

The Arc Spectrum of Cobalt

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(Received June 11, 1940)

The present analysis classifies 2725 lines and identifies 768 multiplets of the doublet, quartet, and sextet systems. The results are in complete agreement with Hund's theory, and indicate that all the important features of the structure of the neutral atom are now known. The results agree closely with those of Catalan and Antunes (who classified 2076 lines) except where changes in term-designations have been made on account of Zeeman data or of a new interpretation of the convergence of the components of multiple terms to their limits. The principal ionization potential is 7.84 volts. Tables are given of terms, electron configurations, and of 3007 lines, of which 91 percent are classified. Zeeman effects have been observed for 871 lines and g values derived for 270 levels. The large majority of these have nearly the theoretical values for LS coupling. There are some cases of g sharing (Table VII). The wave-length list includes measures of 1282 lines made with the interferometer by Dr. Keivin Burns of the Allegheny Observatory, which, by his generosity, are here published for the first time; and also 274 newly measured lines between $\lambda 2230$ and $\lambda 1814$.

1. PREVIOUS INVESTIGATIONS

THE first regularities in the arc spectrum of cobalt were detected by Walters¹ who identified the lowest terms of the quartet system. Catalan² in 1928 classified about 1200 lines. A thorough discussion, classifying 2076 lines, was published in 1936 by Catalan and Antunes.³ This publication is unfortunately difficult of access in this country, and the situation is aggravated by the fact (communicated to us by Dr. Antunes) that the reprints which the authors hoped to distribute were lost in Toledo at the beginning of the Spanish War. We are very greatly indebted to Dr. Antunes for the loan of the single copy of this work in his possession—of which we have retained a photostatic copy.

The present work was begun without knowledge that this investigation was in progress, and has been extended farther with the aid of observations in the infra-red and ultraviolet. In view of the inaccessibility of the results of the earlier analysis, a detailed presentation of ours appears to be in order.

Observations of the Zeeman effect for 151 lines were given by Roth and Bartunek⁴ who

found g values for 93 levels. Our observations include 871 lines, and give g values for 270 levels.

Marvin⁵ has made a theoretical discussion of the energy-levels in the deep configurations of Co I. We have found certain additional terms close to the positions predicted by him.

2. THE OBSERVATIONAL DATA ON WHICH THE PRESENT INVESTIGATION IS BASED

(a) The *wave-lengths* have been compiled from all available sources (listed in Table VIII). We are very greatly indebted to Dr. Keivin Burns for putting at our disposal a long list of unpublished determinations with the interferometer. With his generous consent, these are printed here for the first time. Dr. Burns states that these observations are good to two parts per million. They are distinguished by heavy type in the general list (Table VIII). Next in preference, in order of accuracy, come the measures of Meggers and Kiess in the infra-red, including unpublished data kindly put at our disposal; those given in the *Wavelength Table of the Massachusetts Institute of Technology*; and unpublished measures of grating spectra by Burns. The observations have been extended from $\lambda 2230$ to $\lambda 1814$ by measures made by one of us (C.E.M.) on a plate taken by Dr. A. G. Shen-

¹F. M. Walters, Jr., *J. Washington Acad. Sci.* **14**, 407 (1924).

²M. A. Catalan, *Zeits. f. Physik* **47**, 89 (1928).

³M. A. Catalan and M. T. Antunes, *Anal. Soc. Española de Física y Química* **34**, 103–145, 207–297 (1936).

⁴F. L. Roth and P. F. Bartunek, *Phys. Rev.* **47**, 526 (1935).

⁵H. H. Marvin, *Phys. Rev.* **47**, 521 (1935).

stone with a normal-incidence vacuum spectrograph having a 2-meter glass grating ruled 30,000 lines per inch. The dispersion is 4.2A/mm.⁶ Few standard lines were available, and the measures are not of high precision.

King's temperature classification⁷ has been, as always, of fundamental value in the analysis.

(b) The observations of Zeeman effect were made by one of us (R.B.K.) but include some plates and measures made earlier by A. S. King. They were obtained with the aid of the Weiss magnet and the 15-foot concave grating spectrograph of the Mt. Wilson laboratory. The field strength was slightly in excess of 30,000 gauss. The spectrum was photographed in the second order (dispersion 1.86A/mm) from $\lambda 2200$ to $\lambda 5000$, and in the first order from $\lambda 5000$ to $\lambda 7000$.

Measurements of the Zeeman patterns were made with an ordinary comparator. Most of the complex patterns were unresolved, the n components usually appearing as doublets with the

components widened in some degree, while the p components were either undisplaced, though broadened, or appeared as doublets. Measurements of displacements on complex patterns appearing as doublets were usually made on the centers of gravity of each component of the doublet. In some cases, however, the patterns were on the verge of resolution and were strongly shaded inward or outward making it difficult to locate the center of gravity. Then settings were made on the strong edges of the pattern. These should give, very nearly, the separations of the strongest components of the complex patterns. In many cases one component of a doublet pattern, or one side of a resolved pattern, was badly blended with a neighboring line. In these cases the displacement was measured between the unblended component or components and the no-field line appearing in the adjacent spectra.

The reduction of the observed Zeeman separations in angstrom units to the theoretical unit of the normal Zeeman triplet was done in the usual manner. The field strengths were determined from measurements of the patterns of the sodium D lines and of numerous normal resolved patterns of previously classified Co I lines.

3. RESULTS OF PRESENT ANALYSES

The results of the present analysis agree in general with those of Catalan and Antunes, except among the high levels—both odd and even—where many changes in designation have been made, based largely upon Zeeman data not previously available. The number of terms identified is 99—47 belonging to the doublet system, 43 quartets, and 9 sextets—including 284 energy-levels. There are 43 more levels which have not been grouped into terms—a total of 327 levels, of which 132 are even and 195 odd.

Combinations between these account for 2725 lines—including 69 which are unresolved blends of lines which should be roughly comparable in intensity. There are also 42 faint predicted lines which are masked by strong ones. These are grouped into 768 multiplets, and 204 combinations with miscellaneous levels, observed in whole or in part. Of these 186 are doublet combinations, 197 quartets, 18 sextets, 288 doublet-

TABLE I. Observed and predicted low levels in Co I.

CONFIG.	TERM	PRINCIPAL LEVEL	INTERVALS
$3d^7 4s^2$	a^4F	0	816, 591, 402
		0	808, 594, 406
	b^4P	15,184	590, 422
		14,955	250, 385
	a^2G	16,468	766
		16,051	787
	b^2P	20,500	715
		20,878	787
	a^2H	21,780	695
		20,992	703
	b^2D	21,920	1232
		22,962	1168
	3F	35,798	-320
	3D	56,272	-352
$3d^8 4s$	b^4F	3483	660, 548, 386
		3483	662, 538, 396
	a^2F	7442	1018
		7629	1050
	a^4P	13,795	241, 363
		13,857	498, 243
	a^2D	16,778	-307
		16,799	-359
	a^2P	18,389	385
		18,194	221
	b^2G	23,184	23
		21,294	4
	3S	47,421	
	$3d^9$	c^2D	27,497
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⁶ A. G. Shenstone, Phil. Trans. 237, 453 (1938).

⁷ A. S. King, Astrophys. J. 42, 347 (1915), 51, 179 (1920) Mt. Wilson Contr. Nos. 108 and 181.

TABLE II. *Electron configurations in Co I.**

LIMIT d^7s		a^5F	b^3F	a^5P	3P	3H	1H	3G	1G	3D	1D	3P	1P
Added Electron	4s	a^4F		b^4P		a^2H		a^2G		b^2D		b^2P	
	4p	z^6D^0	x^4D^0	$^6S^0$	x^4S^0	$^4G^0$	$^2G^0$	w^4F^0	$^2F^0$	w^4P^0	$^2P^0$	$^4S^0$	$^2S^0$
		z^6F^0	x^4F^0	$^6P^0$	x^4P^0	$^4H^0$	$^2H^0$	w^4G^0	$^2G^0$	s^4D^0	$^2D^0$	$^4P^0$	$^2P^0$
	z^6G^0	x^4G^0	$^6D^0$	$^4D^0$	$^4I^0$	$^2I^0$	$^4H^0$	$^2H^0$	$^4F^0$	$^2F^0$	$^4D^0$	$^2D^0$	
	z^4D^0	z^2D^0	z^4S^0	z^2S^0	w^2G^0		x^2F^0		$^2P^0$			x^2S^0	
	z^4F^0	z^2F^0	z^4P^0	y^2P^0	y^2H^0		x^2G^0		$^2D^0$			w^2P^0	
	z^4G^0	z^2G^0	w^4D^0	v^2D^0	$^2I^0$		z^2H^0		$^2F^0$			$^2D^0$	

LIMIT d^8		a^3F	3P	1G	1D	LIMIT d^7s		a^5F	b^3F		LIMIT d^8		a^3F		
Added Electron	4s	b^4F	a^4P	b^2G	a^2D	Added Electron	5s	e^6F	f^4F	h^4F	g^2F	Added Electron	5s	e^4F	e^2F
	4p	y^4D^0	y^4S^0	u^2F^0	z^2P^0		4d	e^6P	f^4P	4P	2P		4d	e^4P	e^2P
		y^4F^0	y^4P^0	v^2G^0	x^2D^0			e^6D	f^4D	4D	2D			e^4D	e^2D
	y^4G^0	v^4D^0	x^2H^0	w^2F^0		f^6F	i^4F	4F	2F		g^4F	f^2F			
	y^2D^0	y^2S^0				e^6G	f^4G	4G	2G		e^4G	e^2G			
	y^2F^0	x^2P^0				e^6H	f^4H	4H	2H		e^4H	e^2H			
	y^2G^0	w^2D^0													

* A colon denotes that the assignment of the electron configuration is doubtful.

quartet, and 66 quartet-sextet intercombinations (while 13 are double intercombinations, between doublets and sextets).

The terms and unclassified levels are listed in Table IV. Some of the higher ones are incomplete—the components of small J value having eluded search.

4. ELECTRON CONFIGURATIONS

The *electron-configurations* for the low even terms can be assigned with certainty. Marvin's theoretical study is conclusive,—especially his prediction of the terms a^2H and b^2G close to the positions in which they were later found by Catalan and Antunes and by us, as shown in Table I, where the third column gives the level of the leading component and the next the term intervals—the observed values being in Roman type and the calculated in italics.

Marvin assigns b^2D to $3d^9$; but it fits his prediction for $3d^74s^2$ satisfactorily, and the recently discovered c^2D falls naturally in the other place.

The three remaining terms from the "low" configurations all lie so high that there is little or no hope of finding their combinations.

The odd configurations $3d^74s4p$ and $3d^84p$ give a great number of terms, forming triads, each of which should have its terms roughly at the same level and combine strongly with the related even low term. Many of these triads can be identified with certainty. Among the terms of small L value, especially in the doublets, there is a good deal of mutual perturbation and sharing of relationships, which make assignment difficult.

Among the high even terms, which are also included in the table, the "families" having the same limit-term in Co II are usually clearly separated, and assignments are rarely doubtful.

TABLE III. *Ionization potential of Co I.*

DESIG.	LEVEL	EST. n^*	TERM	Co II	$^4F_4-^3F_4$	FINAL n^*
a^4F	0	1.278	67,188	3350	63,838	1.281
e^6F	45,676	2.277	21,165	3350	63,493	2.276
f^4F	47,524	2.386	19,276	3350	63,450	2.382
e^6H	53,822	2.892	13,121	3350	63,593	2.901
a^4F	0	1.226	73,009	9813	63,193	1.223
h^4F	52,864	2.308	20,600	9813	63,651	2.316
b^4F	3483	1.350	60,213	0	63,696	1.352
a^2F	7442	1.387	57,043	950	63,535	1.387
e^4F	44,782	2.420	18,738	0	63,520	2.421
e^2F	45,924	2.450	18,282	950	63,336	2.433
e^4H	51,142	2.975	12,399	0	63,709	2.978

TABLE IV. Co I terms.

CONFIG.	TERM	OBS. <i>g</i>	C. AND A.	CONFIG.	TERM	OBS. <i>g</i>	C. AND A.	CONFIG.	TERM	OBS. <i>g</i>	C. AND A.		
d^8s	$a^2P_{1\frac{1}{2}}$	18,389.57	1.33	Id	$d^7s(^6F)5s$	$f^4F_{4\frac{1}{2}}$	47,524.47	1.33	Id	$d^8(^6P)4p$	$y^2S_{\frac{1}{2}}$	47,977.94	2.05
	$a^2P_{\frac{3}{2}}$	18,775.01	0.69	Id		$f^4F_{3\frac{1}{2}}$	48,201.60	1.27	Id		$x^2S_{\frac{1}{2}}$	48,026.34	1.70
						$f^4F_{2\frac{1}{2}}$	48,718.57	1.04	Id		$w^2S_{\frac{1}{2}}$	48,837.72	1.50:
d^7s^2	$b^2P_{1\frac{1}{2}}$	20,500.71	1.29	Id		$f^4F_{1\frac{1}{2}}$	49,078.43	0.36	Id		$w^2P_{0\frac{1}{2}}$	43,537.71	1.19
	$b^2P_{\frac{3}{2}}$	21,215.90	0.68	Id	$d^8(^6F)4d$	$g^4F_{4\frac{1}{2}}$	51,170.14	1.34	Id		$w^2P_{0\frac{1}{2}}$	43,130.24	0.71
$d^8(^6F)4d$	$e^2P_{1\frac{1}{2}}$	51,200.60	1.38:	$e^4P_{1\frac{1}{2}}$		$g^4F_{3\frac{1}{2}}$	51,199.58	1.16	Id	$d^8(^6D)4p$	$z^2P_{0\frac{1}{2}}$	46,685.43	1.33
	$e^2P_{\frac{3}{2}}$	52,041.14:	0.48:	$e^4P_{\frac{3}{2}}$		$g^4F_{2\frac{1}{2}}$	52,070.00	1.08	Id		$z^2P_{0\frac{1}{2}}$	47,091.14	0.63
d^8s	$a^2D_{2\frac{1}{2}}$	16,778.16	1.28	Id		$g^4F_{1\frac{1}{2}}$	52,702.76	0.76:	$e^4G_{2\frac{1}{2}}$	$d^8(^6P)4p$	$y^2P_{0\frac{1}{2}}$	48,334.37	1.39
	$a^2D_{1\frac{1}{2}}$	16,470.60	1.09	Id	$d^7s(^6F)5s$	$h^4F_{4\frac{1}{2}}$	52,864.41	1.26	Id		$y^2P_{0\frac{1}{2}}$	48,160.43:	1.20
d^7s^2	$b^2D_{2\frac{1}{2}}$	21,920.09	1.24	Id		$h^4F_{3\frac{1}{2}}$	53,694.57	1.28:	Id	$d^8(^6P)4p$	$x^2P_{0\frac{1}{2}}$	49,025.42	0.94
	$b^2D_{1\frac{1}{2}}$	23,152.57	0.79	Id		$h^4F_{2\frac{1}{2}}$	54,258.75	0.98:	Id		$w^2P_{0\frac{1}{2}}$	49,754.73	1.24
						$h^4F_{1\frac{1}{2}}$	54,426.64		Id	$d^8(^6P)4p$	$w^2P_{0\frac{1}{2}}$	50,925.11	1.32
d^9	$e^2D_{2\frac{1}{2}}$	27,497.06	1.20	Id	$d^7s(^6F)4d$	$i^4F_{4\frac{1}{2}}$	53,788.78	1.27	$e^6D_{4\frac{1}{2}}$		$w^2P_{0\frac{1}{2}}$	50,945.47	0.74
	$e^2D_{1\frac{1}{2}}$	28,470.51	0.82	Id		$i^4F_{3\frac{1}{2}}$	54,477.07		$f^6F_{3\frac{1}{2}}$		$w^2P_{0\frac{1}{2}}$	50,925.11	1.32
$d^8(^6F)4d$	$e^2D_{2\frac{1}{2}}$	52,460.10	0.92	Id		$i^4F_{2\frac{1}{2}}$	54,904.99	0.85	$f^6F_{2\frac{1}{2}}$		$w^2P_{0\frac{1}{2}}$	50,945.47	0.74
	$e^2D_{1\frac{1}{2}}$	53,343.27	0.80	Id	$d^8(^6F)4d$	$e^4G_{3\frac{1}{2}}$	51,203.75	1.21	Id	$d^7s(^6F)4p$	$z^2D_{0\frac{1}{2}}$	33,462.83	1.20
d^8s	$a^2F_{3\frac{1}{2}}$	7442.41	1.16	Id		$e^4G_{4\frac{1}{2}}$	51,267.93	1.13	Id		$z^2D_{0\frac{1}{2}}$	34,352.42	0.82
	$a^2F_{2\frac{1}{2}}$	8460.81	0.86	Id		$e^4G_{3\frac{1}{2}}$	52,162.02	1.13	Id	$d^8(^6F)4p$	$y^2D_{0\frac{1}{2}}$	36,092.44	1.19
$d^8(^6F)5s$	$e^2F_{3\frac{1}{2}}$	45,924.98	1.14	Id		$e^4G_{2\frac{1}{2}}$	52,772.30	0.74	$g^4F_{1\frac{1}{2}}$		$y^2D_{0\frac{1}{2}}$	36,895.13	0.81
	$e^2F_{2\frac{1}{2}}$	46,746.00	0.49:	Id	$d^7s(^6F)4d$	$f^4G_{3\frac{1}{2}}$	53,511.83	1.32	$f^6F_{3\frac{1}{2}}$		$x^2D_{0\frac{1}{2}}$	43,921.89	1.23
$d^8(^6F)4d$	$f^2F_{3\frac{1}{2}}$	52,005.00	1.11	Id		$f^4G_{4\frac{1}{2}}$	54,158.17	1.25:	$f^4F_{4\frac{1}{2}}$		$x^2D_{0\frac{1}{2}}$	43,911.36	1.13
	$f^2F_{2\frac{1}{2}}$	52,970.62	1.13	Id		$f^4G_{3\frac{1}{2}}$	54,514.67	1.23:	$f^4P_{2\frac{1}{2}}$		$x^2D_{0\frac{1}{2}}$	45,688.15	1.19
$d^7s(^6F)5s$	$g^2F_{3\frac{1}{2}}$	52,763.68	0.93	$e^2G_{3\frac{1}{2}}$	$d^8(^6F)4d$	$e^4H_{3\frac{1}{2}}$	51,142.53	1.21	Id		$w^2D_{0\frac{1}{2}}$	46,454.95	0.85
	$g^2F_{2\frac{1}{2}}$	53,704.14	0.98	Id		$e^4H_{3\frac{1}{2}}$	51,174.28	1.13	Id	$d^7s(^6P)4p$	$w^2D_{0\frac{1}{2}}$	46,671.94	1.21
d^7s^2	$a^2G_{3\frac{1}{2}}$	16,467.90	1.11	Id		$e^4H_{4\frac{1}{2}}$	52,121.21	0.96	Id		$w^2D_{0\frac{1}{2}}$	46,186.41	1.18
	$a^2G_{2\frac{1}{2}}$	17,233.68	0.90	Id		$e^4H_{3\frac{1}{2}}$	52,716.70	0.93	Id		$w^2D_{0\frac{1}{2}}$	53,195.98	1.16
d^8s	$b^2G_{4\frac{1}{2}}$	23,184.23	1.11	Id	$d^7s(^6F)4d$	$f^4H_{3\frac{1}{2}}$	53,618.08	1.22	$e^6H_{0\frac{1}{2}}$		$w^2D_{0\frac{1}{2}}$	53,074.92	0.81
	$b^2G_{3\frac{1}{2}}$	23,207.76	0.87	Id		$f^4H_{2\frac{1}{2}}$	54,315.67	1.18	$e^6H_{1\frac{1}{2}}$				
$d^8(^6F)4d$	$e^2G_{3\frac{1}{2}}$	52,156.46	1.12	Id		$f^4H_{4\frac{1}{2}}$	54,860.93	1.10:	$j^4F_{4\frac{1}{2}}$				
	$e^2G_{2\frac{1}{2}}$	52,856.68	0.92	$g^2F_{3\frac{1}{2}}$		$f^4H_{3\frac{1}{2}}$	55,268.75		$e^6H_{3\frac{1}{2}}$				
d^7s^2	$a^2H_{3\frac{1}{2}}$	21,780.47	1.09	Id		$g^4H_{3\frac{1}{2}}$	57,922.06			$d^7s(^6F)4p$	$z^2F_{0\frac{1}{2}}$	31,871.15	1.18
	$a^2H_{4\frac{1}{2}}$	22,475.36	0.94	Id		$g^4H_{4\frac{1}{2}}$	58,441.03				$z^2F_{0\frac{1}{2}}$	32,781.71	0.88
$d^8(^6F)4d$	$e^2H_{3\frac{1}{2}}$	52,113.91	1.13	Id		$g^4H_{3\frac{1}{2}}$	58,673.73			$d^8(^6F)4p$	$y^2F_{0\frac{1}{2}}$	35,450.56	1.12
	$e^2H_{4\frac{1}{2}}$	52,775.47	0.97	Id	$d^7s(^6F)4d$	$g^4H_{4\frac{1}{2}}$	59,314.82:				$y^2F_{0\frac{1}{2}}$	36,329.86	0.96:
d^8s	$a^4P_{2\frac{1}{2}}$	13,795.52	1.64	Id		$e^6F_{3\frac{1}{2}}$	53,789.12	1.81		$d^7s(^6G)4p$	$z^2F_{0\frac{1}{2}}$	43,555.22	1.24
	$a^4P_{1\frac{1}{2}}$	14,036.28	1.72	Id		$e^6F_{2\frac{1}{2}}$	54,445.61	1.67	$f^4D_{2\frac{1}{2}}$		$w^2F_{0\frac{1}{2}}$	43,425.71	1.02
	$a^4P_{\frac{1}{2}}$	14,399.28	2.66	Id	$d^7s(^6F)4d$	$e^6F_{1\frac{1}{2}}$	54,949.97	1.44:	Id	$d^8(^6D)4p$	$w^2F_{0\frac{1}{2}}$	47,225.11	1.25
d^7s^2	$b^4P_{2\frac{1}{2}}$	15,184.04	1.50	Id		$e^6D_{3\frac{1}{2}}$	54,352.30	1.48	Id		$w^2F_{0\frac{1}{2}}$	47,128.96	0.83
	$b^4P_{1\frac{1}{2}}$	15,774.04	1.47	Id		$e^6D_{2\frac{1}{2}}$	54,946.90	1.47:	Id		$w^2F_{0\frac{1}{2}}$	48,317.17	1.18
	$b^4P_{\frac{1}{2}}$	16,195.68	2.68	Id		$e^6D_{1\frac{1}{2}}$	55,407.10:	2.14	Id		$w^2F_{0\frac{1}{2}}$	48,615.56:	1.18
$d^8(^6F)4d$	$e^4P_{2\frac{1}{2}}$	51,042.26	1.59	Id	$d^7s(^6F)5s$	$e^6D_{\frac{1}{2}}$	55,407.10:	2.14	Id	$d^8(^6G)4p$	$w^2F_{0\frac{1}{2}}$	50,578.73	1.15
	$e^4P_{1\frac{1}{2}}$	52,033.26	1.40	Id		$e^6F_{3\frac{1}{2}}$	45,676.00	1.48	Id		$w^2F_{0\frac{1}{2}}$	50,712.45	0.91
	$e^4P_{\frac{1}{2}}$	52,915.92:		$e^2P_{\frac{1}{2}}$		$e^6F_{4\frac{1}{2}}$	46,223.01	1.43	Id	$d^7s(^6F)4p$	$z^2F_{0\frac{1}{2}}$	51,896.75	1.15:
$d^7s(^6F)4d$	$f^4P_{2\frac{1}{2}}$	53,936.68	1.46	$f^6F_{4\frac{1}{2}}$		$e^6F_{3\frac{1}{2}}$	46,706.83	1.40	Id		$z^2F_{0\frac{1}{2}}$	52,796.13	0.92:
	$f^4P_{1\frac{1}{2}}$					$e^6F_{2\frac{1}{2}}$	47,090.65	1.32	Id	$d^8(^6D)4p$	$w^2F_{0\frac{1}{2}}$	53,103.78	1.16
	$f^4P_{\frac{1}{2}}$					$e^6F_{1\frac{1}{2}}$	47,364.73	1.09	Id		$w^2F_{0\frac{1}{2}}$	53,146.91:	1.16
$d^8(^6P)5s$	$g^4P_{2\frac{1}{2}}$	56,545.51:		$42_{2\frac{1}{2}}^*$	$d^7s(^6F)4d$	$e^6F_{\frac{1}{2}}$	47,528.44	-0.71	Id		$w^2F_{0\frac{1}{2}}$	53,146.91:	1.16
	$g^4P_{1\frac{1}{2}}$					$f^6F_{3\frac{1}{2}}$	53,660.37	1.44	$31_{\frac{1}{2}}^*$	$d^7s(^6F)4p$	$z^2G_{0\frac{1}{2}}$	31,699.69	1.11
	$g^4P_{\frac{1}{2}}$					$f^6F_{4\frac{1}{2}}$	54,356.45	1.36	$e^6G_{4\frac{1}{2}}$		$z^2G_{0\frac{1}{2}}$	32,733.07	0.91
$d^8(^6F)4d$	$e^4D_{2\frac{1}{2}}$	51,052.98	1.45	Id		$f^6F_{3\frac{1}{2}}$	54,896.57	1.27	$e^6G_{3\frac{1}{2}}$	$d^8(^6F)4p$	$y^2G_{0\frac{1}{2}}$	33,439.72	1.16
	$e^4D_{2\frac{1}{2}}$	51,560.76	1.18	Id		$f^6F_{2\frac{1}{2}}$	55,283.02	1.17	$e^6G_{2\frac{1}{2}}$		$y^2G_{0\frac{1}{2}}$	34,133.59	0.95
	$e^4D_{1\frac{1}{2}}$	52,264.49:		Id		$f^6F_{1\frac{1}{2}}$	55,577.28:	1.07	$f^4D_{\frac{1}{2}}$	$d^7s(^6G)4p$	$z^2G_{0\frac{1}{2}}$	46,032.10	1.12
	$e^4D_{\frac{1}{2}}$	52,634.62	1.58:	Id	$d^7s(^6F)4d$	$e^6G_{3\frac{1}{2}}$	53,728.36:	1.35	33^*		$z^2G_{0\frac{1}{2}}$	45,766.63	0.93
$d^7s(^6F)4d$	$f^4D_{2\frac{1}{2}}$	53,702.13	1.39	$e^6P_{3\frac{1}{2}}$		$e^6G_{4\frac{1}{2}}$	54,367.43	1.32	$f^4G_{3\frac{1}{2}}$	$d^7s(^6H)4p$	$w^2G_{0\frac{1}{2}}$	50,593.38	1.10
	$f^4D_{2\frac{1}{2}}$	54,282.73:		$i^4F_{3\frac{1}{2}}$		$e^6G_{3\frac{1}{2}}$	54,682.91	1.23	\dagger		$w^2G_{0\frac{1}{2}}$	50,611.22	0.82
	$f^4D_{1\frac{1}{2}}$					$e^6G_{2\frac{1}{2}}$	54,989.62:	1.23	$f^4G_{4\frac{1}{2}}$	$d^8(^6G)4p$	$w^2G_{0\frac{1}{2}}$	53,276.02	1.03
	$f^4D_{\frac{1}{2}}$					$e^6G_{1\frac{1}{2}}$	55,449.97	1.25	$f^4D_{1\frac{1}{2}}$		$w^2G_{0\frac{1}{2}}$	53,373.53	0.86
d^7s^2	$a^4F_{4\frac{1}{2}}$	0.00	1.32	Id	$d^7s(^6F)4d$	$e^6H_{3\frac{1}{2}}$	53,822.08	1.34		$d^7s(^6G)4p$	$z^2H_{0\frac{1}{2}}$	45,540.28	1.12
	$a^4F_{3\frac{1}{2}}$	816.00	1.27	Id		$e^6H_{4\frac{1}{2}}$	54,452.38	1.29	$f^4H_{3\frac{1}{2}}$		$z^2H_{0\frac{1}{2}}$	45,111.48	0.90
	$a^4F_{2\frac{1}{2}}$	1408.84	1.05	Id		$e^6H_{3\frac{1}{2}}$	54,947.68	1.22	$f^4H_{4\frac{1}{2}}$	$d^7s(^6H)4p$	$y^2H_{0\frac{1}{2}}$	50,375.91	1.09:
	$a^4F_{1\frac{1}{2}}$	1809.33	0.42	Id		$e^6H_{2\frac{1}{2}}$	55,312.96	0.94	$f^4H_{3\frac{1}{2}}$		$y^2H_{0\frac{1}{2}}$	50,210.80	0.91
						$e^6H_{1\frac{1}{2}}$	55,520.64		$f^4G_{3\frac{1}{2}}$	$d^8(^6G)4p$	$z^2H_{0\frac{1}{2}}$	50,703.08	1.08
d^8s	$b^4F_{4\frac{1}{2}}$	3482.82	1.34	Id		$e^6H_{\frac{1}{2}}$	55,555.34				$z^2H_{0\frac{1}{2}}$	50,902.61	0.98
	$b^4F_{3\frac{1}{2}}$	4142.66	1.25	Id		$1_{\frac{1}{2}}$	54,561.74	1.36:	$e^6P_{2\frac{1}{2}}$	$d^8(^6G)4p$	$z^2H_{0\frac{1}{2}}$	50,902.61	0.98
	$b^4F_{2\frac{1}{2}}$	4600.18	1.04	Id		$2_{\frac{1$							

TABLE IV.—Concluded.

CONFIG.	TERM	OBS. <i>g</i>	C. AND A.	CONFIG.	TERM	OBS. <i>g</i>	C. AND A.	CONFIG.	TERM	OBS. <i>g</i>	C. AND A.			
$d^7s(^6P)4p$	$z^4P^0_{3/2}$	41,968.89	1.63	Id	$d^7s(^6F)4p$	$z^4F^0_{3/2}$	28,345.86	1.35	Id	$d^7s(^6F)4p$	$z^6F^0_{3/2}$	23,611.78	1.46	Id
	$z^4P^0_{1/2}$	41,982.66	1.73	Id		$z^4F^0_{5/2}$	28,777.27	1.24	Id		$z^6F^0_{5/2}$	23,855.62	1.49	Id
	$z^4P^0_{3/2}$	41,969.90	2.51	Id		$z^4F^0_{7/2}$	29,216.37	1.03	Id		$z^6F^0_{7/2}$	24,326.11	1.40	Id
						$z^4F^0_{9/2}$	29,563.17	0.42	Id		$z^6F^0_{9/2}$	24,733.28	1.33	Id
$d^8(^6P)4p$	$y^4P^0_{3/2}$	44,480.14	1.55	$w^4F^0_{3/2}$	$d^8(^6F)4p$	$y^4F^0_{3/2}$	32,841.99	1.32	Id		$z^6F^0_{11/2}$	25,041.16	1.10	Id
	$y^4P^0_{1/2}$	44,658.03	1.62	$z^2P^0_{1/2}$		$y^4F^0_{5/2}$	33,466.87	1.16	Id		$z^6F^0_{13/2}$	25,232.79	-0.61	Id
	$y^4P^0_{3/2}$	44,857.57	2.44	$z^2S^0_{3/2}$		$y^4F^0_{7/2}$	33,945.90	0.95	Id	$d^7s(^6F)4p$	$z^6G^0_{3/2}$	25,138.88	1.40	Id
						$y^4F^0_{9/2}$	34,196.21	0.47	Id		$z^6G^0_{5/2}$	25,568.68	1.34	Id
$d^7s(^6P)4p$	$x^4P^0_{3/2}$	46,002.83	1.54	$w^2D^0_{3/2}$	$d^7s(^6F)4p$	$x^4F^0_{3/2}$	41,225.76	1.35	Id		$z^6G^0_{7/2}$	25,937.59	1.29	Id
	$x^4P^0_{1/2}$	45,904.68	1.68	$y^4P^0_{3/2}$		$x^4F^0_{5/2}$	41,918.41	1.24	Id		$z^6G^0_{9/2}$	26,232.05	1.15	Id
	$x^4P^0_{3/2}$	45,957.29	2.48	$y^4P^0_{5/2}$		$x^4F^0_{7/2}$	42,434.23	1.04	Id		$z^6G^0_{11/2}$	26,450.02	0.88	Id
$d^7s(^6D)4p$	$w^4P^0_{3/2}$	51,160.03	1.51:	$S^5^0_{3/2}$		$x^4F^0_{9/2}$	42,796.67	0.44	Id		$z^6G^0_{13/2}$	26,597.64	-0.01	Id
	$w^4P^0_{1/2}$	52,014.45	1.68	†	$d^7s(^6G)4p$	$w^4F^0_{3/2}$	43,295.32	1.32	†		$1^0_{3/2}$	41,041.43	1.40	
	$w^4P^0_{3/2}$	52,355.12	2.40	†		$w^4F^0_{5/2}$	43,847.98	1.20	$z^2F^0_{3/2}$		$2^0_{3/2}$	41,104.96	1.34:	
$d^7s(^6F)4p$	$z^4D^0_{3/2}$	29,294.52	1.43	Id		$w^4F^0_{7/2}$	44,201.92	0.95	$z^2F^0_{5/2}$		$3^0_{3/2}$	42,988.12		
	$z^4D^0_{1/2}$	29,948.76	1.35	Id		$w^4F^0_{9/2}$	44,555.71	0.44	$w^4P^0_{1/2}$		$4^0_{3/2}$	43,969.90		
	$z^4D^0_{3/2}$	30,443.63	1.18	Id						$5^0_{3/2}$	44,381.32:			
	$z^4D^0_{5/2}$	30,742.65	-0.01	Id						$6^0_{3/2}$	47,839.15			
$d^8(^6F)4p$	$y^4D^0_{3/2}$	32,027.50	1.41	Id		$w^4F^0_{11/2}$	54,791.2				$7^0_{3/2}$	48,828.87		
	$y^4D^0_{1/2}$	32,654.50	1.39	Id		$w^4F^0_{13/2}$	55,314.04:				$8^0_{3/2}$	48,851.58:		
	$y^4D^0_{3/2}$	33,150.68	1.20	Id		$w^4F^0_{15/2}$	55,684.7				$9^0_{3/2}, 4^0_{3/2}$	49,197.74:		
	$y^4D^0_{5/2}$	33,449.18	0.01	Id	$d^7s(^6F)4p$	$z^4G^0_{3/2}$	28,845.22	1.27	Id		$10^0_{3/2}$	49,484.05	1.25:	$117^0_{3/2}$
$d^7s(^6F)4p$	$x^4D^0_{3/2}$	39,649.16	1.41	Id		$z^4G^0_{5/2}$	29,269.73	1.19	Id		$11^0_{3/2}$	49,847.08	1.09	
	$x^4D^0_{1/2}$	40,345.95	1.35	Id		$z^4G^0_{7/2}$	29,735.18	1.01	Id		$12^0_{3/2}$	50,105.05	0.70:	$87^0_{3/2}$
	$x^4D^0_{3/2}$	40,827.77	1.24	Id		$z^4G^0_{9/2}$	30,102.96	0.58	Id		$13^0_{3/2}, 4^0_{3/2}$	50,738.20		
	$x^4D^0_{5/2}$	41,101.80	-0.03	Id	$d^8(^6F)4p$	$y^4G^0_{3/2}$	32,430.59	1.28	Id		$14^0_{3/2}$	50,806.55		
$d^7s(^6P)4p$	$w^4D^0_{3/2}$	43,398.62	1.33	$z^2F^0_{3/2}$		$y^4G^0_{5/2}$	32,464.73	1.17	Id		$15^0_{3/2}$	51,184.63		
	$w^4D^0_{1/2}$	43,242.95	1.17	$z^2F^0_{5/2}$		$y^4G^0_{7/2}$	33,173.36	1.03	Id		$16^0_{3/2}$	51,863.18		
	$w^4D^0_{3/2}$	43,263.57	1.16	$z^2P^0_{1/2}$	$d^7s(^6F)4p$	$x^4G^0_{3/2}$	41,528.53	1.31	Id		$17^0_{3/2}$	51,989.31:		
	$w^4D^0_{5/2}$	43,435.58	0.14	$y^2P^0_{3/2}$		$x^4G^0_{5/2}$	42,269.32	1.18	Id		$18^0_{3/2}$	52,476.64		
$d^8(^6P)4p$	$v^4D^0_{3/2}$	45,971.19	1.42	$w^4D^0_{3/2}$	$d^7s(^6F)4p$	$x^4G^0_{7/2}$	42,811.44	0.98	Id		$19^0_{3/2}$	52,498.17		
	$v^4D^0_{1/2}$	46,329.63	1.36	$w^4D^0_{5/2}$		$x^4G^0_{9/2}$	43,199.65	0.83	Id		$20^0_{3/2}, 4^0_{3/2}$	52,526.04		
	$v^4D^0_{3/2}$	46,260.02	1.48	$P^0_{1/2}$	$d^7s(^6G)4p$	$w^4G^0_{3/2}$	43,952.06:				$21^0_{3/2}, 4^0_{3/2}$	53,065.96:		
	$v^4D^0_{5/2}$	46,502.15	0.16	$x^1P^0_{1/2}$		$w^4G^0_{5/2}$	44,183.34	1.18	$w^4F^0_{1/2}$		$22^0_{3/2}$	53,463.10		
						$w^4G^0_{7/2}$	44,394.47	1.00	$w^4F^0_{3/2}$		$23^0_{3/2}$	54,165.35	1.36	
	$w^4D^0_{3/2}$	46,872.74	1.30	$v^4D^0_{3/2}$		$w^4G^0_{9/2}$	44,568.47	0.70			$24^0_{3/2}$	54,398.60		
	$w^4D^0_{1/2}$	47,393.93	1.28	$v^4D^0_{5/2}$	$d^7s(^6F)4p$	$z^6D^0_{3/2}$	24,627.79	1.57	Id		$25^0_{3/2}$	54,874.08		
	$w^4D^0_{3/2}$	47,612.18	1.12	$v^4D^0_{7/2}$		$z^6D^0_{5/2}$	25,269.25	1.56	Id		$26^0_{3/2}$	54,932.32		
	$w^4D^0_{5/2}$	47,905.26	0.01	$v^4D^0_{9/2}$		$z^6D^0_{7/2}$	25,739.93	1.66	Id		$27^0_{3/2}$	55,061.49	1.66:	
$d^7s(^6P)4p$	$t^4D^0_{3/2}$	48,217.32	1.19	$w^4D^0_{3/2}$		$z^6D^0_{9/2}$	26,063.11	1.88	Id		$28^0_{3/2}$	55,120.30:		
	$t^4D^0_{1/2}$	48,443.76	1.34	$w^4D^0_{5/2}$	$d^7s(^6F)4p$	$z^6D^0_{11/2}$	26,250.49	3.37	Id		$29^0_{3/2}$	55,387.11:		
	$t^4D^0_{3/2}$	48,546.07	1.05	$w^4D^0_{7/2}$						$30^0_{3/2}$	55,508.78			
	$t^4D^0_{5/2}$	48,571.77	0.36:	$w^4D^0_{9/2}$						$31^0_{3/2}$	55,737.87			
$d^7s(^6D)4p$	$s^4D^0_{3/2}$	50,741.66		Id						$32^0_{3/2}$	55,818.91	1.31:		
	$s^4D^0_{1/2}$	51,139.38	1.33:	Id						$33^0_{3/2}, 4^0_{3/2}$	55,922.3			
	$s^4D^0_{3/2}$	51,847.27		Id						$34^0_{3/2}, 2^0_{3/2}$	56,101.84:			
	$s^4D^0_{5/2}$	52,264.01:								$35^0_{3/2}, 2^0_{3/2}$	56,222.04:			
										$36^0_{3/2}, 4^0_{3/2}$	58,187.39			
										$37^0_{3/2}, 2^0_{3/2}$	59,388.89			

Table II shows the assignments finally adopted. Terms predicted by theory but not found are denoted by the absence of small letters. Most of these terms are either very high, or would combine feebly, if at all, with the low level (e.g. the ${}^6S^0$, ${}^6P^0$, ${}^6D^0$, ${}^4H^0$). The most notable missing terms are the two ${}^2I^0$ terms, which are probably represented by observed lines with no satellites to identify them (§9). Most of the unassigned terms are odd, and all but two lie between 50,000 and 55,000 where the lower terms of the $5p$ configurations should be expected.

