Meridional composite pulses for low-field magnetic resonance

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We discuss procedures for error-tolerant spin control in environments that permit transient, large-angle reorientation of a magnetic bias field. Short sequences of nonresonant magnetic-field pulses in a laboratory-frame meridional plane are derived. These are shown to have band-pass excitation properties comparable to established amplitude-modulated, resonant pulses used in static, high-field magnetic resonance. Using these meridional pulses, we demonstrate robust *z* inversion in proton (1 H) nuclear magnetic resonance near Earth's field.

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I. INTRODUCTION

Pulsed alternating (ac) electromagnetic fields are a staple of atomic, electronic, and nuclear spin resonance spectroscopies. Following decades of development in these disciplines and others, e.g., magnetic resonance imaging (MRI) [1,2] and quantum information processing (QIP) [3,4], there exist many species of ac pulse for precise qubit control that compensate for errors inevitably present in experimental parameters. Among error-tolerant pulses engineered are those utilizing phase modulation [5–10], amplitude modulation [11–13], or both phase-and-amplitude modulation [14–16] of the ac fields.

These pulse composition strategies are available to traditional spin-resonance experiments, which are performed inside strong magnets (e.g., superconducting magnets) with fixed magnitude and direction of the magnetic field. In this scenario, only ac amplitude and phase degrees of freedom remain for spin control. Other strategies are, in principle, possible, however. At a mathematical level, error-compensated pulse design can be traced to a common set of principles, for instance the Magnus expansion [17], impulse-response theory [18], recursive iteration [19], and other time symmetry considerations. When the strong field constraint is removed, new pulse strategies become available, and existing pulse strategies can be implemented using different degrees of freedom.

In this paper we illustrate the above reutilization concept to derive error-tolerant pulses for magnetic resonance experiments where the orientation of the total magnetic field is unconstrained in the laboratory frame of reference. The case includes Earth's field nuclear magnetic resonance (NMR) [20–22] as well as the emerging area of zero to ultralow-field (ZULF) NMR [23,24], which presents attractive regimes for nuclear spin hyperpolarization [25,26], relaxometry [27,28], and precision spectroscopy [29–31] in fields ranging from nT to μ T. Here, standard ac pulses may achieve

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spin-species and/or transition-selective excitation [32]. Optimal control pulses [33] and direct-current (dc) analogs of ac composite pulses (e.g., $90_x 180_y 90_x$) [28,34,35] can also be used for error compensation.

We observe that composite pulses do not always appear to translate directly from ac (high-field) to dc (low-field) techniques. For instance, in high field, a $90_x 180_y 90_x$ pulse is often a first choice for tolerance to error in Rabi frequency and thus pulse length. However, in a low field, the pulse length tolerance of a dc composite pulse can be achieved using analogs of ac pulses that compensate for the offset in the ac carrier frequency (a different source of error). This concept shall be illustrated for dc composite pulses where fields are confined to a single meridional plane of the Bloch sphere (e.g., *x-z* plane, where *z* defines the bias axis). We call such pulses *meridional composite pulses* and show that they are considerably more selective than traditional composite pulses, including $90_x 180_y 90_x$ where the magnetic field is kept in the equatorial plane of the Bloch sphere (*x-y* plane).

II. THEORY

In any NMR scenario, the magnetic field $\mathbf{\tilde{B}}(t)$ is used to produce controlled rotations of a spin $\mathbf{\tilde{S}}$, governed by the Bloch equation

$$\frac{d}{dt}\vec{\mathbf{S}} = \gamma \vec{\mathbf{S}} \times \vec{\mathbf{B}}.$$
 (1)

In a high-field NMR scenario, a strong constant field along the z direction with magnitude B_0 is applied and a weaker orthogonal field $B_x(t)$ is temporally shaped to produce pulses of oscillating field near the Larmor frequency $\omega_L = \gamma B_0$, with a determined detuning, duration, and phase. Via the Bloch equation, such a pulse produces a spin rotation $R(\psi, \vec{n})$, where the spin rotation angle ψ is proportional to the strength and duration of the pulse and the (rotating frame) rotation axis \vec{n} is determined by the phase and frequency of the pulse.

