


Generic optical singularities in Brewster-reflected postparaxial beam fields

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Brewster reflection of a postparaxial optical beam at a plane dielectric interface unravels fundamentally significant optical singularity dynamics. We express the simulated field-component profiles of a Brewster-reflected postparaxial beam field via empirical functions, using which we demonstrate optical beam-shifts and formation of phase singularities. These occurrences naturally reveal the presence and complex transitional dynamics of generic polarization singularities, which we observe via simulation and experiments. A single reflection being the core process, our method becomes a fundamentally appealing way to generate optical singularities and to study their dynamics.

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I. INTRODUCTION

The strong influence of the optical fields carrying well-defined phase and polarization singularities has revolutionized the fundamental studies and applications of the wave fields and their interactions with matter [1–20]. In addition to their significant contribution towards the fundamental understanding of the electromagnetic characteristics of light, optical singularities provide core concepts in many emerging areas of research, including Majorana and Poincarana sphere formalisms [21–23], topological and non-Hermitian photonics [24–30], optical Möbius strips [31–35], polarization knots [36–39], and superoscillations [40–43]. They are also directly related to several interdisciplinary research areas, including crystal dislocation, trapping and rotation of microparticles, classical and quantum communications, microscopy and imaging, etc. [1,44].

Generic optical singularities are broadly classified into two fundamentally related but distinctly characterized categories [1]: (1) phase singularity and (2) polarization singularity. Generic phase singularities are points (in two dimensions) or lines (in three dimensions) in space where both real and imaginary parts of a complex field become zero, thus making the phase of the field undefined [1–8]. Polarization singularities are regions where specific properties of the polarization ellipse are undefined: orientation (for *C*-point), handedness (for *L*-line), and both orientation and handedness (for *V*-point) [1,6,7,9–19]. The polarization ellipses around these singularities organize themselves into unique patterns such as lemon, star, monstar, node, center, saddle, etc. (topological indices, respectively, $+1/2$, $-1/2$, $-1/2$, $+1$, $+1$, -1) [1,6,7,9–19]. Standard methods of generating vortex beams with embedded polarization singularities [1,17,45–54] thus involve, in some form or the other, the inherent inhomogeneous polarization of the considered beam field [55–61].

A classic case of inhomogeneous polarization in the beam cross section occurs for the reflection and transmission of a composite optical wave, where the constituent plane waves reflect and transmit differently due to differences in Fresnel coefficients [62–64], thus generating complicated reflected and transmitted field profiles [55–60,65–72]. This effect is especially unique when a constituent wave with transverse magnetic (TM) polarization is incident at Brewster angle (θ_B) [62–64], because this constituent wave is not reflected at all. Thus, a point of zero TM reflection is created in an otherwise nonzero reflected field profile, indicating the existence of a phase singularity at that zero point. Also, the strongly inhomogeneous polarization around that zero point indicates the existence of polarization singularities.

The presence of phase singularity in a nonparaxial Brewster-reflected beam field was recently observed by Barczyk *et al.* [45]. However, they observed it in a specific experiment and in a complex setup, thus, not explicitly identifying this phase singularity as a generic occurrence irrespective of the used setup. On the other hand, in Ref. [73] we have reported some initial simulation-based observations of polarization singularities in a Brewster-reflected paraxial beam field. But to our knowledge, a detailed analysis of the polarization singularities and their complex transitional dynamics, appearing in a Brewster-reflected beam field, is not currently present in literature.

We address the above-mentioned unexplored and fundamental electromagnetic-optical problems in the present work. We first simulate a Brewster-reflected postparaxial optical beam field. We then express this complete field in terms of empirical functions and use them to demonstrate the occurrences of beam shifts and phase singularities. Then we use the calculated information to perform a detailed analysis of the polarization singularities and their various complex transitional dynamics in the beam field. In particular, we demonstrate effects such as merger of two *C*-point singularities into a higher-order *V*-point singularity [1,14], pair disappearance of singularities at infinity, and isolation of a *C*-point singularity for off-Brewster-angle reflection. Finally, we

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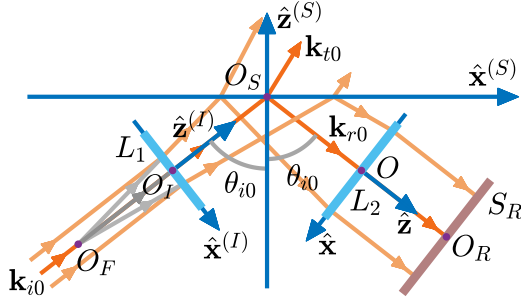


FIG. 1. Schematic of the simulated optical system (description in the text).

verify our analytical and simulated results via experimental observations.

II. THE OPTICAL SYSTEM

To explore Brewster-reflected beam-field profiles, we have simulated an optical system (Fig. 1) based on our formalism developed in Ref. [60]. In a medium of refractive index n_1 , an initial collimated Gaussian beam is converted to a weakly diverging postparaxial Gaussian beam by passing it through a concave lens L_1 of focal length $\mathcal{F}_1 = -O_F O_I$. This beam is incident on an isotropic dielectric interface of refractive index n_2 . The central angle of incidence is θ_{i0} . The reflected beam cross-sectional profile is observed at the screen S_R after collimating it through a convex lens L_2 of focal length $\mathcal{F}_2 = O_F O_I + O_I O_S + O_S O$. By setting $\theta_{i0} = \theta_B$, the Brewster-reflected beam profile is observed.

III. ANALYSIS

We define global incident and reflected beam coordinate systems $I(x^{(I)}, y^{(I)}, z^{(I)})$ and $R(x, y, z)$ with respect to the central incident and reflected wave vectors \mathbf{k}_{i0} and \mathbf{k}_{r0} (Fig. 1). We (1) define the initial input collimated beam (before the lens L_1) in the I coordinate system and (2) analyze the final output collimated beam (after the lens L_2) in the R coordinate system. The incident diverging beam after L_1 and the reflected diverging beam before L_2 are analyzed in the simulation [60] (including the lens transformations), whose mathematical details are not required here. The mathematical forms of only the (1) initial and (2) final collimated beams are relevant for the purpose of the present paper. Both of these beams are approximated via plane wavefronts, which are characterized by conveniently omissible constant phase terms over the beam cross sections. So, we analyze these plane-wave beam fields only in terms of their complex field amplitude vectors, denoted by \mathcal{E} .