5. SERIES LIMITS

The convergence of the components of the terms of Co I to the components of the limit terms in Co II is of interest. Catalan and

Antunes have shown⁸ that, among the terms which have $d^8 {}^3F$ as limit, the quartet and doublet components of lowest J go to 3F_2 , those of next higher J to 3F_3 , leaving two high J quartet components for 3F_4 . This "inverted" convergence was found by one of us⁹ for the limit $d^9 {}^2D$ in Ni II. In Ni I, inverted convergence appears also in the terms having $d^8s {}^2F$ as limit, though that to $d^8s {}^4F$ is normal, but in Co I the convergence to $d^7s {}^3F$ is "normal." The combinations of all four components of h^4F with x^4G^0 are much stronger than those of g^2F , and the reverse is true for z^2F^0 , z^2G^0 ; hence the doublet and quartet levels are correctly identified. But h^4F_{41} , g^2F_{31} are close together; also h^4F_{31} , g^2F_{21} ,

⁸ Reference 3, pp. 132-134.

⁹ H. N. Russell, Phys. Rev. 34, 821 (1929).

and h^4F_{23} , h^4F_{13} . This suggests strongly that the convergence to $d^7s\ ^5F$ should be normal. Catalan and Antunes concluded that it is inverted, and found it difficult to distinguish the sextets and quartets in this pentad by means of the line-intensities. Working on the assumption of normal arrangement, we have been able to arrange the levels into a pentad of terms which combine much more strongly with z^6D^0 , z^6F^0 , z^6G^0 than with any quartet, and another pentad which combine more strongly with the quartets than the sextets. The ten leading components of these terms all lie between 53,511 and 53,936, the second components between 54,158 and 54,477, and so on.

In consequence of this reinterpretation of the situation, our values for the leading components of the sextet pentad, e^6P , e^6D , f^6F , e^6G , e^6H differ from those of the previous authors. Two of them were rejected as not real levels by them, and two not given at all; yet all are determined by good combinations except e^6H_{71} which gives a single very strong line with the right Zeeman pattern. The components of small L and J in this pentad give faint lines, and some of them could not be identified. A level of 54,282 which we have placed in this pentad as f^4D_{23} is classified by Catalan and Antunes as $d^8(^3F)6s\ ^4F_{34}$. It gives no combinations with levels having $J=4\frac{1}{2}$. If their interpretation is correct it seems to us very improbable that the $^4F_{43}$ component, for which they searched in vain, should be missing, as, especially in high series members, it should give stronger lines.

6. IONIZATION POTENTIAL

The available series consist of only two members ($4s$ and $5s$). The best way to determine the ionization potential is that developed by Catalan and Antunes¹⁰ and independently by Meggers and Russell¹¹—estimating the Rydberg denominators n^* by comparison with neighboring elements. Reliable values of n^* are known for Mn, Ni, Cu and Zn, so that those for Co can be interpolated with security. Table III gives the results. Only the components of largest J in the terms, and of greatest L in the pentads, need be

¹⁰ Reference 3, pp. 139–140.

¹¹ W. F. Meggers and H. N. Russell, J. Research Nat. Bur. Stand. 17, 190 (1936); (RP 906).

used. The error of the estimated term value is proportional to $\Delta n^*/n^{*3}$ so that the low terms give poor determinations. Adding this to the level of Co I, and subtracting the height of the limiting level in Co II above the ground-level, we obtain the level of 3F_4 above $^4F_{43}$. The mean for the terms for which $n^* > 2$ is 63,536 corresponding to an ionization potential of 7.84 volts with an estimated probable error of ± 0.02 . The values of n^* corresponding to this limit are given in the last column. The agreement with the estimated values is very close. Catalan and Antunes, by the same method, find 63,339, (7.82 volts). They prefer the value 63,312 obtained from their $6s$ term by a Hicks formula. The level g^4P_{23} , if in series with b^4P_{23} , should give Δn^* about 1.10. This would place the limit at 75,000 above $^4F_{43}$, or 11,500 above 3F_4 of Co II. The still undiscovered term $d^8\ ^3P$ should lie at about this level.

7. TERM TABLE

Table IV gives the term values which have been finally adopted. These were obtained by the usual process of convergent approximation, finding mean values for the odd terms from their combinations with the low even ones, etc. In taking these means, values derived from Burns' interferometer measures were given triple weight, and discordant combinations with deviations of 0.1 cm^{-1} or more were disregarded if better data were available. A colon denotes that the term value is determined with inferior accuracy, but not that the reality of the level itself is doubted.

The term v^4F^0 is doubtful. It gives a good multiplet with b^4F , but its combinations with a^4F are polar lines in the arc, and were originally attributed to Co II.

The term designations given by Catalan and Antunes are listed in the last column, "Id" meaning that they are identical with ours, and a blank that the level does not appear in their list. The numerous differences in assignment arise among the odd terms mainly from the present availability of Zeeman data; among the high even terms, from our reinterpretation of the convergence to the d^7s limits (§5). Three levels which they rejected as not real are restored to our list, and also nine which they regarded as doubtful. Thirty-three energy levels for which

TABLE V. Zeeman patterns of Co I.

ZEEMAN EFFECT			ZEEMAN EFFECT			ZEEMAN EFFECT		
λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED
6872.32	(1.37)1.35	(1.34)1.34	5477.08	(-1.08	(0)1.07s	4904.17	(-0.89:	(0.56)0.99
6814.95	(0.43)1.34	(0.41)1.32	5470.46	(-0.92	(0)0.94	4899.52	(0.46)0.85:	(0.39)0.95
6771.04	(0.36)1.43	(0.33)1.42	5469.30	(0.72)1.59:	(0.66)1.35	4886.99	(-1.06	(0.04)1.12
6632.43	(-1.09	(0)1.10	5454.57	(-1.33	(0.07)1.33	4882.70	(0.77)1.13:	(0.74)1.28
6595.86	(-0.91	(0)0.86s	5452.30	(-0.57	(0)0.54s	4881.31	(?)0.93	(?)0.18
6591.83	(-0.96	(0)0.98s	5444.58	(-1.04	(0)0.96	4867.87	(-1.19A?	(0)1.18
6563.40	(-1.10	(0)1.11	5437.00	(-0.82	(0)0.84	4855.59	(?)0.59	(0)1.50
6490.34	(-0.94	(0)0.99	5434.57	(0.84):1.12:	(0.79)0.90	4849.31	(?)0.97:	(0)0.9116
6477.86	(-0.83	(0)0.88	5431.02	(-0.67?:	(0)0.48s	4843.45	(1.13)1.10	(0.96)1.10
6454.99	(-1.17	(0)1.16	5413.73	(0.78)1.13	(0.77)1.14	4840.25	(-1.12A?	(0)1.14
6451.13	(-1.15	(0)1.19	5408.11	(0.68?:	(0.73)1.07	4815.90	(?)0.93	(0.48)0.96
6450.23	(-1.16	{(0)1.17 (0)0.3)0.90	5407.52	(?)1.43	(0.20, 0.61, 1.02) 0.11...2.15	4813.96	(1.71)0.56	(1.54)0.54
6431.07	(?)1.03	(0)1.02	5402.00	(0.41)0.68:	(0.41)0.62	4813.47	(-1.06A?	{(0)1.10 (0)1.56
6430.34	(-1.10?	(0)1.12	5399.76	(-0.94	(0.07)0.94	4795.85	(0.86):1.00:	(0.74)1.06
6429.91	(-0.90	(0)0.92	5393.72	(-1.83:	(0)1.52	4792.85	(-0.93A?	(0)0.94
6421.70	(-0.85	(0)0.80s	5390.47	(-1.35	(0)1.40	4785.07	(0.71)?	(0.74)1.06
6417.82	(-0.78	(0)0.85	5381.77	(-1.11	(0)1.14s	4781.43	(0.81)1.36:	(0.78)1.35
6395.15	(-0.61	(0)0.55	5381.10	(0.68?:	(0.91)1.14	4779.97	(-0.71	(0)0.72
6351.44	(?)0.97?	(0.26)1.02	5369.59	(-0.87i	(0)0.89s	4778.23	(-0.93	(0.22)0.93
6347.84	(-1.15	(0.12)1.14	5368.90	(-0.93	(0)0.91s	4776.31	(0.36)0.36	(0.36)0.36
6340.80	(-1.15:	(0)1.23	5366.74	(?)1.01:	(0.15)1.14	4771.10	(-1.24	(0)1.20
6320.41	(-1.05	(0)1.14	5364.81	(1.35:	(1.15)0.77	4768.07	(-0.98	(0)1.08
6314.52	(-1.06	{(0.08, 0.25, 0.42) 0.71...1.55	5362.78	(-1.15	(0)1.04s	4767.14	(-0.82	(0)0.82
6313.03	(-1.25	(0)1.16	5359.20	(-0.56	(0)0.61	4756.72	(-1.50?:	(0)1.42
6282.63	(-0.90A	(0)0.79s	5358.01	(?)0.88	(0)0.84	4754.35	(-0.50	(0)0.48s
6273.02	(-1.13	{(0.35)0.96 (0)1.14	5353.50	(-1.06	{(0)1.06 (0)0.92	4749.68	(-1.33	(0)1.28
6271.47	(-1.15?	(0)1.03	5352.04	(-1.14	(0)1.14	4737.76	(1.14)1.10	(0.93)1.14
6257.57	(-0.86	(0)0.88	5349.09	(-1.16	(0)1.05	4734.82	(1.15)1.18	(1.14)0.05, 2.22
6249.50	(-1.11	(0.22)1.14	5347.49	(?)1.06:	(0.09)1.14	4727.93	(0.76)?	(0.85)1.46
6247.28	(-1.09:	(0)1.02	5343.38	(-1.18:	(0)1.04	4718.47	(-1.18	(0)1.06
6246.38	(-1.36:	(0)1.49	5342.70	(-1.01	(0)1.02	4698.38	(2.05)1.32	(2.04)1.33
6232.44	(-1.20	(0)1.21	5341.32	(-1.16	(0.15)1.14	4693.19	(-?, 1.17)	(0.40, 1.19)
6230.96	(0.71)0.44, 1.83	(0.74)0.44, 1.92	5339.52	(-0.86	(0.09)0.94	4682.36	(0.68, 1.49, 2.16?	0.69, 1.48, 2.28
6223.35	(?)1.01:	(0.76)1.22	5336.16	(-1.16?:	(0)1.18	4662.36	(0.75)1.49C?	(0.74)1.49
6211.19	(-1.42	(0)1.37	5334.82	(-1.37?:	{(0)1.15 (0)1.39s	4663.40	(0.48)1.49	(0.47)1.48
6193.54	(-1.02:	(0)1.01	5333.64	(0.87:?)	(0.67)1.20	4657.39	(1.37):0.50:, 3.11:	(1.30)0.58, 3.18
6189.00	(0.54)1.48	(0.63)1.50	5331.45	(0.87:?)	(0.73)0.47, 1.93	4654.83	(?)0.95:	(0.22)0.93
6181.00	(?)1.21:	(0.41)1.34	5325.94	(-1.03:	(0)0.91	4644.31	(-0.86:	(0)0.82
6122.64	(-1.24	(0.09)1.22	5325.27	(-1.22:	(0.31)1.24	4629.35	(0.35)1.54	(0.52)1.50
6116.99	(1.33)1.35	(1.33)1.33	5321.71	(?)0.70	(0.44)0.82	4625.76	(0.41)1.15	(0.37)1.26
6107.93	(?)1.06	(0.57)1.06	5316.77	(-1.15	(0.15)1.15	4596.90	(-1.27	(0)1.23
6100.77	(-1.24?:	(0)0.89	5312.65	(-0.97	(0)0.90	4594.63	(-1.44	(0.06)1.44
6093.14	(0.51)1.43	(0.76)1.45	5310.21	(?)0.76	(0.46)0.84	4581.59	(-1.44	{(0)1.46 -
6086.66	(-1.21	(0.07)1.22	5301.04	(0.60)1.45	(0.55)1.52	4580.13	(-1.26	(0)1.24
6082.43	(-1.34	(0.07)1.34	5292.20	(-1.19:	(0)1.38	4570.02	(-1.24	(0)1.18
6070.67	(-0.79	(0.01)0.80	5287.78	(-1.30	(0.46)1.28	4566.61	(0.75):0.76:	(0.74)0.78
6049.11	(-1.12	(0)0.87	5283.48	(?)1.01	(0.24)1.07	4565.57	(-1.45	(0)1.48
6007.69	(0.46)1.08	(0.37)1.04	5280.63	(-1.07	(0)1.05	4564.15	(-0.92	(0)0.95
6006.35	(-1.18	(0.03)1.12	5276.18	(-0.86	(0)0.84	4552.44	(0.51)?	(0.38)0.38, 1.14
6000.66	(-1.05	(0.04)1.02	5268.49	(-0.80	(0)0.74	4549.65	(-1.46	{(0)1.49 (0)0.60
5991.89	(-1.23	(0.18)1.24	5266.50	(-1.09	(0)1.09	4545.98	(-1.35	(0)1.32
5984.25	(-1.18	{(0)1.12 (0)2.15	5266.30	(-0.88	(0)0.94s	4545.23	(-0.80:	(0)0.80?
5946.48	(-0.41	(0.03)0.43	5267.62	(-1.18	(0)1.18	4543.81	(-1.24	(0.02)1.24
5935.39	(-1.32:	(0)1.30	5254.65	(-1.47	(0.12)1.43	4540.78	(-?)1.00:	(0)0.86
5915.55	(-0.93	(0.15)0.92	5250.00	(-1.35?:	(0)1.45s	4533.98	(-1.50	(0)1.48
5890.48	(-1.17	(0.19)1.14	5247.92	(1.38)1.32	(1.33)1.33	4530.94	(-1.56	(0.09)1.47
5877.42	(-1.29	(0)1.37	5237.08	(-1.35	(0)1.38s	4527.91	(-1.62:	(0)1.87
5876.10	(-0.80	(0)1.08?	5235.18	(-0.92	(0)0.82	4517.09	(0.87)-?, 1.95	(0.84)0.24, 1.93
5846.57	(-1.65	(0)1.53	5230.21	(0.78)1.45	(0.73)1.46	4500.56	(-0.98:	(0)0.86
5830.07	(-1.20	(0.30)1.19	5222.49	(-1.06	(0)1.10s	4494.74	(-1.01	(0)0.98
5826.29	(-2.09?:	(0)1.92s	5219.00	(?)1.80?:	(0)1.97s	4483.91	(-0.68	(0.05)0.66
5790.08	(0.59:?)	(0.56)1.02	5212.69	(-1.33	(0.07)1.34	4478.31	(-1.09	(0)0.1110
5774.37	(?)0.99:	(0.56)1.02	5210.83	(?)0.83	(0.78)0.78	4471.80	(-1.06	(0)1.14
5770.44	(-0.71	(0)0.71	5210.04	(-1.16	(0)1.10	4471.55	(-1.33	(0.02)1.32
5750.95	(-1.12:	(0)1.11	5183.53	(-1.15	(0)1.20	4469.54	(-1.46	(0.22)1.46
5706.16	(-1.20:	(0)1.11	5176.08	(-1.22	(0.20)1.24	4466.88	(-1.42	(0)1.40
5703.03	(?)0.76?:	(1.18)0.76?	5166.06	(-1.22:	(0)1.22s	4431.60	(-0.96	(0.18)0.90
5659.12	(-1.66:	(0)1.67s	5156.36	(-1.11	(0)1.14s	4421.33	(-1.56	(0)1.53
5651.73	(-0.82:	{(0)0.80s (0)0.90	5154.07	(-1.00	(0)1.04	4417.39	(-1.51	(0)1.51
5647.23	(-1.10	(0)1.08	5146.75	(-1.28	(0.09)1.26	4404.93	(0.25)?	(0.22)0.90, 1.35
5637.73	(-1.12	(0)1.16	5133.46	(-1.20	(0)1.22s	4402.67	(-1.23	(0)1.18
5636.12	(-1.08	(0)1.06	5126.20	(-1.07	(0.02)1.04	4395.87	(-0.83?	(0)0.98s
5616.07	(-1.05	(0)1.08	5124.71	(?)1.26	(0)1.36	4391.89	(-1.22	(0.18)1.22
5598.47	(-0.55	(0)0.60	5122.76	(-0.37	(0.08)0.39	4391.56	(-1.52	(0)1.50
5590.74	(0.45)0.98	(0.38)0.96	5108.90	(-1.17	(0.07)1.12	4387.91	(-1.20	(0)1.32
5558.82	(-0.85	(0.04)0.84	5094.95	(-1.30	(0)1.26	4380.07	(-1.34	(0.04)1.34
5546.96	(-1.50?:	(0)1.42	5087.85	(?)1.74:	(0)1.04	4379.26	(?)0.50	(0)0.58
5545.93	(-1.12	(0.38)1.10	4993.00	(?)1.06:	(0.22)1.29	4375.54	(-1.13	(0.04)1.12
5524.99	(-1.25	(0)1.30	4986.44	(?)1.48:	(0.85)1.44	4374.91	(-1.65	(0)1.64
5523.31	(-0.86	(0)0.87s	4979.94	(-0.97	(0)0.97	4373.63	(-0.99	(0)0.90
5515.99	(?)1.08:	(0.28)1.02	4928.29	(?)1.00:	{(0.52)1.36 (0)1.02	4371.13	(-1.58	(0)1.57
5489.66	(-1.18	(0)1.09	4924.99	(-0.86	(0)1.62	4339.62	(0.24)1.23	(0.14)1.24
5488.12	(-1.580?	(0)1.57s	4918.26	(?)0.47	(0.07)1.26	4331.23	(-1.12	(0)1.13s
5483.96	(-1.19	(0)1.16	4915.96	(?)0.86:	(0)0.87	4310.09	(1.05):1.80:	(0.91)1.60
5483.35	(-1.10	(0)1.12	4914.71	(?)0.81:	(0)0.87	4303.23	(-?, 1.10)?	(0.34, 1.02)
			4907.58	(?)0.84:	(0)0.84	4292.25	(-0.96	0.08, 0.76, 1.44 (0)0.96

TABLE V.—Continued.

ZEEMAN EFFECT			ZEEMAN EFFECT			ZEEMAN EFFECT		
λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED
4287.38	(-1.16	(0.38)1.18	3894.07	(-1.02	(0)1.06	3638.34	(-0.98	(0)0.91s
4285.78	(0.77)1.15:	(0.70)1.19	3892.11	(-1.23	(0.15)1.24	3637.31	(0.40)?	(0.40)1.09, 1.88
4276.10	(-0.95	(0)0.98s	3885.27	(0.34)1.13	(0.38)1.10	3636.71	(0.42)1.34	(0.44)1.32
4268.03	(-0.60	(0)0.68	3884.60	(0.22, 0.67)1.51?	(0.21, 0.60)	3634.71	(-0.86	(0)0.82
4252.30	(0.62)1.34	(0.38)1.33			0.28, 1.45	3633.34	(0.57)1.18?	(0.18, 0.55)
4248.18	(0.81)?	(0.76)1.06						1.18, 1.51, 1.86
4207.61	(?)1.14	(0.13)1.10	3881.86	(-0.94)A	(0)0.83s	3632.83	(-1.14	(0)1.01
4190.71	(0.53)1.47	(0.63)1.40	3878.75	(-2.53	(0.08)2.60	3631.94	(0.20)1.10	(0.21)1.08, 1.49
4187.24	(-1.55	{(0)1.54	3876.83	(0.49)1.22, 2.38:?	{(0.55)1.26	3631.39	(-1.50	(0)1.49
4179.22	(-0.94	(0)0.92	3873.95	(-1.14	(0)1.12	3627.80	(-0.91	(0)0.86
4170.88	(-1.09	(0)1.08s	3873.12	(-1.24	(0)1.18	3624.33	(0.47)1.31?	(0.47)1.26, 2.19
4162.16	(-1.24	(0)1.29	3861.16	(-0.80	(0)0.89	3620.42	(-1.85o, B?	(0)1.86s
4158.42	(-0.84	(0)0.86	3851.84	(0.63)1.16	(0.62)1.07	3619.28	(-1.18	(0.41)1.09
4150.42	(-1.42	(0)1.49	3850.09	(?)1.74)1.84?		3615.38	(-0.55i, A	(0)0.35s
4139.45	(-, 1.41)1.56:	(0.47, 1.41)	3845.46	(-1.23	(0)1.16	3611.70	(-0.92	(0)0.93s
		0.62, 1.56, 2.50	3843.69	(-0.49?	(0)0.56	3609.75	(-1.21	(0)1.17
4122.27	(-1.08	(0)1.02	3842.04	(-1.08	(0)1.06s	3605.37	(0.18)1.20	(0.21)1.22
4121.31	(-1.08	(0)1.02	3841.45	(-1.14	(0)1.16	3605.01	(-0.80	(0)0.84
4118.77	(-0.95	(0)0.97	3835.90	(-1.27	(0.06)1.27	3604.46	(-0.95	(0.11)0.92
4110.53	(-0.88	(0.04)0.87	3823.52	(?)1.29, B?		3602.07	(-0.40	(0)0.42
4104.74	(-0.75?	(0.01)0.70	3819.90	(-1.21	(0)1.15	3600.80	(0.53)1.41?	(0.14, 0.42)
4104.41	(0.23)1.19	(0.21)1.16	3817.94	(-1.30	(0.06)1.31			1.05, 1.33, 1.61
4092.84	(0.33)?	(0.32)0.29, 2.36	3816.87	(-1.02?	(0)0.75	3596.51	(-1.25	(0.21)1.26
4092.38	(-1.18	(0.06)1.17	3816.45	(-1.65?	(0)1.75	3594.87	(-1.01	{(0.04)1.04
4086.30	(-1.31	(0)1.30	3816.31	(0.51)1.00, -?	(0.52)0.95, 2.00			(0)1.00
4082.59	(-0.44	(0.03)0.41	3814.45	(0.34)1.65	(0.36)1.60	3591.74	(0.19)1.35	(0.14)1.34
4081.44	(-1.11?	(0)0.99	3813.92	(-1.09?	(0.03)1.24	3587.18	(?)0.95	(0.22)0.91
4077.40	(0.40-)1.30	(0.33)1.30	3812.47	(0.34)1.58?	(0.31)1.72, 2.35	3586.08	(-0.94	(0)0.90
4068.54	(-1.29	(0)1.26	3808.10	(0.18, -, -, -)?	(0.16s)1.92	3585.80	(0.19, -)0.74	(0.17, 0.51)0.77,
4066.36	{(0.90o)	{(0.87s)1.28	3805.77	(0.54)?	(0.44s)1.48			1.11, 1.45, 1.79
	(0.79g)1.26C	(0.74g)	3797.44	(0.92)0.76	(0.91)0.77	3585.15	(0.46)1.34C	(0.47)1.33
4058.60	(0.72)0.53, 1.88:	(0.72)0.62, 1.96	3795.85	(0.42?)1.61?	(0.44)1.29	3581.87	(0.33)0.92?, 1.67?	(0.32)1.01, 1.65
4058.18	(-1.24	(0.03)1.24	3783.73	(?)0.43?	(0.98)1.06	3579.02	(-1.52	(0)1.50s
4057.19	(0.25, 0.74)1.45:	(0.23, 0.69)0.19,	3777.54	(0.46)1.27	(0.28s)1.23	3578.90	(-1.24	(0)1.32s
		0.65, 1.11, 1.57	3774.59	(-1.34	(0)1.37	3569.37	(-1.23	(0.12)1.14
4056.97	(-1.37	(0)1.39	3760.40	(0.42)1.98:	(0.44)1.88	3564.94	(-0.77	(0)0.75
4053.91	(0.38)0.47	(0.28)0.42	3755.44	(-1.40	(0)1.39	3564.11	(-0.86	(0)0.89
4052.91	(-1.29	(0.22)1.30	3754.34	(0.22, 0.71)?	(0.23, 0.69)	3562.09	(0.66)0.61,	(0.24, 0.72)
4045.38	(-1.47o)B?	{(0)1.45s			0.14...1.52			1.05, 1.52
	{-1.34g}B?	{(0)1.24g	3752.78	(-0.55	(0)0.60	3560.89	(0.40, 1.21)	(0.40, 1.20)
4035.54	(-1.10?	(0)1.08	3751.62	(0.39)1.17	(0.57)1.15			0.00, 0.78, 1.59
4027.03	(-1.33	(0)1.28	3749.93	(0.18)1.31o	(0.19)0.90, 1.28	3558.77	(0.34)1.02	{(0.35)0.96
4023.39	(0.83)	(0.79)1.75	3745.49	{(0.82o)1.01C	{(0.73s)1.06			(0.45)1.39
4020.80	(-1.33	(0.04)1.34	3740.18	(0.66g)0.86	(0.62g)1.06	3552.98	(0.51)1.34?	(0.48)1.30
4013.94	(1.34)1.33	(1.36)1.32			(0.13, 0.39)	3552.72	(0.47	(0.46s)2.05
4010.95	(?)0.87?	(0.44)1.32			0.44...1.22	3550.59	(0.34, 0.93)	(0.31, 0.94)0.10,
4003.59	(0.29)0.91, 1.49	(0.25)0.93, 1.43	3735.92	(-1.44	(0)1.42s			0.73, 1.36, 1.99
3997.90	(-1.87o, B	(0)1.91s	3734.13	(-1.12	(0)1.23	3548.43	(-1.60	(0.02)1.64
3995.30	(-1.20	(0)1.18	3733.48	(-1.16	(0)1.14s	3546.70	(-1.51	(0)1.50s
3991.68	(-0.96	(0)0.97	3732.39	(-1.53B	(0.28)1.56			1.12g
3991.52	(-1.17	(0)1.16	3731.26	(-1.10	(0.10)1.12	3543.25	(-1.05g)A	(0)0.90s
3990.29	(0.35)1.35	(0.32)1.36	3730.47	(-1.36	(0)1.33			{(0)1.12
3987.11	(-1.54	(0)1.52	3728.84	(0.50)1.21	(0.51)1.19	3534.76	(-1.20	{(0.24)1.19
3979.51	(-1.38	(0)1.36s	3728.84	(0.24, 0.63)	(0.20, 0.59)	3533.35	(-0.70	(0)0.70
3978.86	(-1.26?	(0)1.26	3726.65		1.06...2.23	3530.55	(-0.75?	(0.03)0.66
3978.65	(-1.05	(0)1.08				3529.81	(-1.04	(0)1.02
3977.75	(-0.95?	(0)0.99	3712.17	(-0.73g	(0)0.34s	3529.03	(-0.98	(0)0.96
3977.18	(0.23)1.35	(0.22)0.90, 1.35	3711.64	(0.99)1.67	(0.98)1.69	3527.94	(-1.31	(0)1.24
3974.72	(0.64o)1.32C?	(0.64s)1.34	3708.82	(-1.12	(0.04, 0.11)	3526.84	(-1.35	(0.11)1.34
3972.50	(-1.25	{(0)1.25			0.92...1.13	3525.87	(0.23)?	(0.15, 0.46)
		-	3707.46	(0.45)0.62, 1.54	(0.47)0.61, 1.56			1.03, 1.96
3969.11	(-1.15	(0)1.12	3704.06	(-1.82o, B	(0)1.77s	3522.85	(-0.97	(0)0.93
3960.99	(-0.91	(0)0.89	3702.23	(-0.93B?	(0)0.98	3521.56	(-1.58B	(0)1.62
3957.92	(0.54, 0.86)	(0.16, 0.47, 0.78)	3693.47	(-1.09	(0.14)1.14	3520.07	(0)1.55	(0)1.57
	- , -, 1.20, -, -	0.57, 0.88, 1.20,	3693.10	(-1.10	(0)1.10	3518.34	(-0.94	(0)0.94s
		1.51, 1.82	3690.71	(-0.84g)A	(0)0.66s	3513.47	(-1.11	(0)1.05
3952.91	{(0.90o)1.05	{(0.87s)1.04	3686.47	(0.39)-?, 1.78	(0.36)1.04, 1.75	3512.64	(-1.02	(0)0.92
	{(0.74g)1.05	{(0.74g)1.04	3684.96	(0.50)1.26:, 2.07:	(0.50)1.18, 2.17	3510.42	(0.53)?	(0.47)1.35
3947.12	(0.74)0.87?, 2.25?	(0.75)0.72, 2.22	3684.47	(-1.41	(0)1.39	3506.31	(-1.20	(0)1.08
3946.63	(-1.25	(0)1.24	3684.47	(-1.25	(0.11)1.26	3504.72	(0.32)1.15	(0.49)1.12
3945.32	(0.13, -, -)1.81o, B	(0.14, 0.42, 0.70)	3676.55	(-1.04	(0)1.04	3503.71	(-0.95?	(0.09)0.92
		0.46...1.86	3670.04	(1.25)1.40	(1.27)1.41	3495.68	(-0.84B	(0)0.96
3942.68	(-1.26	(0)1.28	3662.15	(-1.13	(0)1.08	3491.31	(0.49?, 1.23)	(0.38, 1.14)
3941.72	(-1.14	(0)1.11	3660.69	(0.58:)?	(0.66)1.49			0.04, 0.80, 1.58
3940.88	(0.41?, 1.21)	(0.39, 1.17)	3657.91	(0.17)1.22o	(0.18)0.87, 1.24	3490.73	(0.20, 0.56, 0.92)	(0.18, 0.55, 0.92)
	0.00, 0.80, 1.67	0.01, 0.79, 1.57	3656.96	(0.19, 0.53, -)	(0.18, 0.55, 0.92)			2.17s
3938.85	(-1.26	(0)1.27		-?, 2.20:	0.49...2.34	3489.39	(-1.15	(0)1.12
3935.96	(-1.89o, B	(0)1.88s	3654.44	(0.37)1.10, 1.90	(0.38)1.09, 1.85	3487.71	(-0.42i, A	(0)0.45i
3935.28	(0.57)?	(0.55)1.48	3652.54	(-1.73o, B	(0)1.72s	3485.70	(0.34)1.19?	(0.32)1.15, 1.78
3929.25	(-1.31	(0.30)1.31	3651.25	(-0.93	(0)0.88	3485.36	(-1.16	(0)1.14
3925.15	(0.34)-?, 1.70	(0.32)1.00, 1.65	3649.32	(-1.02	(0)1.04	3483.41	(-1.45B	(0)1.44
3922.75	(-0.89	(0.20)0.90	3648.14	(-0.83	(0.15)0.84	3480.01	(0.19, 0.62)	(0.19, 0.56)
3917.11	(0.26)1.20	(0.28)1.23	3647.65	(0.31, 0.91)	(0.30, 0.91)0.11,	3478.74	(0.66)?	0.95...2.06
3909.93	(-1.40	(0)1.38		-?, 0.73, 1.37, 1.96	0.72, 1.33, 1.94	3478.55	(0.23, 0.62)	(0.25, 0.75)0.08,
3906.28	(0.86o)1.37C	(0.12, 0.36, 0.60)	3647.08	(0.26)-0.94, 1.50	(0.25)0.93, 1.42	3475.83	(-1.25	0.58, 1.08, 1.58
		1.37, 1.61	3643.18	(-1.10	(0.06)1.11	3477.83	(-1.25	(0.22)1.26
3898.48	(-1.69?	(0)1.70	3641.78	(-1.30	(0)1.34	3476.36	(0.25:)-1.18	(0.24)1.19
3894.97	(0.20)0.24, 0.66	(0.20)0.20, 0.60	3639.44	(0.22, 0.55)	(0.15, 0.45)0.72			
				0.51, 0.81, -	1.02, 1.32, 1.62			

TABLE V.—Continued.

ZEEMAN EFFECT			ZEEMAN EFFECT			ZEEMAN EFFECT		
λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED
3474.53	(0.38)1.13?	(0.35)1.12	3338.51	(-1.31	(0.08)1.36	3219.15	(0.16)1.20	(0.26)1.22
3474.01	(-1.40	{(0)1.46	3337.17	(0.66)1.30g}A?	(0.67)1.25g	3216.99	(-1.47	(0)1.52
3471.38	(-1.32	{(0)1.31			(0.67)0.53s	3210.85	(-1.15	
3469.68	(-1.08	(0.09)1.33	3334.14	(-2.09o)B	{(0)1.97s	3210.21	(-1.10	(0.04)1.10
3465.79	(-1.17	(0)1.04s			(0)1.66g	3205.88	(-1.06	(0)1.06
3463.49	(-1.08	(0)1.16			(0.34)0.97	3203.02	(0.53)1.29	(0.41)1.34
3462.80	(0.26, 0.80)	(0.75)0.41, 1.91	3333.38	(1.06)	{(1.05)1.10	3199.32	(0.79)1.25	(0.74)1.22
	0.69, 1.24, 1.80	(0.27, 0.82)0.13,			(0)0.80	3198.66	(-1.65o)B	(0)1.80s
		0.68, 1.23, 1.78	3329.46	(-1.44	(0.24)1.44		(-1.51g)	(0)1.38g
3461.17	(-1.14	(0)1.15	3329.01	(-)?, 1.28, -?	(0)1.29	3196.42	(?)1.18	(0.17)1.20
3458.02	(-1.20o, B?	(0.20)1.24	3328.20	(0.44)1.31	(0.51)1.28	3193.16	(0.29)1.20	(0.38)1.18
3456.92	(0.83o)?C	(0.91s)1.14	3326.99	(-1.45	(0.09)1.45	3192.22	(0.43)-, 1.06, 1.90	(0.42)1.05, 1.89
3456.52	(-1.06	(0.04)1.08	3326.56	(-1.04?	(0)0.65	3191.29	(-0.68	(0)0.74
3455.23	(-0.66o, B	(0)0.63s	3325.24	(0.60)0.90, 2.04?	(0.60)0.88, 2.08	3190.91	(-0.63	(0)0.70
3453.51	(-1.19	(0)1.15			(0.22)1.17	3189.75	(1.20)0.00,	(0.39, 1.17)
3448.35	(-1.20	(0.03)1.14	3322.19	(-1.10	(0.30)1.07		0.80, 1.60	0.03, 0.81, 1.59
3446.08	(-1.05	(0)1.06	3321.91	(-1.34	(0)1.35s	3188.37	(0.32, 0.91)0.00,	(0.32, 0.96)-0.13
3443.64	(0.64)1.15	(0.65)1.14	3319.82	(-1.52	(0)1.50		0.53, 1.11, 1.73	0.51, 1.15, 1.79
3442.91	(-0.95	{(0)0.95	3319.47	(-1.04	(0)1.05	3186.35	(0.41)0.97	(0.37)0.96
3438.90	(-1.01	(1.33)1.33	3319.15	(-1.06	(0)1.06	3185.94	(-1.74	(0)1.69
3438.71	(-1.10	(0)1.02	3318.39	(0.91)0.82, 1.71?	(0.21, 0.62, 1.03)	3182.11	(0.78)0.35, 1.88	(0.78)0.34, 1.90
3435.75	(0.38)1.50	(0.48)1.50			0.62, 1.03, 1.44,	3180.29	(0.54)0.61?, 1.64,	(0.54)0.55, 1.63
3433.04	(-0.46	(0.10)0.44	3315.03	(0.66)1.36	(0.42s)1.19		2.61?	
3432.31	(-0.89?	(0)0.98			- - -	3177.26	(-0.93	
3431.58	(-1.14	(0)1.17	3314.07	(-0.88	{(0)0.37	3174.90	(0.68)1.29	(0.64)1.36
3428.22	(-1.12	{(1.11)1.42	3313.11	(1.47)0.77	(0.03)0.86	3174.14	(-1.03	(0)1.22
3426.45	(-1.42	(0)1.42			(1.37)0.77, 3.51	3173.14	(0.48)1.30	(0.49)1.19, 2.17
3424.50	(-1.58	(0)1.60	3312.82	(0.46)1.46	(0)1.88	3169.76	(-1.05	(0)1.06
3422.90	(0.28?, 0.95?)0.63?	(0.28, 0.83)0.34,	3312.14	(0.51)0.95, 2.00?	(0.51)0.96, 1.97	3168.06	(-1.17?	(0)1.20
		0.89, 1.44, 1.99	3308.81	(-1.40	(0.31)1.40	3161.65	(-1.17	(0)1.14
3421.62	(?)1.30?	(0)1.34s	3308.48	(-1.24	(0)1.25	3159.66	(0.18)0.57	{(0)0.52
3420.79	(0.56)1.45	(0.57)1.41	3307.15	(-1.60	(0)1.60			(0.17)1.00
3420.47	(0.78?)	(0.79)1.44	3306.40	(-1.55	(0)1.50s	3158.77	(-0.98g)A	(0)1.00g
3417.67	(0.50)1.21	(0.50)1.20	3305.73	(-1.20	(0)1.22		(-0.85i)	(0)0.82s
3417.15	(0.32-)0.98	(0.20)1.00	3305.10	(0.49-)0.39 or 1.12	(0)1.00	3154.79	(-1.06	(0)1.05
3414.73	(0.60)	(0.63s)0.61s	3304.79	(?)1.31?	(0)1.00	3154.67	(-1.07	(0)1.06
3409.17	(0.28)1.26	(0.26)1.20	3304.11	(-0.61?	(0)0.98s	3152.70	(1.32)1.33	(1.34)1.34
3406.89	(0.28)1.09	(0.36)2.01	3303.88	(0.50)1.15, 2.07?	(0.52)1.10, 2.14	3152.12	(?)1.82?	(0.88)1.02
3405.12	(-1.37	(0.07)1.33	3298.68	(1.26)1.40	(1.26)1.42	3149.31	(-0.90	(0)0.94
3402.06	(0.72)0.96	(0.26)0.94	3294.53	(0.80)1.87	(0.84)0.23, 1.91	3147.06	(-1.03	(0)1.00
3401.91	(0.31?, 0.89?)0.22?	(0.32, 0.95)	3294.09	(?)1.36?	(0.92)0.44?	3145.02	(0.65?)	(0.74)0.44, 1.92
		0.30, 2.19	3293.86	(0.92)0.44?	(0.98)1.06	3140.71	(0.50)2.15?	(0.49)2.19
3401.61	(0.34-)0.17?	(0.35s)0.03s	3293.21	(-1.01g)A?	(0)0.63s	3139.94	(-1.08	{(0.12
3400.47	(0.80-)	(0.79)0.93, 2.51			(0.72)0.53, 1.96	3137.75	(0.64)0.94	{(0.49)1.30
3395.37	(-0.83	(0)0.84	3292.08	(0.73)0.55	(0)0.63s	3137.32	(-1.16o)B	{(0.59)0.89, 2.07
3390.79	(-0.46	(0)0.48	3287.57	(-1.37	(0)1.36		(-0.99g)	{(0)1.17s
3390.39	(0.69)0.39	(0.70)0.39, 1.78	3287.19	(0.30)1.32	(0.41)1.32	3129.48	(1.66?)	{(1.67s)1.16
3388.16	(0.32, 0.83)0.76	(0.29, 0.86)0.19	3283.77	(-1.46	(0)1.42	3127.25	(-1.79	(0)1.72
	1.34, 1.93*	0.76, 1.33, 1.90	3283.46	(-1.13	(0)1.17s	3126.72	(-1.46	(0)1.53
3385.21	(0.26, 0.78, 1.30)	(0.26, 0.79, 1.32)	3283.32	(-1.26	(0)1.28	3121.56	(-1.42B?)	(0)1.41
	0.43, 0.95, 1.49,	-0.07, 0.46, 0.99,	3279.25	(-1.47	(0)1.48	3121.41	(-1.24	(0)1.16
	2.02, 2.68	1.52, 2.05, 2.68	3278.84	(0.67)0.68	(0.67)0.65, 2.00	3118.24	(-1.38	(0)1.44s
3383.90	(1.06)1.45	(1.07)1.42	3277.66	(0.19)1.43	(0.48)1.42	3113.47	(-1.54	(0)1.58s
3382.07	(0.37)1.01, 1.77	(0.35)1.04, 1.74	3277.30	(0.65)1.33	(0.68)1.34	3110.82	(?)1.64	(0)1.74s
3381.49	(-1.11	(0.04)1.12	3276.48	(-0.95g)A	(0)0.94g	3109.50	(0.80)0.96, 1.48	{(0.27, 0.81)
3378.73	(-0.89	(0)0.97s			(0)0.56s		1.99	{(0.91, 1.46, 1.99
3378.35	(-0.39	(0)0.30	3271.77	(-1.26	(0)1.28			{(0)1.48
3377.06	(-0.94g)A?	(0)0.94g	3270.19	(-1.30	(0.38)1.34	3107.54	(-?)0.71	(0.02)0.71
3374.30	(0.65)1.35	(0.86)1.42	3268.89	(?)0.60i	(0)0.50s	3107.04	(-1.13	(0)1.14
3373.96	(1.26)?	(1.35)1.33	3265.35	(-1.29	(0)1.28	3105.92	(?)1.55?	(0)1.61
3373.22	(0.20)1.08	(0.19)1.14, 1.51			(0.18)0.91, 1.27	3103.98	(-?)1.55	(0.22)1.59
3370.32	(-1.23	(0)1.22	3264.84	(0.22)0.87?, 1.29	(0)1.86	3103.73	(0.45)1.38	(0.48)1.39
3367.11	(0.12, -,-,-)2.37o, B	(0.15i)2.42s			(0)1.31	3102.40	(0.32)1.60	(0.34)1.60
3365.01	(0.61)0.94?, 2.25?	{(0.50)1.18, 2.18	3264.71	(-1.62	(0.14)1.67	3099.66	(-1.42	(0)1.41
		(0.32)1.00, 1.64	3263.21	(0.30)1.18	(0.55)1.14	3098.19	(0.74)0.89	(0.72)0.88
3364.25	(0.13)1.15	(0.13)1.14			(0)0.64g	3098.70	(1.07)0.77, 1.45	(0.33, 0.99)
3363.76	(0.61)0.65:	(0.97)1.40	3260.81	(-0.67g)A	(0)0.44s			0.76, 1.42, 2.08
3362.79	(0.44)1.39	(0.78)1.46			(0)0.44s	3096.40	(0.66)0.70, -?	(0.66)0.66, 1.99
3361.55	(-0.58A	(0)0.26	3258.41	(0.99)1.16?	(0.87)1.16	3095.71	(-0.86A?)	(0)0.82s
3359.28	(-1.17	(0)0.74	3258.03	(-1.57	(0.20)1.60	3090.25	(0.83)0.24?	(0.82)0.23, 1.86
3358.00	(-1.73?	{(0)1.36	3254.20	(-1.39	(0)1.37	3089.59	(0.60)1.11	(0.71)1.15
	(-1.18?	(0)1.14	3253.41	(?)0.76?	(0.66)0.81, 1.12			{(0)0.58
3356.84	(-1.11	(0)1.10	3251.65	(-1.68?	(0)1.68	3088.67	(-0.70	{(0)0.98
3356.46	(-1.26	(0)1.30	3249.99	(-1.29	(0)1.32s	3087.80	(1.24)1.54	(1.16)1.52
3355.11	(-0.58	(0.16)0.52			(0)1.32s	3087.77	(-0.45	(0.07)0.44
3354.37	(-2.18o, B	(0)2.00s	3247.17	(-1.31	{(0)1.32	3086.39	(-2.17o)B	{(0)2.33s
3351.53	(-1.36	(0.07)1.34			(0)0.45		(-2.05g)	{(0)1.98g
3348.11	(-1.57	(0)1.56	3246.99	(0.28)1.35	(0.31)1.36	3082.61	(-1.14	(0)1.10s
3347.57	(-0.66	(0)0.66	3243.84	(-1.51	(0.09)1.52			{(0.56)1.24
3346.93	(-1.42	(0.19)1.46	3243.57	(0.33)1.34	(0.36)1.36, 2.08	3079.39	(-1.66	{(0)1.76
3342.73	(-1.26	(0)1.24	3237.02	(-0.86g)D	(0)0.83g	3073.52	(0.67)1.11, 1.48,	(0.24, 0.71)1.01,
3341.94	(-0.92g)A	(0)0.98g			(0)0.55s		1.90	1.48, 1.95
3341.34	(-1.04	(0)1.02	3235.78	(?)1.65	(1.02)1.65			(0.25s)1.00
3339.78	(0.41)0.94	(0.16, 0.48, 1.12)	3235.53	(-0.99A?	{(0)1.08	3072.34	(0.32)0.97	(0.56)0.62
		0.37, 2.61			(0)1.02	3071.95	(0.58)-, 0.63, -	
			3234.11	(-1.33?	(0.20)1.40	3064.37	(-1.00	(0)0.97
			3232.87	(-1.49	(0)1.42	3062.19	(-1.29	(0)1.36
			3227.75	(-1.17	(0)1.22	3061.82	(0.30)1.21	(0.32)1.22
			3226.98	(0.35)1.03	(0.28)0.97	3060.04	(-1.20	(0)1.25
			3224.63	(-1.79	(0)1.74	3056.66	(?)1.21	(0)1.21