In low-field NMR, it is possible to directly implement a rotation $R(\psi, \vec{n})$ about a (laboratory frame) axis \vec{n} , by applying a dc field of strength *B* along \vec{n} for a time τ to generate rotation

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by an angle $\psi = \gamma B \tau$. Rotations with arbitrary $\mathbf{\vec{n}}$ and ψ can, in principle, be produced with three-axis control of $\mathbf{\vec{B}}(t)$. In this way, any simple rotation $R(\psi, \mathbf{\vec{n}})$ used in high-field NMR can be implemented also in low-field NMR.

Composite pulses are not simple pulses, but rather trains of simple pulses that together implement a desired rotation. Unlike simple pulses, these can be designed to perform nearly the same rotation for a range of parameter values, e.g., γ or B_0 , so these rotations become robust against experimental imperfections. They can also be used to apply different rotations to different γ values and thus implement speciesspecific rotations. Composite pulses do not translate directly from high-field to low-field techniques because parameter variations affect the rotation in different ways. For example, in a resonant rotation, \vec{n} depends on the detuning and thus on γ , whereas for a dc rotation it is ψ that depends on γ .

As a starting point for meridional composite pulse design we use the theorem that successive rotation of a spin (and more generally, any three-dimensional object) by π radians about an arbitrary pair of unit vectors \vec{n}' and \vec{n}'' is equivalent to a single rotation by an angle ϕ about the perpendicular unit vector \vec{n} parallel to $\vec{n}' \times \vec{n}''$, where $\phi/2$ is the angle between \vec{n}' and \vec{n}'' , i.e. $\vec{n}' \cdot \vec{n}'' = |\vec{n}'| |\vec{n}''| \cos(\phi/2)$:

$$R(\pi, \vec{\mathbf{n}}'')R(\pi, \vec{\mathbf{n}}') = R(\phi, \vec{\mathbf{n}}).$$
⁽²⁾

By extension, an equation follows for the cumulative effect of 2*N* rotations-by- π about axes $\vec{n}'_1, \vec{n}''_1, \vec{n}'_2, \vec{n}''_2, \dots, \vec{n}'_N, \vec{n}''_N$ in a common plane normal to \vec{n} :

$$\prod_{j=1}^{N} R(\pi, \vec{\mathbf{n}}_{j}'') R(\pi, \vec{\mathbf{n}}_{j}') \equiv R\left(\sum_{j=1}^{N} \phi_{j}, \vec{\mathbf{n}}\right).$$
(3)

For instance, if all of the $\mathbf{\vec{n}}'$ and $\mathbf{\vec{n}}''$ vectors lie within the Cartesian *x*-*z* plane as defined by vectors $\mathbf{\vec{x}} = (1, 0, 0)$ and $\mathbf{\vec{z}} = (0, 0, 1)$, then the overall rotation is produced about the *y* axis, defined $\mathbf{\vec{y}} = (0, 1, 0)$; $\mathbf{\vec{n}} = \mathbf{\vec{y}}$. A graphical representation of Eq. (2) is shown in Fig. 1.

The problem of interest for robust, spin-selective pulse generation is the approximate implementation of Eq. (3), where a sequence of 2*N* rotations by $\kappa \pi$ is applied about axes $\vec{n}'_1, \vec{n}''_1, \ldots, \vec{n}'_N, \vec{n}''_N$. If, as above, the angle between \vec{n}'_i and \vec{n}''_i is $\phi_i/2$, the objective is to find a sequence of angles $\phi_1, \phi_2, \ldots, \phi_N$ such that the resulting rotation is

$$\tilde{R}(\kappa) \equiv \prod_{j=1}^{N} R(\kappa \pi, \vec{\mathbf{n}}_{j}^{\prime\prime}) R(\kappa \pi, \vec{\mathbf{n}}_{j}^{\prime}) \approx R(\beta, \vec{\mathbf{n}})$$
(4)

for some detuned range of κ (and therefore gyromagnetic ratio $\gamma \propto \kappa$), say ($\kappa \mod 2$) = $(1 + \delta)$, where δ is the detuning. Here β is the target rotation angle.