In the I coordinate system, the Gaussian electric field amplitude profile of the initial collimated beam is given by

$$\mathcal{E}_0^{(I)} = \mathcal{E}_{0x}^{(I)} + e^{i\Phi_E} \mathcal{E}_{0y}^{(I)} = \mathcal{E}_{0x}^{(I)} \hat{\mathbf{x}}^{(I)} + e^{i\Phi_E} \mathcal{E}_{0y}^{(I)} \hat{\mathbf{y}}^{(I)}, \quad (1)$$

$$\mathcal{E}_{0x}^{(I)} = \mathcal{E}_{00} e^{-\rho^{(I)2}/w_0^2} \cos \theta_E; \quad \mathcal{E}_{0y}^{(I)} = \mathcal{E}_{00} e^{-\rho^{(I)2}/w_0^2} \sin \theta_E, \quad (2)$$

where \mathcal{E}_{00} is the electric field magnitude at the beam axis, $\rho^{(I)} = (x^{(I)2} + y^{(I)2})^{1/2}$, w_0 is the half-beam width, and θ_E , Φ_E are angle and relative-phase parameters which deter-

mine the exact polarization of $\mathcal{E}_0^{(I)}$. After passing through the lens L_1 , the beam divergence is obtained as $2\theta_D = -2 \tan^{-1}(w_0/\mathcal{F}_1)$.

With respect to the plane of incidence, $\mathcal{E}_{0x}^{(I)}$ is a TM polarized field and $\mathcal{E}_{0y}^{(I)}$ is a transverse electric (TE) polarized field. The observed field \mathcal{E} at the screen S_R , though collimated by the lens L_2 to approximate a plane-wave beam field, is neither TM nor TE, because, in the intermediate stage, the reflection of the curved incident wavefront at the dielectric interface fundamentally induces polarization-inhomogeneity across the wavefront [55–61]. The final output field \mathcal{E} at the screen S_R is obtained in the form

$$\mathcal{E} = \mathcal{E}^X + e^{i\Phi_E} \mathcal{E}^Y, \quad (3)$$

$$\mathcal{E}^X = \mathcal{E}_x^X \hat{\mathbf{x}} + \mathcal{E}_y^X \hat{\mathbf{y}}, \quad \mathcal{E}^Y = \mathcal{E}_x^Y \hat{\mathbf{x}} + \mathcal{E}_y^Y \hat{\mathbf{y}}, \quad (4)$$

where \mathcal{E}^X and \mathcal{E}^Y are the individual final output fields corresponding to $\mathcal{E}_{0x}^{(I)}$ and $\mathcal{E}_{0y}^{(I)}$, respectively.

Here onwards we set the following parameter values in the simulation: free-space wavelength $\lambda = 632.8$ nm; refractive indices $n_1 = 1$, $n_2 = 1.52$ [$\theta_B = \tan^{-1}(n_2/n_1) \approx 56.66^\circ$]; incident beam power $P_w = 1$ mW; $w_0 = 0.6$ mm; $\mathcal{F}_1 = -5$ cm (thus, $\theta_D \approx 0.7^\circ$); propagation distances $O_I O_S = 5$ cm, $O_S O = 2.5$ cm; and $\mathcal{F}_2 = 12.5$ cm. Using the above-mentioned values of P_w and w_0 in Eq. (A5), we obtain the central field magnitude $\mathcal{E}_{00} \approx 1.15430 \times 10^3$ V/m.

For incidence around the Brewster angle, the Fresnel TM reflection coefficient is much less than the Fresnel TE reflection coefficient [62–64]. So, if $|\mathcal{E}_{0x}^{(I)}| \sim |\mathcal{E}_{0y}^{(I)}|$, then we get $|\mathcal{E}^Y| \gg |\mathcal{E}^X|$, and the subtle effects such as the ones reported here become obscured due to the dominance of \mathcal{E}^Y . It is thus essential to have $|\mathcal{E}^Y| \sim |\mathcal{E}^X|$, which can be achieved by appropriately choosing θ_E in Eq. (2). Here onwards, we choose $\theta_E = 0.5^\circ$ for most of our general observations for $\theta_{i0} = \theta_B$. We also choose $\theta_E = 0^\circ$ in some cases to observe only \mathcal{E}^X for Brewster reflection.

For $\theta_{i0} = \theta_B$ and $\theta_E = 0.5^\circ$, the simulated field-component profiles \mathcal{E}_x^X , \mathcal{E}_y^X , \mathcal{E}_x^Y , and \mathcal{E}_y^Y at the surface S_R , as functions of coordinates (x, y) , are shown in Fig. 2. These profiles show that the functions \mathcal{E}_x^X , \mathcal{E}_y^X , \mathcal{E}_x^Y , and \mathcal{E}_y^Y can be expressed in empirical forms (2D Hermite-Gaussian functions [62,74]) as

$$\mathcal{E}_x^X = A_1 f \cos \phi, \quad \mathcal{E}_y^X = A_2 f \sin \phi, \quad (5)$$

$$\mathcal{E}_x^Y = -A_3 f \sin \phi, \quad \mathcal{E}_y^Y = -A_4 g, \quad (6)$$

$$\text{where } g = e^{-\rho^2/w_R^2}, \quad f = (\rho/w_R)g, \quad (7)$$

where (ρ, ϕ) are the plane polar coordinates corresponding to (x, y) , and A_1, A_2, A_3, A_4, w_R are constants which are determined numerically. For the specific example of Fig. 2, these numerically determined values are $A_1 \approx 3.42226$ V/m, $A_2 \approx 1.44286$ V/m, $A_3 \approx 1.25917 \times 10^{-2}$ V/m, $A_4 \approx 1.59497$ V/m, and $w_R \approx 1.49603$ mm, which give less than 0.02 fractional error in the maximum magnitudes of the considered functions as compared to the exact field-component profiles obtained via simulation. For $\theta_E = 0^\circ$, we automatically get $A_3 = A_4 = 0$ V/m and numerically obtain $A_1 \approx 3.42239$ V/m, $A_2 \approx 1.44292$ V/m, with $w_R \approx 1.49603$ mm remaining unchanged.