* Zeeman pattern from Rybar, Physik. Zeits. 12, 889 (1911).

TABLE V.—*Concluded.*

ZEEMAN EFFECT			ZEEMAN EFFECT			ZEEMAN EFFECT		
λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED	λ	OBSERVED	CALCULATED
3054.72	(-0.75	(0)0.70s	2878.55	(0.70)0.69, 2.03	(0.68)0.64, 2.00	2591.68	(-0.89	(0)0.86s
3050.93	(-1.90B?	(0)1.93	2872.49	(-0.75	(0)0.64	2590.59	(-1.07	(0)1.05
3050.49	(0.66)0.88, 1.98	(0.21, 0.63)	2862.60	(0.22)0.96	(0.20)1.00	2585.33	(-0.78	(0.07)0.84
	1.73	0.84, 1.96, 1.68	2859.65	(-2.02:	(0)1.87	2574.35	(0.58)1.34	(0.49s)1.34
3048.88	(0.30, 0.87)	(0.29, 0.87)0.18,	2850.94	(0.58)0.67	(0.55)0.62	2572.23	(-1.52	(0)1.49
	0.72, 1.33, 1.95	0.76, 1.34, 1.92	2850.04	(-0.64A?	(0)0.61	2567.34	(0.74)1.19	(0.75s)1.20
3048.10	(0.40?)0.94, 2.05	(0.55)0.91, 2.02	2842.38	(0.35)-, 1.10, 1.83	(0.36)1.10, 1.83	2562.12	(?)0.00, 0.83,	(0.41, 1.33)
3044.00	(-1.32	{(0)1.32	2837.15	(-0.92g	(0)0.98g		1.64	0.01, 0.83, 1.65
		{ - -	2833.92	(-1.32	(0)1.37	2556.76	(-1.73	(0)1.35
3042.48	(0.30, 0.82, 1.33)	(0.27, 0.82, 1.37)	2828.46	(-0.85	(0)1.37	2555.07	(-1.79o)B	(0)1.78s
	0.43, 0.95, 1.52,	-0.11, 0.44, 0.99,	2826.79	(-?)1.13	(0)1.12s	2553.33	(-1.43	(0)1.36g
	2.08, 2.60	1.54, 2.09, 2.64	2823.64	(-1.22		2553.00	(-1.37	(0)1.44
3040.81	(?)1.42:	(0.94)1.42	2821.74	(?)0.95	(0)0.97s	2549.29	(0.49, 1.45)	(0.49, 1.47)-0.42,
3039.56	(-1.80	(0)1.87	2820.00	(-0.63	{(0)0.66		0.50, 1.40, -?	0.56, 1.54, 2.52
3038.30	(?)0.71	(0)0.68s	2818.59	(?)1.10?	(0)1.23	2548.33	(-1.06	(0)1.04s
3034.43	(-1.39?	(0)1.39s	2815.55	(0.57)1.29	(0.56s)1.33	2544.25	(-1.53?	(0)0.53
3031.28	(0.40)1.58	(0.39)1.61	2814.97	(-1.77:	(0)1.66	2536.50	(-1.21	(0.03)1.24
3028.18	(-1.45		2803.77	(0.81)1.15	(0.77s)1.20	2535.96	(-0.91	(0)0.91
3026.37	(-0.72g)A	{(0)0.80g	2797.08	(-1.60	{(0.20)0.90	2535.35	(-0.95	(0.41)1.23
	(-0.49i)	{ 0.41s	2792.43	(-1.22	(0)1.15	2532.17	(-0.46	(0.06)0.42
3023.59	(-1.50	(0)1.46	2785.89	(-?)0.43	(0)0.43s	2531.36	(-1.12:	(0)1.07s
3022.35	(-0.87	(0)0.88	2778.81	(-1.54	(0.02)1.50	2521.96	(-1.20	(0)1.16
3017.54	(-2.02o, B	(0)2.07s	2774.96	(-0.56	(0)0.51	2513.11	(-1.21	(0)1.28
3017.25	(-0.78:	(0)0.78	2772.69	(-1.15		2512.90	(-1.30	(0.26)1.20
3015.68	(-1.60	(0)1.58	2766.38	(-0.87	(0)0.89	2507.67	(-?)?, 2.00	(0)1.94s
3013.59	(-2.31o, B	(0)2.34s	2766.21	(-0.88	(0.12)0.88	2506.87	(0.77)?	(0.74)0.87
3006.52	(-1.18	(0.74)1.20	2764.18	(-1.17	(0)1.22	2504.51	(-1.24	(0)1.36
3005.97	(-1.48		2763.06	(-0.97		2496.71	(-1.04	(0)1.06
3005.76	(0.45)1.41	(0.35)1.42	2761.36	(-1.06	(0)1.00s	2495.55	(-1.69	(0)1.62
3000.54	(0.98)1.18C	(0.94)1.11	2758.53	(?)1.62	(0.29)1.58	2494.73	(-1.51	(0)1.52
2999.71	(-1.98	(0)2.15s	2752.07	(-0.79	{(0)0.79	2493.93	(-0.74	(0)0.72
2996.94	(?)0.90	(0)0.95	2746.02	(-1.16	{(0)0.86s	2489.24	(?)0.62	(0.62s)
2996.54	(-2.01	(0)2.18s	2745.09	(-1.24	(0.26)1.22	2483.61	(0.70)1.11	(0.74)1.12
2995.24	(?)1.05	(0)1.09	2740.45	(-1.05	(0)1.07	2476.64	(-1.54	(0)1.58
2995.15	(-0.87	(0.24)0.86	2731.11	(0.39)0.95	(0.39)0.95	2476.43	(-1.43	
2989.59	(0.64)1.24	(0.59)1.24	2728.75	(-1.00	(0)1.02	2473.90	(-1.51	(0)1.49
2987.16	(-1.94o)B	{(0)1.88s	2722.10	(-1.29	(0)1.27s	2472.92	(?)2.29	(0)2.62s
	(-1.65g)	{ 1.60g	2719.58	(-?)1.37	(0)1.42	2467.68	(-1.51	(0)1.48
2982.26	(-0.43	(0)0.42	2715.98	(-1.07	(0.30)1.07	2460.80	(-1.95o, B	(0)1.97s
2978.95	(0.80-)1.91	(0.72)1.96	2695.84	(-1.49	(0)1.52	2460.19	(?)1.64	(0)1.64
2978.01	(-1.33	(0)1.32	2685.33	(-1.52	(0)1.49	2456.23	(0.67)1.25	(0.72s)1.26
2977.46	(0.60-)1.40:	(0.84)1.42	2679.75	(-0.91	(0)1.02	2441.04	(?)1.03	
2975.46	(0.64)1.15	(0.78)1.46	2678.91	(?)1.23	(0)1.22	2435.09	(-1.07	
2971.36	(?)1.05?		2661.71	(-1.30	(0)1.24	2432.21	(-0.96?, 1.56?	(0.09)1.26
2969.61	(-1.33	(0)1.32	2650.26	(-0.42	(0.06)0.42	2429.22	(-0.44iA	(0)0.37s
2967.67	(-0.95	(0)0.99	2649.93	(-0.64	(0)0.62	2428.99	(-1.39	
2955.38	(0.67)0.78	{(0)1.21	2648.63	(-0.95	{(0)1.04	2426.99	(-1.52	
		{ - -	2646.41	(-1.23	{(0.04)1.34	2424.93	(-1.31	(0.11)1.33
2929.50	(-1.11	(0.04)1.10	2629.97	(0.77)1.30	(0.74)1.33	2422.56	(-1.05	(0.04)1.65
2928.81	(?)2.52	(0)2.62s	2627.63	(-1.14	(0)1.17s	2413.18	(-0.45	(0)0.46
2927.66	(-1.23	(0)1.25	2622.43	(-1.88	(0)1.94s	2410.50	(-0.80	
2919.55	(-0.75	(0)0.78	2617.85	(1.11)0.87?	(1.07)0.78	2402.16	(-1.54	{(0)1.47
2911.56	(?)1.10:	(0)1.17	2613.49	(-1.26		2402.05	(-1.56	{(0)1.56
2907.67	(?)1.36	(0.50)1.40	2606.12	(-0.51	(0)0.53s	2384.85	(?)1.48	{(0)1.46
2903.19	(0.50)1.04	(0.48)1.04	2600.97	(-1.63	(0)1.69s	2380.48	(0.69)1.12	{(0.86)1.12
2899.81	(-1.22	(0)1.18				2369.67	(-1.07	{(0)1.11
2892.24	(-1.21					2365.05	(0.54-)1.25	{(0.52)1.25
2886.44	(0.26)1.19	(0.44)1.20				2350.28	(-1.47	(0)1.51
2885.30	(?)1.49	(0.66)1.49						
2882.21	(0.71)1.05	{(0.73)1.07						
		{(0.31)1.12						

i Inside component. A n component shaded outward.
o Outside component. B n component shaded inward.
g Center of gravity of pattern. C p component shaded inward.
s Strongest component calculated. D p component shaded outward.
: Doubtful value.

we have given term designations are not given by Catalan and Antunes. Each of the low terms b^2G and c^2D accounts for 42 lines. Most of the higher levels are confirmed by from three to ten combinations; g^4H_{61} and $x^2H_{51}^0$ have but two, and e^6H_{71} only one (§5).

Six levels to which they have given designations (in the pentads discussed in §5) are placed in our list of unclassified levels—either because of irregular intensities in the multiplets or because other levels, in a more probable position,

were discovered. We have been constrained to reject as unreal five of their high odd levels (four in this pentad) and the low c^2D at 22,247, 23,392, which they regarded as doubtful. Of our 37 unclassified odd levels, all but two are new. More than two-thirds of these depend on the new measures in the ultraviolet.

8. ZEEMAN DATA

The observed separations are given in Table V. The g values given in Table IV were found from

TABLE VI. The *g* sums for Co I.

CONFIG.		$d^7s,$ $d^8s,$ d^9	$d^8(^3F),$ $d^7s(^3F),$ $d^7s(^3F) + 4p$	OTHER ODD TERMS	HIGH EVEN TERMS	ALL TERMS
J $\frac{1}{2}$	<i>N</i>	4	5	13	1	23
	<i>O</i>	6.71	2.73	17.80	-0.71	26.53
	<i>T</i>	6.67	2.67	17.33	-0.67	26.00
$1\frac{1}{2}$	<i>N</i>	9	11	19	7	46
	<i>O</i>	9.33	9.55	24.63	7.30	50.81
	<i>T</i>	9.33	9.33	25.07	7.33	51.06
$2\frac{1}{2}$	<i>N</i>	8	16	15	15	54
	<i>O</i>	9.81	17.26	17.79	17.39	62.25
	<i>T</i>	9.71	16.85	17.89	17.55	62.02
$3\frac{1}{2}$	<i>N</i>	5	16	12	18	51
	<i>O</i>	5.45	19.24	13.55	21.70	59.94
	<i>T</i>	5.40	19.14	13.74	21.27	59.55
$4\frac{1}{2}$	<i>N</i>	5	11	8	14	38
	<i>O</i>	5.82	14.18	8.54	17.13	45.67
	<i>T</i>	5.80	14.00	8.56	17.49	45.85
$5\frac{1}{2}$	<i>N</i>	1	5	2	9	17
	<i>O</i>	1.09	6.66	2.20	11.38	21.33
	<i>T</i>	1.09	6.62	2.18	11.36	21.34
$6\frac{1}{2}$	<i>N</i>		1		4	5
	<i>O</i>		1.40		5.06	6.46
	<i>T</i>		1.39		5.13	6.51
$7\frac{1}{2}$	<i>N</i>				1	1
	<i>O</i>				1.34	1.34
	<i>T</i>				1.33	1.33
All	<i>N</i>	32	65	69	69	235
	<i>O</i>	38.21	71.02	84.51	80.59	274.33
	<i>T</i>	38.00	70.00	84.77	80.79	273.56

these in the usual manner, starting with the unresolved patterns, and then using the formulae of Shenstone and Blair¹² in the case of unresolved patterns, when it appeared probable that the mean of a blend had been observed; or sometimes the formulae for the strongest line when this was probably observed. The computed patterns are derived from these empirical *g* values. For unresolved patterns, the center of gravity of the group is usually given. When the strongest component is entered instead, it is denoted by *s*. When two assignments are given in Table VIII, both calculated patterns are entered here.

The accuracy of the *g* values may be estimated by comparison with those of Roth and Bartunek.¹³ Grouping the levels according to their *J* values the mean differences in the sense authors'

¹² A. G. Shenstone and H. A. Blair, Phil. Mag. 8, 765 (1929); H. N. Russell, Phys. Rev. 36, 1590 (1930).

¹³ F. L. Roth and P. F. Bartunek, Phys. Rev. 47, 526 (1935).

values minus those of *R* and *B* are as follows in units of 0.01.

<i>J</i> No.	$\frac{1}{2}$ 7	$1\frac{1}{2}$ 20	$2\frac{1}{2}$ 26	$3\frac{1}{2}$ 21	$4\frac{1}{2}$ 15	$5\frac{1}{2}$ 6	$6\frac{1}{2}$ 1
Alg. mean	-4.3	-1.7	+0.8	+0.4	-0.5	+0.6	(+2)
Arith. mean	±5.7	±3.5	±2.5	±1.5	±1.4	±1.0	(±2)
Comp.	6.8	3.4	2.3	1.7	1.4	1.1	

The accuracy increases steadily with *J*, which is to be expected, for the displacement of the strongest *n* component of a resolved pattern is $J_1g_1 - J_2g_2$ and that of an unresolved blend is $\frac{1}{2}\{(J+1)g_1 - J_2g_2\}$. The observations therefore determine, on the average, the value of $(J+x)g$, where *x* should be of the order of $\frac{1}{2}$. The values of $6.8/(J+\frac{1}{2})$ are given in the last line and closely represent the observed mean discordances. The average value of *J* is 2.9, corresponding to a discordance of ±0.02 in the *g* values. If the two sets of determinations were of equal accuracy, the probable error of either would be ±0.012, confirming Roth and Bartunek's statement: "Most of the *g* factors are estimated to be reliable to about 0.01."

Most of the *g* values are in good agreement with those derived from the elementary theory (*LS* coupling). The *g* sums for various configurations are given in Table VI. Here for each group of configurations *N* is the number of levels of given *J* for which reliable *g* values were derived (omitting the doubtful values marked with colons in Table IV), *O* the sum of the observed *g* values, and *T* that of those from *LS* coupling. For the first two sets of configurations *g* values have been found for all the levels, so that the *g* sum test is strictly applicable. For the others some levels are missing and the test is not exact. The excess of *O* above *T* for the first two sets suggests that the observed values may be about one percent too great; but the others do not confirm this.

TABLE VII. Conspicuous examples of the sharing of *g* values.

TERM	LEVEL	<i>O</i> - <i>T</i>	TERM	LEVEL	<i>O</i> - <i>T</i>
$b^4P_{1\frac{1}{2}}$	15,774	-0.26	$y^4S^0_{1\frac{1}{2}}$	46,562	-0.75
$a^2D_{1\frac{1}{2}}$	16,470	+0.29	$v^4D^0_{1\frac{1}{2}}$	46,260	+0.28
			$v^2D^0_{1\frac{1}{2}}$	46,186	+0.38
$b^4P_{2\frac{1}{2}}$	15,184	-0.10	$e^2D_{2\frac{1}{2}}$	52,460	-0.28
$a^2D_{2\frac{1}{2}}$	16,778	+0.08	$f^2F_{2\frac{1}{2}}$	52,970	+0.27
$x^2F^0_{2\frac{1}{2}}$	43,425	+0.16	$g^2F_{3\frac{1}{2}}$	52,763	-0.21
$w^4D^0_{2\frac{1}{2}}$	43,242	-0.20	$e^4H_{3\frac{1}{2}}$	52,716	+0.26

TABLE VIII. Arc spectrum of cobalt (Co I).

REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION
1	11,894.93	10	8404.65	$c^2D_{13} - y^2D_{03}$	2	9544.52	300	10,474.35	$y^2F_{03} - e^2F_{03}$
1	11,630.93	40	8595.41	$c^2D_{23} - y^2D_{03}$	2	9527.17	10h	10,493.42	$w^4F_{03} - i^4F_{03}$
1	11,508.4	6h	8686.9	$b^2G_{43} - z^2F_{03}$	2	9517.33	1	10,504.27	$\{w^4F_{03} - e^2D_{03}\}$ $\{x^4G_{03} - g^2F_{03}\}$
1	11,402.20	3h	8767.84		2	9513.42	1	10,508.59	$w^4F_{03} - f^4F_{03}$
1	11,318.27	40	8832.85	$c^2D_{23} - y^2F_{03}$	2	9482.75	1	10,542.57	$x^4P_{03} - g^4P_{03}$
1	11,305.0	2h	8843.2	$b^2G_{43} - y^4D_{03}$	2	9470.74	2	10,555.94	$b^4F_{03} - z^2D_{03}$
1	11,158.6	2	8959.2	$b^4P_{13} - z^2F_{03}$	2	9454.23	3h	10,574.38	$w^4D_{03} - g^4F_{03}$
1	11,106.34	8	9001.40	$y^2D_{03} - e^4F_{03}$	2	9442.34	4h	10,587.69	$x^4G_{03} - e^2G_{03}$
1	11,094.7	3h	9010.8		2	9435.70	3	10,595.15	$x^4G_{03} - h^4F_{03}$
1	11,091.94	50	9013.09	$y^2D_{03} - e^4F_{03}$	2	9428.8	1	10,602.9	$x^2F_{03} - f^4G_{03}$
1	11,085.4	1h?	9018.4	$w^4D_{03} - e^2G_{03}$	2	9422.60	3h	10,609.87	$w^4F_{03} - f^4G_{03}$
1	11,081.1	1h?	9073.5	$z^4P_{03} - e^4F_{03}$	2	9406.12	4h	10,628.46	
1	11,015.9	2h	9075.3	$w^4D_{03} - f^4F_{11}$	2	9395.11	2	10,640.92	$x^4P_{03} - g^4P_{03}$
1	10,957.0	2h	9124.1	$x^4F_{03} - e^4F_{03}$	2	9356.98	200	10,684.28	$a^2H_{03} - y^4G_{03}$
1	10,946.88	10h	9132.52		2	9351.06	3	10,691.04	
1	10,935.42	4	9142.10	$b^4P_{03} - z^2F_{03}$	2	9347.88	2h	10,694.68	$w^4F_{03} - f^2F_{03}$
1	10,805.9	10h	9251.7	$x^4F_{03} - g^4F_{03}$	2	9344.93	20	10,698.06	$a^2H_{03} - y^4G_{03}$
1	10,785.4	3h	9269.3	$a^2D_{13} - z^2D_{03}$	2	9340.54	3h	10,703.09	$w^4F_{03} - i^4F_{03}$
1	10,771.3	1?	9281.4	$x^4F_{03} - g^4F_{03}$	2	9319.53	2	10,727.21	$w^4F_{03} - f^2F_{03}$
1	10,739.0	6h	9309.3	$x^2F_{03} - h^4F_{03}$	2	9280.42	5	10,772.42	$y^2F_{03} - e^2F_{03}$
1	10,713.4	1	9331.6	$y^2F_{03} - e^4F_{03}$	2	9262.5	2	10,793.3	$b^2D_{13} - y^4F_{03}$
1	10,692.6	3h	9349.7	$x^4F_{03} - e^4G_{03}$	2	9258.18	4	10,798.30	$x^4F_{03} - e^4H_{03}$
1	10,681.82	30h	9359.14		2	9245.60	1	10,812.99	$b^2D_{03} - z^2G_{03}$
1	10,660.17	30	9378.14	$c^2D_{23} - y^2D_{03}$	2	9233.64	1	10,827.00	$a^2P_{13} - z^2F_{03}$
1	10,561.3	2	9465.9	$w^4D_{03} - h^4F_{03}$	2	9207.96	1	10,857.19	$x^4F_{03} - e^2H_{03}$
1	10,521.3	3h	9501.9	$b^2D_{13} - y^4D_{03}$	2	9204.11	5	10,861.73	$b^2D_{03} - z^2F_{03}$
1	10,471.96	15	9546.69	$y^2F_{03} - e^4F_{03}$	2	9185.95	2	10,883.21	$x^4G_{03} - h^4F_{03}$
1	10,447.39	4h	9569.15	$w^4F_{03} - h^4F_{03}$	2	9181.75	5	10,888.19	$x^4F_{03} - e^2H_{03}$
1	10,442.11	20	9573.99	$b^2G_{03} - z^2F_{03}$	2	9177.93	20	10,892.72	$x^4G_{03} - z^2F_{03}$
1	10,398.38	4h	9614.25	$x^4G_{03} - e^4H_{03}$	2	9165.52	2	10,907.46	$x^4F_{03} - g^2F_{03}$
1	10,382.16	50	9629.27	$b^2D_{13} - z^2F_{03}$	2	9133.24	6	10,946.02	$x^4F_{03} - h^4F_{03}$
1	10,367.95	2	9642.47	$x^4F_{03} - e^4D_{03}$	2	9130.50	2	10,949.30	$b^2G_{03} - y^2G_{03}$
1	10,364.4	1	9645.8	$x^4G_{03} - e^4H_{03}$	2	9111.64	1	10,971.96	$y^2G_{03} - e^4F_{03}$
1	10,354.45	60	9655.04	$y^2F_{03} - e^4F_{03}$	2	9095.37	50	10,991.59	$a^2H_{03} - y^4F_{03}$
1	10,348.1	1?	9661.0	$x^4F_{03} - f^2F_{03}$	2	9071.35	4h	11,020.70	
1	10,335.39	4h	9672.85	$w^4D_{03} - g^4F_{03}$	2	9052.44	2	11,043.72	$b^2D_{13} - y^4F_{03}$
1	10,332.66	3h	9675.40	$x^4G_{03} - e^4G_{03}$	2	9040.0	1	11,058.9	$x^4G_{03} - h^4F_{03}$
1	10,276.80	4h	9728.00	$x^4F_{03} - e^4G_{03}$	2	9037.87	50	11,061.52	$a^2H_{03} - y^4F_{03}$
1	10,172.85	20h	9827.39	$x^4F_{03} - e^4D_{03}$	3	9032.70	1	11,067.86	$x^2D_{03} - e^2G_{03}$
1	10,167.58	200	9832.48	$y^2D_{03} - e^2F_{03}$	2	8986.51	3	11,124.74	
1	10,154.90	2	9844.77	$x^4G_{03} - e^2H_{03}$	2	8972.89	7	11,141.63	$w^4F_{03} - e^4G_{03}$
1	10,152.95	4	9846.66	$w^4F_{03} - h^4F_{03}$	2	8958.37	15	11,150.68	$y^4F_{03} - e^4F_{03}$
1	10,131.37	2	9867.63	$b^4P_{13} - z^2D_{03}$	2	8953.72	2	11,165.48	$y^4F_{03} - 5h^4F_{03}$
1	10,128.06	150	9870.86	$y^2D_{03} - e^2F_{03}$	2	8939.14	5	11,183.69	$w^4D_{03} - h^4F_{03}$
1	10,111.0	1h	9887.5	$x^4G_{03} - e^2G_{03}$	2	8926.21	50	11,199.89	$b^2D_{13} - z^2D_{03}$
1	10,105.43	2	9892.96	$x^4G_{03} - e^4G_{03}$	2	8904.63	30	11,227.03	$x^4G_{03} - h^4F_{03}$
1	10,092.1	3h	9906.0	$x^4F_{03} - e^4F_{03}$	2	8892.49	1	11,242.36	$a^4D_{03} - e^4F_{03}$
1	10,078.62	100	9919.28	$a^2H_{03} - z^2G_{03}$	2	8888.70	8h	11,247.15	$x^4D_{03} - e^2H_{03}$
1	10,052.98	8	9944.58	$x^4F_{03} - e^4H_{03}$	2	8878.28	3	11,260.35	$x^4F_{03} - h^4F_{03}$
1	10,048.80	3	9948.71	$x^4F_{03} - e^4H_{03}$	2	8870.70	8	11,269.98	$x^4F_{03} - g^2F_{03}$
1	10,046.31	150	9951.18	$b^2D_{03} - z^2F_{03}$	2	8856.56	3	11,287.96	
1	10,031.45	5	9965.92	$b^4P_{13} - z^2D_{03}$	2	8850.70	30	11,295.44	$y^2F_{03} - e^2F_{03}$
1	10,021.47	4h	9975.84	$x^4F_{03} - e^4G_{03}$	2	8837.90	4h	11,311.80	
1	10,019.08	30h	9978.22	$x^4F_{03} - e^4G_{03}$	2	8835.21	20	11,315.25	$x^4F_{03} - e^4F_{03}$
1	10,007.80	3	9989.47	$a^2H_{03} - y^4G_{03}$	2	8819.11v	100	11,335.90	$x^4G_{03} - h^4F_{03}$
2	9952.2	3h	10,045.3	$\{x^2F_{03} - e^4F_{13}\}$ $\{x^4G_{03} - e^2G_{03}\}$	4	8779.20	3	11,387.44	$w^4F_{03} - e^2G_{03}$
2	9940.69	2	10,056.91	$w^4F_{03} - h^4F_{03}$	2	8774.71	2	11,393.26	$x^4D_{03} - e^4P_{03}$
2	9918.1	1	10,079.8	$w^4D_{03} - e^2D_{03}$	2	8772.04	2	11,396.73	$w^4F_{03} - 4z^2$
2	9912.73	10	10,085.28	$b^4P_{03} - z^2D_{03}$	2	8766.55	4h	11,403.87	$x^4D_{03} - e^4D_{03}$
2	9909.52	1h	10,088.54	$w^4F_{03} - f^4P_{03}$	2	8759.58	3	11,412.94	
2	9890.92	30	10,107.51	$b^2D_{03} - y^4D_{03}$	2	8750.13	60	11,425.27	$x^4G_{03} - h^4F_{03}$
2	9859.90	1	10,139.31	$z^2F_{03} - h^4F_{03}$	2	8745.56	8	11,431.24	$x^4G_{03} - e^4F_{03}$
2	9852.5	1	10,146.9	$z^2F_{03} - f^4D_{03}$	2	8744.37	10	11,432.80	
2	9847.7	2	10,151.9	$x^4F_{03} - e^4F_{03}$	2	8733.27	40	11,447.32	$x^4G_{03} - h^4F_{03}$
2	9823.52	4h	10,176.86	$x^4F_{03} - f^2F_{03}$	2	8722.12	2	11,461.96	$x^4F_{03} - h^4F_{03}$
2	9798.37	2h	10,202.98	$x^4F_{03} - e^4H_{03}$	2	8678.65	3	11,519.37	$x^4G_{03} - i^4F_{03}$
2	9785.39	40	10,216.52	$w^4F_{03} - f^4G_{03}$	2	8675.02	20	11,524.19	$z^2D_{03} - e^4F_{03}$
2	9769.0	1h	10,233.66	$w^4F_{03} - i^4F_{03}$	4	8661.06v	60	11,542.76	$b^2D_{03} - z^2D_{03}$
2	9764.53	5h	10,238.34	$z^2F_{03} - e^2G_{03}$	2	8658.14	3	11,546.66	$b^2D_{03} - y^4F_{03}$
2	9746.02	100	10,257.79	$a^2H_{03} - z^2G_{03}$	2	8655.73	3h	11,549.87	$x^4F_{03} - e^2H_{03}$
2	9735.53	2	10,268.84	$z^2F_{03} - h^4F_{03}$	2	8648.79	4	11,559.14	$a^2P_{13} - z^2D_{03}$
2	9729.54	3	10,275.16	$w^4F_{03} - i^4F_{03}$	3	8596.09	3h	11,630.00	$x^4F_{03} - h^4F_{13}$
2	9696.60	5	10,310.07	$\{b^2D_{13} - z^2D_{03}\}$ $\{w^4F_{03} - f^4G_{03}\}$	4	8589.78v	50	11,638.55	$\{x^4F_{03} - e^4F_{03}\}$ $\{x^4F_{03} - h^4F_{03}\}$
2	9694.0	2	10,312.8	$w^4F_{03} - f^4G_{03}$	4	8586.68v	30	11,642.75	$z^2D_{03} - e^4F_{03}$
2	9678.21	10h	10,329.66	$x^4F_{03} - z^2F_{03}$	4	8575.32v	50	11,658.17	$a^2H_{03} - y^2G_{03}$
2	9670.20	2	10,338.21	$x^4F_{03} - e^4G_{03}$	4	8574.46v	50	11,659.34	$a^2H_{03} - y^2G_{03}$
2	9659.94	3	10,349.20	$w^4F_{03} - i^4F_{03}$	3	8569.72	18	11,665.79	$\{z^2G_{03} - e^4F_{03}\}$ $\{x^4G_{03} - e^4F_{03}\}$
2	9629.83	3h	10,381.56		5	8559.07	10	11,680.31	$x^4F_{03} - e^4F_{03}$
2	9613.46	4	10,399.23	$w^4F_{03} - h^4F_{03}$	5	8513.52	5h	11,742.80	$z^2G_{03} - e^4F_{03}$
2	9606.52	5	10,406.74	$x^4F_{03} - f^4D_{03}$	5	8489.50	30	11,772.02	$x^4F_{03} - h^4F_{03}$
2	9597.90	200	10,416.09	$y^2F_{03} - e^2F_{03}$	3	8478.45	8	11,791.37	$x^4G_{03} - e^2F_{03}$
2	9592.3	2h	10,422.2	$x^4F_{03} - e^2G_{03}$	3	8454.71	1	11,824.48	$\{w^4D_{03} - 3z^2\}$ $\{x^4F_{03} - h^4F_{03}\}$
2	9585.28	2	10,429.81	$w^4F_{03} - e^2D_{03}$	3	8409.03	10Wh	11,888.71	$w^4D_{03} - 3z^2$
2	9580.63	3	10,434.87	$w^4F_{03} - f^4D_{03}$	3	8379.44v	35	11,930.69	$x^4G_{03} - f^4G_{03}$
2	9569.00	5h	10,447.55						$y^4F_{03} - e^4F_{03}$
2	9548.66	4	10,469.80						