One route to a solution is to recognize that for $\kappa = (1 + \delta)$ one can cast Eq. (4) (see Appendix) into a form

$$\tilde{R}(\kappa) = \prod_{j=1}^{N} R\left(\frac{\phi_j}{2}, \vec{\mathbf{y}}\right) R(\pi[1+\delta], \vec{\mathbf{z}}) R\left(-\frac{\phi_j}{2}, \vec{\mathbf{y}}\right)$$
$$\times R(\pi[1+\delta], \vec{\mathbf{z}})$$
$$= R_z^{2N} \prod_{j=1}^{N} \left[\hat{R}_z^{2j}(\delta) R\left(\frac{\phi_j}{2}, \vec{\mathbf{y}}\right)\right] \left[\hat{R}_z^{2j-1}(\delta) R(-\frac{\phi_j}{2}, \vec{\mathbf{y}})\right], \quad (5)$$



FIG. 1. Some graphical examples of Eq. (2) for $\phi = 90^{\circ}$ (top row) and $\phi = 180^{\circ}$ (bottom row). The solid red curves show the trajectory undertaken by a particle starting at the point $\vec{z} = (0, 0, 1)$, following successive 180° rotations about the pair of axes \vec{n}' and \vec{n}'' , as indicated by the purple arrows, which subtend an angle $\phi/2$ and lie within the *x*-*z* plane.

where $\hat{R}^{d}_{\tau}(\delta)$ is the *d*th power of the right-acting superoperator $\hat{R}_{z}(\delta)$, which rotates operators $R(\phi, \vec{\mathbf{n}})$ by an angle $\pi(1+\delta)$ about **z**, as defined by $\hat{R}_z(\delta)R(\phi, \vec{\mathbf{n}}) \equiv R(-\pi[1+\delta)R(\phi, \vec{\mathbf{n}}))$ δ], $\mathbf{\vec{z}}$) $R(\phi, \mathbf{\vec{n}})R(\pi[1+\delta], \mathbf{\vec{z}})$ [36]. The form of Eq. (5) indicates that, relative to the ideal transformation ($\kappa = 1$), the error δ has the effect of shifting the spins' frame of reference by an offset 2δ about \vec{z} between each ϕ_i rotation. In this way, the problem of finding a suitable set of ϕ_i s is mapped onto another problem that of compensating for frame offset. Frame-offset compensation is a well-explored topic in physics and is of high importance in NMR, MRI, and QIP. One representative strategy uses broadband uniform-rotation pure-phase (BURP [13]) pulses, as first developed by Geen and Freeman [14]. A BURP pulse is an amplitude-modulated ac pulse of duration τ_p , with the carrier resonant with the nominal Larmor frequency. The carrier envelope is chosen such that for detuning $\delta = 0$, the (rotating frame) rotation is $R(\beta(t), \mathbf{y})$, where for $0 \leq t \leq \tau_p$ the accrued flip angle is

$$\beta(t) = a_0 \frac{t}{\tau_p} + b_0 + \sum_{k=1}^{n_{\text{cut}}} \left[a_k \sin\left(\frac{2\pi kt}{\tau_p}\right) + b_k \cos\left(\frac{2\pi kt}{\tau_p}\right) \right].$$
(6)

This is a truncated Fourier series and a cutoff of $n_{\text{cut}} \sim 6$ typically gives sufficient precision [13,14]; numerical values for a_k and b_k are given in the Supplemental Material [37]. BURP pulses generously tolerate mismatch between the carrier and Larmor precession frequencies, with an excitation pass-band inversely proportional to the BURP pulse length.

Using dc pulse pairs as described in Eq. (3), we can make a pointwise approximation of $\beta(t)$: We define intermediate

TABLE I.	Composi	ite pul	lses f	or t	he in	version	operati	ion z	\rightarrow	−z . Al	l ang	les ¢	b_j a	are g	iven	in c	legrees
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				angles	ngles (degree)					Stopband	Passband	Reference		
Ν	ϕ_1	ϕ_2	ϕ_3	ϕ_4	ϕ_5	ϕ_6	ϕ_7	ϕ_8	ϕ_9	$[\tilde{R}_{zz}(\kappa) > 0.99]$	$[\tilde{R}_{zz}(\kappa) < -0.95]$			
2	60	-240								$ \kappa < 0.20$	$0.83 < \kappa < 1.17$	This work		
3	59	-298	59							$ \kappa < 0.36$	$0.93 < \kappa < 1.07$	Shaka <i>et al.</i> [12]		
3	24	-97	253							$ \kappa < 0.24$	$0.75 < \kappa < 1.25$	This work		
4	-34	123	-198	289						$ \kappa < 0.29$	$0.86 < \kappa < 1.14$	Shaka [11], Yang et al. [39]		
4	27	-81	263	-30						$ \kappa < 0.29$	$0.75 < \kappa < 1.25$	This work		
5	325	-263	56	-263	325					$ \kappa < 0.41$	$0.95 < \kappa < 1.05$	Shaka <i>et al.</i> [12]		
9	70	-238	-355	296	276	296	-355	-238	70	$ \kappa < 0.55$	$0.89 < \kappa < 1.11$	This work		