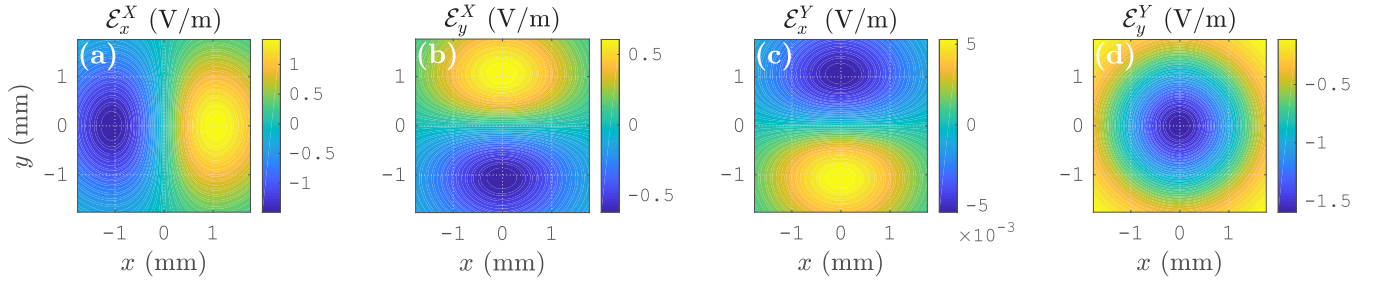


FIG. 2. Simulated field-component profiles [Eqs. (3, 4)] at the screen S_R (Fig. 1): (a) \mathcal{E}_x^X , (b) \mathcal{E}_y^X , (c) \mathcal{E}_x^Y , (d) \mathcal{E}_y^Y for the chosen system parameters and for $\theta_{i0} = \theta_B$, $\theta_E = 0.5^\circ$ [Eq. (2)]. The color bars express the concerned functions in V/m.

Physically, the constant w_R is a half-beam-width term corresponding to the profiles of Fig. 2, as understood from the functional form of g [Eq. (7)]. The constants A_j ($j = 1, 2, 3, 4$) are field magnitude terms. Each A_j can be expressed in the form $A_j = a_j \mathcal{E}_{00}$; where a_j is a dimensionless quantity giving the ratio A_j/\mathcal{E}_{00} . For example, as per the calculated value of \mathcal{E}_{00} and the numerically obtained values of A_j for the case of Fig. 2, the ratios are $a_1 \approx 2.96479 \times 10^{-3}$, $a_2 \approx 1.24999 \times 10^{-3}$, $a_3 \approx 1.09085 \times 10^{-5}$, and $a_4 \approx 1.38176 \times 10^{-3}$. These ratios signify the fractional contributions of \mathcal{E}_{00} in the formation of the field profiles \mathcal{E}_x^X , \mathcal{E}_y^X , \mathcal{E}_x^Y , and \mathcal{E}_y^Y via Eqs. (5) and (6). The ratios are as small as $\sim 10^{-3}$ and $\sim 10^{-5}$, signifying the very small reflected beam intensity as compared to the incident beam intensity under the concerned Brewster-incidence and near-Brewster-incidence conditions.

For the purpose of the present paper, it is sufficient to proceed further by considering the empirical functions of Eqs. (5) and (6). Our complete mathematical analysis of the exact field \mathcal{E} [Eq. (3)], based on the reflection and transmission coefficient matrix formalism [60], will be reported elsewhere.

We use Eqs. (4)–(6) in Eq. (3) to find the empirical form of the field \mathcal{E} ; and then express it in terms of the $\hat{\sigma}^\pm$ spin states as

$$\mathcal{E} = \mathcal{E}_+ \hat{\sigma}^+ + \mathcal{E}_- \hat{\sigma}^-, \quad \text{where } \mathcal{E}_\pm = a_\pm + ib_\pm, \quad (8)$$

$$a_\pm = \frac{g}{\sqrt{2}} \left[\left(A_1 \frac{x}{w_R} - A_3 \frac{y}{w_R} \cos \Phi_E \right) \mp A_4 \sin \Phi_E \right], \quad (9)$$

$$b_\pm = \frac{g}{\sqrt{2}} \left[-A_3 \frac{y}{w_R} \sin \Phi_E \mp \left(A_2 \frac{y}{w_R} - A_4 \cos \Phi_E \right) \right], \quad (10)$$

where $x = \rho \cos \phi$, $y = \rho \sin \phi$ are used. The intensities I , I_\pm of the fields \mathcal{E} , $\mathcal{E}_\pm \hat{\sigma}^\pm$ are then obtained in the form $I = (n_1/2\mu_0 c) |\mathcal{E}|^2$ as

$$I = \frac{n_1}{2\mu_0 c} g^2 \left[A_1^2 \frac{x^2}{w_R^2} + (A_2^2 + A_3^2) \frac{y^2}{w_R^2} - 2 \left(A_1 A_3 \frac{xy}{w_R^2} + A_2 A_4 \frac{y}{w_R} \right) \cos \Phi_E + A_4^2 \right], \quad (11)$$

$$I_\pm = \frac{I}{2} \mp \frac{n_1}{2\mu_0 c} g^2 \left(A_1 A_4 \frac{x}{w_R} - A_2 A_3 \frac{y^2}{w_R^2} \right) \sin \Phi_E. \quad (12)$$

Thus, the fields $\mathcal{E}_\pm \hat{\sigma}^\pm$ have different intensities I_\pm but satisfy energy conservation $I_+ + I_- = I$. Equations (8)–(12) are the primary corollaries of our central assumptions [Eq. (5)–(7)]. Based on these, the secondary corollaries such as the total

powers, centroid positions, and singularity positions are derived.

Powers: From I , I_\pm , we obtain the corresponding powers P , P_\pm in the form $P = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} I dx dy$ as

$$P = \frac{n_1}{2\mu_0 c} \frac{\pi w_R^2}{8} A_0^2, \quad (13)$$

$$P_\pm = \frac{P}{2} \pm \frac{n_1}{2\mu_0 c} \frac{\pi w_R^2}{8} A_2 A_3 \sin \Phi_E, \quad (14)$$

$$\text{where } A_0 = (A_1^2 + A_2^2 + A_3^2 + 4A_4^2)^{\frac{1}{2}}. \quad (15)$$

Here $P_+ \neq P_-$ because $I_+ \neq I_-$ [Eq. (12)]. However, as per the numerically obtained constant values, $A_3 \ll A_0$. So the power difference is very small.