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION
4	8378.34v	50	11,932.26	$y^4G_{03} - e^4F_{03}$	5	7704.92	12	12,975.16	$a^2H_{43} - y^2F_{03}$
4	8372.79v	80h	11,940.18	$y^4F_{03} - e^4F_{43}$	5	7701.90	12	12,980.24	$b^2P_{13} - y^4F_{03}$
5	8345.55	20h	11,979.15	$y^4F_{03} - e^2F_{03}$	5	7695.94	10h	12,990.29	$x^2F_{03} - e^4P_{03}$
5	8342.63	50Wh	11,983.33	$x^4G_{03} - f^4G_{03}$	3	7685.65	1	13,007.69	$z^2P_{03} - e^4P_{03}$
5	8331.69	20	11,999.07	$a^2D_{03} - z^2F_{03}$	5	7648.08	12h	13,071.59	$y^4G_{03} - e^2F_{03}$
3	8318.55	5Wh	12,018.03	$x^4F_{03} - f^4P_{03}$	3	7641.43	1	13,082.96	$y^4F_{03} - e^2F_{03}$
5	8315.35	20	12,022.66	$z^2D_{03} - e^4F_{13}$	3	7637.63	4	13,089.47	
5	8301.45	5h	12,042.79	$x^4F_{03} - i^4F_{13}$	5	7634.50	3	13,094.84	$z^2F_{03} - e^4F_{23}$
4	8298.95v §§	60h	12,046.41	$x^4G_{03} - f^4H_{03}$	5	7618.64	2	13,122.09	$b^2G_{03} - y^2F_{03}$
4	8296.82v	50h	12,049.50	$x^4G_{03} - f^4H_{43}$	3	7616.13	1	13,126.42	$x^4F_{03} - e^6D_{03}$
5	8283.48	50h	12,068.90	$x^4G_{03} - f^4H_{03}$	5	7610.24	2-IV	13,136.58	$b^2P_{13} - z^2D_{03}$
3	8275.55	8h	12,080.47	$x^4F_{03} - f^4G_{03}$	3	7606.30	2-V	13,143.38	$\{z^2F_{03} - e^2F_{03}\}$
5	8272.38	5h	12,085.10	$x^4G_{03} - f^6F_{03}$	3	7604.30	1	13,146.84	$\{z^2G_{03} - e^4F_{23}\}$
5	8269.38	80h	12,089.48	$x^4G_{03} - f^4H_{03}$	3	7600.11	1	13,154.09	$w^4D_{03} - e^4P_{03}$
3	8243.38	1	12,127.62	$x^4F_{03} - 1_{03}$	3	7594.18	1	13,164.36	$x^4G_{03} - e^6G_{03}?$
4	8208.57v	80	12,179.05	$y^4F_{03} - e^4F_{13}$	3	7590.57	2-III	13,170.62	$x^4F_{03} - 4_{03}$
4	8192.97v	125	12,202.24	$y^4G_{03} - e^4F_{03}$	3	7588.71	1	13,173.85	$a^2D_{03} - z^4D_{03}$
5	8189.32	10h	12,207.68	$x^4G_{03} - i^4F_{03}$	5	7586.72	20	13,177.31	$b^2P_{13} - y^4G_{03}$
5	8167.88	20Wh	12,239.71	$x^4F_{03} - f^4G_{43}$	5	7586.72	20	13,177.31	$b^2D_{13} - y^2F_{03}$
5	8160.65	40	12,250.57	$y^4G_{03} - z^2F_{03}$	3	7578.34	1	13,191.88	$z^2G_{03} - e^2F_{03}$
3	8154.31	10h	12,260.09	$x^4G_{03} - i^4F_{43}$	5	7564.96	20	13,215.21	$x^4D_{03} - h^4F_{43}$
4	8151.95v	60	12,263.64	$y^4F_{03} - e^4F_{23}$	5	7561.06	15	13,222.03	$y^4D_{03} - e^4F_{03}$
5	8150.19	50	12,266.29	$b^2G_{43} - y^2F_{03}$	5	7559.65	15	13,224.49	$y^4D_{03} - e^4F_{13}$
5	8140.43	40	12,280.99	$b^2P_{13} - z^2F_{03}$	4	7553.48	4-IV	13,234.43	$z^2F_{03} - e^4F_{03}$
5	8137.08	80	12,286.05	$x^4F_{03} - f^4G_{03}$	5	7526.29	1-IV	13,270.43	$y^4D_{03} - e^2F_{03}$
4	8116.37v	80	12,317.40	$y^4G_{03} - e^4F_{43}$	5	7526.29	2	13,283.11	$z^2D_{03} - e^2F_{03}$
5	8114.04	10h	12,320.93	$x^4G_{03} - e^6H_{03}$	3	7524.07	1	13,287.03	$x^4F_{03} - 5_{13}$
3	8112.13	5Wh	12,323.83	$z^2F_{03} - e^4F_{03}$	3	7515.28	1	13,302.56	$w^4D_{03} - e^4P_{03}$
4	8093.932v	8-III	12,351.54	$y^4G_{03} - e^4F_{43}$	5	7502.72	3h	13,324.84	$x^4D_{03} - h^4F_{13}$
5	8085.54	5h	12,364.36	$x^4F_{03} - f^4D_{03}$	5	7489.37	10	13,348.59	$x^4D_{03} - h^4F_{03}$
3	8082.60	1	12,368.86	$x^4F_{03} - f^4G_{23}$	3	7484.00	1	13,358.16	$x^4D_{03} - e^2F_{03}$
5	8080.23	60	12,372.49	$z^2G_{03} - e^4F_{03}$	3	7478.77	3	13,367.51	$b^2P_{13} - z^4F_{03}$
5	8066.49	60	12,393.56	$z^2D_{03} - e^2F_{03}$	3	7471.21	1	13,381.03	$y^4F_{03} - e^6F_{03}$
3	8062.98	5Wh	12,398.96	$x^4G_{03} - 4_{03}$	4	7457.342v	6-V	13,405.92	$z^2G_{03} - e^4F_{03}$
4	8055.996v	2-V	12,409.71	$y^4F_{03} - e^4F_{23}$	5	7443.43	10h	13,430.97	$x^4D_{03} - h^4F_{03}$
3	8053.50	2h	12,413.55	$\{z^2D_{03} - e^6G_{43}\}$	5	7437.16	1-III A	13,442.29	$b^2P_{13} - z^2F_{03}$
5	8050.76	5Wh	12,417.77	$x^4D_{03} - e^2F_{03}$	5	7429.00	10	13,457.05	$x^4F_{03} - e^6G_{43}$
4	8043.306v	2-V	12,429.28	$y^4F_{03} - e^4F_{13}$	4	7417.38v	10-II	13,478.14	$a^2D_{13} - z^4D_{03}$
5	8041.37	20	12,432.28	$b^2D_{03} - e^4F_{13}$	3	7406.23	1	13,498.43	$e^2D_{13} - z^4D_{03}$
5	8037.64	10h	12,438.04	$\{a^2D_{03} - z^2F_{03}\}$	3	7398.72	1	13,512.14	$e^2D_{13} - z^4F_{03}$
4	8029.217v	80	12,451.10	$y^4D_{03} - e^4F_{43}$	4	7388.689v	5-III	13,530.48	$y^4G_{03} - z^2F_{03}$
5	8024.73	40	12,458.05	$y^4F_{03} - e^2F_{03}$	3	7365.77	1	13,572.58	$b^2G_{03} - e^2F_{03}$
5	8022.087v	40	12,462.16	$z^2D_{03} - e^2F_{03}$	4	7354.579v	3-III	13,593.23	$b^2P_{13} - z^4F_{03}$
5	8017.86	15h	12,468.73	$x^4F_{03} - h^4F_{03}$	5	7353.47	25	13,595.28	$y^4D_{03} - e^2F_{03}$
5	8016.56	15h	12,470.76	$x^4F_{03} - i^4F_{03}$	3	7351.55	1	13,598.83	$x^4D_{03} - h^4F_{03}$
5	8012.99	20Wh	12,476.31	$x^4F_{03} - i^4D_{03}$	3	7349.68	1	13,602.29	$x^4F_{03} - e^6H_{03}$
4	8007.239v	5-V	12,485.27	$y^4G_{03} - e^4F_{03}$	5	7315.73	25	13,665.42	$a^2D_{03} - z^4D_{03}$
5	7998.09	12h	12,499.55	$x^4F_{03} - e^6D_{43}$	3	7307.86	1	13,680.13	$x^4F_{03} - 4_{03}$
5	7996.80	10h	12,501.57	$\{a^2G_{03} - z^4G_{03}\}$	5	7285.28#	4-IV	13,722.53	$b^2D_{03} - y^2D_{03}$
4	7987.36v	5-III	12,516.34	$\{x^4G_{03} - e^6H_{43}\}$	5	7263.58	6	13,763.53	$x^4F_{03} - e^6G_{03}?$
3	7984.22	1	12,521.27	$a^2D_{03} - z^2D_{03}$	5	7250.12	1-III A	13,789.08	$b^2P_{13} - z^4F_{03}$
3	7980.57	3h	12,526.99	$x^4G_{03} - 5_{13}$	5	7217.34	8	13,851.71	$b^2P_{13} - z^2D_{03}$
5	7966.08	40	12,549.77	$x^4F_{03} - e^6P_{03}?$	4	7193.56v	4-V	13,897.50	$y^4D_{03} - e^2F_{03}$
3	7962.40	3Wh	12,555.58	$y^4F_{03} - e^2F_{03}$	3	7185.63	1Cr?	13,912.84	$x^4D_{03} - h^4F_{03}$
5	7960.55	25h	12,558.50	$x^4F_{03} - e^6G_{03}$	3	7173.37	1	13,936.61	$x^4D_{03} - h^4D_{03}$
5	7957.76	40h	12,562.90	$x^4F_{03} - i^4F_{43}$	4	7159.153v	6-V	13,964.29	$z^2F_{03} - e^2F_{03}$
4	7926.525v	3-V	12,612.40	$y^2G_{03} - e^2F_{03}$	4	7154.688v	8-II	13,973.00	$a^2D_{13} - z^4D_{03}$
5	7919.48	15h	12,623.62	$x^2D_{03} - g^4P_{03}$	4	7134.290v	5-V	14,012.96	$a^2D_{03} - e^2F_{03}$
4	7912.90	1	12,634.12	$x^2D_{03} - g^4P_{03}$	5	7124.47	1-III	14,032.27	$b^2P_{13} - z^4F_{03}$
4	7908.679v	6-III?	12,640.86	$x^4G_{03} - e^4F_{03}$	3	7117.91	2	14,045.20	$x^4D_{03} - h^4F_{03}$
3	7907.14	1	12,643.32	$x^4F_{03} - 1_{03}$	6	7113.98	1	14,052.96	$x^4D_{03} - f^4D_{03}$
5	7885.25	10Wh	12,678.43	$x^4G_{03} - e^4H_{03}$	4	7113.538v	5-V	14,053.84	$z^2F_{03} - e^2F_{03}$
5	7877.49	20	12,690.91		5	7102.55	25	14,075.58	
5	7873.32	10h	12,697.63	$w^4F_{03} - g^4P_{03}$	3	7101.77	1	14,077.12	$x^4D_{03} - i^4F_{23}$
4	7871.370v	2-V	12,700.78	$y^4G_{03} - e^4F_{13}$	3	7097.84	1	14,084.92	$y^2G_{03} - f^4F_{43}$
4	7869.868v	2-V	12,703.20	$y^4G_{03} - e^4F_{03}$	5	7094.53	1-IV	14,091.49	$y^4D_{03} - e^2F_{03}$
3	7866.10	1	12,709.29	$x^4G_{03} - e^6H_{03}$	5	7084.974v	100-I	14,110.49	$b^2P_{13} - z^4D_{03}$
5	7859.39	10Wh	12,720.14	$x^4G_{03} - e^6G_{03}$	5	7079.20	10	14,122.00	$x^4D_{03} - e^6P_{13}$
5	7960.55	25h	12,558.50	$x^4F_{03} - i^4F_{43}$	5	7070.41	20	14,139.56	$x^4D_{03} - i^4F_{43}$
5	7957.76	40h	12,562.90	$x^4F_{03} - i^4F_{43}$	5	7055.88	25	14,168.68	$x^4D_{03} - f^4G_{03}$
4	7926.525v	3-V	12,612.40	$y^2D_{03} - g^4P_{03}$	4	7054.042v	10-III	14,172.37	$b^2D_{03} - y^2D_{03}$
5	7919.48	15h	12,623.62	$x^2D_{03} - g^4P_{03}$	4	7052.872v	60-I	14,174.72	$b^2P_{13} - z^4D_{03}$
4	7912.90	1	12,634.12	$x^4F_{03} - e^4F_{03}$	5	7042.58	5h	14,195.43	$y^4D_{03} - e^6F_{43}$
4	7908.679v	6-III?	12,640.86		5	7032.52	25	14,215.74	$x^4D_{03} - 1_{03}$
3	7907.14	1	12,643.32		4	7027.797v	6-V	14,225.29	$z^2G_{03} - e^2F_{03}$
5	7885.25	10Wh	12,678.43		4	7016.602v	35-I	14,247.99	$b^2P_{13} - z^4D_{03}$
5	7877.49	20	12,690.91		5	7015.18	5	14,250.88	$x^4D_{03} - 2_{13}$
5	7873.32	10h	12,697.63		5	7004.81	3-III	14,271.98	$a^2D_{13} - z^4D_{03}$
4	7871.370v	2-V	12,700.78		5	6997.22	4d-V	14,287.45	$x^4D_{03} - f^4D_{03}$
4	7869.868v	2-V	12,703.20		3	6977.02	1	14,328.82	$b^2P_{13} - z^2G_{03}$
3	7866.10	1	12,709.29		3	6972.70	1	14,337.70	$x^4D_{03} - f^4G_{03}$
5	7859.39	10Wh	12,720.14		5	6946.31	10	14,392.17	$a^2P_{13} - z^2F_{03}$
5	7855.821v	40h	12,725.92		5	6937.81	4-III	14,409.80	$D_{23} - y^2F_{03}$
4	7843.64	12	12,745.68		5	6910.84	15	14,466.04	$a^2G_{03} - z^2G_{03}$
4	7839.997v	40	12,751.60		5	6908.08	30	14,471.81	$e^2D_{03} - z^4P_{03}$
4	7838.121v	3-V	12,754.66		5	6906.39	1	14,475.36	$x^4D_{03} - f^6F_{13}$
3	7822.12	2Wh	12,780.74		3	6901.52	5	14,485.57	$e^2D_{03} - z^4F_{03}$
3	7818.25	5h	12,787.07		4	6872.32v	40-I	14,547.01	$b^2P_{13} - z^4D_{03}$
3	7817.15	1	12,788.87		5	6864.91	10	14,562.82	$z^4P_{03} - e^4P_{03}$
5	7810.30	10h	12,800.09						
5	7809.24	20	12,801.83						
5	7794.13	5h	12,826.64						
3	7786.63	1	12,839.00						
5	7764.02	12	12,876.38						
5	7743.27	4	12,910.89						
5	7735.45	10h	12,923.94						
5	7734.23	40	12,925.98						
5	7725.95	12	12,939.84						
4	7712.661v	6-III	12,962.13						

TABLE VIII.—Continued.

REF.	λ IA	INT.—TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.—TC	WAVE No. VAC.	MULTIPL DESIGNATION
5	6858.38	25	14,576.69	$z^4P_{03} - z^4P_{23}$	4	6337.963v	5	15,773.59	$z^4G_{03} - z^4F_{23}$
5	6846.97	25	14,600.98	$x^4D_{03} - z^4D_{13}$	8	6322.919	2h	15,811.12	$z^4D_{03} - z^4F_{23}$
3	6845.66	10	14,603.77	$x^4D_{03} - z^4P_{13}$	4	6320.418v	8-IV	15,817.37	$y^4F_{03} - z^4G_{23}$
5	6838.11	15	14,619.89		8	6318.551	4n	15,822.05	$z^4G_{03} - z^4F_{23}$
3	6829.92	1	14,637.43	$a^2G_{03} - z^2F_{03}$	5	6315.779	2h	15,828.99	$b^2P_{13} - z^2F_{03}$
5	6826.96	3	14,643.77	$x^4D_{03} - z^2G_{03}$	4	6314.528v	50	15,832.13	$z^2F_{03} - z^4G_{23}$
5	6819.53	20	14,659.73	$c^2D_{13} - z^2P_{03}$	4	6313.032v	50	15,835.88	$z^2G_{03} - z^4F_{23}$
4	6814.950v	40-I	14,669.58	$b^4P_{13} - z^4D_{03}$	3	6302.50	1	15,862.34	$x^4G_{03} - z^4H_{23}$
5	6808.94	25h	14,682.53	$y^4F_{03} - z^4F_{23}$	3	6296.96	2h	15,876.30	$a^2D_{23} - y^4D_{03}$
3	6807.43	1	14,685.78	$y^2D_{03} - z^4D_{23}$	4	6291.829v	5	15,889.24	$z^4F_{03} - z^4F_{23}$
5	6799.40	6h	14,703.13	$x^4D_{03} - z^4D_{23}$	4	6282.636v	40-I	15,912.49	$a^4P_{13} - z^4D_{03}$
3	6792.35	1	14,718.39	$y^4D_{03} - z^2F_{23}$	5	6278.19	1	15,923.76	$z^4S_{03} - z^4P_{23}$
5	6789.26	15	14,725.09	$x^4D_{03} - 6z$	4	6276.608v	40	15,927.78	$\{z^4D_{03} - z^4F_{23}$ $y^4D_{03} - z^4F_{23}$
5	6784.85	25	14,734.66	$y^4F_{03} - z^4F_{23}$	5	6275.133#	25	15,931.52	$z^4D_{03} - z^4F_{23}$
3	6778.06	1	14,749.42	$x^4D_{03} - z^4F_{23}$	5	6273.026	4-III?	15,936.87	$\{z^2F_{03} - z^4F_{23}$ $z^4G_{03} - z^4F_{23}$
4	6771.040v	50-I	14,764.71	$b^4P_{23} - z^4D_{03}$	7	6271.900	1	15,939.73	$\{a^2G_{03} - y^4G_{03}$ $a^4P_{23} - z^4G_{03}$
5	6767.394	15	14,772.67	$y^4F_{03} - z^4F_{23}$	4	6271.472v	5	15,940.82	$y^2D_{03} - z^4P_{13}$
5	6758.10	25	14,792.99	$c^2D_{13} - w^4D_{03}$	3	6265.97	1	15,954.82	$a^2D_{23} - z^2G_{03}$
5	6756.57	25	14,796.33	$x^4D_{03} - z^4P_{23}$	5	6262.825	5h	15,962.82	$\{a^2P_{13} - z^2D_{03}$ $a^2G_{23} - y^4G_{03}$
5	6742.17	5	14,827.93	$x^4D_{03} - z^4F_{23}$	4	6257.578v	6-III	15,976.22	$z^4D_{03} - z^4F_{23}$
5	6722.71	4	14,870.85	$y^2F_{03} - z^2P_{13}$	4	6257.066v	3	15,977.52	$y^2D_{03} - z^4F_{23}$
5	6720.95	4	14,874.75	$z^2F_{03} - z^2F_{23}$	5	6253.940	2h	15,985.51	$z^4G_{03} - z^4F_{23}$
5	6717.64	5h	14,882.08	$y^4F_{03} - z^4F_{23}$	4	6249.504v	8-II	15,996.86	$a^4G_{23} - y^4G_{03}$
5	6712.71	8h	14,893.01	$x^4D_{03} - 5z$	4	6247.284v	8	16,002.54	$z^4D_{03} - z^4F_{23}$
5	6703.92	15	14,912.53	$x^4D_{03} - 1z$	4	6246.389v	5h	16,004.83	$z^4F_{03} - z^4F_{23}$
3	6700.99	1	14,919.06	$b^4P_{23} - z^4G_{03}$	4	6232.440v	2-IV?	16,040.65	$z^4D_{23} - z^2P_{03}$
5	6692.87	4	14,937.15	$x^4D_{03} - z^4F_{23}$	5	6230.968	10-III	16,044.44	$a^4P_{13} - z^4D_{03}$
4	6684.875v	30	14,955.02	$b^2D_{23} - y^2D_{03}$	4	6223.355v	10	16,064.07	$y^4D_{03} - z^4F_{23}$
5	6684.08	30	14,956.80		5	6222.329	3	16,066.72	$a^4P_{13} - z^4G_{03}$
3	6682.30	1w	14,960.78	$y^2D_{03} - z^4D_{23}$	4	6211.197v	2-IV?	16,095.51	$y^4D_{03} - z^4F_{23}$
3	6680.35	1	14,965.15	$c^2D_{13} - w^4D_{03}$	5	6205.503	3h	16,110.28	$z^4F_{03} - z^4D_{23}$
4	6678.818v	5-II	14,968.58	$b^4P_{13} - z^4D_{03}$	5	6203.701	2h	16,114.96	$x^4G_{03} - z^4H_{23}$
3	6672.96	2	14,981.72	$a^4P_{23} - z^4F_{03}$	5	6197.837	5h	16,130.21	$y^4F_{03} - z^4D_{23}$
5	6665.29	4	14,998.97	$x^4D_{03} - 6z$	4	6193.540v	15	16,141.40	$z^4G_{03} - z^4F_{23}$
5	6663.72	3h	15,002.50	$z^4G_{03} - z^4F_{23}$	4	6189.005v	10-IIA	16,153.23	$a^4P_{23} - z^4P_{03}$
5	6652.29	3h	15,028.28	$y^4G_{03} - z^4F_{23}$	3	6181.90	1	16,171.79	$x^4G_{03} - z^4H_{23}$
3	6649.97	5	15,033.52	$x^4D_{03} - z^4G_{23}$	4	6181.008v	10h	16,174.43	$y^4D_{03} - z^4F_{23}$
5	6645.33	4h	15,044.01	$y^4G_{03} - z^4F_{23}$	5	6175.029	1	16,189.79	$z^4D_{03} - z^4F_{23}$
10	6644.03	1	15,046.96	$z^4G_{03} - z^4F_{23}$	5	6171.43	1	16,199.23	$x^4D_{03} - z^4P_{23}$
3	6638.40	1	15,059.72	$y^4G_{03} - z^4F_{23}$	3	6168.86	2h	16,205.97	$a^2G_{03} - z^2G_{03}$
3	6635.12	25h	15,067.16	$c^2D_{13} - z^2P_{03}$	3	6160.04	1	16,229.18	$a^2G_{03} - z^2D_{03}$
4	6632.438v	15-II	15,073.26	$a^2P_{13} - z^2D_{03}$	3	6158.53	2h	16,233.16	$a^2G_{03} - z^4F_{03}$
4	6623.780v	2-III?	15,092.96	$a^2D_{23} - z^2F_{03}$	3	6146.38	3h	16,265.25	$a^2G_{03} - z^2G_{03}$
6	6623.36	1	15,093.92	$y^4G_{03} - z^4F_{23}$	7	6143.764	5h	16,272.17	$z^4G_{03} - z^4F_{23}$
4	6617.572v	3n-V	15,107.12	$y^2D_{03} - z^4F_{23}$	5	6132.410	10h	16,302.30	$z^4D_{03} - z^4F_{23}$
4	6617.126v	6n-V	15,108.14	$y^2D_{03} - z^4P_{13}$	3	6130.41	1	16,307.62	$a^4P_{23} - z^4G_{03}$
4	6595.869v	12-V	15,156.83	$z^4D_{03} - z^4F_{23}$	4	6129.118v	20w	16,311.06	$a^2D_{13} - z^2F_{03}$
7	6591.834	15	15,166.10	$z^4D_{03} - z^2P_{13}$	4	6128.214v	5	16,313.46	$z^4F_{03} - z^4F_{23}$
3	6588.02	1	15,174.88	$x^4D_{03} - z^4H_{23}?$	4	6122.640v	8-IV?	16,328.31	$z^4F_{03} - z^4F_{23}$
4	6579.373v	15	15,194.83	$y^2D_{03} - z^4F_{23}$	4	6116.994v	8-I	16,343.38	$a^4P_{13} - z^4D_{03}$
4	6563.403v	40-II	15,231.80	$a^2G_{43} - z^2G_{03}$	4	6107.937v	2-V	16,367.62	$y^2D_{23} - z^2D_{03}$
8	6554.840	2n	15,251.70	$y^4F_{03} - z^4F_{23}$	5	6105.470	10h	16,374.23	$a^2G_{43} - z^4F_{03}$
8	6554.382	2n	15,252.76	$x^4D_{03} - 4z$	4	6100.778v	4h	16,386.83	$y^2F_{03} - z^4H_{23}$
4	6551.466v	3-III	15,259.55	$b^4P_{23} - z^4D_{03}$	8	6098.270	3	16,393.56	$x^4G_{03} - z^4H_{23}$
3	6540.64	1	15,284.81	$a^2P_{13} - z^4G_{03}$	4	6093.144v	10-I	16,407.35	$a^4P_{13} - z^4D_{03}$
5	6535.13	2h	15,297.69	$x^4D_{03} - z^4D_{23}$	4	6086.663v	7-II?	16,424.83	$c^2D_{23} - z^2D_{03}$
5	6517.00	3h	15,340.25	$x^4D_{03} - z^4G_{03}$	5	6083.283	2h	16,433.96	$y^2F_{03} - z^2F_{03}$
4	6508.785v	5h	15,359.62	$y^4F_{03} - z^4F_{23}$	4	6082.431v	15-III	16,436.25	$z^4F_{03} - z^4F_{23}$
4	6504.213v	15	15,370.41	$z^4G_{03} - z^4F_{23}$	4	6070.671v	2-V	16,468.09	$z^4D_{03} - z^4D_{13}$
3	6502.29	1	15,374.96	$x^4D_{23} - 5z$	4	6058.233v	3	16,501.90	$z^2G_{03} - z^4F_{23}$
3	6496.18	1	15,389.42	$y^2D_{03} - z^4D_{13}$	4	6049.110v	6-V	16,526.79§	$y^2F_{03} - z^4G_{03}$
4	6490.344v	6-III	15,403.26	$a^2G_{43} - z^2F_{03}$	4	6015.384v	2	16,619.45	$y^2F_{03} - z^4F_{23}$
4	6483.305	1n	15,419.98	$z^2F_{03} - z^4F_{23}$	4	6013.653v	30†	16,624.23	$y^2D_{03} - z^4H_{23}$
4	6482.806	2h	15,421.17	$a^2P_{13} - z^4F_{03}$	4	6011.402v	2h	16,630.46	$z^4D_{03} - z^4F_{23}$
4	6477.861v	10-V	15,432.94	$z^4D_{03} - z^4F_{23}$	4	6007.690v	5-V	16,640.73	$y^2F_{03} - z^2F_{03}$
4	6474.558v	25w	15,440.81	$c^2D_{13} - z^2D_{03}$	4	6006.352v	5-IV?	16,644.44	$z^4F_{03} - z^4F_{23}$
4	6470.128v	3	15,451.38	$y^2D_{03} - z^4D_{23}$	4	6005.030v	8	16,648.11	$a^4P_{23} - z^4D_{03}$
4	6463.060v	25h	15,468.28	$z^4D_{03} - z^4F_{23}$	4	6002.459v	2	16,655.24	$z^4G_{03} - z^4F_{23}$
4	6454.998v	40-III	15,487.60	$z^4D_{03} - z^4F_{23}$	4	6000.668v	5-I	16,660.21§	$z^4F_{03} - z^4F_{23}?$
4	6451.136v	3n-V	15,496.87	$\{a^4P_{23} - z^4D_{03}$ $(a^2G_{23} - z^2G_{03})$ $z^4G_{03} - z^4F_{23}$	4	5996.915v	2	16,670.63	$y^2F_{03} - z^4H_{23}$
4	6450.230v	80-I	15,499.05		3	5993.48	1	16,680.19	$a^2D_{13} - z^4D_{03}$
4	6444.678v	2-V	15,512.40		4	5991.890v	20-III	16,684.62	$a^2D_{23} - z^2D_{03}$
5	6439.171	80	15,525.67		3	5990.46	1	16,688.60	$a^2D_{23} - z^4F_{03}$
4	6431.075v	5h	15,545.21	$y^4G_{03} - z^4F_{23}$	3	5989.58	1	16,691.05	$y^4D_{03} - z^4F_{23}$
7	6430.342	2-V	15,546.98	$y^4D_{03} - z^4F_{23}$	8	5984.582	4n	16,704.99	$c^2D_{23} - w^4F_{03}$
4	6429.913v	4-III	15,548.02	$a^2G_{23} - z^2F_{03}$	4	5984.253v	3-III?	16,705.91	$y^2F_{03} - z^4G_{23}$
5	6425.115	5	15,559.63	$a^2G_{43} - z^4D_{03}$	4	5984.092v	3-III?	16,706.36	$a^4P_{13} - z^4D_{03}$
4	6421.703v	2-V	15,567.90	$y^4D_{03} - z^4F_{23}$	4	5983.278v	2	16,708.63	$z^4F_{03} - z^4F_{23}$
5	6417.824	15-III	15,577.31	$a^2P_{13} - z^2D_{03}$	4	5981.990v	3h	16,712.22	$z^4F_{03} - z^4F_{23}$
9	6414.67	1	15,584.97	$y^2D_{03} - z^4D_{23}$	5	5965.661	2h	16,757.96	$a^2D_{23} - z^4F_{03}$
4	6407.510v	1	15,602.38	$y^2F_{03} - z^4D_{23}$	11	5965.040	2h	16,759.72	$z^4D_{03} - z^4F_{23}$
5	6396.524	2-V	15,629.18	$y^4D_{03} - z^4F_{23}$	3	5963.39	1	16,764.35	$y^2D_{03} - z^4G_{03}$
4	6395.158v	8-V	15,632.52	$z^4D_{03} - z^4F_{23}$	3	5951.73	2	16,797.20	

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPLY DESIGNATION	REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPLY DESIGNATION
4	5935.391v	6-III	16,843.44	$b^4P_{3/2} - y^4D_{3/2}$	4	5489.666v	5-III?	18,211.00	$y^4F_{3/2} - e^4D_{3/2}$
10	5923.13	1	16,878.30	$y^2D_{3/2} - f^2F_{3/2}$	4	5488.121v	1	18,216.12	$y^4F_{3/2} - e^4G_{3/2}$
5	5922.365	3	16,880.48	$b^4F_{1/2} - y^4D_{3/2}$	4	5483.962v	10-V	18,229.94	$z^4D_{3/2} - f^4F_{3/2}$
3	5916.88	2h	16,896.13	$x^4D_{3/2} - g^4G_{3/2}$	4	5483.354v	40-I	18,231.96	$a^4P_{3/2} - y^4D_{3/2}$
4	5915.551v	10-III	16,899.92	$a^2G_{3/2} - e^2F_{3/2}$	9	5479.74	1	18,243.99	$z^4D_{3/2} - h^4F_{3/2}$
4	5905.584v	2h	16,928.45	$z^4D_{3/2} - e^2F_{3/2}$	4	5477.089v	5-V	18,252.82	$z^4D_{3/2} - f^4F_{3/2}$
4	5890.487v	12-III	16,971.83	$a^2G_{3/2} - y^2D_{3/2}$	5	5476.906	400wNi	18,253.42	$(y^2F_{3/2} - e^2F_{3/2})$
3	5886.52	1	16,983.27	$e^2D_{3/2} - y^4F_{3/2}$	10	5476.47	<1	18,254.88	$z^4D_{3/2} - f^4F_{3/2}$
4	5883.421v	3	16,992.22	$a^2D_{1/2} - e^2D_{3/2}$	4	5470.460v	4-V	18,274.92	$z^4D_{3/2} - f^4F_{3/2}$
5	5881.077	2-1?	16,998.99	$a^2G_{3/2} - y^4F_{3/2}$	5	5469.305	4-III A	18,278.79	$b^4P_{3/2} - e^2D_{3/2}$
11	5878.047	1	17,007.75	$b^4P_{1/2} - e^2F_{3/2}$	9	5457.45	1	18,318.50	$y^4F_{3/2} - e^4D_{1/2}$
4	5877.427v	4h	17,009.54	$y^2F_{3/2} - e^2D_{3/2}$	4	5454.573v	20-V	18,328.16	$y^4F_{3/2} - e^4F_{3/2}$
4	5876.102v	4h	17,013.38	$y^2F_{3/2} - e^2D_{1/2}$	4	5453.338v	1	18,332.31	$y^4F_{3/2} - e^4H_{3/2}$
4	5846.575v	2-V	17,099.30	$z^4F_{3/2} - e^4F_{3/2}$	4	5452.305v	3-V	18,335.78	$z^4D_{3/2} - f^4F_{1/2}$
4	5834.628v	1	17,134.32	$y^2G_{3/2} - e^4G_{3/2}$	9	5447.93	1	18,350.51	$z^2D_{1/2} - e^4F_{3/2}$
4	5830.070v	4-V	17,147.71	$z^4F_{3/2} - e^2F_{3/2}$	4	5444.585v	20-IV?	18,361.78	$y^4F_{3/2} - e^4G_{1/2}$
4	5826.299v	3	17,158.81	$z^4F_{3/2} - e^4F_{1/2}$	4	5437.002v	3-III?	18,387.39	$y^4G_{3/2} - e^4D_{3/2}$
3	5818.09	2	17,183.02	$z^4F_{3/2} - e^2F_{3/2}$	4	5434.576v	2-III?	18,395.60	$y^4G_{3/2} - e^4F_{3/2}$
3	5806.34	1	17,217.79	$e^2D_{1/2} - w^2D_{3/2}$	4	5431.027v	2-V	18,407.62	$e^2D_{3/2} - e^4P_{3/2}$
3	5793.92	1Fe?	17,254.70	$y^4F_{3/2} - e^2P_{1/2}$	10	5428.00	0	18,417.89	$z^2F_{3/2} - e^4F_{3/2}$
4	5790.084v	2	17,266.13	$y^2F_{3/2} - e^4H_{3/2}$	12	5427.39	2	18,419.96	$z^2D_{1/2} - e^4G_{3/2}$
4	5774.375v	2	17,313.10	$y^2F_{3/2} - e^2F_{3/2}$	12	5427.21	2	18,420.57	$y^4G_{3/2} - f^2F_{3/2}$
4	5770.443v	2-V	17,324.90	$y^2F_{3/2} - e^4H_{3/2}$	4	5426.734v	1	18,422.18	$b^4P_{1/2} - y^4F_{3/2}$
3	5768.71	1	17,330.10	$z^4F_{3/2} - e^6F_{3/2}$	4	5425.621v	4	18,425.96	$\{y^4F_{3/2} - e^4G_{3/2}\}$
3	5760.39	1	17,355.13	$z^4G_{3/2} - e^6F_{3/2}$	4	5421.98	1	18,438.34	$\{b^2D_{3/2} - x^4D_{3/2}\}$
11	5754.079	1	17,374.17	$y^2F_{3/2} - e^2F_{3/2}$	5	5413.734	2-V	18,466.42	$y^4F_{3/2} - e^4D_{1/2}$
5	5752.883	2h	17,377.78	$z^4G_{3/2} - e^6F_{3/2}$	7	5408.119	2-III?	18,485.59	$z^2G_{3/2} - f^4F_{3/2}$
5	5750.952	2	17,383.61	$y^2D_{1/2} - h^4F_{3/2}$	5	5407.520v	5-V	18,487.64	$a^2P_{1/2} - y^2D_{3/2}$
10	5741.50	1	17,412.23	$z^4D_{3/2} - e^2F_{3/2}$	4	5402.000v	3-V	18,506.53	$y^4G_{3/2} - e^4G_{3/2}$
5	5740.986	2h	17,413.79	$y^2F_{3/2} - h^4F_{3/2}$	4	5399.762v	10	18,514.20	$y^4F_{3/2} - e^4F_{1/2}$
3	5739.59	1	17,418.03	$a^2D_{3/2} - y^4D_{3/2}$	4	5397.729	3h	18,534.91	$y^4F_{3/2} - e^2D_{3/2}$
3	5736.52	1	17,427.35	$y^2G_{3/2} - e^4D_{3/2}$	5	5393.81	2	18,544.95	$z^2G_{3/2} - e^4G_{3/2}$
3	5734.25	1	17,434.25	$e^2D_{1/2} - x^4P_{3/2}$	12	5390.478v	2-IV?	18,546.09	$y^4D_{3/2} - e^4F_{3/2}$
3	5733.28	1	17,437.20	$z^4G_{3/2} - e^6F_{3/2}$	4	5381.105	5-III	18,578.39	$y^4D_{3/2} - e^2P_{1/2}$
3	5730.45	1	17,445.81	$z^4F_{3/2} - e^6F_{3/2}$	4	5378.20	1	18,588.42	$y^4D_{3/2} - e^4G_{3/2}$
3	5720.80	1	17,475.24	$a^2D_{1/2} - y^4F_{3/2}$	5	5373.958v	1	18,603.10	$b^4P_{1/2} - z^2D_{3/2}$
3	5715.91	1	17,490.19	$z^4F_{3/2} - e^6F_{3/2}$	9	5372.75	1	18,607.32	$y^4G_{3/2} - e^4F_{3/2}$
10	5706.160v	1	17,520.07	$y^2F_{3/2} - f^2F_{3/2}$	4	5370.350	1	18,615.60	$z^2D_{3/2} - e^4F_{3/2}$
5	5703.031	2h	17,529.68	$z^4F_{3/2} - e^2F_{3/2}$	4	5369.591v	20-I	18,618.23	$a^2P_{1/2} - y^4D_{3/2}$
3	5696.75	1	17,549.01	$b^4P_{3/2} - z^2G_{3/2}$	4	5368.904v	30	18,620.61	$e^2D_{1/2} - y^2P_{3/2}$
5	5688.593	2-II	17,574.17	$a^2D_{3/2} - z^2D_{3/2}$	4	5366.743v	5	18,628.11	$y^4F_{3/2} - f^2F_{3/2}$
11	5688.169	1	17,575.48	$y^4F_{3/2} - e^4P_{3/2}$	4	5364.816v	4	18,634.80	$z^4D_{3/2} - f^4F_{1/2}$
3	5686.96	3	17,579.22	$z^4F_{3/2} - e^2F_{3/2}$	4	5362.781v	15-III	18,641.87	$z^2G_{3/2} - e^4H_{3/2}$
3	5684.69	1	17,586.24	$y^4F_{3/2} - e^4D_{3/2}$	4	5359.200v	6-III?	18,654.33	$y^4F_{3/2} - e^4F_{1/2}$
10	5681.04	1	17,597.54	$b^4P_{3/2} - z^2F_{3/2}$	4	5358.923	2-IV	18,655.29	$z^2G_{3/2} - f^2F_{3/2}$
3	5679.637	1	17,601.89	$y^2D_{3/2} - h^4F_{3/2}$	5	5358.01	1	18,658.47	$e^2D_{1/2} - w^2F_{3/2}$
3	5676.49	2	17,611.64	$y^4D_{3/2} - z^2F_{3/2}$	9	5353.500v	25-III	18,674.19	$\{z^2G_{3/2} - e^4H_{3/2}\}$
5	5675.421	3h	17,614.96	$y^4F_{3/2} - e^4D_{3/2}$	4	5352.046v	20-III	18,679.26	$\{a^2D_{3/2} - y^2F_{3/2}\}$
4	5659.121v	3-II	17,665.70	$a^2G_{3/2} - y^2G_{3/2}$	4	5349.091v	4-V	18,689.58	$z^4F_{3/2} - e^2G_{3/2}$
3	5656.10	1	17,675.13	$b^4D_{1/2} - x^4D_{1/2}$	4	5347.490v	4-V	18,695.15	$y^4F_{3/2} - e^4G_{3/2}$
5	5651.734	12h	17,688.79	$\{b^4P_{1/2} - z^2D_{3/2}\}$	4	5344.383v	20-III	18,705.39	$y^4G_{3/2} - e^4G_{3/2}$
4	5647.234v	3-II	17,702.88	$\{z^2D_{1/2} - e^2P_{3/2}\}$	4	5342.703v	50-III	18,711.93	$y^4G_{3/2} - e^4H_{3/2}$
5	5643.087	5h	17,715.89	$e^2P_{1/2} - y^2D_{3/2}$	4	5341.328v	7-V	18,716.74	$z^4G_{3/2} - e^4F_{3/2}$
5	5642.542	2h	17,717.60	$e^2D_{1/2} - g^4F_{3/2}$	4	5339.528	4-V	18,723.05	$z^2G_{3/2} - e^2G_{3/2}$
5	5639.991	1-III A	17,725.62	$a^2D_{1/2} - y^4F_{3/2}$	5	5337.330	1n	18,730.76	$z^2G_{3/2} - h^4F_{3/2}$
4	5637.734v	3-V	17,732.71	$y^4F_{3/2} - e^4F_{3/2}$	4	5336.163v	3-V	18,734.86	$y^4G_{3/2} - e^4F_{3/2}$
4	5636.455v	1	17,736.73	$z^2D_{3/2} - e^4F_{3/2}$	4	5334.821v	6-V	18,739.57	$\{y^4G_{3/2} - e^4G_{3/2}\}$
4	5636.128v	3-V	17,737.77	$z^2D_{3/2} - e^2F_{3/2}$	4	5333.647v	5-III	18,743.70	$y^4G_{3/2} - e^4H_{3/2}$
5	5627.726	2	17,764.25	$y^4G_{3/2} - e^4G_{3/2}$	4	5332.652v	5-III	18,747.20	$z^4F_{3/2} - f^4F_{3/2}$
5	5616.077	5	17,801.09	$y^4F_{3/2} - e^4G_{3/2}$	4	5331.456v	15-II	18,751.40	$a^4P_{1/2} - y^4D_{3/2}$
9	5602.26	1	17,845.00	$y^4F_{3/2} - e^2P_{3/2}$	10	5329.82	1	18,757.16	$y^4F_{3/2} - z^4F_{1/2}$
5	5598.478	50Ca?	17,857.05	$b^2G_{3/2} - 1s_{3/2}$	9	5328.01	2-V	18,763.53	$y^4F_{3/2} - e^4F_{1/2}$
4	5594.778v	2	17,868.86	$y^4G_{3/2} - e^4P_{3/2}$	5	5326.247	3-IV	18,769.74	$z^4D_{3/2} - f^4F_{3/2}$
10	5593.13	1	17,874.13	$z^4F_{3/2} - e^6F_{3/2}$	4	5325.949v	4-III	18,770.79	$y^4F_{3/2} - e^4H_{3/2}$
5	5592.185	2	17,877.15	$z^4F_{3/2} - e^6F_{3/2}$	4	5325.276v	10-III	18,773.16	$y^4G_{3/2} - e^4G_{3/2}$
4	5590.744v	10-II	17,881.75	$a^2D_{1/2} - z^2D_{3/2}$	4	5321.719v	2-V	18,785.71	$y^4G_{3/2} - e^2D_{3/2}$
3	5589.27	1g?	17,886.47	$y^4G_{3/2} - e^4D_{3/2}$	4	5316.772v	7-III	18,803.19	$y^4G_{3/2} - e^4G_{3/2}$
3	5581.28	2	17,912.08	$z^2D_{1/2} - e^4D_{3/2}$	4	5312.650v	8-III	18,817.78	$y^4F_{3/2} - e^2F_{3/2}$
11	5576.045	1	17,928.89	$y^2F_{3/2} - h^4F_{3/2}$	4	5310.219v	20	18,826.39	$y^4F_{3/2} - e^4G_{3/2}$
9	5573.65	1	17,936.60	$z^2G_{3/2} - e^4F_{3/2}$	10	5308.55	1	18,832.31	$y^2F_{3/2} - f^4D_{3/2}$
11	5569.678	1Fe?	17,949.39	$b^2D_{1/2} - x^4D_{3/2}$	4	5307.208v	0	18,837.07	$z^2G_{3/2} - f^2F_{3/2}$
3	5565.87	1	17,961.67	$z^4F_{3/2} - e^2F_{3/2}$	4	5301.042v	15-II	18,858.98	$a^4P_{1/2} - y^4D_{3/2}$
4	5563.69	1	17,968.71	$z^4F_{3/2} - e^2F_{3/2}$	4	5292.203	1n	18,890.48	$y^4D_{3/2} - e^2P_{3/2}$
3	5558.825v	2-III?	17,984.42	$e^2D_{1/2} - w^2D_{3/2}$	13	5290.49	0	18,896.60	$a^4G_{3/2} - e^4F_{3/2}$
5	5546.968	4	18,022.88	$y^2G_{3/2} - e^2G_{3/2}$	4	5287.785v	5-V	18,906.26	$y^4D_{3/2} - e^4F_{3/2}$
4	5545.937v	2-III?	18,026.22	$y^4G_{3/2} - e^4F_{3/2}$	5	5287.574	3-V	18,907.02	$z^4D_{3/2} - f^4F_{3/2}$
9	5544.28	1	18,031.61	$e^2D_{1/2} - w^2D_{3/2}$	4	5286.48	1	18,910.93	$y^4F_{3/2} - e^2G_{3/2}$
11	5533.070	1	18,068.14	$y^4F_{3/2} - e^4D_{3/2}$	9	5284.08	1	18,919.52	$y^4D_{3/2} - e^4F_{3/2}$
4	5530.780v	10-II	18,075.62	$a^4P_{3/2} - z^2F_{3/2}$	4	5283.487v	4-V	18,921.64	$y^4G_{3/2} - f^2F_{3/2}$
3	5527.19	1	18,087.36	$y^4F_{3/2} - e^4F_{1/2}$	4	5280.631v	20-III	18,931.88	$z^4G_{3/2} - f^4F_{3/2}$
11	5525.674	1	18,092.33	$e^2D_{1/2} - y^4S_{$					