rotation angles

$$\phi_j = \beta \left(\frac{\tau_p j}{N}\right) - \beta \left(\frac{\tau_p (j-1)}{N}\right),\tag{7}$$

and then construct a sequence of nominally π rotations

$$\tilde{R}(\kappa) \equiv \prod_{j=1}^{N} R(\kappa \pi, \vec{\mathbf{n}}_{j}'') R(\kappa \pi, \vec{\mathbf{n}}_{j}'), \qquad (8)$$

with $\vec{\mathbf{n}}'_j = [+\sin(\phi_j/4), 0, \cos(\phi_j/4)]$ and $\vec{\mathbf{n}}''_j = [-\sin(\phi_j/4), 0, \cos(\phi_j/4)]$. This defines a *meridional composite pulse*, i.e., a series of $\kappa\pi$ rotations about pairs of axes in the *x*-*z* plane, separated by angles $\phi_j/2$ [38]. Values of ϕ_j from N = 10 up to N = 40 are tabulated in the Supplemental Material [37].

The performance of the discretized BURP pulses can be analyzed by numerical simulation. As a first example, we study the inversion pulse I-BURP-1 [13], as shown in Fig. 2. Continuous and pointwise $\beta(t)$ values agree closely with one another for $N \ge n_{\text{max}}$. For instance, for N > 10, the fractional difference between $\beta(t)$ and the connecting line between sampling points $\beta(j\tau_p/N)$ is below 0.05 for all time points.

We quantify the inversion by $\tilde{R}_{zz}(\kappa) \equiv \vec{z}^T \tilde{R}(\kappa)\vec{z}$, where $\tilde{R}(\kappa)$ is the matrix representation of the net rotation operator $\tilde{R}(\kappa)$. A value $\tilde{R}_{zz}(\kappa) = -1$ implies complete spin inversion, while $\tilde{R}_{zz}(\kappa) = +1$ indicates zero net rotation of the spin away from \vec{z} . From plots on the right side of Fig. 2, $\tilde{R}_{zz}(\kappa)$ shows an inversion passband of full width at half-maximum $2\delta \approx 5/N$, which for moderate values $N \sim 20$ should be wide enough to provide generous error tolerance, e.g., $2\delta \sim 0.25$, while being selective in γ .

DC field pulses are typically produced by field coils, with each coil contributing the field component along one Cartesian axis. To implement the pulse sequence of Eq. (5), for example, X (field along \vec{x}) and Z (field along \vec{z}) coils could be used. We now analyze the effect of a miscalibration of the Z coil by a factor of s, so that the produced field is

$$\mathbf{B} = B_0(\sin\varphi, 0, s\cos\varphi),\tag{9}$$

where B_0 is the intended field strength and φ is the intended angle in the *x*-*z* plane. For $s \approx 1$, the effect on the rotation angle, i.e., on δ , is first order in s - 1, and the effect on $\vec{\mathbf{n}}$ is a nonsimple function of φ and ϕ . For symmetric displacement of $\vec{\mathbf{n}}'$ and $\vec{\mathbf{n}}''$ about $\vec{\mathbf{z}}$ (and thus $\vec{\mathbf{n}}'_j + \vec{\mathbf{n}}''_j$ parallel to $\vec{\mathbf{z}}$, when $\varphi = \pm \phi/2$) the excitation profile remains mostly unchanged with respect to *s* and the passband center shifts to $\kappa \approx (1 + s)/2$. Representative profiles for the I-BURP-1 pulse are shown in Fig. 2.