Centroids and beam shifts: The centroid positions (x_C, y_C) , $(x_{C\pm}, y_{C\pm})$ of the intensity profiles I , I_\pm are obtained in the form

$$x_C = \frac{1}{P} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} x I dx dy; \quad y_C = \frac{1}{P} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} y I dx dy.$$

We thus get

$$x_C = 0; \quad y_C = -2w_R \frac{A_2 A_4}{A_0^2} \cos \Phi_E, \quad (16)$$

$$x_{C\pm} = \mp \frac{2w_R A_1 A_4 \sin \Phi_E}{A_0^2 \pm 2A_2 A_3 \sin \Phi_E}, \quad (17)$$

$$y_{C\pm} = -\frac{2w_R A_2 A_4 \cos \Phi_E}{A_0^2 \pm 2A_2 A_3 \sin \Phi_E}. \quad (18)$$

Zero x_C [Eq. (16)] implies zero GH shift [55–59,65,66] of the field \mathcal{E} [75]. However, nonzero IF shift [55–59,67–69] y_C [Eq. (16)] of \mathcal{E} and longitudinal and transverse spin shifts $x_{C\pm}$ [Eq. (17)] and $y_{C\pm}$ [Eq. (18)] (i.e., x -shifts and y -shifts of $\mathcal{E}_\pm \hat{\sigma}^\pm$) are observed.

Since $A_2, A_4 \sim A_0$, Eq. (16) shows that $|y_C| \sim w_R$ for appropriate ranges of Φ_E . Thus, for such Φ_E ranges, a giant IF shift of the order of the half-beam-width w_R is observed. This result has been experimentally demonstrated by Götte *et al.* [76].

A graphical description of the origin of IF shift is obtained from the profiles of Fig. 2. The \mathcal{E}_y^Y profile is negative everywhere, whereas the \mathcal{E}_y^X profile is positive in the $y > 0$ region and negative in the $y < 0$ region. So, for $-\pi/2 < \Phi_E < \pi/2$, these two fields undergo destructive interference in the $y > 0$ region and constructive interference in the $y < 0$ region. The opposite happens for $-\pi < \Phi_E < -\pi/2$ and $\pi/2 < \Phi_E \leq \pi$. This gives rise to an asymmetry in the total intensity profile

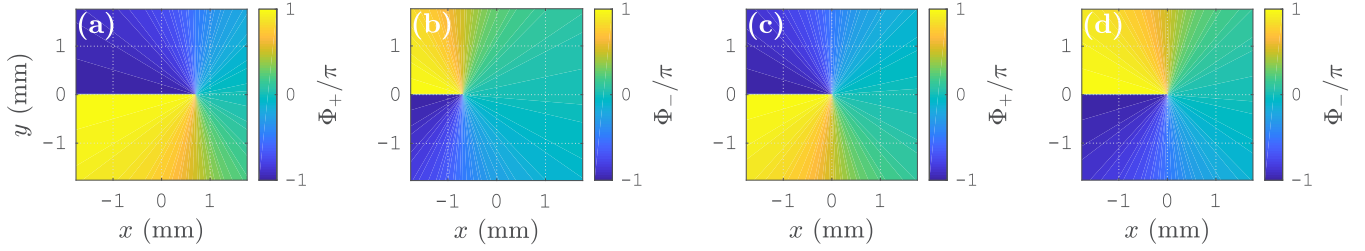


FIG. 3. (a), (b) Simulated Φ_{\pm} phase profiles [Eq. (22)] of the fields $\mathcal{E}_{\pm}\hat{\sigma}^{\pm}$ [Eq. (8)] for $\theta_{i0} = \theta_B$, $\theta_E = 0.5^\circ$, $\Phi_E = \pi/2$, showing l^{\mp} phase singularities at $(x_{S\pm}, y_{S\pm})$ [Eqs. (23–26)]. (c), (d) Similar Φ_{\pm} profiles for $\theta_{i0} = \theta_B$, $\theta_E = 0^\circ$, with phase-singularity coordinates $x_{S\pm} = y_{S\pm} = 0$.

l about the x axis, thus resulting in the IF shift. Though we have demonstrated this effect in the specific case of Brewster reflection, we have verified via simulation that this behavior and explanation are valid for any angle of incidence.

Now, with the approximation $A_3 \ll A_0$, we rewrite $(x_{C\pm}, y_{C\pm})$ [Eqs. (17, 18)] as

$$x_{C\pm} = 2w_R \frac{A_1 A_4}{A_0^2} \sin \Phi_E \left(2 \frac{A_2 A_3}{A_0^2} \sin \Phi_E \mp 1 \right), \quad (19)$$

$$y_{C\pm} = y_C + \delta_{\pm}, \quad (20)$$

$$\text{where } \delta_{\pm} = \pm 4w_R \frac{A_2^2 A_3 A_4}{A_0^4} \cos \Phi_E \sin \Phi_E. \quad (21)$$

The first term in the parentheses of Eq. (19) is small, since $A_3 \ll A_0$. So, for appropriate ranges of Φ_E , the $x_{C\pm}$ shifts are large (i.e., comparable to w_R) and are approximately opposite to each other. Thus, while Qin *et al.* [77] report wavelength order in-plane spin-shifts for non-Brewster-reflection cases, the present Brewster-reflection case shows “giant” (beam-size-order) longitudinal spin shifts.

The transverse spin shifts $y_{C\pm}$ [Eq. (20)] are the IF shift y_C [Eq. (16)] with added correction terms δ_{\pm} [Eq. (21)]. These δ_{\pm} terms are the spin Hall shifts [55,70,71,78,79]. The effect that the spin Hall shifts in Brewster reflection appear on both sides of IF shift has been demonstrated by Xie *et al.* [79].