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION
9	5264.83	1	18,988.69	$y^4G_{23} - e^4G_{23}$	11	4961.891	1	20,148.00	$y^2F_{03} - 4z_1$
4	5264.203v	2-IV	18,990.96	$z^2D_{03} - e^2D_{13}$	4	4959.682v	5	20,156.97	$b^4F_{13} - z^2F_{03}$
6	5262.48	2	18,997.17	$z^2D_{03} - e^2D_{23}$	4	4953.179v	2-IA	20,183.44	$b^4F_{23} - z^2F_{03}$
4	5257.621v	10-III	19,014.73	$y^4D_{03} - e^4P_{23}$	5	4951.828	2	20,188.95	$z^2F_{03} - f^2F_{03}$
4	5254.652v	8-IV	19,025.48	$y^4D_{03} - e^4D_{23}$	4	4948.589v	4	20,202.16	$y^4D_{03} - e^2G_{23}$
10	5253.84	1	19,028.42	$y^4G_{03} - g^4F_{13}$	5	4945.784	4	20,213.61	
4	5250.003v	7-V	19,042.32	$y^4G_{03} - e^4H_{23}$	9	4945.55	1	20,214.57	$b^2G_{43} - w^4D_{03}?$
4	5247.921v	15-II	19,049.88	$a^4P_{13} - y^4D_{03}$	7	4944.735	1n	20,217.90	$b^2G_{23} - x^2F_{03}$
10	5243.541	1	19,065.79	$e^2D_{23} - y^4S_{03}$	5	4943.282	2	20,223.85	$z^2F_{03} - f^2F_{23}$
4	5237.085v	5	19,089.29	$y^4G_{03} - g^2F_{23}$	5	4942.350	2	20,227.66	$y^4F_{03} - h^4F_{23}$
4	5235.188v	15-II	19,096.21	$a^2G_{23} - e^2F_{03}$	9	4941.65	1	20,230.53	$y^4F_{03} - h^4F_{13}$
9	5234.67	1	19,098.10	$y^4G_{03} - e^4G_{23}$	4	4941.354v	3	20,231.73	$z^2D_{03} - h^4F_{23}$
10	5230.363	1	19,113.82	$y^4D_{03} - e^4D_{13}$	4	4936.418v	6	20,251.97	$(y^4G_{03} - e^4H_{23})$
4	5230.210v	25-II	19,114.38	$a^4F_{13} - y^4D_{03}$	5	4935.222	2	20,256.87	$z^2G_{23} - e^4F_{23}$
4	5222.490v	4-IV	19,142.64	$y^4D_{03} - g^4F_{13}$	5	4934.065	25Ba?	20,261.63	
10	5221.243	1	19,147.21	$y^4F_{03} - e^2D_{13}$	4	4932.883v	5	20,266.48	$b^4P_{23} - y^2F_{03}$
4	5219.008v	2-V	19,155.41	$z^2F_{03} - f^4F_{23}$	11	4931.346	1	20,272.80	$b^2D_{13} - x^2F_{03}?$
4	5214.751v	1	19,171.05	$z^2F_{03} - e^4P_{23}$	11	4930.783	3	20,275.11	
10	5214.440	0	19,172.19	$y^4D_{03} - g^4F_{23}$	11	4928.818	1	20,283.19	$(b^2D_{13} - w^4D_{03})$
4	5212.699v	25-III	19,178.59	$z^2F_{03} - f^4F_{23}$	4	4928.290v	2-III	20,285.37	$e^2D_{13} - x^4S_{03}$
4	5211.832v	3-IV	19,181.78	$z^2F_{03} - e^4D_{23}$	4	4925.676	1	20,296.13	$z^2G_{03} - e^2F_{23}$
10	5211.714	2	19,182.22	$y^4G_{03} - e^2G_{23}$	4	4924.998v	4	20,298.93	$z^2F_{03} - e^2G_{43}$
4	5210.834v	3-IV	19,185.46	$y^4D_{03} - e^4D_{13}$	11	4925.676	1	20,296.13	$z^2G_{23} - e^2F_{23}$
4	5210.042v	3-IV	19,188.38	$e^2D_{23} - y^2P_{03}$	4	4920.272v	4	20,318.42	$y^4G_{03} - h^4F_{23}$
4	5192.358v	4-V	19,253.73	$y^4D_{03} - g^4F_{13}$	4	4920.272v	1-III A	20,318.42	$b^4P_{13} - y^2D_{03}$
9	5183.53	1	19,286.52	$y^4G_{03} - e^2D_{03}?$	11	4918.266	2	20,326.71	$b^2P_{13} - x^4D_{03}?$
9	5183.04	1	19,288.34	$z^2F_{03} - g^4F_{23}$	11	4915.960	3	20,336.24	$a^2H_{43} - x^4G_{03}$
9	5180.13	1	19,299.18	$z^2F_{03} - e^4F_{23}$	11	4914.714	3	20,341.40	
9	5179.66	1	19,300.92	$z^2D_{03} - g^2F_{23}$	4	4912.399v	1-IA	20,350.99	$b^4F_{23} - z^2F_{03}$
10	5177.585	1n	19,308.66	$y^4F_{03} - e^2H_{43}$	11	4910.934	4R	20,357.06	
10	5177.363	1	19,309.49	$y^4D_{03} - e^2D_{23}$	4	4908.481v	3	20,367.23	$e^2D_{13} - w^4S_{03}$
4	5176.085v	20-III	19,314.26	$a^2D_{23} - y^2D_{03}$	9	4907.58	1	20,370.96	$b^2G_{43} - x^2F_{03}$
6	5173.48	0	19,323.98	$y^2G_{43} - g^2F_{23}$	5	4907.125	2	20,372.86	$b^4F_{43} - e^2F_{03}$
4	5172.292v	2	19,328.42	$z^2F_{03} - g^4F_{23}$	4	4904.172v	1-III	20,385.13	$b^2D_{13} - z^2P_{03}$
4	5166.060v	2-V	19,351.74	$z^2D_{03} - g^2F_{23}$	9	4902.52	1	20,392.00	$y^4G_{03} - e^2G_{23}$
4	5165.156v	3-IV?	19,355.12	$a^4P_{23} - y^4D_{03}$	4	4899.520v	2-III A	20,404.48	$e^2D_{13} - y^2D_{03}$
4	5158.854v	2-IV?	19,378.77	$y^4D_{03} - e^4P_{13}$	4	4897.182v	15	20,414.22	$z^2G_{03} - e^2H_{43}$
5	5158.431	2-IV?	19,380.36	$z^2F_{03} - e^4G_{23}$	10	4892.76	1n	20,432.67	$y^4D_{03} - e^2D_{23}$
4	5156.366v	10-IV?	19,388.12	$z^2G_{03} - e^4H_{43}$	7	4892.508	1	20,433.73	$y^4G_{03} - h^4F_{23}$
12	5154.87	3	19,393.74	$z^2D_{03} - e^2G_{23}$	4	4886.995v	5	20,456.78	$z^2G_{03} - e^2G_{43}$
4	5154.070v	8-IV?	19,396.75	$z^2D_{03} - e^2G_{23}$	4	4882.704v	2-III	20,474.76	$z^2G_{03} - e^2F_{23}$
4	5149.796v	4-II	19,412.85	$a^4P_{13} - y^4D_{03}$	11	4881.311	4	20,480.60	$(y^4F_{03} - h^4F_{13})$
4	5149.108v	2-IV?	19,415.45	$y^4D_{03} - g^4F_{23}$	12	4880.25	2	20,485.05	$b^4F_{13} - z^2D_{03}$
4	5146.753v	15-IV?	19,424.33	$z^2F_{03} - f^4F_{23}$	12	4878.356v	0	20,493.00	$z^2G_{03} - e^2F_{23}$
4	5145.512	2-IV?	19,429.01	$z^2G_{03} - e^4G_{23}$	4	4869.377v	10	20,530.79	$y^4G_{03} - e^2F_{23}$
4	5142.471v	3	19,440.50	$y^4D_{03} - f^4F_{23}$	4	4867.870v	25-II	20,537.15	$z^2G_{03} - e^2F_{23}$
9	5141.03	1	19,445.95	$z^2F_{03} - f^4F_{23}$	5	4863.461	5	20,555.76	$b^4P_{13} - y^2F_{03}$
11	5135.543	1	19,466.73	$y^4D_{03} - e^4P_{13}$	4	4862.097v	1	20,561.53	$z^2F_{03} - e^2D_{13}$
4	5133.467v	15-V	19,474.60	$z^2G_{03} - e^4H_{43}$	9	4857.938	1	20,579.13	$b^4F_{23} - z^2D_{03}$
4	5126.201v	10-IV?	19,502.20	$z^2F_{03} - f^4F_{23}$	7	4855.590	1	20,589.08	$z^2F_{03} - e^2D_{23}$
4	5125.715v	7-IV?	19,504.05	$z^2G_{03} - e^4G_{23}$	4	4855.235v	0	20,590.58	$b^4F_{23} - z^2F_{03}$
4	5124.718v	2-IV?	19,507.85	$y^4F_{03} - g^2F_{23}$	11	4853.309	3	20,598.76	$z^2D_{03} - e^4P_{23}$
4	5122.767v	8-IV?	19,515.28	$z^2F_{03} - f^4F_{23}$	11	4851.973	1	20,604.43	$b^2P_{13} - 2z_1$
5	5113.232	6-IV?	19,551.67	$a^2D_{23} - y^2F_{03}$	11	4849.315	2	20,615.73	$y^4F_{03} - 1z_1$
4	5108.903v	10-V	19,568.24	$z^2G_{03} - e^4G_{23}$	4	4843.454v	3-III	20,640.67	$z^2G_{03} - e^2z_1$
9	5108.27	1	19,570.66	$y^2G_{03} - g^2F_{23}$	4	4840.253v	25-III	20,654.32	$z^2G_{03} - e^2F_{23}$
10	5103.11	1	19,590.45	$y^4G_{03} - e^2F_{23}$	10	4837.948	2	20,664.16	$b^4F_{13} - z^2D_{03}$
7	5100.034	1N	19,602.27	$y^4G_{03} - e^2H_{43}$	10	4834.359	—	20,679.50	$b^4P_{13} - y^2D_{03}$
9	5098.02	1	19,610.01	$y^4D_{03} - e^4D_{13}$	4	4832.088v	0	20,689.22	$y^4D_{03} - e^4H_{23}$
4	5094.955v	8-III	19,621.81	$a^2D_{13} - y^2D_{03}$	10	4818.411	1	20,747.95	$y^4D_{03} - e^2H_{43}$
10	5091.282	1	19,635.97	$b^4F_{23} - z^2F_{03}$	9	4817.43	1	20,752.17	$y^4G_{03} - h^4F_{13}$
4	5087.858v	3-V	19,649.18	$y^4G_{03} - e^2H_{43}$	4	4815.900v	1-III	20,758.77	$b^2D_{13} - z^2D_{03}$
10	5085.695	1	19,657.53	$b^4F_{13} - z^2F_{03}$	4	4813.966v	2-III	20,767.11	$z^2G_{13} - e^2F_{13}$
4	5077.410v	3-III?	19,689.61	$z^2F_{03} - e^4D_{23}$	4	4813.476v	20-III	20,769.22	$(b^2D_{13} - x^2D_{03})$
9	5076.83	1	19,691.86	$y^4G_{03} - e^2G_{43}$	10	4808.24	1	20,791.84	$y^4F_{03} - h^4F_{23}$
9	5067.55	2-IV?	19,727.92	$e^2D_{23} - w^2F_{03}$	10	4801.79	1	20,819.76	$z^2D_{03} - f^4D_{23}$
11	5059.849	1	19,757.94	$y^4F_{03} - g^2F_{23}$	4	4797.835v	1	20,836.93	$y^4D_{03} - h^4F_{13}$
11	5057.990	1	19,765.20	$y^4D_{03} - e^4P_{13}$	4	4797.750v	1	20,837.30	$e^2D_{23} - z^2P_{03}$
11	5050.601	1	19,794.12	$a^2H_{43} - x^4G_{03}$	4	4796.378v	1-III A	20,843.26	$b^4F_{43} - z^2F_{03}$
7	5034.970	1N	19,855.57	$z^2F_{03} - f^4F_{23}$	4	4795.853v	2-V	20,845.54	$z^2F_{03} - e^4H_{23}$
12	5034.06	3	19,859.16	$a^2D_{13} - y^2F_{03}$	9	4794.27	1	20,852.42	$y^4F_{03} - h^4F_{23}$
4	5033.36	1N	19,861.92	$z^2D_{03} - f^4F_{23}$	4	4792.855v	15-III	20,858.58	$z^2G_{03} - e^2F_{23}$
4	5022.118v	2	19,906.38	$z^2D_{03} - h^4F_{23}$	4	4785.070v	50	20,892.51	$z^2F_{03} - g^2F_{23}$
4	5013.326v	1n	19,941.29	$b^4F_{13} - z^2F_{03}$	11	4782.561	1	20,903.47	$a^2F_{23} - z^2F_{03}$
4	5007.286v	5	19,965.35	$b^4F_{13} - z^2F_{03}$	4	4781.432v	3-III A	20,908.41	$b^4P_{23} - z^2D_{03}$
10	5004.187	1	19,977.71	$b^2D_{13} - z^2P_{03}$	4	4779.979v	10-III	20,914.76	$z^2G_{03} - e^2F_{23}$
10	5000.877	1	19,990.93	$z^2G_{03} - e^2F_{43}$	4	4778.233v	2-IV	20,922.41	$z^2F_{03} - g^2F_{23}$
4	4993.006v	5	20,022.44	$y^4F_{03} - h^4F_{43}$	4	4776.311v	6-III	20,930.83	$z^2G_{03} - e^2F_{13}$
4	4988.035v	10	20,042.40	$z^2G_{03} - e^2H_{43}$	11	4773.498	1	20,943.16	$y^4D_{03} - f^2F_{23}$
4	4987.853v	2-IA	20,043.13	$b^4F_{23} - z^2F_{03}$	5	4771.108	6-III	20,953.65	$z^2D_{03} - e^2F_{43}$
4	4986.443v	10	20,048.80	$b^2D_{23} - z^2P_{03}$	4	4768.072v	5-III	20,966.99	$z^2D_{03} - e^2F_{23}$
10	4983.04	1	20,062.49	$(y^4F_{03} - h^4F_{23})$	4	4767.142v	100	20,971.08	$z^2G_{03} - g^2F_{23}$
4	4981.789v	0	20,067.53	$y^4D_{03} - f^2F_{23}$	11	4762.353	1Mn?	20,992.17	$z^2G_{03} - e^4D_{43}$
4	4979.944v	60	20,074.96	$z^2F_{03} - e^2G_{23}$	4	4756.722v	100	21,017.02	$z^2G_{03} - e^2F_{23}$
9	4974.47	1	20,097.05	$a^2D_{23} - y^2D_{03}$	4	4754.358v	3-III	21,027.47	$z^2D_{03} - e^2F_{23}$
4	4971.935v	2-IV	20,107.30	$z^2G_{03} - e^2F_{23}$	9	4751.57	1	21,039.81	$z^2D_{03} - h^4F_{23}$
4	4971.015v	6	20,111.02	$b^2D_{13} - w^4D_{03}$	4	4749.68v	10-III	21,048.18	$z^2G_{03} - e^2F_{23}$
4	4967.902v	10w	20,123.62	$z^2G_{03} - e^2G_{23}$	4	4746.115v	100	21,063.99	$z^2G_{03} - g^2F_{23}$
5	4967.528	3	20,125.14	$y^2G_{03} - h^4F_{23}$	12	4742.22	2	21,081.29	$y^4G_{03} - f^4G_{23}$
4	4966.581v	2-IA	20,128.98	$b^4F_{43} - z^2F_{03}$	11	4738.097	1	21,099.64	$z^2F_{03} - f^2F_{23}$

TABLE VIII.—Continued.

REF.	λ Å	INT.-TC	WAVE NO. VAC.	MULTIPLY DESIGNATION	REF.	λ Å	INT.-TC	WAVE NO. VAC.	MULTIPLY DESIGNATION
4	4737.769v	2-IIA	21,101.10	$b^4F_{13} - 3^2D_{013}$	10	4547.75	<1	21,982.75	$a^2F_{23} - 3^4D_{013}$
9	4736.22	1	21,108.00	$3^4D_{013} - 4^4F_{23}$	11	4546.873	1	21,986.99	$c^2D_{23} - 10^23$
4	4734.828v	2-III?	21,114.20	$2^8D_{03} - e^6F_{23}$	4	4545.985v	1-III	21,991.29	$b^2D_{23} - 2^2D_{013}$
4	4732.051v	40	21,126.59	$b^4F_{23} - 2^8D_{03}$	4	4545.238v	50	21,994.90	$2^2G_{03} - 4^4F_{23}$
7	4729.058	2	21,139.97		11	4544.541	1	21,998.27	$2^2G_{03} - e^4G_{13}$
4	4727.930v	3-IA	21,144.98	$b^4F_{13} - 2^8D_{013}$	4	4543.810v	6-III	22,001.82	$b^2D_{23} - 2^2D_{023}$
11	4727.746	1	21,145.83	$b^4F_{23} - 2^2F_{023}$	9	4541.65	1	22,012.28	$3^4G_{03} - 4^4F_{23}$
4	4725.250v	1	21,157.00	$2^2G_{03} - e^2G_{23}$	4	4540.786v	30	22,016.47	$2^2D_{03} - e^2D_{23}$
4	4718.470v	50	21,187.40	$3^4G_{03} - f^4H_{23}$	10	4534.353	1	22,047.70	$b^2P_{13} - 2^4D_{013}$
9	4709.04	1	21,229.83	$3^4G_{03} - f^4H_{23}$	4	4533.985v	7-III	22,049.49	$2^2F_{03} - e^2F_{23}$
4	4704.386v	3	21,250.83	$2^4D_{03} - g^4F_{23}$	11	4532.605	1	22,056.20	$a^2P_{13} - 2^2D_{023}$
11	4704.144	1	21,251.93	$2^4D_{03} - e^2P_{13}$	4	4530.949v	30-II	22,064.26	$2^2F_{03} - e^2F_{23}$
4	4699.180v	25	21,274.37	$a^2F_{23} - 2^2G_{03}$	4	4527.919v	2-III	22,079.03	$2^2D_{03} - e^2F_{23}$
4	4698.389v	3-IV?	21,277.96	$2^8D_{03} - e^6F_{23}$	4	4526.794v	2-III	22,084.52	$2^2D_{03} - e^4F_{13}$
9	4697.52	1	21,281.89	$3^4D_{03} - f^4F_{23}$	4	4526.518v	4	22,085.86	$b^4F_{13} - 2^8G_{03}$
11	4697.000	1	21,284.25	$c^2D_{13} - 2^2P_{03}$	5	4525.787	0	22,089.43	$b^4F_{23} - 2^8G_{03}$
4	4693.190v	6-IV?	21,301.53	$2^8D_{03} - e^6F_{23}$	12	4524.72	3	22,094.64	
9	4689.98	1	21,316.11	$3^4D_{03} - e^6F_{13}$	4	4519.283v	40	22,121.22	$2^4D_{03} - g^4F_{23}$
4	4688.489v	20	21,322.88	$3^4F_{03} - f^4G_{13}$	9	4517.96	1	22,127.70	$2^2G_{03} - f^4H_{13}$
4	4685.858v	30	21,334.86	$b^2D_{23} - 2^4D_{013}$	4	4517.094v	4-III	22,131.94	$2^2F_{03} - e^2F_{13}$
9	4683.95	1	21,343.55	$b^2D_{23} - 2^4F_{013}$	4	4514.177v	1-IV	22,146.24	$2^4D_{03} - f^2F_{23}$
4	4682.361v	9-III?	21,350.79	$2^8D_{03} - e^6F_{23}$	11	4508.664	1	22,173.32	$2^2D_{03} - e^4F_{13}$
11	4677.528	1	21,372.85	$b^4F_{23} - 2^8D_{013}$	4	4500.562v	5	22,213.24	$2^2D_{03} - e^4G_{23}$
5	4677.251	4	21,374.12	$b^4F_{13} - 2^6G_{03}$	5	4499.261	3	22,219.66	$b^2P_{13} - 2^4D_{013}$
4	4676.705v	0	21,376.61	$c^2D_{13} - 11^23$	4	4494.746v	2-IV	22,241.98	$c^2D_{13} - e^2F_{023}$
9	4670.92	1	21,403.09	$b^2D_{13} - 2^4F_{013}$	9	4493.05	1	22,250.38	$2^2D_{03} - f^4F_{23}$
4	4667.861v	10	21,417.11		5	4492.076	5	22,255.20	$\{2^2D_{03} - f^4F_{23}\}$ $\{3^4D_{03} - f^4D_{23}\}$
4	4663.403v	12-III	21,437.59	$2^8D_{03} - e^6F_{23}$	5	4490.309	2	22,263.96	$2^2G_{03} - f^4F_{23}$
4	4657.390v	100	21,465.26	$2^8D_{03} - e^6F_{23}$	9	4489.40	1	22,268.46	$2^2G_{03} - f^4F_{23}$
4	4654.834v	25	21,477.05	$2^2F_{03} - 4^4F_{23}$	4	4486.706v	50	22,281.84	$b^2D_{23} - 2^4F_{023}$
10	4654.519	1	21,478.50	$b^2D_{23} - 2^4D_{013}$	4	4484.513v	60	22,292.73	$a^2F_{23} - 2^2G_{03}$
4	4653.770v	1	21,481.96	$b^2P_{13} - 2^4P_{013}$	4	4483.918v	3-III	22,295.69	$2^2F_{03} - e^2F_{23}$
11	4652.470	1	21,487.96	$a^2F_{23} - 2^4D_{023}$	5	4483.586	20h	22,297.34	$2^2G_{03} - e^4H_{23}$
12	4651.84	3	21,490.87		11	4481.577	5	22,307.34	$b^4F_{23} - 2^8G_{03}$
5	4648.652	5	21,505.61	$\{b^2D_{23} - 2^2F_{023}\}$ $\{b^2D_{13} - 3^4P_{013}\}$	5	4478.657	5	22,321.87	$b^2P_{13} - 2^2P_{013}$
4	4645.153v	0	21,521.81	$b^4F_{13} - 2^8G_{013}$	4	4478.319v	4-III	22,323.56	$2^2F_{03} - e^2F_{13}$
4	4644.317v	70	21,525.68	$2^2G_{03} - 4^4F_{23}$	4	4477.212v	30wh	22,329.08	$\{2^2G_{03} - e^4H_{13}\}$ $\{3^4D_{03} - f^4F_{23}\}$
4	4643.733v	15	21,528.39	$c^2D_{23} - 2^2P_{013}$	4	4471.809v	1-III	22,356.06	$b^2G_{13} - 2^2H_{023}$
9	4642.79	1	21,532.76	$2^2G_{03} - e^4G_{13}$	4	4471.550v	5-III	22,357.36	$2^2F_{03} - e^2F_{23}$
4	4640.820v	10	21,541.90	$b^4F_{23} - 2^8G_{03}$	10	4471.271	1	22,358.75	$2^2G_{03} - e^4G_{23}$
9	4639.07	1	21,550.03	$3^4G_{03} - e^6G_{23}$	11	4471.046	1	22,359.88	$2^2G_{03} - f^2F_{23}$
9	4631.10	1	21,587.12	$2^2G_{03} - f^4F_{23}$	4	4469.547v	15-III	22,367.38	$2^2F_{03} - e^2F_{43}$
9	4630.52	1	21,589.82	$2^4D_{03} - e^4P_{13}$	4	4467.53	1	22,377.47	$3^4D_{03} - 6^4$
4	4629.359v	15-III	21,595.24	$2^8D_{03} - e^6F_{23}$	4	4466.881v	10-III	22,380.72	$2^2F_{03} - e^6F_{23}$
4	4628.908v	125	21,597.34	$b^4F_{23} - 2^8D_{023}$	4	4465.817v	5	22,386.06	$2^2G_{03} - e^4H_{13}$
9	4627.44	1	21,604.19	$3^4D_{03} - 4^4F_{23}$	11	4460.725	1	22,411.61	$2^2F_{03} - f^4D_{23}$
4	4625.767v	2-III	21,612.00	$2^4D_{03} - e^4D_{23}$	4	4458.594v	10	22,422.32	$2^2F_{03} - g^4F_{23}$
4	4624.561v	10	21,617.64	$b^2D_{23} - 2^2F_{013}$	11	4458.242	1	22,424.09	$3^4D_{03} - 21^4$
4	4623.020v	150	21,624.84	$2^8D_{03} - e^6F_{13}$	11	4452.166	1	22,454.70	$b^4F_{23} - 21^4$
4	4622.691v	30	21,626.38	$2^4D_{03} - g^4F_{23}$	9	4450.79	1	22,461.61	$2^2D_{23} - f^4F_{23}$
4	4620.824v	25	21,635.12	$b^2D_{23} - 2^2F_{023}$	4	4445.711v	4-III	22,487.29	$2^2F_{03} - e^2F_{13}$
10	4619.329	1	21,642.12	$a^2F_{23} - 2^4G_{03}$	4	4445.040v	2-IV	22,490.65	$2^2F_{03} - e^4G_{13}$
4	4614.003v	60	21,667.11	$3^4D_{03} - 4^4F_{23}$	4	4441.952v	5	22,506.33	$a^2F_{23} - 2^4D_{023}$
9	4612.41	1	21,674.58	$3^4D_{03} - 4^4F_{23}$	9	4441.02	1	22,511.05	$\{2^2D_{03} - e^2D_{23}\}$ $\{3^4D_{03} - e^4G_{13}\}$
4	4608.908v	8	21,691.06	$b^4F_{23} - 2^8D_{013}$	4	4437.872v	2	22,527.02	$2^4D_{03} - f^2F_{23}$
4	4601.158v	30	21,727.59	$2^4D_{03} - f^4G_{13}$	4	4436.193v	15	22,535.55	$\{b^2D_{13} - 2^2D_{023}\}$ $\{2^2G_{03} - f^4H_{13}\}$
4	4596.903v	5-IV	21,747.70	$2^4D_{03} - e^4P_{23}$	4	4431.608v	3-III	22,558.86	$b^2G_{23} - 2^2G_{023}$
4	4594.633v	4-IV	21,758.45	$2^8D_{03} - e^6D_{23}$	4	4429.33	1	22,570.46	$3^4D_{03} - 51^4$
11	4594.356	1	21,759.76	$b^4F_{23} - 2^8G_{03}$	9	4422.00	1	22,607.87	$\{2^2F_{03} - e^2G_{13}\}$ $\{c^2D_{23} - 12^4\}$
11	4591.375	1	21,773.89	$a^2F_{23} - e^2F_{023}$	4	4421.337v	4-III	22,611.26	$2^2F_{03} - e^2F_{43}$
9	4589.36	1	21,783.44	$2^4G_{03} - e^2D_{03}$	9	4420.86	1	22,613.70	$2^2G_{03} - e^4H_{13}$
4	4588.730v	1-IA	21,786.44	$b^4F_{13} - 2^8D_{023}$	9	4420.43	1	22,615.90	$2^2G_{03} - f^4H_{13}$
4	4586.936v	15	21,794.96	$b^4F_{23} - 2^8G_{013}$	10	4418.000	<1	22,628.34	$\{2^2G_{03} - f^4F_{13}\}$ $\{3^4D_{03} - f^4F_{23}\}$
4	4581.596v	20-III	21,820.36	$\{2^4D_{03} - e^4D_{13}\}$ $\{2^8D_{03} - e^6F_{23}\}$	9	4417.76	1	22,629.57	$b^2P_{13} - 2^2P_{013}$
11	4581.380	1	21,821.39	$2^8D_{03} - e^6F_{23}$	4	4417.398v	5-III	22,631.43	$2^2F_{03} - e^2F_{13}$
11	4580.964	1	21,823.37	$2^2F_{03} - 4^4F_{23}$	4	4416.482v	3	22,636.12	$a^2H_{13} - 2^2H_{023}$
4	4580.139v	4-IA	21,827.30	$a^2F_{23} - 2^2G_{03}$	4	4412.727v	1	22,655.38	$2^2D_{03} - f^4F_{23}$
5	4579.364	25	21,831.00	$2^2F_{03} - f^4D_{23}$	4	4411.786	7	22,660.21	$a^2F_{23} - 2^4G_{23}$
10	4577.27	1	21,840.99	$3^4F_{03} - e^6G_{13}$	4	4411.685v	0	22,660.73	$2^2G_{03} - e^2F_{23}$
4	4574.942v	20	21,852.10	$a^2F_{23} - 2^4D_{023}$	4	4410.02	2	22,669.29	$2^2G_{03} - e^2G_{23}$
4	4570.024v	2-IV	21,875.61	$2^4D_{03} - g^4F_{23}$	9	4404.932v	3-III	22,695.47	$b^2P_{13} - 2^2D_{013}$
5	4567.533	2	21,887.54	$3^4G_{03} - e^6D_{23}$	9	4404.28	1	22,698.83	$b^2P_{13} - 2^4G_{023}$
4	4566.610v	100	21,891.97	$2^4D_{03} - e^4D_{13}$	4	4402.674v	3-III	22,707.11	$2^2F_{03} - e^4D_{23}$
4	4565.578v	15-III	21,896.91	$2^2F_{03} - e^2F_{13}$	10	4396.717	1	22,737.88	$b^2D_{23} - 3^4P_{013}$
5	4564.843	10	21,900.44	$2^4G_{03} - g^4F_{13}$	4	4395.871v	1-III A	22,742.25	$b^2P_{13} - 2^4D_{023}$
4	4564.153v	35	21,903.75	$b^2G_{23} - 2^2H_{043}$	9	4394.54	1	22,749.15	$b^4F_{23} - 2^8G_{03}$
5	4563.989	10	21,904.53	$2^4G_{03} - e^4H_{23}$	4	4391.890v	3-III	22,762.86	$b^2P_{13} - 2^4D_{013}$
10	4563.85	1	21,905.20	$2^4D_{03} - g^4F_{23}$	4	4391.568v	4-III	22,764.54	$2^2F_{03} - e^2F_{23}$
9	4563.38	1	21,907.46	$b^4F_{23} - 2^8G_{13}$	4	4387.915v	3	22,783.49	$2^2F_{03} - e^2D_{23}$
9	4563.02	1	21,909.19	$3^4D_{03} - f^4P_{23}$	9	4381.50	1	22,816.84	$2^2F_{03} - e^2F_{13}$
4	4561.948v	25	21,914.34	$b^2P_{13} - 2^2P_{013}$	4	4380.07v			