Another result of this approach is dc analogs of wideoffset-tolerant ac composite pulses. These pulses in highfield NMR are often termed "phase-alternating composite pulses" [11,12,39–41] due to the alternating sign of flip angle in the ac frame, e.g., $(\beta_1, \beta_2, \beta_3) = (59^\circ, -298^\circ, 59^\circ)$ [12]. These angles can be directly mapped to a meridional composite pulse using $\phi_j = \beta_j$ and using the same paradigm of dc pulse pairs to generate the required flip angles.

Selected phase-alternating composite pulses for inversion and the widths of their passbands are listed in Table I. Highly uniform inversion can be achieved using only a few pulses (N < 10), with a degree of selectivity comparable to, if not better than, I-BURP-1. We note that the passband widths vary between the works of different authors because of different optimization criteria. Uniform excitation within the passband is often given the highest priority, followed by rejection in the stopband. Because in some low-field NMR applications both figures of merit may have equal priority, the present work includes some additional solutions. The original sequences we report in Table I are found in a few minutes with a standard desktop computer, by randomly sampling \sim 50 000 points in a N-1-dimensional space of ϕ values $\phi_1, \phi_2, \ldots, \phi_{N-1}$, with resolution $0.02 \times \pi$ rad. The final angle is constrained to be $\phi_N = \pi - \sum_{j=1}^{N-1} \phi_j$, so that $\beta = \pi$. Our merit function is $l_1 + l_2$, where l_1 is the mean value of $[1 + \tilde{R}_{zz}(\kappa)]^2$ over the range $0.8 < \kappa < 1$ and l_2 is the mean of $[1 - \tilde{R}_{zz}(\kappa)]^2$ for $|\kappa| < 0.5$. Angle sets up to length N = 9 giving widest passband and stopband widths are presented in Table I. Generally, we observe these sequences can have a wider passband than the existing phase-alternating composite pulses of the same length N. An increased width of the stopband is more challenging and requires higher N. The performance of these pulses is illustrated in Fig. 3; in addition, the Supplemental Material [42] provides a set of animations to help visualize the spin vector trajectories undertaken during the pulses.

III. EXPERIMENTAL RESULTS

The band-pass profiles of meridional composite pulses such as those shown in Figs. 2 and 3 can be measured using a sample containing only a single spin species, e.g., ¹H in water (¹H₂O). We note that the rotation axes $\mathbf{\vec{n}}'$ and $\mathbf{\vec{n}}''$ are independent of γ , while κ is directly proportional to γ and



FIG. 2. Band-pass spin inversion using dc pulses derived from I-BURP-1 [13]. The left column shows time profiles of flip angle accumulated in the *x*-*z* plane for the conventional (β , black) and discretized (ϕ_j , red) pulses with N = 1, 2, 4, 10, 20, 40. The plots to the right show *z* inversion performance $\tilde{R}_{zz}(\kappa)$ for the discretized pulse, using scaling factors s = 1 (red), s = 0.9 (gray), s = 1.1 (light gray) as defined in Eq. (9). The dashed vertical lines show values of $\kappa(S)/\kappa(^1\text{H}) \equiv \gamma_S/\gamma_H$, for the case $\kappa(^1\text{H}) = 1$.

the pulse duration. Thus the effects of a change in γ can be simulated by a corresponding change in the pulse duration.

The experimental setup and testing protocol are shown in Fig. 4(a). Water, prepolarized along *z*, flows through a cell surrounded by two coils (*X* and *Z*) that produce uniform fields along \vec{x} and \vec{z} , respectively. Bipolar current control of the *X* coil is provided by a simple electronic circuit comprising a digital-to-analog converter, amplifier and H-bridge module. A constant current is passed through the *Z* coil, as in Fig. 4(b) (right). In this arrangement [unlike what is suggested



FIG. 3. Spin vector trajectories in the Bloch sphere and bandpass inversion profiles for selected composite pulses listed in Table I. The black, blue, and red trajectories are for values $\kappa = 0.25$, $\kappa = 0.85$, and $\kappa = 1.0$. Rotation axes indicated by purple arrows are displaced symmetrically about \vec{z} in the *x*-*z* plane. The solid red curve indicates the band-pass profile $\vec{z} \rightarrow -\vec{z}$ for s = 1; dashed and dotted gray curves correspond to profiles for s = 0.9 and s = 1.1, respectively.

by Eq. (9)], the field strength B_0 depends on the angle φ . The pulse duration τ is compensated accordingly, so that the nominal rotation angle $\psi = \gamma B_0 \tau$ is always π . Further details are given in the Sec. V.