Phase singularities: From Eq. (8) we obtain the phases of $\mathcal{E}_{\pm}\hat{\sigma}^{\pm}$ as

$$\Phi_{\pm} = \tan^{-1}(b_{\pm}/a_{\pm}). \quad (22)$$

The phase singularities of $\mathcal{E}_{\pm}\hat{\sigma}^{\pm}$ appear where $a_{\pm} = b_{\pm} = 0$. Applying this condition to the expressions of a_{\pm}, b_{\pm} [Eqs. (9, 10)], we obtain the singularity coordinates $(x_{S\pm}, y_{S\pm})$ as

$$x_{S\pm} = \frac{w_R A_4 (A_3 \pm A_2 \sin \Phi_E)}{A_1 (A_2 \pm A_3 \sin \Phi_E)}, \quad (23)$$

$$y_{S\pm} = \frac{w_R A_4 \cos \Phi_E}{A_2 \pm A_3 \sin \Phi_E}, \quad (24)$$

which we rewrite by using the approximation $A_3 \ll A_1, A_2, A_4$ as

$$x_{S\pm} = w_R \frac{A_3 A_4}{A_1 A_2} \cos^2 \Phi_E \pm w_R \frac{A_4}{A_1} \sin \Phi_E, \quad (25)$$

$$y_{S\pm} = w_R \frac{A_4}{A_2} \cos \Phi_E \mp w_R \frac{A_3 A_4}{A_2^2} \cos \Phi_E \sin \Phi_E. \quad (26)$$

The first term in $x_{S\pm}$ [Eq. (25)] is small, since A_3 is small. So the second term dominates for appropriate ranges of Φ_E , and hence, for those Φ_E ranges, x_{S+} and x_{S-} are almost opposite

to each other and $|x_{S\pm}| \sim w_R$. However, for other appropriate Φ_E ranges, the first term in $y_{S\pm}$ [Eq. (26)] dominates while the second term is small due to the presence of A_3 . Thus, the difference between y_{S+} and y_{S-} is small as compared to $y_{S\pm}$.

The simulated Φ_+ profile [Eq. (22)] for $\theta_{i0} = \theta_B$, $\theta_E = 0.5^\circ$, $\Phi_E = \pi/2$ [Fig. 3(a)] shows an l^- (i.e., $l = -1$) phase singularity at (x_{S+}, y_{S+}) . The Φ_- profile for the same simulation parameters [Fig. 3(b)] shows an l^+ (i.e., $l = +1$) phase singularity at (x_{S-}, y_{S-}) . These singularities show the l^{\mp} orbital angular momenta (OAM) of the $\mathcal{E}_{\pm}\hat{\sigma}^{\pm}$ fields. The total angular momenta of the $l^{\mp}\hat{\sigma}^{\pm}$ combinations and of the total field \mathcal{E} are zero, implying conservation of total angular momentum.

Special case: For the special case of $\theta_E = 0^\circ$, we get $\mathcal{E}_0^{(l)} = \mathcal{E}_{0x}^{(l)}$ [Eqs. (1) and (2)], and hence $\mathcal{E} = \mathcal{E}^x$ [Eq. (3)]. All A_3 and A_4 terms in Eqs. (6)–(26) are zero in this case, and hence several simplified symmetries in the fields are observed: $l_+ = l_- = l/2$ [Eqs. (11) and (12)]; $P_+ = P_- = P/2$ [Eqs. (13) and (14)]; $y_C = 0$ [Eq. (16)], implying zero IF shift of the \mathcal{E} field; $x_{C\pm} = y_{C\pm} = 0$ [Eqs. (19) and (20)], implying zero spin shifts of both $\mathcal{E}_{\pm}\hat{\sigma}^{\pm}$ fields; and $x_{S\pm} = y_{S\pm} = 0$ [Eqs. (25) and (26)], implying singularity positions at the screen center O_R (Fig. 1) for both $\mathcal{E}_{\pm}\hat{\sigma}^{\pm}$ fields [Figs. 3(c) and 3(d)].

IV. POLARIZATION SINGULARITIES

Equations (19) and (25) show that $x_{C\pm}$ and $x_{S\pm}$ are in directions opposite to each other. For example, for $\Phi_E = \pi/2$, we get $x_{C+}, x_{S-} \sim -w_R$ and $x_{C-}, x_{S+} \sim w_R$. Thus, in the $x < 0$ region, the $\mathcal{E}_+\hat{\sigma}^+$ field with an almost constant phase profile is superposed on the relatively weak $\mathcal{E}_-\hat{\sigma}^-$ field with an l^+ phase singularity, whereas, in the $x > 0$ region, the $\mathcal{E}_-\hat{\sigma}^-$ field with an almost constant phase profile is superposed on the relatively weak $\mathcal{E}_+\hat{\sigma}^+$ field with an l^- phase singularity. These $(l^{\pm}\hat{\sigma}^{\mp} + l^0\hat{\sigma}^{\pm})$ superpositions around the phase singularities generate lemon polarization patterns in the complete field \mathcal{E} [17]. The resulting \mathcal{E} field profile for $\Phi_E = \pi/2$ is shown in Fig. 4(a), where two opposite lemon patterns around C -point singularities, symmetrically separated by an L -line singularity, are observed.

The other fundamental polarization pattern around a C -point singularity is the star pattern, which is obtained via $(l^{\pm}\hat{\sigma}^{\pm} + l^0\hat{\sigma}^{\mp})$ superpositions [17]. Due to conservation of total angular momentum, the $l^{\pm}\hat{\sigma}^{\pm}$ combinations do not appear automatically in the \mathcal{E} field, and hence the automatic appearance of the star pattern in Brewster reflection is fundamentally prohibited. However, by passing the \mathcal{E} beam field through a half-wave plate (HWP), its $(l^{\pm}\hat{\sigma}^{\mp} + l^0\hat{\sigma}^{\pm})$ superpositions can