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION
4	4374.446v	2vh	22,853.64	$z^1F_{0\frac{1}{2}} - g^1F_{\frac{3}{2}}$	4	4192.856v	3h	23,843.40	$a^2D_{\frac{3}{2}} - z^2S_{\frac{1}{2}}$
4	4373.634v	6-IV	22,857.88	$z^1F_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	10	4192.473	<1	23,845.57	$z^2F_{\frac{3}{2}} - f^4F_{\frac{1}{2}}$
9	4372.08	1	22,866.00	$y^4D_{0\frac{1}{2}} - e^2H_{\frac{3}{2}}$	4	4190.712v	20-I	23,855.60	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$
4	4371.130v	5-III	22,870.96	$a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$	9	4189.50	1	23,862.50	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$
9	4368.08	1	22,886.94	$z^1G_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	4	4187.246v	4-II	23,875.34	$\{a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}\}$ $\{z^2F_{0\frac{1}{2}} - f^4F_{\frac{1}{2}}\}$
9	4367.03	1	22,892.44	$z^1G_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	9	4184.50	1	23,891.01	$y^4D_{0\frac{1}{2}} - g^1P_{\frac{3}{2}}$
4	4366.213v	2	22,896.73	$z^2D_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	4	4180.695v	0	23,912.75	$z^1F_{0\frac{1}{2}} - f^4F_{\frac{1}{2}}$
4	4361.913v	2h	22,919.30	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	9	4179.226v	2-III	23,921.14	$b^2G_{\frac{3}{2}} - w^2F_{0\frac{1}{2}}$
5	4361.031	2	22,923.94	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	4	4177.59	1	23,930.52	$z^1F_{0\frac{1}{2}} - z^2D_{0\frac{1}{2}}$
4	4360.830v	10	22,924.99	$b^2P_{\frac{1}{2}} - z^2F_{0\frac{1}{2}}$	9	4172.039v	0	23,939.42	$z^1F_{0\frac{1}{2}} - e^1H_{\frac{3}{2}}$
4	4359.426v	15	22,932.38	$z^2D_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	4	4172.569	1	23,959.32	$z^1G_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
9	4358.96	1	22,934.83	$b^2P_{\frac{1}{2}} - w^4D_{0\frac{1}{2}}$	10	4170.888v	4	23,968.98	$z^1G_{0\frac{1}{2}} - g^2F_{\frac{3}{2}}$
9	4358.08	1	22,939.46	$z^2F_{0\frac{1}{2}} - 5\frac{1}{2}, 2\frac{1}{2}$	4	4168.44	1	23,983.05	$z^1D_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
5	4357.173	10	22,944.23	$y^4D_{0\frac{1}{2}} - 4\frac{1}{2}$	9	4168.114	<1	23,984.93	$z^2F_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$
4	4356.900v	3	22,945.67	$z^1F_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	9	4167.85	1	23,986.45	$z^1F_{0\frac{1}{2}} - z^2F_{0\frac{1}{2}}$
4	4353.824v	4	22,961.88	$y^4D_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}?$	9	4167.61	1	23,987.83	$z^1D_{0\frac{1}{2}} - f^4P_{\frac{3}{2}}$
4	4350.630v	1	22,978.74	$z^2D_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	5	4162.169	2-IV	24,019.18	$z^1G_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
9	4350.10	1	22,981.54	$z^1G_{0\frac{1}{2}} - e^1H_{\frac{3}{2}}$	9	4160.70	8 Co II?	24,027.67	$c^2D_{\frac{1}{2}} - 19\frac{1}{2}$
10	4343.724	<1	23,015.27	$z^2D_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	4	4158.420v	4-III	24,040.84	$b^2G_{\frac{3}{2}} - w^2F_{0\frac{1}{2}}$
4	4342.486v	0	23,021.83	$z^1D_{0\frac{1}{2}} - z^2F_{0\frac{1}{2}}$	9	4156.91	1	24,049.57	$a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
9	4341.19	1	23,028.71	$z^1G_{0\frac{1}{2}} - g^2F_{0\frac{1}{2}}$	10	4156.646	—	24,051.10	$b^2D_{\frac{3}{2}} - v^4D_{0\frac{1}{2}}$
7	4340.240	1n	23,033.75	$\{b^2D_{\frac{3}{2}} - v^2D_{0\frac{1}{2}}\}$ $\{z^2F_{0\frac{1}{2}} - z^2F_{0\frac{1}{2}}\}$	9	4155.97	—	24,055.01	$b^2P_{\frac{1}{2}} - w^4F_{0\frac{1}{2}}$
4	4339.625v	5-III	23,037.01	$b^2P_{\frac{1}{2}} - z^2P_{0\frac{1}{2}}$	9	4151.74	1	24,079.52	$z^1F_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$
9	4339.03	1	23,040.17	$z^1G_{0\frac{1}{2}} - e^2H_{\frac{3}{2}}$	9	4151.20	1	24,082.65	$\{b^2D_{\frac{3}{2}} - z^2P_{0\frac{1}{2}}\}$ $\{z^1D_{0\frac{1}{2}} - 63\}$
9	4337.54	2	23,048.09	$z^1F_{0\frac{1}{2}} - e^2D_{\frac{1}{2}}$	4	4150.429v	2-IIA	24,087.13	$b^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$
9	4334.37	1	23,064.94	$e^2H_{\frac{3}{2}} - z^2H_{0\frac{1}{2}}$	4	4139.452v	3-III	24,151.00	$a^2D_{\frac{3}{2}} - z^2S_{\frac{1}{2}}$
9	4333.14	1	23,071.49	$z^1F_{0\frac{1}{2}} - z^1D_{\frac{1}{2}}$	10	4138.393	1	24,157.18	$b^2P_{\frac{1}{2}} - z^1P_{0\frac{1}{2}}$
9	4331.64	1	23,079.55	$a^1F_{\frac{3}{2}} - y^2D_{0\frac{1}{2}}$	5	4132.155	4-I	24,193.64	$a^2F_{0\frac{1}{2}} - y^4D_{0\frac{1}{2}}$
4	4331.231v	3-IV	23,081.66	$z^2D_{0\frac{1}{2}} - u^2F_{0\frac{1}{2}}$	9	4131.85	3-V	24,195.43	
9	4326.406v	0	23,107.40	$b^2D_{\frac{3}{2}} - v^4D_{0\frac{1}{2}}$	7	4130.538	1n	24,203.12	$b^1F_{\frac{3}{2}} - z^1F_{0\frac{1}{2}}$
9	4324.32	1	23,118.54	$z^2F_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	5	4122.271	2-III	24,251.66	$a^2H_{0\frac{1}{2}} - z^2G_{0\frac{1}{2}}$
4	4320.385v	2	23,139.60	$z^1F_{0\frac{1}{2}} - g^4F_{\frac{1}{2}}$	4	4121.318v	60-II	24,257.26	$a^2F_{0\frac{1}{2}} - z^2G_{0\frac{1}{2}}$
4	4313.403v	0	23,177.05	$b^2D_{\frac{3}{2}} - v^4D_{0\frac{1}{2}}$	4	4118.774v	50-II	24,272.25	$a^2F_{0\frac{1}{2}} - z^2G_{0\frac{1}{2}}$
4	4310.093v	2	23,194.85	$a^2P_{\frac{1}{2}} - z^1P_{0\frac{1}{2}}$	4	4110.532v	25-I	24,320.91	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$
4	4309.437v	2	23,198.38	$z^2F_{0\frac{1}{2}} - z^1F_{\frac{1}{2}}$	5	4110.073	5h	24,323.63	$z^1G_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
4	4307.439v	2-V	23,209.15	$z^1F_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	7	4109.706	1d-(IA)	24,325.80	$\{a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}\}$ $\{c^2D_{\frac{1}{2}} - z^2F_{0\frac{1}{2}}\}$
4	4303.235v	3-IA	23,231.82	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	11	4108.488	1	24,333.01	$a^1F_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
4	4301.026v	3	23,243.75	$z^1F_{0\frac{1}{2}} - e^2D_{\frac{1}{2}}$	9	4108.34	1	24,333.89	$z^1D_{0\frac{1}{2}} - f^4D_{\frac{1}{2}}$
4	4297.928v	2	23,260.50	$z^2D_{0\frac{1}{2}} - g^2F_{\frac{3}{2}}$	10	4106.462	<1	24,345.02	$z^2F_{0\frac{1}{2}} - f^4F_{\frac{1}{2}}$
4	4292.250v	3h	23,291.27	$e^2H_{\frac{3}{2}} - z^2G_{0\frac{1}{2}}$	10	4106.306	<1	24,345.94	$a^2P_{\frac{1}{2}} - z^2P_{0\frac{1}{2}}$
9	4291.94	1	23,292.95	$z^1F_{0\frac{1}{2}} - z^1F_{0\frac{1}{2}}$	4	4104.743v	4-III	24,355.21	$a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
9	4290.206	1	23,302.37	$b^2D_{\frac{3}{2}} - w^2D_{0\frac{1}{2}}$	4	4104.418v	2-III	24,357.14	$a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
9	4288.54	1	23,311.42	$z^1G_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	4	4097.193v	2	24,400.09	$z^1D_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
4	4287.381v	2	23,317.72	$z^1F_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	4	4095.925v	2-V	24,407.64	$z^1D_{0\frac{1}{2}} - f^4D_{0\frac{1}{2}}$
4	4283.782v	6-I	23,339.78	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	5	4093.053	2-V	24,424.77	$z^1G_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
4	4282.567v	—	23,343.94	$b^2P_{\frac{1}{2}} - w^4F_{0\frac{1}{2}}$	5	4092.848	3-III	24,426.00	$b^4P_{\frac{1}{2}} - z^1S_{0\frac{1}{2}}$
4	4276.107v	2	23,379.20	$z^1F_{0\frac{1}{2}} - e^1H_{\frac{3}{2}}$	4	4092.386v	25-I	24,428.75	$a^2F_{0\frac{1}{2}} - z^2F_{0\frac{1}{2}}$
7	4275.069	3	23,384.88	$z^1F_{0\frac{1}{2}} - e^1G_{\frac{3}{2}}$	5	4090.354	20h	24,440.89	
4	4270.427v	2	23,410.30	$a^2F_{0\frac{1}{2}} - z^2F_{0\frac{1}{2}}$	4	4088.291v	1-IA	24,453.22	$a^1F_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
4	4268.446v	2-III	23,421.16	$b^2P_{\frac{1}{2}} - z^2D_{0\frac{1}{2}}$	9	4086.92	1	24,461.42	$z^1D_{0\frac{1}{2}} - z^1F_{\frac{1}{2}}?$
5	4268.032	3h	23,423.43	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	4	4086.300v	15-II	24,465.14	$b^4P_{\frac{1}{2}} - z^1D_{0\frac{1}{2}}$
9	4267.18	—	23,428.11	$c^2D_{\frac{1}{2}} - v^2P_{0\frac{1}{2}}$	4	4084.113v	2	24,478.24	$z^1F_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
10	4264.642	—	23,442.05	$b^2P_{\frac{1}{2}} - y^4P_{0\frac{1}{2}}$	9	4083.63	1-IV	24,481.13	
4	4263.743v	2	23,447.00	$z^1G_{0\frac{1}{2}} - e^1H_{\frac{3}{2}}$	4	4082.593v	2-IA	24,487.35	$b^1F_{\frac{3}{2}} - z^1F_{0\frac{1}{2}}$
10	4263.333	<1	23,449.25	$z^2D_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	9	4081.440v	2-V	24,494.27	$z^1D_{0\frac{1}{2}} - z^1F_{\frac{1}{2}}$
4	4259.865v	2	23,468.34	$z^2F_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	9	4079.42	1	24,506.39	$z^1D_{0\frac{1}{2}} - e^2P_{\frac{1}{2}}$
4	4255.22	1	23,493.96	$z^1G_{0\frac{1}{2}} - g^2F_{0\frac{1}{2}}$	5	4077.406	2-V	24,518.49	$z^1F_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
4	4252.302v	12-I	23,510.08	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	11	4077.382	2-III	24,518.64	
4	4248.188v	2-V	23,532.84	$b^2D_{\frac{3}{2}} - y^2P_{0\frac{1}{2}}$	4	4076.565v	3h	24,523.56	$z^1G_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$
4	4245.578v	2-V	23,547.31	$z^1F_{0\frac{1}{2}} - g^2F_{\frac{3}{2}}$	4	4076.124v	3-IA	24,526.21	$b^1F_{\frac{3}{2}} - z^1F_{0\frac{1}{2}}$
5	4241.886	2-III	23,567.81	$a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$	4	4069.540v	1-IV	24,565.89	$z^1D_{0\frac{1}{2}} - f^4G_{\frac{1}{2}}$
4	4241.516v	2-V	23,569.86	$z^1D_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$	4	4068.541v	8-II	24,571.92	$b^4P_{\frac{1}{2}} - z^1D_{0\frac{1}{2}}$
9	4240.79	1	23,573.90	$z^2D_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	4	4066.365v	15-I	24,585.07	$a^2F_{0\frac{1}{2}} - y^4D_{0\frac{1}{2}}$
4	4238.442v	2	23,586.96	$z^1G_{0\frac{1}{2}} - e^2G_{\frac{3}{2}}$	4	4063.174v	3h	24,604.38	$\{b^1F_{\frac{3}{2}} - z^1D_{0\frac{1}{2}}\}$ $\{c^2D_{\frac{1}{2}} - u^2D_{0\frac{1}{2}}\}$
4	4237.341v	1-III	23,593.08	$a^2P_{\frac{1}{2}} - z^1P_{0\frac{1}{2}}$	9	4061.76	1	24,612.94	$z^1D_{0\frac{1}{2}} - 1\frac{1}{2}$
7	4233.996†	$\{2-IA\}$ $\{2-IA\}$	23,611.72	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	10	4059.321	1-(IA)	24,627.73	$a^1F_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
4	4229.955v	3h	23,634.28	$a^1F_{\frac{3}{2}} - z^2F_{0\frac{1}{2}}$	7	4058.762	1	24,631.12	$a^2D_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
11	4228.861	1	23,640.39	$z^1F_{0\frac{1}{2}} - e^2G_{\frac{3}{2}}$	4	4058.600v	6-II	24,632.11	$b^4P_{\frac{1}{2}} - z^1D_{0\frac{1}{2}}$
9	4228.54	1	23,642.19	$c^2D_{\frac{1}{2}} - z^1D_{0\frac{1}{2}}$	4	4058.183v	8-I	24,634.64	$b^1F_{\frac{3}{2}} - z^1F_{0\frac{1}{2}}$
4	4225.110v	2-III	23,661.38		4	4057.195v	5-I	24,640.63	$a^1F_{\frac{3}{2}} - z^2G_{0\frac{1}{2}}$
4	4223.768v	0	23,668.89	$z^2F_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	5	4056.979	2-V	24,641.95	$z^1D_{0\frac{1}{2}} - f^4P_{\frac{3}{2}}$
10	4222.254	<1	23,677.39	$z^2F_{0\frac{1}{2}} - f^4F_{\frac{3}{2}}$	4	4054.618v	2-(IA)	24,656.30	$a^1F_{\frac{3}{2}} - z^2D_{0\frac{1}{2}}$
9	4221.09	1	23,683.92	$z^1D_{0\frac{1}{2}} - h^4F_{\frac{1}{2}}$	4	4053.918v	1-IV	24,660.55	$a^2P_{\frac{1}{2}} - w^4D_{0\frac{1}{2}}$
4	422								

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION
4	4020.898v	20-I	24,863.06	$b^4F_{43} - z^4F_{043}$	7	3902.390	1n	25,618.09	$z^4G_{03} - 5\frac{1}{2}z_{23}$
4	4019.288v	5-I	24,873.02	$\{b^4F_{23} - z^4F_{043}\}$	10	3899.996	<1	25,633.82	$a^4F_{23} - z^4G_{043}$
5	4019.140	5	24,873.94	$\{b^4F_{13} - z^4D_{043}\}$	4	3898.485v	4-III	25,643.75	$b^4F_{23} - z^4D_{043}$
7	4016.830	2-V	24,888.24	$a^2P_{13} - w^4D_{043}$	4	3894.976v	20-II	25,666.85	$b^4F_{23} - z^4D_{043}$
4	4015.222v	2	24,898.21	$z^4G_{04} - f^4G_{41}$	4	3894.073v	60-II	25,672.81	$a^2F_{23} - z^4G_{043}$
4	4013.942v	7-II	24,906.15	$b^4P_{13} - z^4D_{043}$	5	3893.303	2-V	25,677.88	$z^4G_{04} - e^4H_{043}$
4	4012.143v	2	24,917.32	$z^4F_{043} - h^4F_{043}$	7	3893.067	2-III	25,679.44	$a^2P_{13} - z^4S_{043}$
4	4011.089v	2-IA	24,923.86	$a^4F_{043} - z^4D_{043}$	7	3892.968	1n	25,680.09	$z^4F_{043} - f^4F_{043}$
4	4010.931v	3h	24,924.85	$z^4F_{043} - f^4D_{043}$	4	3892.210	1	25,685.09	$b^4D_{13} - w^4S_{043}$
4	4007.923v	1-III	24,943.55	$z^4G_{043} - f^4F_{043}$	7	3892.118v	3-III	25,685.70	$b^4F_{13} - w^4D_{043}$
11	4007.273	1	24,947.60	$z^4G_{043} - e^4G_{043}$	5	3891.680	2-V	25,688.59	$z^4F_{043} - f^4F_{043}$
4	4003.596v	2-III	24,970.51	$b^2P_{13} - w^4D_{043}$	4	3890.734v	1	25,694.84	$c^2D_{13} - 2z_{043}$
11	3999.180	1	24,998.08	$z^4D_{043} - e^4D_{043}$	4	3889.978v	2-III	25,699.83	$z^4F_{043} - f^4F_{043}$
7	3998.554	1n	25,001.99	$a^2F_{23} - z^4D_{043}$	4	3885.275v	6-I	25,730.94	$a^2F_{23} - y^4F_{043}$
4	3997.901v	40-II	25,006.08	$a^2F_{23} - y^4F_{043}$	4	3884.601v	10-I	25,735.41	$a^2F_{23} - y^4F_{043}$
11	3997.051	1	25,011.40	$z^4F_{043} - f^4F_{043}$	4	3881.869v	25-I	25,753.52	$a^2F_{23} - z^4D_{043}$
4	3995.306v	60-II	25,022.32	$z^4F_{043} - f^4F_{043}$	5	3881.006	3	25,759.24	$b^2F_{13} - w^4D_{043}$
4	3994.542v	6-I	25,027.11	$a^4F_{13} - z^4G_{043}$	5	3880.839	8	25,760.35	
9	3992.36	1	25,040.79	$z^4D_{043} - e^4G_{043}$	12	3880.40	3	25,763.26	
10	3992.014	1	25,042.95	$a^4F_{23} - z^4G_{043}$	4	3878.750v	70r	25,774.23	$b^4P_{13} - z^4P_{043}$
5	3991.831	15	25,044.10	$b^2P_{13} - w^4D_{043}$	4	3876.831v	20-I	25,786.98	$\{b^4F_{43} - z^4G_{043}\}$
4	3991.684v	6-I	25,045.03	$b^4F_{23} - z^4G_{043}$	4	3873.953v	40-II	25,806.14	$b^4F_{33} - z^4D_{043}$
4	3991.528v	4-IV	25,046.00	$z^4G_{043} - f^4H_{043}$	4	3873.120v	60-II	25,811.69	$b^4F_{43} - z^4D_{043}$
4	3990.299v	6-II	25,053.72	$b^4P_{13} - x^4D_{043}$	4	3870.534v	4-III	25,828.93	$b^2P_{13} - w^4D_{043}$
11	3989.687	1	25,057.56	$z^4D_{043} - e^4D_{043}$	4	3866.832v	2	25,853.66	$a^2F_{23} - x^4D_{043}$
4	3988.884v	2	25,062.61	$z^4G_{043} - f^4G_{043}$	7	3863.966	1	25,872.84	$b^2D_{13} - w^4P_{043}$
4	3987.117v	6-I	25,073.71	$b^4F_{23} - z^4F_{043}$	5	3863.607	2-III	25,875.24	$b^2P_{13} - z^4P_{043}$
7	3985.449	2h	25,084.21	$z^4D_{043} - 6z_{043}$	4	3861.164v	20-I	25,891.61	$a^2F_{23} - z^4D_{043}$
4	3979.518v	10-I	25,121.59	$a^4F_{23} - z^4G_{043}$	12	3860.42	4	25,896.60	
5	3978.864	4-V	25,125.72	$z^4G_{043} - f^4H_{043}$	4	3856.796v	4-III	25,920.93	$b^4P_{23} - 2z_{043}$
4	3978.650v	10-I	25,127.07	$b^4F_{23} - z^4G_{043}$	4	3851.848v	2-III	25,954.23	$b^2P_{13} - w^4D_{043}$
9	3977.75	1	25,132.76	$b^2G_{43} - w^4F_{043}$	4	3850.945v	4-IA	25,960.32	$b^4F_{33} - z^4G_{043}$
4	3977.184v	3-III	25,136.33	$a^2P_{13} - x^4D_{043}$	4	3850.097v	5-III	25,966.03	$c^2D_{23} - 2z_{043}$
4	3975.320v	3-III	25,148.12	$a^2P_{13} - z^4P_{043}$	4	3845.468v	60-II	25,997.29	$a^2F_{23} - z^4G_{043}$
4	3974.726v	10-I	25,151.88	$b^4F_{23} - z^4D_{043}$	7	3844.866	1	26,001.36	$b^2P_{13} - w^4D_{043}$
5	3973.561	15Ni?	25,159.25	$z^4F_{043} - f^4F_{043}$	4	3843.692v	4-III	26,009.30	$a^2G_{03} - w^4D_{043}$
4	3973.144v	10-II	25,161.89	$b^4P_{23} - x^4D_{043}$	4	3842.047v	30-II	26,020.44	$a^2F_{23} - z^4D_{043}$
4	3972.506v	6-III	25,165.93	$\{z^4F_{043} - f^4G_{043}\}$	4	3841.458v	5-I	26,024.43	$a^2F_{23} - y^4F_{043}$
4	3969.116v	8-III	25,187.43	$\{z^4G_{043} - f^4H_{043}\}$	5	3835.900	8	26,062.13	$b^2P_{13} - y^4S_{043}$
9	3968.61	1-III	25,190.64	$\{a^2D_{23} - z^4P_{043}\}$	5	3835.689	10	26,063.57	
10	3966.438	—	25,204.43	$\{a^2D_{23} - z^4P_{043}\}$	5	3835.497	3	26,064.87	$a^2P_{13} - z^4S_{043}$
4	3965.236v	2-III	25,212.07	$a^2F_{23} - y^4D_{043}$	4	3832.899v	2	26,082.54	$a^2P_{13} - y^4P_{043}$
7	3965.011	1-III	25,213.50	$a^2F_{23} - y^4D_{043}$	11	3830.096	1n	26,101.63	$z^4D_{043} - z^4P_{043}$
4	3960.997v	6-II	25,239.05	$b^2P_{13} - w^4D_{043}$	9	3823.52	1-IV	26,146.52	
9	3958.60	1	25,254.34	$z^4G_{043} - e^4G_{043}$	4	3819.908v	4-II	26,171.24	$b^2P_{13} - w^4D_{043}$
4	3957.928v	15-II	25,258.62	$b^4F_{23} - z^4D_{043}$	4	3817.940v	18	26,184.73	$b^2P_{13} - y^4P_{043}$
7	3957.629	10	25,260.53	$b^4F_{23} - z^4D_{043}$	4	3816.876v	5-II	26,192.03	$a^2G_{03} - x^4P_{043}$
9	3956.59	1	25,267.17	$z^4F_{043} - f^4F_{043}$	4	3816.458v	15-I	26,194.00	$b^4P_{23} - z^4P_{043}$
4	3956.270v	15	25,269.21	$z^4D_{043} - 1z_{043}$	4	3816.318v	15-I	26,195.86	$b^4P_{23} - z^4P_{043}$
4	3954.954v	1	25,277.62	$a^4F_{13} - z^4I_{043}$	4	3814.457v	5-III	26,208.64	$b^4P_{23} - z^4P_{043}$
7	3953.612	1n	25,286.20	$z^4D_{043} - 5\frac{1}{2}z_{043}$	5	3813.925	30r	26,212.29	$z^4F_{043} - e^4G_{043}$
5	3952.917	25-II	25,290.64	$b^2P_{13} - w^4D_{043}$	5	3812.470	4-III	26,222.30	$a^2P_{13} - z^4S_{043}$
5	3952.326	8-I	25,294.42	$a^2F_{23} - z^4G_{043}$	4	3811.065v	5-I	26,231.97	$a^2F_{23} - y^4G_{043}$
4	3951.717v	4h	25,298.32	$a^2F_{23} - z^4G_{043}$	4	3808.102v	10-I	26,252.38	$b^4F_{43} - z^4G_{043}$
4	3947.125v	3-II	25,327.75	$b^4F_{13} - z^4F_{043}$	4	3805.775v	2-III	26,268.43	$a^2P_{13} - y^4P_{043}$
4	3946.633v	2-II	25,330.91	$b^4P_{13} - x^4D_{043}$	7	3801.233	1	26,299.81	$b^2G_{43} - 10z_{043}$
4	3945.326v	15-I	25,339.30	$a^2F_{23} - z^4F_{043}$	11	3799.808	1	26,309.68	$a^4P_{13} - x^4D_{043}$
5	3944.950	1-IV	25,341.72	$z^4F_{043} - f^4F_{043}$	4	3797.442v	1	26,326.07	$a^2D_{13} - x^4F_{043}$
9	3944.41	1	25,345.19	$z^4F_{043} - 1z_{043}$	4	3795.856v	1	26,337.07	$z^4F_{043} - e^4G_{043}$
4	3942.684v	2-IV	25,356.28	$z^4F_{043} - f^4D_{043}$	7	3787.345	1	26,396.25	$b^2P_{13} - w^4D_{043}$
4	3941.728v	20-II	25,362.43	$b^4F_{43} - z^4G_{043}$	4	3783.731v	5h	26,421.46	$a^2D_{23} - x^4G_{043}$
4	3940.887v	12-I	25,367.84	$b^4F_{13} - z^4D_{043}$	4	3777.543v	6-III	26,464.74	$a^2D_{23} - w^4D_{043}$
9	3939.07	2-V	25,379.54	$z^4F_{043} - e^4D_{043}$	5	3777.078	1-III	26,468.00	$a^2P_{13} - y^4P_{043}$
4	3938.856v	3-V	25,380.92	$z^4F_{043} - f^4G_{043}$	4	3774.599v	8-II	26,485.38	$a^2D_{23} - w^4D_{043}$
5	3937.949	7h	25,386.76	$z^4F_{043} - e^4P_{13}$	11	3771.851	1	26,504.68	$z^4F_{043} - 5\frac{1}{2}z_{043}$
4	3935.964v	30-II	25,399.58	$a^2F_{23} - y^4F_{043}$	11	3769.703	1	26,519.78	$z^4F_{043} - e^4I_{043}$
5	3935.287	1-III	25,403.94	$b^2P_{13} - w^4P_{043}$	4	3760.401v	4-II	26,585.38	$a^4P_{13} - z^4S_{043}$
4	3934.712v	1-III	25,407.65	$b^2G_{03} - w^4F_{043}$	4	3759.684v	3-III	26,590.45	$b^2P_{13} - y^4P_{043}$
4	3933.918v	6-I	25,412.78	$b^4F_{23} - z^4F_{043}$	9	3756.30	1	26,614.40	$a^2G_{03} - w^4F_{043}$
5	3933.654	80Ca?	25,414.48	$b^4F_{23} - z^4G_{043}$	4	3755.447v	10-II	26,620.45	$a^2D_{23} - w^4D_{043}$
7	3933.159	1n	25,417.69	$z^4G_{043} - e^4H_{043}$	4	3754.346v	4-III	26,628.26	$b^2P_{13} - w^4F_{043}$
10	3930.076	1	25,437.63	$b^4P_{23} - z^4S_{043}$	4	3752.787v	10	26,639.32	$b^2G_{03} - 11z_{043}$
4	3929.256v	3-III	25,442.93	$z^4F_{043} - f^4F_{043}$	9	3752.18	1	26,643.63	$z^4F_{043} - e^4G_{043}$
4	3925.151v	3-III	25,469.54	$b^2P_{13} - y^4P_{043}$	11	3751.805	1	26,646.29	$y^4D_{043} - z^4H_{043}$
4	3922.755v	7-I	25,485.10	$a^2F_{23} - y^4F_{043}$	4	3751.625v	5-III	26,647.57	$a^2D_{23} - x^4P_{043}$
4	3921.104v	1-IV	25,495.83	$z^4G_{043} - 4z_{043}$	4	3749.930v	9-II	26,659.62	$a^2D_{13} - z^4P_{043}$
4	3920.729v	4-II	25,498.27	$a^2D_{13} - z^4F_{043}$	4	3745.491v	25-I	26,691.21	$a^2F_{23} - y^4G_{043}$
5	3920.581	2-III	25,499.23	$a^2D_{13} - z^4F_{043}$	4	3740.186v	5-II	26,729.07	$a^2D_{13} - x^4G_{043}$
4	3920.135v	2-III	25,502.13	$b^2P_{13} - w^4P_{043}$	4	3739.441v	0	26,734.39	$b^4P_{23} - x^4F_{043}$
5	3919.635	4	25,505.38	$z^4F_{043} - f^4F_{043}$	9	3739.20	1	26,736.12	$a^2G_{03} - 4z_{043}$
10	3918.627	1	25,511.94	$a^2D_{13} - z^4F_{043}$	5	3735.928	12-II	26,759.53	$a^2D_{23} - z^4P_{043}$
4	3917.115v	8-II	25,5						

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION
4	3707.465v	6-II	26,964.96	$a^2D_{1\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3581.873v	4-II	27,910.42	$a^2P_{\frac{1}{2}}-y^2P_{0\frac{1}{2}}$
10	3707.01	—	26,968.28	$a^2G_{2\frac{1}{2}}-w^4F_{0\frac{1}{2}}$	4	3579.15v	3	27,931.63	$b^2G_{2\frac{1}{2}}-z^4D_{0\frac{1}{2}}$
4	3704.060v	25-I	26,989.75	$a^2F_{2\frac{1}{2}}-y^2F_{0\frac{1}{2}}$	5	3579.029	6-II	27,932.60	$a^4P_{\frac{1}{2}}-z^4P_{0\frac{1}{2}}$
4	3702.237v	12-III	27,003.04	$b^2G_{2\frac{1}{2}}-y^2H_{0\frac{1}{2}}$	5	3578.903	6-II	27,933.58	$a^4P_{\frac{1}{2}}-z^4P_{0\frac{1}{2}}$
5	3699.017	2n-IV	27,026.55	$b^2G_{2\frac{1}{2}}-y^2H_{0\frac{1}{2}}$	4	3578.076v	6-II	27,940.03	$a^2P_{\frac{1}{2}}-v^4D_{0\frac{1}{2}}$
4	3693.476v	8-I	27,067.09	$a^2D_{1\frac{1}{2}}-z^2P_{0\frac{1}{2}}$	5	3577.688	2-V	27,943.06	$\{a^2G_{2\frac{1}{2}}-f^4D_{0\frac{1}{2}}\}$
5	3693.364	2-III	27,067.91	$b^4P_{\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3577.260v	3-II	27,946.41	$\{z^2G_{2\frac{1}{2}}-f^4G_{0\frac{1}{2}}\}$
4	3693.106v	8-I	27,069.80	$a^2D_{2\frac{1}{2}}-w^4F_{0\frac{1}{2}}$	4	3575.361v	60R-II	27,961.25	$a^4F_{2\frac{1}{2}}-z^4P_{0\frac{1}{2}}$
4	3690.715v	7-II	27,087.34	$a^2G_{2\frac{1}{2}}-z^2F_{0\frac{1}{2}}$	4	3574.967v	25r-I	27,964.33	$b^4F_{2\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
4	3686.477v	2-III	27,118.49	$b^2P_{\frac{1}{2}}-z^2P_{0\frac{1}{2}}$	4	3573.37v	1	27,976.81	$\{b^2G_{2\frac{1}{2}}-15\phi_{\frac{1}{2}}\}$
4	3684.960v	2-III	27,129.64	$a^2P_{\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3570.35v	4n-II	28,000.48	$\{z^2G_{2\frac{1}{2}}-h^4F_{1\frac{1}{2}}\}$
5	3684.479	10-III	27,133.18	$a^2D_{2\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3569.370v	80R-II	28,008.18	$b^2G_{2\frac{1}{2}}-15\phi_{\frac{1}{2}}$
4	3683.047v	20-II	27,143.73	$a^2D_{2\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3568.426	2-III	28,015.59	$b^4P_{2\frac{1}{2}}-z^4G_{0\frac{1}{2}}$
11	3677.980	1	27,181.13	$b^4F_{2\frac{1}{2}}-z^2F_{0\frac{1}{2}}$	5	3564.947v	25r-I	28,042.93	$b^4F_{2\frac{1}{2}}-z^2G_{0\frac{1}{2}}$
10	3677.835	1	27,182.20	$a^2P_{\frac{1}{2}}-z^4P_{0\frac{1}{2}}$	5	3564.643	2	28,045.32	$b^2P_{1\frac{1}{2}}-f^4D_{0\frac{1}{2}}$
4	3676.552v	12-III	27,191.68	$b^2G_{2\frac{1}{2}}-y^2H_{0\frac{1}{2}}$	4	3564.115v	4-III	28,049.48	$z^2G_{2\frac{1}{2}}-f^4H_{0\frac{1}{2}}$
4	3670.041v	3-III	27,239.92	$b^4F_{2\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3562.912v	7-II	28,058.95	$b^4P_{2\frac{1}{2}}-w^4D_{0\frac{1}{2}}$
9	3669.237v	1	27,245.89	$a^4P_{2\frac{1}{2}}-1\phi_{\frac{1}{2}}$	4	3562.097v	6-III	28,065.37	$b^4P_{2\frac{1}{2}}-w^4D_{0\frac{1}{2}}$
9	3668.66	1-III	27,250.18	$b^4P_{2\frac{1}{2}}-z^4F_{0\frac{1}{2}}$	4	3561.38v	1	28,070.98	$b^2P_{1\frac{1}{2}}-f^4D_{0\frac{1}{2}}$
4	3666.4	1n	27,280.37	$z^2D_{0\frac{1}{2}}-e^2D_{1\frac{1}{2}}$	4	3560.891v	20r-I	28,074.87	$b^4F_{1\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
4	3662.158v	12-II	27,298.56	$a^2P_{1\frac{1}{2}}-w^2D_{0\frac{1}{2}}$	5	3560.306	5-III	28,079.48	$b^4P_{2\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
4	3660.699v	5	27,309.44	$a^4P_{2\frac{1}{2}}-2\phi_{\frac{1}{2}}$	7	3559.597	1-IV	28,085.08	$a^2D_{1\frac{1}{2}}-w^4F_{0\frac{1}{2}}$
4	3657.918v	2-III	27,330.20	$b^2P_{\frac{1}{2}}-f^4D_{0\frac{1}{2}}$	4	3558.772v	12-I	28,091.59	$\{b^4F_{2\frac{1}{2}}-z^2F_{0\frac{1}{2}}\}$
4	3656.962v	7-I	27,337.34	$b^4F_{2\frac{1}{2}}-y^4D_{0\frac{1}{2}}$	4	3557.980	2	28,097.84	$\{z^2G_{2\frac{1}{2}}-f^4F_{1\frac{1}{2}}\}$
10	3656.33	<1	27,342.07	$b^4P_{\frac{1}{2}}-z^2P_{0\frac{1}{2}}$	4	3556.120	1	28,112.54	$a^2D_{1\frac{1}{2}}-w^4G_{0\frac{1}{2}}$
4	3654.441v	5-II	27,356.20	$b^4F_{1\frac{1}{2}}-z^2F_{0\frac{1}{2}}$	5	3553.161	2-III	28,135.95	$a^2H_{2\frac{1}{2}}-w^4G_{0\frac{1}{2}}$
4	3652.541v	15-I	27,370.43	$a^4F_{2\frac{1}{2}}-z^4F_{0\frac{1}{2}}$	4	3552.989v	8-II	28,137.31	$b^4P_{1\frac{1}{2}}-z^4D_{0\frac{1}{2}}$
4	3651.254v	4-III	27,380.08	$a^2G_{2\frac{1}{2}}-w^4F_{0\frac{1}{2}}$	4	3552.720v	8-I	28,139.44	$a^4F_{1\frac{1}{2}}-z^4D_{0\frac{1}{2}}$
4	3649.329v	8-III	27,394.52	$b^2G_{2\frac{1}{2}}-w^4G_{0\frac{1}{2}}$	4	3551.666v	2-III	28,147.79	$b^4P_{1\frac{1}{2}}-z^4D_{0\frac{1}{2}}$
4	3648.140v	3-III	27,403.45	$b^2G_{2\frac{1}{2}}-w^4G_{0\frac{1}{2}}$	5	3550.592v	20r-I	28,156.30	$a^4F_{1\frac{1}{2}}-z^4F_{0\frac{1}{2}}$
4	3647.658v	12-I	27,407.07	$a^4P_{1\frac{1}{2}}-z^4G_{0\frac{1}{2}}$	4	3550.20v	5	28,159.38	$z^2G_{2\frac{1}{2}}-e^2G_{0\frac{1}{2}}$
5	3647.388	1-III	27,409.10	$b^2G_{2\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3548.438v	7-II	28,173.40	$a^4P_{2\frac{1}{2}}-z^4P_{0\frac{1}{2}}$
4	3647.081v	5-III	27,411.41	$a^2P_{2\frac{1}{2}}-w^4F_{0\frac{1}{2}}$	4	3546.88v	1	28,185.73	$b^4P_{\frac{1}{2}}-5\phi_{\frac{1}{2}}$
4	3645.190v	3-III	27,423.75	$b^4G_{2\frac{1}{2}}-z^4G_{0\frac{1}{2}}$	4	3546.707v	6-III	28,187.14	$a^4P_{2\frac{1}{2}}-z^4P_{0\frac{1}{2}}$
4	3645.005	1g?	27,427.02	$b^4G_{2\frac{1}{2}}-w^4C_{0\frac{1}{2}}$	4	3543.256v	15-II	28,214.59	$b^4P_{2\frac{1}{2}}-w^4D_{0\frac{1}{2}}$
4	3643.181v	9-II	27,440.75	$a^2D_{1\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3542.976	2-IIA	28,216.83	$b^4F_{1\frac{1}{2}}-z^2C_{0\frac{1}{2}}$
4	3641.784v	6-II	27,451.28	$a^2D_{1\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3542.508	2h	28,220.55	$z^2G_{2\frac{1}{2}}-f^4G_{0\frac{1}{2}}$
7	3641.673	1n	27,452.11	$a^2D_{1\frac{1}{2}}-33\phi_{\frac{1}{2}}?$	5	3540.40v	3w	28,237.33	$z^2F_{2\frac{1}{2}}-f^2F_{0\frac{1}{2}}$
4	3639.443v	10-II	27,468.93	$b^4F_{1\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3539.442v	1	28,245.00	$z^2G_{2\frac{1}{2}}-f^4F_{0\frac{1}{2}}$
4	3638.346v	1-III	27,477.21	$b^4P_{1\frac{1}{2}}-y^2S_{0\frac{1}{2}}$	4	3538.44v	4	28,253.00	$b^2P_{1\frac{1}{2}}-z^4S_{0\frac{1}{2}}$
4	3637.45v	1	27,483.98	$a^2G_{2\frac{1}{2}}-w^4C_{0\frac{1}{2}}$	4	3537.707v	1-III	28,258.85	$b^4P_{\frac{1}{2}}-z^2S_{0\frac{1}{2}}$
4	3637.319v	4-III	27,484.97	$a^2P_{\frac{1}{2}}-v^4D_{0\frac{1}{2}}$	4	3534.769v	4-III	28,282.34	$\{a^2P_{1\frac{1}{2}}-v^2D_{0\frac{1}{2}}\}$
4	3636.713v	6-II	27,489.55	$b^4F_{1\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3533.356v	25r-I	28,293.65	$\{z^2G_{2\frac{1}{2}}-f^4G_{0\frac{1}{2}}\}$
4	3635.06v	2	27,502.02	$a^2G_{2\frac{1}{2}}-4\phi_{\frac{1}{2}}$	6	3533.081	2	28,295.84	$a^4F_{1\frac{1}{2}}-z^4G_{0\frac{1}{2}}$
4	3634.713v	7-III	27,504.68	$b^2G_{2\frac{1}{2}}-w^2F_{0\frac{1}{2}}$	5	3530.554	1-III	28,316.10	$a^2P_{1\frac{1}{2}}-y^2P_{0\frac{1}{2}}$
4	3633.340v	2-III	27,515.07	$a^2P_{1\frac{1}{2}}-z^4P_{0\frac{1}{2}}$	4	3529.816v	80R-II	28,322.03	$b^4F_{2\frac{1}{2}}-y^4G_{0\frac{1}{2}}$
4	3632.839v	7-III	27,518.87	$b^2G_{2\frac{1}{2}}-z^2H_{0\frac{1}{2}}$	4	3529.032v	30r-I	28,328.31	$a^4F_{2\frac{1}{2}}-z^4G_{0\frac{1}{2}}$
5	3631.948	2-III	27,525.61	$b^2P_{1\frac{1}{2}}-z^2S_{0\frac{1}{2}}$	5	3527.947	5-III	28,337.02	$b^2P_{1\frac{1}{2}}-w^2S_{0\frac{1}{2}}$
4	3631.390v	20r-I	27,529.85	$a^4F_{2\frac{1}{2}}-z^4F_{0\frac{1}{2}}$	4	3526.847v	100R-II	28,345.86	$a^4F_{2\frac{1}{2}}-z^4F_{0\frac{1}{2}}$
7	3628.228	2n	27,553.84	$b^2G_{2\frac{1}{2}}-13\phi_{\frac{1}{2}}$	5	3525.872	3-III	28,353.70	$b^4P_{2\frac{1}{2}}-z^2P_{0\frac{1}{2}}$
4	3627.806v	25r-I	27,557.04	$b^4F_{2\frac{1}{2}}-z^2G_{0\frac{1}{2}}$	5	3525.089	2k	28,360.00	$b^4P_{2\frac{1}{2}}-z^2P_{0\frac{1}{2}}$
4	3626.020v	2-III A	27,570.62	$a^4P_{\frac{1}{2}}-z^4P_{0\frac{1}{2}}$	5	3525.089	2k	28,360.00	$b^4P_{2\frac{1}{2}}-z^2P_{0\frac{1}{2}}$
4	3625.56v	3	27,574.09	$z^2G_{2\frac{1}{2}}-f^4G_{0\frac{1}{2}}$	5	3523.701	7-II	28,371.17	$b^4P_{2\frac{1}{2}}-z^2F_{0\frac{1}{2}}$
4	3624.955v	8-I	27,578.71	$b^4F_{1\frac{1}{2}}-y^4D_{0\frac{1}{2}}$	4	3523.423v	25r-I	28,373.41	$b^4F_{1\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
4	3624.337v	5-III	27,583.42	$a^4P_{\frac{1}{2}}-z^4P_{0\frac{1}{2}}$	7	3522.856	4-III	28,377.98	$z^2G_{2\frac{1}{2}}-f^4H_{0\frac{1}{2}}$
4	3623.02v	2	27,593.44	$z^2F_{0\frac{1}{2}}-e^2D_{1\frac{1}{2}}$	5	3521.731	5-I	28,387.04	$\{a^2D_{1\frac{1}{2}}-z^2P_{0\frac{1}{2}}\}$
4	3622.35v	1	27,598.57	$b^2G_{2\frac{1}{2}}-14\phi_{\frac{1}{2}}$	5	3521.567	30r-I	28,388.36	$\{b^4F_{1\frac{1}{2}}-z^2D_{0\frac{1}{2}}\}$
4	3621.70v	15R	27,603.49	$z^2D_{0\frac{1}{2}}-e^2D_{1\frac{1}{2}}$	4	3520.075v	15-II	28,400.39	$b^4F_{1\frac{1}{2}}-z^2F_{0\frac{1}{2}}$
4	3620.422v	5-III	27,613.25	$a^2P_{1\frac{1}{2}}-z^4P_{0\frac{1}{2}}$	4	3518.340v	50R-II	28,414.40	$a^4F_{2\frac{1}{2}}-z^4F_{0\frac{1}{2}}$
4	3620.03v	2	27,616.26	$a^2D_{2\frac{1}{2}}-w^4G_{0\frac{1}{2}}$	4	3516.675	1-III	28,427.85	$b^4P_{1\frac{1}{2}}-w^4S_{0\frac{1}{2}}$
11	3619.285	1	27,621.92	$b^2P_{\frac{1}{2}}-w^2S_{0\frac{1}{2}}$	5	3516.418	2	28,429.93	$z^2G_{2\frac{1}{2}}-e^2G_{0\frac{1}{2}}$
4	3618.010v	4-II A	27,631.65	$a^2F_{2\frac{1}{2}}-y^2D_{0\frac{1}{2}}$	4	3516.04v	3	28,433.03	$z^2D_{0\frac{1}{2}}-f^4D_{0\frac{1}{2}}$
4	3617.48v	2	27,635.69	$b^2P_{\frac{1}{2}}-8\phi_{\frac{1}{2}}$	4	3513.82v	3?	28,450.92	$z^2G_{2\frac{1}{2}}-e^2G_{0\frac{1}{2}}$
4	3615.387v	6-II	27,651.70	$b^4P_{1\frac{1}{2}}-z^2F_{0\frac{1}{2}}$	4	3513.478v	50R-II	28,453.72	$a^4F_{2\frac{1}{2}}-z^4G_{0\frac{1}{2}}$
4	3614.34v	1	27,659.74	$b^2P_{1\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3512.640v	60R-II	28,460.51	$b^4F_{2\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
4	3614.10v	0	27,661.51	$b^4P_{1\frac{1}{2}}-w^4D_{0\frac{1}{2}}$	4	3512.41v	2	28,462.35	$b^4P_{\frac{1}{2}}-y^4P_{0\frac{1}{2}}$
4	3611.701v	10-II	27,679.92	$a^2P_{\frac{1}{2}}-w^2D_{0\frac{1}{2}}$	4	3510.426v	30r-I	28,478.46	$a^4F_{2\frac{1}{2}}-z^4D_{0\frac{1}{2}}$
4	3609.752v	4-III	27,694.86	$b^2G_{2\frac{1}{2}}-z^2H_{0\frac{1}{2}}$	4	3509.843v	50r-II	28,483.19	$b^4F_{2\frac{1}{2}}-y^4G_{0\frac{1}{2}}$
4	3608.82v	3	27,702.02	$a^2D_{2\frac{1}{2}}-y^4P_{0\frac{1}{2}}$	4	3506.310v	80R-II	28,511.89	$b^4F_{2\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
5	3608.307	3-II A	27,705.96	$b^4F_{1\frac{1}{2}}-z^2F_{0\frac{1}{2}}$	4	3505.133v	3-III	28,521.46	$z^2G_{2\frac{1}{2}}-f^2F_{0\frac{1}{2}}$
4	3607.04v	0	27,715.72	$b^4P_{\frac{1}{2}}-z^2D_{0\frac{1}{2}}$	4	3504.728v	5-III	28,524.76	$b^2P_{1\frac{1}{2}}-w^2P_{0\frac{1}{2}}$
4	3606.69v	7	27,718.39	$b^2G_{2\frac{1}{2}}-z^2H_{0\frac{1}{2}}$	5	3503.717	3-III	28,532.98	$a^2G_{2\frac{1}{2}}-z^2G_{0\frac{1}{2}}$
4	3605.370v	20r-I	27,728.52	$b^4F_{2\frac{1}{2}}-z^2F_{0\frac{1}{2}}$	7	3502.998	2d	28,538.84	$b^2P_{\frac{1}{2}}-w^2P_{0\frac{1}{2}}$
5	3605.015	5-III	27,731.25	$a^2D_{1\frac{1}{2}}-w^4F_{0\frac{1}{2}}$	4	3502.63v	20r-I	28,541.81	$a^4F_{2\frac{1}{2}}-z^4D_{0\frac{1}{2}}$
4	3604.469v	4-II	27,735.45	$a^2H_{2\frac{1}{2}}-y^2H_{0\frac{1}{2}}$	4	3502.278v	100R-II	28,544.71	$b^4F_{2\frac{1}{2}}-y^4D_{0\frac{1}{2}}$
4	3602.38v	2	27,751.52	$a^2D_{1\frac{1}{2}}-35\phi_{\frac{1}{2}}$	5	3496.794	6-III	28,589.47	$z^2G_{2\frac{1}{2}}-e^2G_{0\frac{1}{2}}$
4	3602.079v	40R-II	27,753.86	$a^4F_{1\frac{1}{2}}-z^4F_{0\frac{1}{2}}$	5	3496.681	15-I	28,590.40	$b^4F_{2\frac{1}{2}}-z^2C_{0\frac{1}{2}}$
4	3600.803v	3-III	27,763.69	$b^2P_{1\frac{1}{2}}-z^2P_{0\frac{1}{2}}$	5	3496.070	3-III	28,595.39	$a^2H_{2\frac{1}{2}}$