The performance of the spin-selective inversion pulses is measured by applying a composite pulse, then immediately applying a dc pulse of flip angle 90 ° along $+\vec{\mathbf{x}}$. The peak field of the composite pulse is controlled such that I-BURP-1 pulse lengths are of comparable length for different $N: (\tau_p/\kappa) \sim$ 8 ms for ¹H. An alkali-metal-vapor magnetometer [27] adjacent to the flow cell detects the resulting ¹H free precession signal (FID).

The observed FID amplitude for composite pulses of duration $\kappa \tau_p$ is denoted S_{κ} , and the FID amplitude with no applied composite pulse is S_0 . The ratio S_{κ}/S_0 equals $\tilde{R}_{zz}(\kappa)$, which takes values between -1 (for complete spin inversion) and +1(for no spin inversion) and is plotted up to $\kappa = 4$ for various pulses in Fig. 5.

The experimental and simulated profiles agree closely, with residuals below the experimental error margins. This result confirms that spin selective pulses can indeed be designed



FIG. 4. The experimental setup to test dc meridional composite pulses. (a) NMR detection apparatus and electrical circuit used to supply variable current to X and Z field coils. Typical field switching and settling times are $< 2 \,\mu$ s. M = alkali-atom vapor magnetometer used to detect NMR signals. F = Flow cell containing spin-polarized water, MCU = Microcontroller Unit. TTL = 3.3 V transistortransistor logic signal. (b) Time profile of dc field amplitude for the N = 4 sequence $(\phi_1, \phi_2, \phi_3, \phi_4) = (27^\circ, -81^\circ, 263^\circ, -30^\circ)$, where magnetic fields are applied in the *x*-*z* plane. Two possible implementations are shown. On the left, total field amplitude B_0 and pulse duration are kept constant during each pulse section, while on the right, the pulse lengths and amplitudes are scaled for constant B_z .

using the approach of Eq. (3). It also suggests that any imperfections in the pulses are small compared to the compensation limits, which is remarkable considering the simplicity of the electronic drive circuitry.

IV. DISCUSSION AND CONCLUSION

It is shown theoretically and confirmed by experiment that efficient, robust, and spin-selective composite pulses can be composed using switched dc fields in a meridional plane. Also identified is an equivalence between the problems of flip-angle tolerance in low-field NMR and the well-studied problem of frame rotation tolerance in high-field NMR.

In contrast to high-field NMR, where phase or frequency offsets and flip-angle offsets originate in distinct imperfections of the experimental system and have different effects on the generated spin rotations, in low-field NMR flip angle and axis are both determined by the dc field strengths. As shown, this allows a single composite pulse strategy to be robust against variations of each, something that is uncommon in high-field composite pulses.

Also, unlike many high-field NMR composite pulses, the criterion determining total flip angle of a meridional composite pulse [Eq. (3)] is not limited to special angles (e.g., 90°,

180°) and thus should allow one to obtain pulses of arbitrary flip angle. This general design approach, coupled with the above error compensation properties, should prove valuable in spin resonance applications at low field that require robust and selective control. The pulses demonstrated here are much shorter in duration than high-frequency ac pulses of equivalent compensation bandwidth, such as swept-frequency adiabatic inversion pulses [43], and can be performed without tuned high-frequency circuitry [44]. Application is expected in sub-MHz NMR spectroscopy and MRI, field-cycling relaxation measurements, nuclear spin polarimetry, as well as portable NMR spectrometers for use outside of the research laboratory.

The pulse durations τ_p in the present study are limited by hardware timer resolution (2µs) and the field-to-current ratio of the X coil. Faster clock speeds and stronger fields, subject to the electrical inductance of the coils, could shorten pulse lengths by at least one order of magnitude, giving τ_p between 10 µs and 100 µs. These durations are much shorter than the periods of the spin-spin scalar couplings between common nuclear spin species and thus should be applicable to heteronuclear quantum control in low-field NMR in which pulses selectively rotate one or more spins in a multispecies system. The selectivity and error tolerance should be complementary to existing control methods based on equatorial composite pulses [28,45].