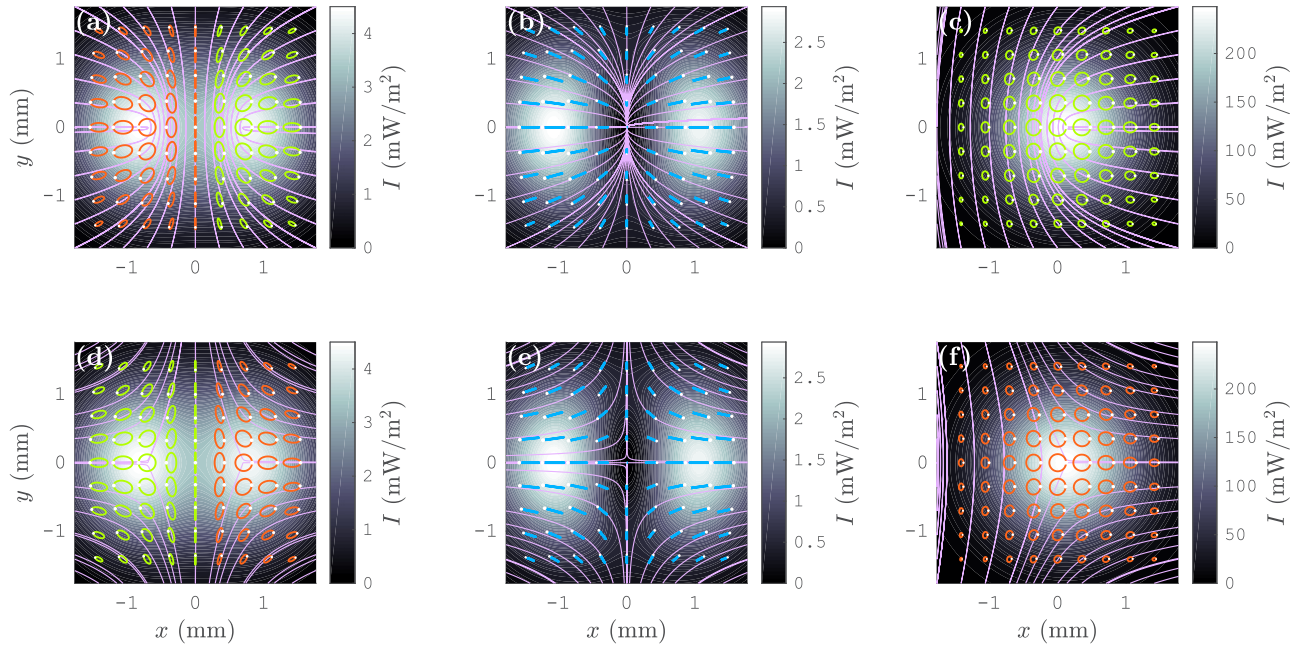


FIG. 4. Simulated profiles: (a) complete field \mathcal{E} [Eq. (3)] for $\theta_{i0} = \theta_B$, $\theta_E = 0.5^\circ$, $\Phi_E = \pi/2$, showing two C -point singularities (double lemon pattern) separated by an L -line singularity. (b) Field \mathcal{E}^X [Eq. (4)], obtained from the field \mathcal{E} of Fig. 4(a) by reducing θ_E to 0° . The field \mathcal{E}^X contains a node singularity. (c) Complete field \mathcal{E} for $\Delta\theta_{i0} = -2.0^\circ$, $\theta_E = 3.2^\circ$, $\Phi_E = \pi/2$, showing an isolated C -singularity (single lemon pattern). (d) The double star pattern, (e) the saddle singularity, and (f) the single star pattern, created by passing the fields of Figs. 4(a), 4(b), and 4(c), respectively through a HWP (fast axis along \hat{x} or \hat{y}). The field-representation color codes are light green: LEP; dark orange: REP; light blue: linear polarization; white dot: the tip of the field vector \mathcal{E} , originated at the ellipse center, at time $t = 0$ (the complete description of this color-code representation is given in Ref. [60]). The intensity profile I [Eq. (11)] of the field \mathcal{E} is shown at the background of each \mathcal{E} profile.

be converted to $(l^\pm \delta^\pm + l^0 \delta^\mp)$ superpositions, thus creating star patterns. The double lemon pattern of Fig. 4(a) is thus converted to the double star pattern of Fig. 4(d) with either \hat{x} or \hat{y} orientation of the HWP's fast axis.

The simulated \mathcal{E}^X field profile, obtained for $\theta_E = 0^\circ$, is shown in Fig. 4(b). It contains a node singularity, whose formation can be described in terms of a singularity-merger phenomenon [1,14]. As the angle θ_E [Eq. (2)] is gradually changed from a nonzero value to 0° , the contribution of \mathcal{E}^Y in the total field \mathcal{E} [Eq. (3)] is gradually reduced. Consequently, $|x_{S\pm}|$ and $|y_{S\pm}|$ [Eqs. (25) and (26)] gradually reduce to zero. The phase profiles of Figs. 3(a) and 3(b) thus gradually transform to the phase profiles of Figs. 3(c) and 3(d), respectively; and correspondingly, the two lemon C -points of Fig. 4(a) approach each other to eventually merge at the screen center O_R . This explains the formation of the node singularity of Fig. 4(b) for $\theta_E = 0^\circ$. The streamlines in Fig. 4(b) are not radial because of the complicated nature of the exact contributions of $\mathcal{E}_x^X \hat{x}$ and $\mathcal{E}_y^X \hat{y}$ [Eqs. (4) and (5)] in the field \mathcal{E}^X , as understood from Figs. 2(a) and 2(b).

Observed through a HWP (fast axis along \hat{x} or \hat{y}), the above-mentioned merger phenomenon is equivalent to the merger of the two star C -points of Fig. 4(d) to form the saddle singularity [1,14] of Fig. 4(e).

Though we emphasize on considering small θ_E values giving $|\mathcal{E}^Y| \sim |\mathcal{E}^X|$, it is also essential to observe that, as θ_E is gradually increased to 90° , the total field \mathcal{E} gradually transforms to only \mathcal{E}^Y [Eqs. (1)–(3)], a nonsingular field [Figs. 2(c)

and 2(d)]. Correspondingly, in terms of polarization singularities, $|x_{S\pm}|$ and $|y_{S\pm}|$ [Eqs. (25) and (26)] gradually increase (depending on Φ_E). The two C -lemons of Fig. 4(a) thus gradually move farther apart and eventually disappear at infinity for $\theta_E = 90^\circ$. This process, though not equivalent, is comparable to the disappearance of phase vortices at infinity due to free-space propagation [1,4].