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPLY DESIGNATION	REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPLY DESIGNATION
4	3487.29v	2	28,667.37	$2^6D_{3/2} - f^4F_{3/2}$	4	3426.454v	3-III	29,176.36	$2^6D_{3/2} - e^6P_{3/2}$
4	3485.700v	4-II	28,680.46	$b^4P_{1/2} - g^2S_{1/2}$	4	3424.500v	10-II	29,193.00	$a^2D_{3/2} - e^6D_{3/2}$
4	3485.368v	15-III	28,683.20	$2^6G_{3/2} - e^6H_{3/2}$	4	3424.00v	1	29,197.30	$b^4P_{3/2} - 5^6S_{3/2}$
4	3483.80v	6	28,696.10	$a^4F_{3/2} - g^2G_{3/2}$	4	3423.35v	1	29,202.84	$a^4P_{3/2} - y^2S_{3/2}$
4	3483.410v	20v-I	28,699.32	$b^4F_{3/2} - y^4F_{3/2}$	4	3422.900v	4-III	29,206.65	$a^4P_{3/2} - w^4D_{3/2}$
5	3483.141	2-III	28,701.54	$a^2P_{1/2} - y^2P_{1/2}$	5	3422.784	7	29,207.64	$2^6D_{3/2} - e^6F_{3/2}$
7	3482.590	1n	28,706.07	$b^4P_{1/2} - y^4P_{1/2}$	11	3422.497	1-IV	29,210.09	$2^6D_{3/2} - e^6F_{3/2}$
4	3482.07v	3	28,710.40	$b^2D_{1/2} - 1^6G_{3/2}$	4	3422.29v	2	29,211.84	$2^6D_{3/2} - e^6H_{3/2}$
4	3481.52v	1	28,714.85	$2^6G_{3/2} - e^6D_{3/2}$	4	3421.628v	3-III	29,217.51	$a^2D_{3/2} - w^6D_{3/2}$
4	3481.42v	1	28,715.74	$2^6G_{3/2} - f^6G_{3/2}$	5	3421.348	3	29,219.90	$2^6D_{3/2} - f^6F_{3/2}$
4	3480.29v	3	28,725.03	$c^2D_{3/2} - 3^6S_{3/2}$	7	3421.029	1	29,222.62	$a^2P_{1/2} - w^4D_{3/2}$
4	3480.012v	6-II	28,727.34	$b^4P_{3/2} - x^2D_{3/2}$	4	3420.790v	7-III	29,224.66	$a^2D_{3/2} - x^4P_{1/2}$
11	3479.579	1-III	28,730.92	$a^4P_{3/2} - z^2P_{1/2}$	4	3420.474v	5-II	29,227.36	$a^4P_{3/2} - w^4D_{3/2}$
5	3478.744	7-II	28,737.81	$b^4P_{3/2} - x^2D_{3/2}$	5	3417.795	6-I	29,250.27	$b^4F_{3/2} - z^4G_{3/2}$
5	3478.555	8-III	28,739.37	$a^2P_{1/2} - w^2F_{3/2}$	5	3417.673	5-III	29,251.31	$a^2P_{1/2} - x^2S_{1/2}$
4	3477.836v	4-III	28,745.31	$2^6G_{3/2} - 1^6D_{3/2}$	7	3417.353	1d	29,254.05	$b^2P_{1/2} - w^2F_{3/2}$
4	3477.64v	1	28,746.91	$2^6G_{3/2} - f^6H_{3/2}$	4	3417.154v	50v-II	29,255.76	$b^4F_{3/2} - y^4F_{3/2}$
5	3476.360#	5n-IV	28,757.51	$2^6G_{3/2} - e^6G_{3/2}$	4	3415.519v	5-I	29,269.76	$b^4F_{3/2} - z^4G_{3/2}$
11	3476.002	1	28,760.48	$a^4P_{1/2} - x^4F_{1/2}$	5	3414.736	200W	29,276.47	$b^4F_{3/2} - z^4D_{3/2}$
4	3474.530v	6-I	28,772.66	$b^4F_{3/2} - z^2D_{3/2}$	4	3413.52v	3NI?	29,286.94	$a^4F_{3/2} - z^4G_{3/2}$
4	3474.26v	6-2	28,774.86	$2^6D_{3/2} - f^6G_{3/2}$	4	3413.33v	1	29,288.53	$2^6G_{3/2} - e^6H_{3/2}$
11	3474.018	100R-II	28,776.90	$\{a^4F_{3/2} - z^4F_{3/2}$ $b^4F_{3/2} - w^4F_{3/2}$	4	3412.87v	2	29,292.50	$\{b^2G_{3/2} - 1^6H_{3/2}$ $2^6D_{3/2} - 1^6D_{3/2}$
7	3473.455	1-III	28,781.57	$b^4P_{1/2} - w^4F_{1/2}$	5	3412.633	80R-II	29,294.52	$a^4F_{3/2} - z^4D_{3/2}$
5	3472.707	6	28,787.76	$2^6G_{3/2} - f^6F_{3/2}$	5	3412.339	80R-II	29,297.04	$b^4F_{3/2} - y^2G_{3/2}$
7	3472.196	1-IV	28,792.00	$2^6G_{3/2} - e^6G_{3/2}$	5	3409.646	15	29,320.18	$b^4F_{3/2} - z^2D_{3/2}$
4	3471.382v	7-III	28,798.75	$2^6G_{3/2} - e^6G_{3/2}$	5	3409.177	60v-II	29,324.21	$b^4F_{3/2} - y^4F_{3/2}$
7	3469.683	8	28,812.85	$a^2H_{3/2} - w^2G_{3/2}$	5	3408.891	2-IV?	29,326.67	$\{2^6D_{3/2} - e^6G_{3/2}$ $2^6D_{3/2} - 2^6H_{3/2}$
4	3468.973v	3-III	28,818.75	$2^6G_{3/2} - f^6H_{3/2}$	4	3407.467v	2	29,338.93	$2^6D_{3/2} - 2^6H_{3/2}$
5	3468.52v	1-IV	28,821.92	$2^6D_{3/2} - 1^6D_{3/2}$	9	3406.89	1	29,343.89	$2^6D_{3/2} - e^6D_{3/2}$
11	3467.262	1-IV	28,832.97	$2^6G_{3/2} - f^6F_{3/2}$	5	3405.816	30R	29,353.15	
4	3465.792v	100R-II	28,845.20	$a^4F_{3/2} - z^4G_{3/2}$	5	3405.120	150R-II	29,359.15	$b^4F_{3/2} - y^4F_{3/2}$
4	3464.95v	1	28,852.24	$2^6G_{3/2} - e^6G_{3/2}$	5	3404.05v	1	29,368.36	$a^4F_{3/2} - h^4F_{3/2}$
5	3463.499	3-III	28,864.30	$a^4P_{1/2} - w^4D_{1/2}$	11	3403.166	1	29,376.00	$2^6F_{3/2} - f^6D_{3/2}$
4	3462.804v	60v-II	28,870.09	$b^4F_{1/2} - y^4F_{1/2}$	4	3402.18v	2	29,384.50	$b^4P_{3/2} - w^4G_{3/2}$
4	3461.173v	15-III	28,883.70	$2^6G_{3/2} - e^6H_{3/2}$	5	3402.064	4-III	29,385.52	$a^2P_{3/2} - x^2P_{3/2}$
4	3460.85v	1	28,886.43	$b^2D_{3/2} - 1^4G_{3/2}$	5	3401.913	20	29,386.82	$2^6D_{3/2} - e^6G_{3/2}$
4	3460.719	4-I	28,887.48	$a^2P_{3/2} - y^2F_{3/2}$	5	3401.617	2-III	29,389.38	$a^4P_{1/2} - z^2F_{1/2}$
4	3460.58v	1	28,888.69	$2^6D_{3/2} - f^6G_{3/2}$	4	3400.471v	1-III	29,399.29	$a^4P_{1/2} - w^4D_{1/2}$
5	3458.028	3-III	28,909.96	$a^2D_{3/2} - w^2D_{3/2}$	4	3399.93v	1w	29,403.95	$2^6G_{3/2} - e^6H_{3/2}$
4	3456.924v	9-I	28,919.20	$a^4F_{3/2} - z^4G_{3/2}$	4	3399.44v	1-IV	29,408.22	$a^2D_{3/2} - e^6D_{3/2}$
7	3456.525	1-IV	28,922.53	$a^2H_{3/2} - x^2H_{3/2}$	4	3398.811v	3-III	29,413.64	$2^6D_{3/2} - e^6G_{3/2}$
5	3456.437	1-IV	28,923.27	$2^6G_{3/2} - f^6H_{3/2}$	5	3396.457	1-III	29,434.03	$a^2D_{3/2} - e^6G_{3/2}$
4	3455.237v	25v-I	28,933.32	$a^4F_{1/2} - z^4D_{1/2}$	4	3395.370v	40v-II	29,443.45	$b^4F_{3/2} - y^2G_{3/2}$
4	3454.61v	2d?	28,938.54	$2^6G_{3/2} - g^6H_{3/2}$	5	3394.916	2-III	29,447.39	$a^4P_{3/2} - w^4D_{3/2}$
4	3454.47v	0	28,939.77	$2^6G_{3/2} - e^6G_{3/2}$	4	3393.16v	2	29,462.67	$2^6F_{3/2} - f^4F_{3/2}$
4	3453.514v	200R-II	28,947.75	$b^4F_{3/2} - y^4G_{3/2}$	4	3390.94v	1	29,481.92	$a^2D_{3/2} - w^4D_{1/2}$
4	3452.324v	3-III	28,957.73	$2^6G_{3/2} - e^6H_{3/2}$	7	3390.797	3-III	29,483.16	$2^6D_{3/2} - 3^6D_{3/2}$
4	3452.18v	2	28,958.98	$2^6G_{3/2} - f^6F_{3/2}$	4	3390.494	5-III	29,486.65	$a^2D_{3/2} - x^4P_{3/2}$
5	3449.706	5	28,979.70	$2^6G_{3/2} - f^6F_{3/2}$	11	3388.677	1-III	29,501.60	$a^4P_{1/2} - z^2P_{1/2}$
5	3449.441	60R-II	28,981.93	$b^4F_{3/2} - y^4G_{3/2}$	5	3388.494	3	29,503.20	$a^4G_{3/2} - w^4D_{3/2}$
5	3449.170	60R-II	28,984.21	$b^4F_{3/2} - y^4G_{3/2}$	5	3388.163v	30v-II	29,506.08	$b^4P_{3/2} - y^4F_{3/2}$
5	3448.358	4-III	28,991.03	$2^6G_{3/2} - 3^6D_{3/2}$	4	3387.47v	1-IV	29,512.09	$a^4P_{1/2} - x^2D_{1/2}$
5	3447.281	3-IV	29,000.09	$2^6G_{3/2} - e^6H_{3/2}$	5	3387.061	1-IV	29,515.68	$a^4P_{1/2} - w^4D_{1/2}$
4	3446.66v	1	29,005.33	$b^2D_{3/2} - e^2P_{3/2}$	11	3386.471	1g?	29,520.82	$2^6F_{3/2} - 1^6D_{3/2}$
5	3446.088	12-III	29,010.13	$2^6G_{3/2} - e^6H_{3/2}$	4	3385.559	6	29,528.77	$2^6D_{3/2} - f^6H_{3/2}$
4	3445.68v	2	29,013.54	$2^6D_{3/2} - f^6D_{3/2}$	4	3385.219v	25v-II	29,531.74	$2^6D_{3/2} - y^4G_{3/2}$
7	3445.445	1n	29,015.54	$2^6D_{3/2} - 2^6H_{3/2}$	4	3384.78v	4	29,535.57	$b^4F_{3/2} - y^4F_{3/2}$
4	3445.17v	1-III	29,017.87	$b^4P_{3/2} - w^4F_{3/2}$	4	3383.909v	4-III	29,543.17	$2^6D_{3/2} - e^6F_{3/2}$
4	3443.644v	80R-II	29,030.74	$b^4F_{3/2} - y^4G_{3/2}$	4	3383.18v	3	29,549.51	$2^6F_{3/2} - f^6D_{3/2}$
4	3443.42v	4	29,032.64	$2^6D_{3/2} - f^6F_{3/2}$	4	3382.96v	1	29,551.45	$a^2D_{3/2} - e^6D_{3/2}$
5	3443.203	5-III?	29,034.43		7	3382.071	2-III	29,559.22	$a^2P_{3/2} - x^2P_{1/2}$
4	3442.918v	40v-II	29,036.84	$\{a^4F_{3/2} - z^4D_{3/2}$ $(a^4P_{1/2} - w^4D_{1/2})$	5	3381.498	4-III	29,564.23	$a^2G_{3/2} - x^2G_{3/2}$
6	3441.255	3	29,050.87	$2^6G_{3/2} - f^6F_{3/2}$	4	3379.71v	1	29,570.86	$2^6G_{3/2} - e^6H_{3/2}$
5	3441.140	2-IV	29,051.84	$2^6G_{3/2} - e^6G_{3/2}$	4	3378.736v	5-III	29,588.40	$a^2P_{3/2} - y^2S_{1/2}$
4	3439.39v	4	29,066.62	$2^6D_{3/2} - h^4F_{3/2}$	4	3378.357v	3-III	29,591.72	$2^6D_{3/2} - f^6H_{3/2}$
5	3438.909	5-IV	29,070.69	$2^6G_{3/2} - e^6H_{3/2}$	4	3377.90v	2	29,595.75	$2^6G_{3/2} - e^6H_{3/2}$
5	3438.713	4-III	29,072.35	$a^2G_{3/2} - z^2H_{3/2}$	5	3377.060v	5-II	29,603.08	$a^4P_{3/2} - w^4D_{3/2}$
4	3438.47v	2	29,074.43	$2^6D_{3/2} - f^6D_{3/2}$	5	3376.934	2	29,604.18	$b^2P_{1/2} - 1^2H_{1/2}$
4	3438.18v	3w	29,076.81	$2^6G_{3/2} - g^6H_{3/2}$	4	3376.206v	2-III	29,610.57	$2^6F_{3/2} - f^4P_{3/2}$
4	3437.680v	6m-III	29,081.08	$2^6G_{3/2} - e^6H_{3/2}$	7	3375.238	1	29,619.06	$2^6F_{3/2} - e^6D_{3/2}$
11	3437.453	1	29,083.00	$2^6D_{3/2} - e^6D_{3/2}$	5	3374.303	5-III	29,627.27	$2^6D_{3/2} - f^6F_{3/2}$
4	3436.955v	3-III	29,087.22	$2^6D_{3/2} - f^6F_{3/2}$	4	3373.969v	4-III	29,630.20	$a^4P_{3/2} - z^2F_{3/2}$
10	3436.169	1	29,093.86	$a^4P_{1/2} - z^2P_{1/2}$	4	3373.33v	2	29,635.78	$2^6D_{3/2} - f^4F_{3/2}$
4	3435.95v	1	29,095.71	$a^2G_{3/2} - w^4D_{3/2}$	4	3373.226v	7-III	29,636.73	$a^2P_{3/2} - z^2S_{1/2}$
5	3435.753	8	29,097.39	$2^6D_{3/2} - e^6D_{3/2}$	4	3372.45v	2	29,643.58	$b^2D_{1/2} - f^2F_{3/2}$
11	3435.149	1	29,102.50	$2^6D_{3/2} - f^6G_{3/2}$	5	3371.015	2	29,656.17	$2^6F_{3/2} - f^6G_{3/2}$
4	3433.045v	60R-II	29,120.34	$b^4F_{1/2} - y^4F_{1/2}$	4	3370.80v	2	29,658.02	$2^6D_{3/2} - 5^6H_{3/2}$
5	3432.845	3	29,122.04	$a^2H_{3/2} - x^2H_{3/2}$	10	3370.322v	10-I	29,662.27	$b^4F_{3/2} - z^2D_{3/2}$
5	3432.318	3-III	29,126.51	$a^2D_{3/2} - x^4P_{1/2}$	4	3368.67	1	29,676.81	$a^2D_{3/2} - w^2D_{1/2}$
4	3431.582v	50v-II	29,132.76	$a^$					

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION
4	3362.797v	6-III	29,728.64	$2^8D_{04} - f^6F_{14}$	4	3305.109v	2-IV	30,247.51	
10	3362.085	1	29,734.93	$a^4F_{43} - 2^8G_{34}?$	4	3304.791v	1-IV	30,250.42	$a^2P_{13} - w^2P_{01}$
4	3361.553v	57-III	29,739.64	$2^8D_{04} - e^6G_{04}$	4	3304.119v	3-IV	30,256.57	$2^8F_{03} - e^6G_{03}$
5	3361.267	18	29,742.17	$a^4P_{23} - 2^8P_{01}$	4	3303.881v	4-II	30,258.75	$a^4P_{13} - y^4P_{01}$
5	3361.093	5	29,743.71	$2^8F_{03} - i^4F_{23}$	7	3302.781	1	30,268.83	$2^8D_{04} - f^6F_{14}$
4	3359.284v	6-III	29,759.73	$a^4P_{23} - 2^8F_{03}$	4	3299.11v	0	30,302.49	$2^8F_{03} - f^6G_{14}$
4	3359.066v	3-III	29,761.66	$b^4P_{13} - 2^8P_{01}$	4	3298.680v	6-III	30,306.46	$b^4P_{13} - v^4D_{01}$
4	3358.003v	3-III	29,771.08	$\{a^2P_{13} - 2^8P_{01}$ $\{a^2P_{13} - i^4D_{01}$	4	3297.22v	6	30,319.85	$2^8D_{04} - e^6H_{04}$
4	3356.842v	3-III	29,781.38	$2^8F_{03} - f^6G_{14}$	4	3296.19v	3	30,329.36	$2^8D_{04} - 4_{23}$
4	3356.464v	6-III	29,784.73	$a^2D_{13} - y^4S_{01}$	4	3294.536	2-IV	30,344.58	$2^8F_{03} - f^6F_{14}$
4	3355.940v	2-III	29,789.38	$a^2D_{13} - v^4D_{01}$	4	3294.48v	1	30,345.09	$a^4P_{13} - 5_{01}$
5	3355.118	3-III	29,796.68	$a^2P_{13} - i^4D_{01}$	5	3294.098	3	30,348.61	$2^8F_{03} - e^6G_{14}$
4	3354.374v	20-II	29,803.29	$b^4F_{33} - y^4F_{03}$	5	3293.861	2-III	30,350.80	$a^2D_{23} - w^2F_{03}$
5	3354.213	4-III?	29,804.72	$2^8F_{03} - f^6F_{14}$	4	3293.210v	3-III	30,356.80	$2^8F_{03} - e^6G_{14}$
4	3351.539v	3-III	29,828.50	$2^8F_{03} - 1_{23}$	4	3292.44v	2	30,363.94	$a^2P_{13} - 2^8S_{01}$
4	3351.138v	1-IV	29,832.06	$2^8F_{03} - f^6G_{14}$	4	3292.22v	1	30,365.96	$2^8F_{03} - e^6D_{13}$
5	3350.376	4h	29,838.85	$2^8F_{03} - h^4F_{23}$	4	3292.081v	3-III	30,367.21	$b^4P_{13} - y^4S_{01}$
4	3349.519v	7	29,846.49	$2^8F_{03} - f^6D_{13}$	5	3287.827	5	30,406.49	$a^4P_{23} - w^4F_{03}$
4	3349.204v	3h	29,849.29	$2^8D_{04} - i^4F_{23}$	4	3287.575v	2-III	30,408.83	$2^8F_{03} - e^6G_{14}$
4	3348.112v	8-II	29,859.03	$a^2D_{13} - v^4D_{03}$	4	3287.192v	7-II	30,412.37	$b^4P_{13} - v^2D_{01}$
5	3347.574	7	29,863.82	$2^8F_{03} - i^4F_{23}$	5	3286.545	1-III	30,418.35	$a^4P_{13} - 2^8S_{01}$
4	3346.932v	8-III	29,869.55	$2^8F_{03} - e^6D_{13}$	5	3285.874	5	30,424.57	$b^4P_{13} - v^2P_{01}?$
5	3346.310	1-III A	29,875.10	$a^4P_{13} - 2^8D_{03}$	5	3283.777	3-II	30,444.00	$a^4P_{13} - y^4P_{01}$
4	3345.57v	2	29,881.69	$b^2G_{43} - 21_{03}, 4_{3}$	5	3283.466v	9-I	30,446.88	$a^2D_{23} - w^2F_{03}$
7	3345.146	1	29,885.50	$a^4P_{13} - 2^8D_{03}$	5	3283.329	4-III	30,448.15	$a^2P_{13} - 2^8S_{01}$
4	3345.02v	3	29,886.63	$2^8D_{04} - f^6G_{14}$	5	3282.232	1-III	30,458.32	$a^4P_{13} - y^4P_{01}$
5	3344.245	2-III	29,893.55	$a^2D_{23} - v^2D_{03}$	7	3282.041	1-IV	30,460.10	$2^8F_{03} - f^6H_{14}$
7	3343.530	1	29,899.94	$a^2D_{23} - f^6G_{14}$	7	3281.820	2	30,462.15	$a^2P_{13} - 8_{01}$
5	3342.734	8-III	29,907.07	$a^2D_{23} - y^2P_{01}$	4	3281.585v	2-IA	30,464.34	$a^4F_{23} - 2^8F_{03}$
5	3342.564	4	29,908.59		4	3279.254v	5-II	30,485.99	$b^4P_{13} - v^4D_{01}$
4	3341.947v	5-III	29,914.11	$b^4P_{13} - w^2D_{03}$	4	3278.842v	6-III	30,489.82	$b^4P_{13} - y^2P_{01}$
4	3341.341v	5-III	29,919.53	$b^2G_{43} - 2^8F_{03}$	4	3278.105v	2-IV	30,496.67	$2^8F_{03} - e^6L_{03}$
4	3341.04v	5	29,922.22	$b^2D_{13} - u^2L_{01}$	4	3277.662v	3-III	30,500.79	$2^8F_{03} - f^6F_{14}$
4	3339.780v	8-III	29,933.51	$2^8F_{03} - e^6P_{23}$	4	3277.304v	4-III	30,504.12	$b^4P_{23} - w^2D_{03}$
4	3339.15v	4	29,939.15	$b^2G_{43} - 2^8F_{03}$	4	3276.483v	4-III	30,511.77	$2^8F_{03} - e^6G_{14}$
4	3338.71v	2	29,943.07	$b^2D_{23} - 1_{03}$	4	3276.23v	2	30,514.08	$2^8F_{03} - e^6H_{14}$
5	3338.519	1-III	29,944.82	$a^2P_{13} - 2^8P_{01}$	4	3275.66v	1	30,519.40	$a^4P_{13} - w^4F_{03}$
4	3337.50v	3	29,954.00	$2^8D_{04} - 3_{23}$	5	3273.931	10	30,535.55	$2^8F_{03} - f^6G_{14}$
4	3337.171v	8-I	29,956.92	$b^4F_{43} - y^2G_{04}$	4	3272.76v	1	30,546.49	$2^8F_{03} - f^6F_{14}$
4	3334.45v	1	29,981.38	$2^8D_{04} - 5_{13}, 2_{23}$	5	3272.405	3	30,549.79	$2^8F_{03} - f^6F_{14}$
4	3334.146v	30r-II	29,984.10	$\{b^4F_{43} - y^4F_{03}$ $\{a^2D_{13} - w^2D_{03}$ $\{b^2G_{43} - u^2D_{03}$	4	3271.198	8-II	30,555.64	$b^4P_{13} - v^4D_{03}$
7	3333.688	1n	29,988.22	$\{b^4F_{43} - y^4F_{03}$ $\{a^2D_{13} - w^2D_{03}$ $\{b^2G_{43} - u^2D_{03}$	4	3269.30v	2-IV	30,570.40	$2^8F_{03} - i^4F_{23}$
4	3333.388v	10-I	29,990.91	$\{b^4P_{13} - v^2D_{03}$ $\{b^4P_{13} - v^2D_{03}$	4	3268.894v	1-III	30,582.60	$b^4P_{23} - 2^8C_{03}$
4	3331.67v	2	30,006.36	$2^8F_{03} - f^6H_{14}$	4	3268.56v	2w	30,585.77	$a^4P_{23} - 5_{01}$
4	3330.81v	4w	30,014.12	$2^8D_{04} - f^6F_{14}$	4	3267.998v	1-IV	30,590.99	
4	3329.466v	5-III	30,026.24	$2^8F_{03} - e^6D_{13}$	4	3267.68v	2	30,593.98	$2^8P_{01} - G_{1}$
4	3329.013v	2-III	30,030.33	$2^8F_{03} - f^6F_{14}$	4	3266.47v	4	30,605.30	$a^2G_{03} - 6_{03}$
4	3328.207v	3-III	30,037.60	$2^8F_{03} - 2_{13}$	4	3265.352v	3-III	30,615.77	$a^2D_{23} - u^4D_{03}$
4	3327.50v	4w	30,043.94	$2^8D_{04} - e^6H_{14}$	4	3264.842v	5-I	30,620.56	$\{a^2D_{13} - y^2P_{01}$ $\{a^4F_{23} - y^4D_{03}$ $\{2^8F_{03} - e^6D_{13}$
5	3326.991	8-III	30,048.57	$2^8F_{03} - f^6F_{14}$	7	3264.718	7h	30,621.72	$a^4P_{13} - y^4P_{01}$
5	3326.564	2-III A	30,052.43	$a^4P_{23} - w^4F_{03}$	4	3263.213v	4-II	30,635.84	$a^2P_{13} - w^2P_{01}$
4	3326.38v	0	30,054.10	$a^2P_{13} - i^4D_{03}$	4	3260.814v	9-II	30,658.38	$a^2D_{13} - w^2F_{03}$
4	3326.27v	1	30,055.06	$\{a^4P_{13} - 2^8S_{01}$ $\{2^8D_{04} - e^6C_{04}$	4	3260.72v?	-	30,659.31	$b^2P_{13} - w^4P_{03}$
4	3325.43v	2	30,062.69	$a^2P_{13} - w^4S_{01}$	5	3260.286	5	30,663.34	$2^8F_{03} - e^6G_{14}$
4	3325.240v	10-II	30,064.40	$b^4P_{13} - v^4D_{01}$	5	3259.847	3	30,667.48	
4	3324.81v	2w	30,068.26	$b^2G_{43} - v^2G_{04}$	4	3259.20v	6	30,673.60	$2^8F_{03} - e^6D_{13}$
4	3324.70v	1	30,069.31	$b^2D_{23} - 1_{70}, 1_{3}$	4	3258.418v	1-III	30,680.92	$b^4P_{13} - w^2D_{03}$
4	3322.198v	8-III	30,091.93	$\{a^2D_{13} - y^4S_{01}$ $\{b^2G_{43} - v^2G_{04}$	4	3258.035v	4-III	30,684.53	$a^4P_{23} - y^4P_{03}$
5	3321.912	2-III	30,094.51	$a^2D_{23} - u^4D_{03}$	4	3254.63v	9	30,716.60	$2^8F_{03} - e^6G_{14}$
4	3319.822v	4-III	30,113.46	$2^8F_{03} - e^6D_{13}$	4	3254.202v	12-II	30,720.67	$b^4P_{23} - 2^8P_{01}$
5	3319.561	8	30,115.83	$a^4P_{23} - 2^8D_{03}$	4	3253.416	1-IV	30,728.09	$b^4P_{13} - v^4D_{01}$
5	3319.478	8-II	30,116.58	$2^8F_{03} - e^6G_{03}$	4	3251.656v	2	30,744.72	$a^4F_{23} - f^6F_{14}$
5	3319.156	4-III	30,119.51	$2^8F_{03} - e^6P_{23}$	4	3250.51v	5w	30,755.57	$2^8F_{03} - e^6G_{14}$
4	3318.60v	1	30,124.60	$2^8F_{03} - f^6G_{14}$	5	3250.335	4	30,757.22	$a^2G_{43} - w^2F_{03}$
4	3318.398v	4-II	30,126.38	$a^4P_{23} - 2^8D_{03}$	4	3249.995v	6-II	30,760.44	$b^4F_{23} - w^4F_{03}$
4	3317.93v	0	30,130.63	$b^4P_{13} - 2^8P_{01}$	4	3247.170v	8-II	30,787.20	$\{b^4P_{23} - v^4D_{03}$ $\{2^8F_{03} - e^6H_{14}$
5	3315.035	3-III	30,156.94	$\{a^2P_{13} - i^4D_{03}$ $\{2^8F_{03} - e^6G_{14}$	5	3246.997	4-III	30,788.83	$b^4P_{13} - y^4S_{01}$
5	3314.345	2-V	30,163.22	$2^8F_{03} - f^6F_{14}$	4	3245.750v	3	30,800.67	$a^2H_{43} - 2^8G_{04}$
4	3314.073v	8-III	30,165.70	$\{b^2G_{43} - v^2G_{04}$ $\{2^8F_{03} - i^4F_{23}$	4	3243.840v	8-II	30,818.80	$b^4P_{23} - 2^8P_{01}$
4	3313.38v	1	30,171.99	$2^8F_{03} - i^4F_{23}$	5	3243.579	2-III	30,821.28	$a^4P_{13} - y^4P_{03}$
4	3313.116v	2-IV	30,174.41	$\{a^2P_{23} - e^6D_{13}$ $\{a^4P_{23} - 4_{03}$	5	3241.548v	5	30,840.59	$2^8F_{03} - e^6H_{03}$
4	3312.825v	3-III	30,177.06	$\{2^8F_{03} - i^4F_{23}$ $\{a^2P_{13} - i^4D_{03}$	4	3241.05v	3	30,845.31	$a^4F_{13} - y^4D_{03}$
5	3312.277	3	30,182.05	$b^4P_{13} - 2^8P_{01}$	7	3239.256	1	30,862.41	$a^4P_{23} - y^4P_{01}$
5	3312.148	7-II	30,183.23	$b^4P_{13} - 2^8P_{01}$	4	3238.92v	5	30,865.59	$2^8F_{03} - 4_{23}$
4	3311.48v	3	30,189.28	$b^2G_{43} - v^2G_{04}$	4	3237.80v	2	30,876.25	$b^2D_{23} - 2^8F_{03}$
4	3310.16v	1	30,201.32	$a^2D_{13} - v^4D_{03}$	4	3237.028v	8-II	30,883.65	$a^4F_{23} - 2^8G_{04}$
5	3309.017	2	30,211.79	$b^2P_{13} - u^2F_{03}$	5	3235.783	5h	30,895.53	$b^4P_{13} - y^2P_{01}$
4	3308.814v	4-III	30,213.64	$2^8F_{03} - e^6D_{23}$	4	3235.532v	6-II	30,897.93	$\{a^2H_{43} - e^6G_{03}$ $\{b^4P_{13} - v^2D_{03}$
7	3308.688	1	30,214.79	$a^2D_{13} - y^2P_{01}$	5	3234.119	1-IV	30,911.43	$a^4P_{13} - y^4S_{01}$
4	3308.482v	4-III	30,216.68	$2^8F_{03} - e^6P_{13}$	4	3232.874v	60	30,923.33	$a^2D_{13} - w^2D_{03}$