V. METHODS

Experimental testing of the composite pulses utilized a continuous-flow (a.k.a. "polarization on tap") test sample for the high-throughput measurement. As shown in Fig. 4(a), distilled water from a reservoir of several liters' capacity drained continuously under gravity (flow rate $\sim 1 \text{ mLs}^{-1}$) through a low-homogeneity 1.5 T magnet [46] allowing the ¹H spins to reach thermal equilibrium polarization. The liquid subsequently flowed into the $\sim 1 \text{ mL}$ sample chamber, with the sample magnetization of around 1 pT being aligned parallel to the axis of the background field, along \vec{z} .

Centered on the sample chamber was a solenoid coil (~7.5 mT/A) and a saddle coil (~80 μ T/A) to produce magnetic fields along \vec{z} and \vec{x} , respectively. Currents applied to the saddle coil were controlled using a simple dc switch comprising a microcontroller (ARM Cortex M4F) digital-to-analog converter (DAC) (12 bits, 0 to 3.3 V), operational amplifier (L272M, STMicroelectronics), and an H-bridge module (Texas Instruments DRV8838 on Pololu 2990 carrier board), as shown in Fig. 4(a). Rabi curves were measured for different values of the DAC output to confirm a linear output of voltage across the coils between 0.4 and 10 V (see Supplemental Material [37]). This determined the switchable range of field for a given series resistance of the coil. The 10 V and ground op-amp rails were connected to a standard laboratory power supply unit (Hameg HM7042-5).

Details of the magnetometer used to measure the NMR signals can be found in previous work [27]. The signals S_{κ} and S_0 of the two pulse sequences are acquired in an interleaved fashion to minimize the effect of drifts.

The raw data generated in this study have been deposited in the OpenAIRE database [47].



FIG. 5. The experimental (black circles) versus simulated (solid red curves) band-pass inversion profiles for meridional composite pulses with N = 2, 3, 4 listed as "this work" in Table I and for discrete I-BURP-1 pulses with N = 10, 12, 14, 16, 18, 20 and 40. Each data point represents the mean signal amplitude of approximately 10 NMR transients.

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APPENDIX: DERIVATION OF EQ. (5)

Starting from Eq. (4), we choose rotation axes $\vec{\mathbf{n}}_j' = \vec{\mathbf{z}}$ and $\vec{\mathbf{n}}_j'' = (\sin[\phi_j/2], 0, \cos[\phi_j/2])$ that subtend the angle $\phi_j/2$

and then use the Euler *YZY* convention to rewrite the product in terms of rotations about the Cartesian \vec{z} and \vec{y} axes:

$$\tilde{R}(\beta, \vec{\mathbf{n}}) = \prod_{j=1}^{N} \left[R\left(\frac{\phi_j}{2}, \vec{\mathbf{y}}\right) R(\pi[1+\delta], \vec{\mathbf{z}}) R\left(-\frac{\phi_j}{2}, \vec{\mathbf{y}}\right) \times R(\pi[1+\delta], \vec{\mathbf{z}}) \right].$$
(A1)

Then by using $y_j \equiv R(\phi_j/2, \vec{y})$, $z \equiv R(\pi[1 + \delta], \vec{z})$, and an overbar to denote opposite sign of ϕ , the product in Eq. (A1) can be written in a shorthand notation

$$\tilde{R}(\beta, \vec{\mathbf{n}}) = \prod_{j=1}^{N} (y_j z \overline{y}_j) z \equiv y_N z \overline{y}_N \dots z y_2 z \overline{y}_2 z y_1 z \overline{y}_1 z.$$
(A2)

The next step is to insert the identity operation $1 \equiv z^j z^{-j}$ in between every zy or $z\overline{y}$ product to obtain products of the form $z^{-j}yz^j$. The right side of Eq. (A2) then equals

$$z^{2N}(z^{-2N}y_Nz^{2N})(z^{1-2N}\overline{y}_Nz^{2N-1})\dots(z^{-2}y_1z^2)(z^{-1}\overline{y}_1z),$$
 (A3)

and therefore also equals the right side of Eq. (5) when writing it back in long form, using $z^{-i}y_jz^i = \hat{R}_z^i R(\phi_j/2, \vec{y}), z^{-i}\overline{y}_jz^i = \hat{R}_z^i R(-\phi_j/2, \vec{y})$, and so on.

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