	$\frac{9}{2}$		$\frac{11}{2}$
6	$\frac{1}{2}$	1	$\frac{3}{2}$	2	$\frac{5}{2}$	3	$\frac{7}{2}$	4	$\frac{9}{2}$	5	$\frac{11}{2}$	

the $\pm l$ th mode shifts to the $\mp(l+1)$ th mode for rotation about the positive z axis [or shifts to the $\mp(l-1)$ th mode for rotation about the negative z axis], as shown in Table I.

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