Manipulation of our setup based on the above understanding enables us to generate various other polarization-singular patterns. For instance, the symmetry of Brewster reflection can be broken by taking θ_{i0} away from θ_B . For $\theta_{i0} = \theta_B + \Delta\theta_{i0}$, where $|\Delta\theta_{i0}| \gtrsim \theta_D$ and $|\Delta\theta_{i0}| \ll \theta_B$, the \mathcal{E} field profile takes the form of either the right or the left lemon pattern of Fig. 4(a). Such a lemon pattern for $\Delta\theta_{i0} = -2.0^\circ$, $\theta_E = 3.2^\circ$, $\Phi_E = \pi/2$ is shown in Fig. 4(c). This single lemon pattern is converted to the single star pattern of Fig. 4(f) by passing the beam field through a HWP (fast axis along \hat{x} or \hat{y}).

V. EXPERIMENTAL OBSERVATIONS

The fundamental phase and polarization (lemons, node) singularity patterns, simulated based on our formalism of Ref. [60] applied to a Brewster-reflected postparaxial optical beam, are also experimentally observed [80]. The schematic of the experimental setup is shown in Fig. 5. A He-Ne laser beam ($\lambda = 632.8$ nm) is first collimated using a lens pair. The desired polarization ellipticity of this collimated beam is then realized by using a half-wave-plate–Glan-Thompson-polarizer–quarter-wave-plate (HWP-GTP-QWP)

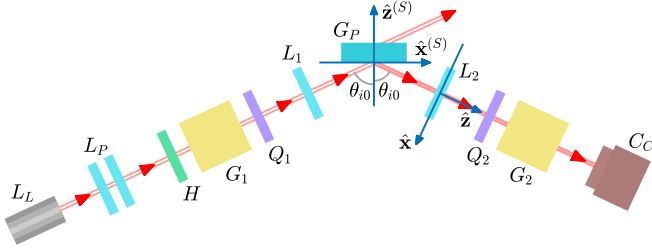


FIG. 5. The experimental setup. Here L_L : He-Ne laser; L_P : collimating lens pair; H : half-wave plate; G_1, G_2 : Glan-Thompson polarizers; Q_1, Q_2 : quarter-wave plates; L_1 : concave lens of focal length $\mathcal{F}_1 = -5$ cm (Fig. 1); L_2 : convex lens of focal length $\mathcal{F}_2 = 12.5$ cm (Fig. 1); G_P : glass plate, whose $-\hat{z}^{(S)}$ -facing surface is used as the concerned dielectric interface (Fig. 1); and C_C : CCD camera, used as the screen S_R (Fig. 1).

combination. The resultant elliptically polarized plane-wave beam is then used as the input $\mathbf{k}_{i0}-\mathcal{E}_0^{(I)}$ beam in a schematic identical to Fig. 1, with identical parameter values used in the simulations (as given in Sec. III). A surface of a glass plate is used as the concerned dielectric interface. A CCD camera is used as the screen S_R to observe the collimated beam field \mathcal{E} after the lens L_2 . The state of polarization of this final beam field is measured via Stokes parameters method [81] using a QWP-GTP combination positioned in front of the camera.

The experimentally generated \mathcal{E} profile [Eqs. (3) and (8)] for $\theta_{i0} = \theta_B$, $\theta_E = 0.5^\circ$, $\Phi_E = \pi/2$ is shown in Fig. 6(a), which transforms to the profile of Fig. 6(b) for $\theta_E = 0^\circ$, i.e., for the $\mathcal{E} = \mathcal{E}^X$ case [Eq. (3)]. The total field profile for the off-Brewster-incidence case of $\Delta\theta_{i0} = -2^\circ$, $\theta_E = 3.2^\circ$, $\Phi_E = \pi/2$ is shown in Fig. 6(c). The experimentally obtained field profiles of Figs. 6(a)–6(c) match well with the corresponding simulation-generated profiles of Figs. 4(a)–4(c), respectively, thus verifying the formation of generic optical singularities in the Brewster-reflected postparaxial beam field.

To observe the underlying OAM structure in the $\mathcal{E}_\pm \hat{\mathbf{d}}^\pm$ fields [Eq. (8)] for the $\theta_E = 0^\circ$ case, we first pass the output beam through an appropriately oriented QWP to transform the \mathcal{E} beam field to

$$\mathcal{E}_Q = \mathcal{E}_+ \hat{\mathbf{d}}^+ + \mathcal{E}_- \hat{\mathbf{d}}^-, \quad (27)$$

where $\hat{\mathbf{d}}^\pm = (\hat{\mathbf{x}} \pm \hat{\mathbf{y}})/\sqrt{2}$. The constituent $\mathcal{E}_\pm \hat{\mathbf{d}}^\pm$ beam fields are then independently extracted by using a GTP with

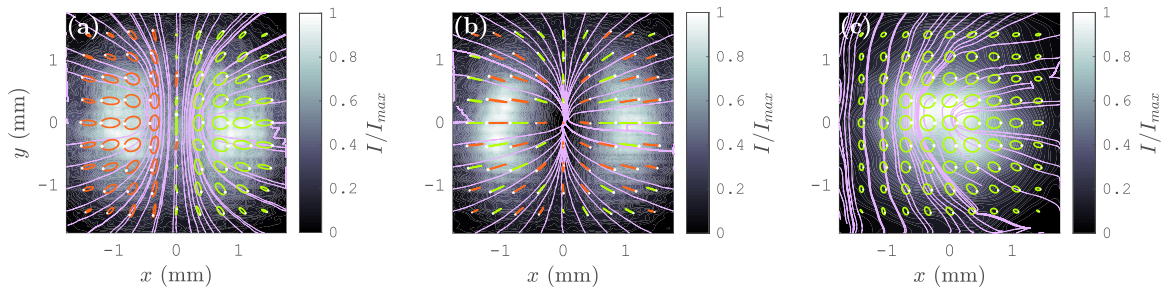


FIG. 6. (a), (b), (c) Experimental field profiles corresponding to the simulated profiles of Figs. 4(a), 4(b), and 4(c), respectively. The intensity profiles in the background are expressed in normalized form, I/I_{\max} .

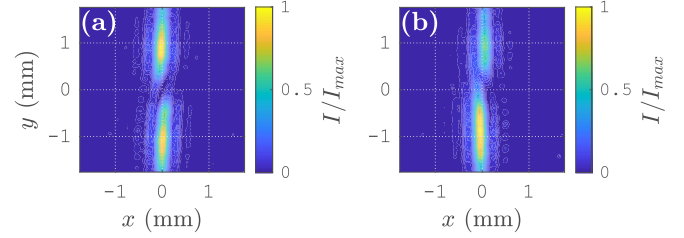


FIG. 7. Experimental single-slit diffraction patterns of the fields (a) $\mathcal{E}_+ \hat{\mathbf{d}}^+$ and (b) $\mathcal{E}_- \hat{\mathbf{d}}^-$ [Eq. (27)], showing l^\mp OAM.

appropriate orientations. The individual $\mathcal{E}_\pm \hat{\mathbf{d}}^\pm$ beams are then passed through a single vertical slit (width = 0.55 mm), placed along $x = 0$. The far-field diffraction patterns given by $\mathcal{E}_+ \hat{\mathbf{d}}^+$ and $\mathcal{E}_- \hat{\mathbf{d}}^-$ are shown in Figs. 7(a) and 7(b), respectively. These patterns are the characteristic single-slit diffraction patterns of beams with l^\mp OAM [82]. Hence, these patterns directly show the existence of l^\mp OAM in the $\mathcal{E}_\pm \hat{\mathbf{d}}^\pm$ fields and hence in the $\mathcal{E}_\pm \hat{\mathbf{d}}^\pm$ component beam fields.

VI. CONCLUSION

Even if standard methods [1,17,19,45–54] utilize special optical elements and setups to generate well-refined optical singularities, the singularity generation itself is a remarkably fundamental phenomenon. We have demonstrated the formation of generic optical singularities due to Brewster reflection of a postparaxial beam field. The core process in this singularity generation is a single reflection at a plane dielectric interface, one of the most elementary field transformations in optics. The complex transitional dynamics of these singularities are demonstrated via simple modifications of the input beam parameters. The formation and transitional dynamics of these generic optical singularities are thus clear demonstrations of the significant polarization inhomogeneity [55–61] of the Brewster-reflected postparaxial beam field. Hence, the present work serves the purpose of initiating a potential series of research works exploring the polarization patterns in a reflected beam field under Brewster-incidence and near-Brewster-incidence conditions. Our subsequent works in this direction will be reported elsewhere.

From a practical perspective, the simplicity of our singularity-generation process comes at the cost of losing most of the beam intensity in the transmitted beam (Figs. 1

and 5), as understood from the numerically obtained ratios $a_j = A_j/\mathcal{E}_{00}$ (Sec. III). Also, the generated beam is not in a pure LG mode [1,7,62]. However, our clear aim here is to explore the optical singularities in a Brewster-reflected postparaxial beam field, rather than to use the process as a singularity-generation technique. The above-mentioned inconveniences do not impact at all in analyzing the generic properties of the generated singularities, because, as long as the singularities exist, their generic properties also exist irrespective of the beam intensity and exact mode composition [1]. Nevertheless, due to the simplicity of the process, one can also use it to readily generate optical singularities within any optical setup as necessary.

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APPENDIX: DETERMINATION OF THE CENTRAL FIELD MAGNITUDE OF THE INITIAL INPUT BEAM

In this Appendix we determine the central field magnitude \mathcal{E}_{00} of the initial input beam field $\mathcal{E}_0^{(l)}$ [Eq. (1)] from the total beam power P_w . By using Eqs. (1) and (2), we express the field $\mathcal{E}_0^{(l)}$ as

$$\mathcal{E}_0^{(l)} = \mathcal{E}_{00} e^{-\rho^{(l)2}/w_0^2} (\cos \theta_E \hat{\mathbf{x}}^{(l)} + e^{i\Phi_E} \sin \theta_E \hat{\mathbf{y}}^{(l)}). \quad (\text{A1})$$

The corresponding magnetic field is

$$\begin{aligned} \mathcal{H}_0^{(l)} &= (\mathbf{k}_{i0} \times \mathcal{E}_0^{(l)})/\omega\mu_0 \\ &= \frac{n_1}{\mu_0 c} \mathcal{E}_{00} e^{-\rho^{(l)2}/w_0^2} (-e^{i\Phi_E} \sin \theta_E \hat{\mathbf{x}}^{(l)} + \cos \theta_E \hat{\mathbf{y}}^{(l)}), \end{aligned} \quad (\text{A2})$$

where μ_0 = magnetic permeability of free space and c = speed of light in free space. The time-averaged Poynting vector is then given by

$$\langle \mathbf{S} \rangle = \frac{1}{2} \text{Re}(\mathcal{E}_0^{(l)*} \times \mathcal{H}_0^{(l)}) = \frac{n_1}{2\mu_0 c} \mathcal{E}_{00}^2 e^{-2\rho^{(l)2}/w_0^2} \hat{\mathbf{z}}^{(l)}. \quad (\text{A3})$$

Then the time-averaged beam power passing through the $z^{(l)} = 0$ plane is obtained as

$$P_w = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \langle \mathbf{S} \rangle \cdot \hat{\mathbf{z}}^{(l)} dx^{(l)} dy^{(l)} = \frac{n_1}{2\mu_0 c} \mathcal{E}_{00}^2 \frac{\pi w_0^2}{2}. \quad (\text{A4})$$

Thus, the power P_w of the initial input Gaussian beam is equivalent to the power of a hypothetical plane-wave beam having a wave vector \mathbf{k}_{i0} and a uniform field magnitude \mathcal{E}_{00} over a circular cross section of radius $w_0/\sqrt{2}$.

In an actual experiment, the power P_w and the half-beam width w_0 of the input Gaussian beam are known. Using these known quantities, the central field magnitude \mathcal{E}_{00} is obtained by rearranging Eq. (A4) as

$$\mathcal{E}_{00} = \frac{2}{w_0} \left(\frac{\mu_0 c}{n_1 \pi} P_w \right)^{\frac{1}{2}}. \quad (\text{A5})$$

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