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPLT DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPLT DESIGNATION
5	3223.147	1-III A	31,016.65	$b^4F_{13} - y^2D_{0\frac{1}{2}}$	4	3109.506v	4-III	32,150.15	$\left\{ \begin{array}{l} a^4P_{13} - y^2D_{0\frac{1}{2}} \\ (a^2P_{13} - y^2P_{0\frac{1}{2}}) \end{array} \right.$
4	3220.62v	4	31,040.99	$z^6F_{0\frac{1}{2}} - f^6F_{0\frac{1}{2}}$	4	3108.48v	1	32,160.74	$a^2F_{13} - z^4S_{0\frac{1}{2}}$
4	3219.150v	5-II	31,055.17	$a^4F_{13} - z^2F_{0\frac{1}{2}}$	4	3108.223	1	32,163.40	$a^2P_{13} - y^4S_{0\frac{1}{2}}$
5	3216.996	1-III	31,075.95	$b^4P_{13} - y^4D_{0\frac{1}{2}}$	4	3107.540v	1-IV	32,170.49	$a^2P_{13} - y^2P_{0\frac{1}{2}}$
4	3215.332v	1-IV	31,092.04	$z^6F_{0\frac{1}{2}} - e^6H_{0\frac{1}{2}}$	5	3107.044	3-III	32,175.62	$a^2P_{13} - y^4D_{0\frac{1}{2}}$
4	3211.01v	4	31,133.87	$z^6F_{0\frac{1}{2}} - e^6G_{0\frac{1}{2}}$	4	3106.142v	1-III A	32,184.97	$b^4F_{13} - y^2D_{0\frac{1}{2}}$
4	3210.85v	3n-IV	31,135.41		4	3105.929v	3-II	32,187.18	$b^4F_{13} - y^2F_{0\frac{1}{2}}$
4	3210.219v	5-III	31,141.56	$a^2D_{13} - u^4D_{0\frac{1}{2}}$	5	3103.983	5-III	32,207.35	$a^2P_{13} - u^4P_{0\frac{1}{2}}$
4	3209.80v	1	31,145.57	$b^4P_{13} - y^4D_{0\frac{1}{2}}$	4	3103.735v	5-III	32,209.93	$b^4P_{13} - u^4S_{0\frac{1}{2}}$
4	3208.85v	1	31,154.84	$b^2D_{13} - u^2D_{0\frac{1}{2}}$	4	3102.405v	4-III	32,223.74	$a^2P_{13} - y^4D_{0\frac{1}{2}}$
4	3205.883v	1-IV	31,183.67	$b^2D_{13} - z^2F_{0\frac{1}{2}}$	4	3100.33v	5	32,245.32	$b^2D_{13} - 23_{0\frac{1}{2}}$
4	3205.40v	0	31,188.34	$a^2F_{13} - z^4D_{0\frac{1}{2}}$	4	3100.15v	6d	32,247.22	$a^2D_{13} - u^2P_{0\frac{1}{2}}$
4	3204.77v	1	31,194.54	$z^6F_{0\frac{1}{2}} - e^6H_{0\frac{1}{2}}$	4	3099.667v	2-III	32,252.20	$b^4P_{13} - z^2S_{0\frac{1}{2}}$
4	3203.026v	4-I	31,211.49	$a^4F_{13} - y^4D_{0\frac{1}{2}}$	4	3098.194v	10-II	32,267.53	$a^4F_{13} - y^4C_{0\frac{1}{2}}$
4	3199.322v	4-I	31,247.62	$a^4F_{13} - y^4D_{0\frac{1}{2}}$	4	3096.705v	2-III	32,283.05	$a^2D_{13} - z^4S_{0\frac{1}{2}}$
4	3198.660v	5-II	31,254.09	$b^4F_{13} - y^2F_{0\frac{1}{2}}$	4	3096.402v	3-III	32,286.21	$a^4P_{13} - y^2P_{0\frac{1}{2}}$
4	3196.93v	2v	31,270.96	$b^4P_{13} - u^2D_{0\frac{1}{2}}$	4	3095.716v	3-III	32,293.36	$a^4P_{13} - y^4D_{0\frac{1}{2}}$
4	3196.74v	1	31,272.86	$z^6F_{0\frac{1}{2}} - 4s_1?$	4	3090.251v	4-III	32,350.47	$b^4P_{13} - u^4D_{0\frac{1}{2}}$
7	3196.423	1	31,275.96	$b^2D_{13} - u^2D_{0\frac{1}{2}}$	4	3089.596v	10-II	32,357.33	$\left\{ \begin{array}{l} a^4F_{13} - y^4C_{0\frac{1}{2}} \\ (a^2F_{13} - z^4D_{0\frac{1}{2}}) \\ (a^2D_{13} - u^2S_{0\frac{1}{2}}) \end{array} \right.$
4	3193.164v	5-II	31,307.88	$b^4F_{13} - y^2F_{0\frac{1}{2}}$	4	3087.806v	3-III	32,376.09	$b^4P_{13} - u^4D_{0\frac{1}{2}}$
4	3192.220v	3-III	31,317.14	$b^4P_{13} - y^2P_{0\frac{1}{2}}$	4	3087.35v	2	32,380.91	$a^2D_{13} - 8_{0\frac{1}{2}}$
4	3191.297v	4-II	31,326.20	$a^4F_{13} - z^2C_{0\frac{1}{2}}$	4	3086.83v?	1?	32,386.30	$b^4P_{13} - z^2P_{0\frac{1}{2}}$
7	3190.910	1	31,329.99	$a^2P_{13} - 12_{0\frac{1}{2}}$	4	3086.777v	15r-II	32,386.88	$a^4F_{13} - y^4F_{0\frac{1}{2}}$
4	3189.752v	5-I	31,341.37	$a^4F_{13} - y^4D_{0\frac{1}{2}}$	4	3086.393v	4-III	32,390.90	$a^4P_{13} - y^2D_{0\frac{1}{2}}$
4	3188.377v	7-III	31,354.88	$b^4P_{13} - u^2F_{0\frac{1}{2}}$	4	3085.65v	3	32,398.72	$a^2H_{13} - 25_{0\frac{1}{2}}$
4	3187.60v	3	31,362.52	$b^2P_{13} - 16_{0\frac{1}{2}}$	4	3083.749v	1	32,418.68	$a^4P_{13} - u^2D_{0\frac{1}{2}}$
4	3187.34v	4	31,365.13	$a^2P_{13} - u^2P_{0\frac{1}{2}}$	4	3082.844	2-III	32,428.19	$b^4P_{13} - u^4D_{0\frac{1}{2}}$
4	3186.350v	5-I	31,374.83	$a^4F_{13} - z^2F_{0\frac{1}{2}}$	4	3082.614v	12r-II	32,430.61	$\left\{ \begin{array}{l} a^4F_{13} - y^4C_{0\frac{1}{2}} \\ (a^2F_{13} - z^4D_{0\frac{1}{2}}) \end{array} \right.$
4	3185.948v	2-III	31,378.79	$b^4P_{13} - y^4S_{0\frac{1}{2}}$	4	3079.394v	5-II	32,464.52	$\left\{ \begin{array}{l} a^4P_{13} - y^4C_{0\frac{1}{2}} \\ (a^2P_{13} - u^4D_{0\frac{1}{2}}) \end{array} \right.$
4	3182.118v	7-III	31,416.55	$b^4P_{13} - u^4D_{0\frac{1}{2}}$	4	3073.520v	3-III	32,526.56	$a^4P_{13} - y^4S_{0\frac{1}{2}}$
4	3180.290v	2-III	31,434.61	$a^2D_{13} - u^4D_{0\frac{1}{2}}$	5	3072.664	20	32,535.62	$a^2P_{13} - u^2P_{0\frac{1}{2}}$
4	3179.828v	1-IV	31,439.18	$a^2D_{13} - u^4D_{0\frac{1}{2}}$	4	3072.341v	15r-II	32,539.04	$a^4F_{13} - y^4F_{0\frac{1}{2}}$
4	3177.266v	8-III	31,464.53		4	3071.957v	6-I	32,543.11	$a^4F_{13} - z^2D_{0\frac{1}{2}}$
4	3174.905v	4-III	31,487.93	$b^4P_{13} - y^2D_{0\frac{1}{2}}$	4	3070.857	1-IV	32,554.77	$a^2D_{13} - u^2P_{0\frac{1}{2}}$
4	3174.140v	2-III	31,495.51	$a^2H_{13} - y^2C_{0\frac{1}{2}}$	5	3070.752	5	32,555.88	$a^2P_{13} - z^2P_{0\frac{1}{2}}$
4	3173.56v	1	31,501.30	$b^4P_{13} - z^2P_{0\frac{1}{2}}$	7	3070.550	1	32,558.02	$b^4P_{13} - z^4S_{0\frac{1}{2}}$
4	3173.140v	1-III	31,505.44	$a^4P_{13} - z^4P_{0\frac{1}{2}}$	4	3070.34v	1	32,560.26	$b^4P_{13} - z^2P_{0\frac{1}{2}}$
4	3169.766v	9-III	31,538.97	$a^2D_{13} - y^2F_{0\frac{1}{2}}$	7	3069.032	1	32,574.13	$b^2P_{13} - u^2D_{0\frac{1}{2}}$
4	3168.060	6-III	31,555.96	$a^2D_{13} - z^2P_{0\frac{1}{2}}$	4	3064.370v	5-II	32,623.68	$a^4F_{13} - y^2C_{0\frac{1}{2}}$
5	3161.652v	5-III	31,619.91	$b^4P_{13} - u^4D_{0\frac{1}{2}}$	4	3063.25v	1	32,635.58	$a^2P_{13} - y^2D_{0\frac{1}{2}}$
4	3159.662v	10-II	31,639.83	$\left\{ \begin{array}{l} a^4F_{13} - y^4D_{0\frac{1}{2}} \\ (b^4F_{13} - y^2F_{0\frac{1}{2}}) \end{array} \right.$	4	3062.46v	1	32,643.97	$a^2F_{13} - 2_{0\frac{1}{2}}?$
4	3158.772v	12-II	31,648.74	$a^4F_{13} - y^4C_{0\frac{1}{2}}$	4	3062.199v	5-II	32,646.81	$a^4F_{13} - z^2L_{0\frac{1}{2}}$
7	3158.458	1	31,651.89	$a^4P_{13} - u^2D_{0\frac{1}{2}}$	4	3061.983	1	32,649.11	$a^4P_{13} - y^2P_{0\frac{1}{2}}$
7	3158.293	1	31,653.54	$a^4P_{13} - z^2D_{0\frac{1}{2}}$	7	3061.822v	20r-II	32,650.83	$a^4F_{13} - y^4F_{0\frac{1}{2}}$
4	3157.090v	1-III	31,665.60	$a^2D_{13} - u^4D_{0\frac{1}{2}}$	4	3061.013v	1-III	32,659.46	$a^4P_{13} - u^2D_{0\frac{1}{2}}$
4	3154.794v	10-II	31,688.65	$b^4P_{13} - u^4D_{0\frac{1}{2}}$	4	3060.048v	5-III	32,669.76	$b^4P_{13} - u^4D_{0\frac{1}{2}}$
5	3154.678	5-III	31,689.81	$a^2D_{13} - z^2P_{0\frac{1}{2}}$	4	3056.668v	2	32,705.88	$a^2D_{13} - 10_{0\frac{1}{2}}$
7	3153.692	1	31,699.72	$a^4F_{13} - z^2P_{0\frac{1}{2}}$	5	3054.724	4-II	32,726.69	$a^4F_{13} - y^2C_{0\frac{1}{2}}$
4	3152.707v	6-III	31,709.62	$b^4P_{13} - u^4D_{0\frac{1}{2}}$	5	3054.132	18	32,733.04	$a^4F_{13} - z^2G_{0\frac{1}{2}}$
7	3152.120	1	31,715.53	$b^4P_{13} - u^4D_{0\frac{1}{2}}$	5	3050.932	60	32,767.37	$a^4F_{13} - y^4S_{0\frac{1}{2}}$
5	3150.819	2-V	31,728.62	$a^2P_{13} - 12_{0\frac{1}{2}}$	4	3050.496v	3-III	32,772.05	$b^4P_{13} - u^4D_{0\frac{1}{2}}$
5	3150.655	2-V	31,730.27		4	3048.888v	12r-II	32,789.34	$a^4F_{13} - y^4F_{0\frac{1}{2}}$
4	3149.310v	10-II	31,743.82	$a^4F_{13} - y^4D_{0\frac{1}{2}}$	4	3048.108v	2-IV	32,797.73	$b^4P_{13} - u^4D_{0\frac{1}{2}}$
4	3147.060v	15r-II	31,766.52	$a^4F_{13} - y^4C_{0\frac{1}{2}}$	4	3044.004v	30R-II	32,841.94	$\left\{ \begin{array}{l} a^4F_{13} - y^4F_{0\frac{1}{2}} \\ (b^4P_{13} - y^2F_{0\frac{1}{2}}) \end{array} \right.$
4	3145.49v	15r?	31,782.37	$b^4P_{13} - y^4S_{0\frac{1}{2}}$	4	3042.481v	8-II	32,858.38	$a^4F_{13} - y^4C_{0\frac{1}{2}}$
4	3145.022v	3-III	31,787.10	$a^4P_{13} - y^2D_{0\frac{1}{2}}$	4	3040.812v	1-IV	32,876.42	$a^2P_{13} - y^2D_{0\frac{1}{2}}$
4	3143.814v	2	31,799.32	$b^4F_{13} - y^2D_{0\frac{1}{2}}$	4	3039.563v	3-III	32,889.93	$a^2P_{13} - y^2P_{0\frac{1}{2}}$
4	3140.715v	2-IV	31,830.69	$b^4P_{13} - z^2S_{0\frac{1}{2}}$	4	3038.302v	2-III	32,903.57	$a^2F_{13} - z^4D_{0\frac{1}{2}}$
4	3139.947v	12-II	31,838.48	$\left\{ \begin{array}{l} a^4F_{13} - y^4D_{0\frac{1}{2}} \\ (b^4P_{13} - u^4D_{0\frac{1}{2}}) \end{array} \right.$	4	3034.432v	6-II	32,945.53	$a^4P_{13} - z^2D_{0\frac{1}{2}}$
7	3138.893	1	31,849.17	$a^2G_{13} - z^2F_{0\frac{1}{2}}$	4	3034.08v	1	32,949.30	$\left\{ \begin{array}{l} b^2D_{13} - 34_{0\frac{1}{2}, 2\frac{1}{2}} \\ (b^2P_{13} - 23_{0\frac{1}{2}}) \end{array} \right.$
4	3138.36v	2	31,854.58	$b^2P_{13} - u^2P_{0\frac{1}{2}}$	4	3031.51v	0	32,977.28	$a^2G_{13} - y^2H_{0\frac{1}{2}}$
4	3137.755v	4-III	31,860.72	$a^4P_{13} - y^4D_{0\frac{1}{2}}$	4	3031.288v	2-III	32,979.70	$b^4P_{13} - z^4S_{0\frac{1}{2}}$
7	3137.454	3-III	31,863.78	$a^2D_{13} - z^2P_{0\frac{1}{2}}$	4	3028.184v	1	33,013.51	
4	3137.328v	10-II	31,865.05	$a^4F_{13} - y^4C_{0\frac{1}{2}}$	4	3026.373v	6-III	33,033.26	
5	3136.999	1-III	31,868.40	$a^4P_{13} - z^4P_{0\frac{1}{2}}$	4	3024.400v	1	33,054.81	$\left\{ \begin{array}{l} a^4P_{13} - u^2P_{0\frac{1}{2}} \\ (b^4P_{13} - 7_{0\frac{1}{2}}) \end{array} \right.$
4	3136.726v	5-II	31,871.17	$a^4F_{13} - z^2F_{0\frac{1}{2}}$	4	3023.590v	1	33,063.67	$b^4P_{13} - u^2S_{0\frac{1}{2}}$
4	3134.62v	2	31,892.56	$a^4P_{13} - u^2D_{0\frac{1}{2}}$	4	3023.11v	0	33,077.18	$a^2D_{13} - 11_{0\frac{1}{2}}$
4	3132.218v	4-II	31,917.04	$a^4F_{13} - z^2C_{0\frac{1}{2}}$	4	3022.355v	3-III	33,077.18	$a^4P_{13} - u^4D_{0\frac{1}{2}}$
4	3131.829v	1-IV	31,921.00	$a^4P_{13} - z^4P_{0\frac{1}{2}}$	4	3020.96v	1	33,092.46	$a^4P_{13} - u^2F_{0\frac{1}{2}}$
4	3129.481v	3-III	31,944.95	$b^4P_{13} - u^2F_{0\frac{1}{2}}$	4	3020.85v	2	33,093.65	$a^2H_{13} - 25_{0\frac{1}{2}}$
4	3129.006v	3-II	31,949.80	$b^4F_{13} - y^2D_{0\frac{1}{2}}$	4	3017.548v	15r-II	33,129.87	$a^4F_{13} - y^4F_{0\frac{1}{2}}$
4	3127.252v	7-I	31,967.72	$b^4F_{13} - y^2F_{0\frac{1}{2}}$	4	3017.254v	3-III	33,133.09	$b^4P_{13} - y^2F_{0\frac{1}{2}}$
5	3126.725	4-III	31,973.11	$a^2D_{13} - u^4D_{0\frac{1}{2}}$	4	3015.686v	3-III	33,150.32	$b^4P_{13} - z^2P_{0\frac{1}{2}}$
5	3126.488	1-IV	31,975.53	$a^2D_{13} - z^4S_{0\frac{1}{2}}$	4	3013.592v	8-II	33,173.36	$a^4F_{13} - y^4C_{0\frac{1}{2}}$
5	3121.566	10-II	32,025.95	$a^4F_{13} - y^4F_{0\frac{1}{2}}$	4	3010.01v	0	33,212.85	$a^4P_{13} - u^4D_{0\frac{1}{2}}$
5									

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION
4	2996.76v	2	33,359.70	$a^2G_{33} - w^2G_{043}$	4	2859.654v	40	34,959.02	$b^4F_{23} - x^4D_{033}$
4	2996.549v	1-IV	33,362.02	$b^4P_{23} - t^4D_{013}$	4	2857.98v	0	34,979.48	$b^2G_{23} - 36^0_{33}, 43$
7	2995.248	1	33,376.51	$a^2D_{13} - 11^0_{23}$	4	2857.21v	1	34,988.97	$a^4F_{13} - w^2F_{013}$
4	2995.150v	50	33,377.60	$a^2G_{33} - w^2G_{033}$	4	2856.98v	0	34,991.72	$a^2F_{23} - x^4F_{023}$
4	2990.51v	4	33,429.42	$a^4P_{23} - w^2F_{033}$	4	2856.04v	1	35,003.20	$b^2G_{43} - 36^0_{33}, 43$
4	2989.590v	15r-II	33,439.68	$a^4F_{43} - y^2G_{043}$	4	2851.74v	2	35,056.03	$a^4P_{13} - 8^0_{13}$
4	2987.166v	15r-II	33,466.81	$a^4F_{43} - y^2F_{023}$	4	2850.947v	30	35,065.79	$a^4F_{13} - y^2D_{013}$
4	2986.10v	0	33,478.74	$a^2G_{33} - u^2F_{023}$	4	2850.047v	75	35,076.86	$a^2F_{23} - z^2P_{013}$
4	2983.68v	0	33,505.88	$a^4P_{13} - u^4D_{03}$	4	2849.38v	2	35,085.03	$a^2D_{23} - 16^0_{23}$
4	2983.50v	2	33,507.96	$a^2F_{23} - z^2P_{023}$	4	2848.61v	0	35,094.59	$a^2F_{23} - x^2F_{023}?$
4	2982.262v	1-III	33,521.84	$a^2F_{23} - z^2P_{013}$	4	2842.382v	30	35,171.44	$b^4P_{13} - w^2P_{013}$
7	2978.950	1n	33,559.11	$b^4P_{23} - w^2P_{013}$	4	2837.154v	75r	35,236.25	$a^2D_{23} - w^4P_{013}$
4	2978.010v	30	33,569.70	$b^4P_{23} - x^4S_{013}$	4	2836.64v	0	35,242.68	$a^2G_{33} - 18^0_{33}$
4	2977.462v	1	33,575.88	$a^4P_{13} - u^4D_{013}$	4	2834.428v	50	35,270.14	$b^4F_{13} - x^4D_{023}$
4	2975.464v	4	33,598.43	$a^4P_{23} - u^4D_{023}$	4	2833.922v	40	35,276.43	$a^4F_{23} - y^2D_{023}$
4	2975.35v	1	33,599.68	$a^2P_{13} - 17^0_{23}$	4	2828.466v	15	35,344.48	$b^4P_{13} - s^4D_{023}$
4	2973.123v	1	33,624.88	$a^2P_{13} - w^4P_{013}$	4	2826.797v	50W	35,365.34	$a^2D_{13} - s^4D_{013}$
4	2972.93v	1	33,627.05	$a^4P_{13} - x^2S_{013}$	4	2825.89v	0	35,376.66	$a^2D_{13} - s^4D_{013}$
4	2972.30v	0	33,634.23	$a^2D_{13} - 12^0_{23}$	5	2825.151	75w	35,385.95	$b^4P_{13} - w^4P_{023}$
4	2971.363v	1	33,644.78	$b^4P_{23} - 7^0_{23}$	4	2824.62v	1	35,392.58	$a^2D_{13} - 16^0_{23}$
4	2969.79v	1	33,662.60	$a^2F_{23} - 2^0_{23}$	4	2824.45v	1	35,394.68	$b^4P_{23} - u^2F_{023}$
7	2969.617	1w	33,664.58	$a^2G_{33} - x^2H_{043}$	5	2823.647	5h	35,404.80	$a^2G_{43} - t^2F_{033}?$
4	2969.24v	2	33,668.84	$a^2F_{23} - x^2F_{043}$	5	2821.745	30h	35,428.66	$(a^2F_{23} - a^2D_{013})$
4	2959.16v	1	33,783.52	$a^2F_{23} - x^2F_{043}$	4	2820.002v	50	35,450.55	$(a^2F_{43} - a^2D_{023})$
4	2957.672v	50	33,800.53	$a^2D_{23} - u^2F_{023}$	5	2819.174	10	35,460.97	$a^2F_{23} - a^2D_{023}$
4	2955.382v	30	33,826.72	$a^2D_{23} - w^2G_{033}$	4	2818.592v	30	35,468.29	$a^2F_{23} - y^2D_{023}$
4	2954.83v	1?	33,833.01	$a^4P_{13} - u^4D_{033}$	4	2815.555v	50r	35,468.29	$a^2F_{23} - x^2D_{023}$
4	2951.69v	1	33,868.99	$a^2G_{33} - s^4D_{023}$	4	2814.970v	25	35,513.85	$b^4F_{23} - x^4D_{023}$
4	2948.49v	1	33,905.74	$a^2G_{43} - y^2H_{033}$	5	2812.449	3	35,545.75	$b^4F_{23} - x^4D_{023}$
4	2948.30v	2	33,907.94	$a^2G_{43} - y^2H_{033}$	4	2811.508v	50w	35,557.65	$b^4F_{13} - x^4S_{013}$
4	2946.01v	0	33,934.36	$a^2G_{33} - u^2F_{023}$	4	2811.126v	50	35,562.48	$a^2G_{33} - t^2F_{023}$
4	2944.58v	2	33,950.79	$a^2G_{33} - 15^0_{23}?$	4	2811.098v	5	35,651.61	$b^4P_{13} - s^4D_{013}$
4	2943.479v	30	33,963.50	$a^2D_{23} - s^4D_{023}$	4	2803.770v	100	35,655.78	$b^4F_{23} - x^4D_{023}$
4	2942.624v	1	33,973.37	$a^2P_{23} - x^4F_{023}$	4	2800.42v	00	35,698.48	$a^2D_{23} - 18^0_{23}$
4	2941.993v	1	33,980.66	$b^4P_{13} - w^2S_{013}$	4	2799.37v	0	35,711.83	$a^2H_{43} - 36^0_{43}, 43$
4	2941.182v	1	33,990.03	$(a^4F_{23} - y^2F_{033})$	4	2797.081v	50	35,741.04	$(a^2F_{23} - w^4F_{023})$
4	2936.546v	1	34,043.68	$(a^4P_{23} - 6^0_{23})$	4	2796.228v	50	35,751.94	$(b^4P_{23} - w^2P_{013})$
4	2934.014v	5	34,073.06	$b^4P_{13} - 11^0_{23}$	4	2796.228v	50	35,751.94	$b^4F_{13} - x^4D_{013}$
4	2929.505v	75	34,125.50	$a^2G_{43} - w^2G_{043}$	5	2795.819	15	35,757.17	$a^2F_{23} - x^4G_{023}$
4	2928.812v	50	34,133.58	$a^2G_{43} - w^2G_{043}$	4	2792.436v	40	35,800.49	$a^2F_{23} - w^2D_{023}$
4	2927.970v	4	34,143.39	$a^2G_{43} - w^2G_{043}$	4	2791.430v	2	35,813.39	
4	2927.667v	50	34,146.92	$a^2D_{23} - w^2P_{013}$	4	2791.009v	50	35,818.80	$b^4P_{13} - w^4P_{013}$
4	2919.552v	30	34,241.83	$a^2D_{13} - u^2F_{023}$	4	2790.284v	30h	35,828.10	
4	2917.12v	1	34,270.38	$a^2G_{43} - 13^0_{23}, 43$	4	2787.016v	5	35,870.11	$a^2G_{33} - s^2F_{023}$
7	2916.041	1	34,283.06	$a^4F_{13} - y^2D_{023}$	4	2785.899v	50	35,884.49	$a^2D_{13} - w^4P_{013}$
4	2914.608v	7	34,299.91	$a^2P_{13} - u^2D_{013}$	4	2782.258v	3	35,931.45	$b^4F_{23} - z^4S_{013}$
4	2911.970v	5	34,330.99	$b^4P_{13} - 12^0_{23}$	4	2782.11v	0	35,933.40	$a^2F_{23} - w^4G_{023}?$
4	2911.560v	5	34,335.82	$a^2F_{23} - x^4F_{013}$	5	2781.032	8	35,947.28	
4	2910.31v	1	34,350.61	$a^2F_{23} - x^4G_{033}$	4	2778.813v	75	35,975.99	$b^4P_{23} - w^4P_{023}$
4	2909.984v	4	34,354.42	$a^4P_{13} - x^4S_{013}$	4	2775.578v	50	36,017.92	$a^2D_{23} - t^2F_{023}$
7	2907.670	1	34,381.75	$(a^2D_{23} - w^4P_{023})$	4	2774.960v	50	36,025.94	$b^4F_{13} - x^4D_{013}$
7	2905.576	1	34,406.53	$(a^2P_{13} - t^2F_{023})$	4	2773.68v	3	36,042.56	$a^2G_{33} - y^2G_{023}?$
7	2905.496	1	34,407.48	$(a^2D_{23} - 15^0_{23})$	4	2772.692v	30h	36,055.41	$a^2D_{13} - 20^0_{13}, 23$
4	2905.132v	3	34,411.79	$a^4P_{13} - t^4D_{023}$	4	2772.541v	15h	36,057.37	
4	2904.290v	2	34,421.76	$a^4P_{23} - t^4D_{023}$	4	2771.697v	9h	36,068.35	$b^4P_{13} - s^4D_{013}$
4	2903.197v	25	34,434.72	$a^2G_{43} - x^2H_{043}$	4	2771.324v	1	36,073.21	$b^4P_{13} - s^4D_{013}$
4	2901.53v	1	34,454.48	$a^2D_{13} - w^2P_{013}$	4	2770.10v	0	36,089.13	$b^4P_{13} - 16^0_{23}$
4	2899.819v	25	34,474.83	$a^2D_{13} - w^2P_{013}$	4	2769.659v	10	36,094.89	$a^2F_{23} - w^4F_{013}$
4	2899.73v	4	34,475.90	$a^2F_{23} - x^4F_{023}$	4	2768.686v	20	36,107.58	$a^2F_{23} - w^4G_{023}$
5	2895.891	3	34,521.59	$a^2F_{23} - x^4F_{023}$	5	2768.294	9	36,112.69	$a^2F_{23} - x^2F_{023}$
5	2895.485	20	34,526.44	$a^4P_{23} - w^2F_{023}$	4	2766.382v	50	36,137.65	$b^4F_{23} - x^2D_{013}$
5	2895.335	4	34,528.23	$a^2F_{23} - z^4P_{023}$	4	2766.215v	50	36,139.83	$a^2G_{33} - w^2G_{023}$
4	2892.242v	25	34,565.15		4	2764.188v	100r	36,166.33	$b^4F_{43} - x^4D_{033}$
4	2889.845v	3	34,593.81		4	2763.062v	1	36,181.07	$b^2G_{33} - 37^0_{33}, 33$
4	2887.14v	1	34,626.16	$a^4P_{13} - w^2P_{013}$	4	2761.366v	75	36,203.29	$b^4P_{13} - x^4D_{023}$
4	2886.86v	2	34,629.61	$a^2G_{33} - 16^0_{23}$	4	2758.538v	30	36,240.40	$b^4P_{13} - w^4P_{013}$
4	2886.444v	50	34,634.57	$a^4F_{23} - y^2F_{033}$	4	2754.26v	1	36,296.64	$a^2D_{23} - u^2D_{013}$
7	2885.307	3	34,648.22	$a^4P_{23} - t^4D_{023}$	4	2752.070v	40	36,325.57	$(a^2D_{13} - t^2F_{023})$
7	2884.074	1	34,663.03	$(a^2G_{33} - t^2F_{033})$	5	2750.141	15	36,351.05	$(a^2D_{23} - s^2F_{033})$
4	2883.602v	15	34,668.71	$(b^4P_{23} - 11^0_{23})$	4	2746.028v	50	36,405.49	$a^2F_{23} - w^4F_{023}$
4	2882.219v	30	34,685.34	$(a^2D_{13} - s^4D_{023})$	4	2745.098v	50	36,417.82	$a^2F_{23} - x^2D_{023}$
4	2881.876v	5	34,689.47	$(a^2P_{13} - u^2D_{013})$	4	2740.457v	50	36,479.49	$b^4P_{13} - w^4P_{013}$
4	2879.612v	25	34,716.74	$(a^4F_{23} - y^2D_{023})$	4	2732.848v	2 Co II?	36,581.05	$b^4P_{13} - w^4P_{013}$
4	2878.558v	12	34,729.45	$a^2D_{13} - w^4P_{023}$	4	2731.112v	50W	36,604.31	$a^2D_{13} - u^2D_{013}$
4	2876.86v	2	34,749.91	$a^2G_{43} - 15^0_{23}$	4	2728.754v	3	36,635.94	$a^2G_{43} - s^2F_{023}$
4	2876.82v	2	34,750.47	$b^4P_{13} - w^2P_{013}$	4	2723.05v	0	36,712.71	$b^4P_{23} - t^2F_{023}$
4	2876.383v	3	34,755.71	$b^4P_{13} - w^2P_{013}$	4	2722.106v	50w	36,725.40	$a^2D_{13} - u^2D_{023}$
4	2875.438v	2	34,767.13	$a^4P_{23} - t^4D_{013}$	4	2719.581v	25	36,759.50	$a^2F_{23} - w^4F_{023}$
4	2874.196v	4	34,782.16	$a^2G_{33} - 17^0_{23}$	4	2715.987v	75w	36,808.14	$a^2G_{43} - w^2G_{043}$
4	2873.32v	5	34,792.77	$a^2F_{23} - w^4D_{023}$	4	2709.29v	0	36,899.10	$b^4F_{23} - 1^0_{23}?$
4	2872.497v	15	34,802.73	$a^4P_{23} - t^4D_{023}$	4	2708.810v	30	36,905.66	$a^2G_{43} - w^2G_{043}$
4	2871.06v	1g?	34,820.16	$a^4P_{23} - t^4D_{023}$	4	2707.99v	1 Co II?	36,916.86	$a^4P_{23} - u^2F_{023}$
4	2870.506v	3	34,826.87	$a^2F_{23} - x^2F$					

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPLT DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPLT DESIGNATION
4	2679.751v	75W	37,305.83	$a^2F_{3/2} - x^2G_{3/2}$	4	2530.546v	5	39,505.29	$b^4F_{3/2} - 3p_{3/2}$
4	2677.021v	0	37,343.88	$a^4P_{3/2} - s^4D_{3/2}$	4	2530.134v	40w Co II?	39,511.72	$b^4F_{3/2} - w^4F_{3/2}$
4	2675.980v	10W Co II?	37,358.40	$b^4F_{1/2} - x^4F_{3/2}$	5	2528.967	50R	39,529.96	$a^4F_{3/2} - x^4D_{3/2}$
4	2675.546v	1	37,364.46	$a^4P_{3/2} - w^4F_{3/2}$	4	2528.186v	3 Co II?	39,542.16	$b^4F_{3/2} - 31p_{3/2}$
4	2673.918v	25	37,387.21	$a^2D_{3/2} - 23p_{3/2}$	4	2525.626v	4	39,582.24	$b^4F_{1/2} - x^4P_{3/2}$
4	2669.575v	2	37,448.03	$a^4P_{3/2} - s^4D_{3/2}$	4	2523.00v	4 Co II?	39,623.45	$b^4F_{3/2} - 32p_{3/2}$
4	2668.08v	1	37,468.97	$b^4D_{3/2} - 37p_{3/2, 3/2}$	5	2521.363	75R Co II?	39,649.16	$a^4F_{3/2} - x^4D_{3/2}$
4	2661.714v	2 Co II?	37,558.62	$b^4F_{3/2} - 1p_{3/2}$	4	2520.908v	3	39,656.31	
4	2657.340v	0	37,620.44	$a^2D_{3/2} - 24p_{3/2}$	4	2518.988v	3	39,686.54	$a^2F_{3/2} - w^2F_{3/2}$
4	2650.266v	50w	37,720.85	$b^4F_{1/2} - x^4F_{3/2}$	5	2517.869	10w	39,704.17	$b^4F_{3/2} - w^4G_{3/2}$
4	2649.931v	50w	37,725.61	$a^2F_{3/2} - w^2D_{3/2}$	4	2517.792v	6	39,705.39	$b^4F_{3/2} - w^4F_{3/2}$
5	2648.635	5 Co II?	37,744.07	$b^4F_{3/2} - x^4F_{3/2}$	4	2515.075v	1	39,748.28	$b^4F_{3/2} - 26p_{3/2}$
4	2646.413v	10w	37,775.76	$b^4F_{3/2} - x^4F_{3/2}$	4	2513.119v	4	39,779.22	$b^4F_{3/2} - x^2D_{3/2}$
4	2644.772v	10w	37,799.20	$a^2F_{3/2} - w^4D_{3/2}$	4	2512.900v	5	39,782.68	$a^2F_{3/2} - w^2F_{3/2}$
4	2642.884v	10r	37,826.20	$b^4F_{3/2} - w^4F_{3/2}$	4	2511.019v	10r Co II?	39,812.48	$b^4F_{3/2} - w^4F_{3/2}$
5	2636.365	5 Co II?	37,919.72	$b^4P_{3/2} - s^2F_{3/2}$	4	2510.10v	0 Co II?	39,827.01	$b^4F_{3/2} - 4p_{3/2}$
4	2632.89v	3	37,969.73	$b^4P_{3/2} - 23p_{3/2}$	4	2509.234v	2	39,840.80	
7	2631.215	1n	37,993.94	$a^2F_{3/2} - w^2D_{3/2}$	4	2508.730v	1	39,848.80	$b^4P_{3/2} - w^4F_{3/2}$
4	2629.970v	30	38,011.93	$b^4P_{3/2} - w^2D_{3/2}$	4	2507.678v	40w	39,865.52	$a^2F_{3/2} - x^2P_{3/2}$
5	2628.761	3	38,029.41		4	2507.169v	2	39,873.62	$b^4F_{3/2} - x^2G_{3/2}$
4	2627.638v	50W	38,045.66	$b^4F_{3/2} - x^4G_{3/2}$	4	2506.873v	10w	39,878.32	
4	2627.031v	2	38,054.45	$a^4P_{3/2} - w^2P_{3/2}$	4	2505.107v	3	39,906.43	
7	2626.122	1	38,067.62	$a^4P_{3/2} - 16p_{3/2}$	4	2504.518v	4 Co II?	39,915.82	$b^4F_{3/2} - w^4D_{3/2}$
4	2624.795v	1	38,086.86		4	2503.860v	1	39,926.30	
4	2623.96v	5	38,098.95	$a^4P_{3/2} - 19p_{3/2}$	4	2503.24v	1	39,936.26	$b^4P_{3/2} - 28p_{3/2}$
4	2623.755v	40	38,101.97	$a^2F_{3/2} - y^4S_{3/2}$	4	2502.284v	5	39,951.45	$a^2F_{3/2} - w^4D_{3/2}$
4	2623.440v	2	38,106.54	$b^4F_{3/2} - x^4F_{3/2}$	4	2501.508v	2	39,963.84	$b^4F_{3/2} - 31p_{3/2}$
4	2622.430v	30r	38,121.21	$b^4F_{3/2} - x^4G_{3/2}$	4	2501.257v	2	39,967.85	$b^4F_{3/2} - y^4P_{3/2}$
4	2622.250v	3	38,123.83	$b^4F_{3/2} - x^4G_{3/2}$	4	2500.494v	10h	39,980.05	
4	2622.059v	40w Co I+II	38,126.61	$b^4F_{3/2} - x^4G_{3/2}$	4	2496.713v	12	40,040.59	$b^4F_{3/2} - w^4G_{3/2}$
4	2619.276v	50w	38,167.11	$b^4F_{3/2} - w^4D_{3/2}$	4	2496.45v	1	40,044.86	$b^4F_{3/2} - 32p_{3/2}$
4	2617.859v	50w	38,187.77	$b^4F_{3/2} - w^4D_{3/2}$	4	2495.551v	10	40,059.23	$b^4F_{3/2} - w^4F_{3/2}$
4	2616.260v	40w	38,211.11	$a^2F_{3/2} - w^2D_{3/2}$	4	2494.730v	9	40,072.42	$b^4F_{3/2} - x^2F_{3/2}$
4	2615.336v	10	38,224.61	$a^2F_{3/2} - y^2P_{3/2}$	4	2493.930v	30w	40,085.27	$a^2F_{3/2} - w^4D_{3/2}$
4	2614.124v	30	38,242.33	$a^4F_{3/2} - x^4D_{3/2}$	4	2491.15v	1	40,130.00	$b^4F_{3/2} - w^4F_{3/2}$
4	2613.894v	4	38,245.69	$a^2F_{3/2} - w^2D_{3/2}$	4	2490.02v	0	40,148.2	$b^4F_{3/2} - 33p_{3/2, 3/2}$
4	2613.492v	25 Co I+II	38,251.58	$a^2F_{3/2} - w^2D_{3/2}$	4	2489.62v	3	40,154.6	$a^2F_{3/2} - w^2F_{3/2}$
4	2610.762v	40w	38,291.57	$b^4F_{3/2} - x^4F_{3/2}$	4	2489.507v	1	40,156.48	
4	2608.900v	1g?	38,318.90	$a^4P_{3/2} - w^4P_{3/2}$	4	2489.249v	4	40,160.64	$a^4F_{3/2} - w^2P_{3/2}$
4	2606.120v	40	38,359.77	$b^4F_{3/2} - w^4D_{3/2}$	4	2488.461v	4	40,173.36	$a^4F_{3/2} - w^2P_{3/2}$
4	2602.581v	1	38,411.93	$a^2F_{3/2} - w^4D_{3/2}$	4	2485.952v	1	40,213.90	
4	2600.977v	10w	38,435.62	$b^4F_{3/2} - x^4F_{3/2}$	4	2483.613v	12 Co II?	40,251.77	$b^4F_{3/2} - w^4C_{3/2}$
4	2599.200v	5	38,461.89	$b^4F_{3/2} - w^2P_{3/2}$	4	2481.09v	0	40,292.7	$a^2F_{3/2} - x^4S_{3/2}$
4	2595.986v	0	38,509.51	$a^4P_{3/2} - 19p_{3/2}$	4	2478.293v	2	40,338.17	
4	2595.214v	1	38,520.97	$b^4F_{3/2} - x^4C_{3/2}$	4	2476.640v	40w	40,365.09	$b^4F_{3/2} - w^4F_{3/2}$
4	2594.161v	10w	38,536.60	$a^4F_{3/2} - x^4D_{3/2}$	9	2476.43	1 Co II?	40,368.5	$a^2F_{3/2} - 7p_{3/2}$
4	2593.070v	1	38,552.81	$b^4F_{3/2} - w^4D_{3/2}$	4	2474.702v	5	40,396.70	$a^2F_{3/2} - 6p_{3/2}$
4	2592.563v	0	38,560.35	$a^2F_{3/2} - x^4F_{3/2}$	4	2473.901v	8	40,409.77	$a^4F_{3/2} - x^4F_{3/2}$
4	2591.686v	10r	38,573.40	$b^4F_{3/2} - w^4D_{3/2}$	4	2472.922v	7	40,425.77	$b^4F_{3/2} - w^4G_{3/2}$
5	2590.594	75W	38,589.65	$a^2F_{3/2} - x^2G_{3/2}$	4	2472.066v	3	40,439.77	
4	2589.30v	00	38,608.95	$a^2D_{3/2} - 29p_{3/2}$	4	2470.270v	20w	40,469.17	$b^4F_{3/2} - w^4G_{3/2}$
4	2585.335v	50W	38,668.15	$a^2F_{3/2} - w^2F_{3/2}$	4	2467.685v	20w	40,511.55	$a^4F_{3/2} - x^4F_{3/2}$
4	2583.03v	3	38,702.59	$a^4P_{3/2} - 19p_{3/2}$	4	2465.111v	3	40,553.86	$b^4P_{3/2} - 31p_{3/2}$
4	2580.838v	50W	38,735.52	$b^4F_{3/2} - x^2F_{3/2}$	4	2464.615v	3	40,562.02	$a^4F_{3/2} - w^2P_{3/2}$
4	2578.924v	30	38,764.26	$a^2F_{3/2} - w^2F_{3/2}$	4	2464.459v	2	40,564.59	$a^2F_{3/2} - w^2P_{3/2}$
4	2577.446v	1	38,786.49	$b^4F_{3/2} - x^4C_{3/2}$	4	2463.776v	4	40,575.84	$a^4F_{3/2} - w^2P_{3/2}$
4	2575.733v	2	38,812.29	$a^4F_{3/2} - x^4S_{3/2}$	4	2462.122v	20	40,603.09	$a^4P_{3/2} - 24p_{3/2}$
4	2574.351v	6r	38,833.12	$a^4F_{3/2} - x^4D_{3/2}$	4	2461.562v	2	40,612.32	$b^4F_{3/2} - w^2D_{3/2}$
4	2573.538v	30r	38,845.39	$b^4F_{3/2} - 3p_{3/2}$	4	2460.800v	20	40,624.90	$a^4F_{3/2} - x^4F_{3/2}$
4	2573.395v	40	38,847.55	$b^4F_{3/2} - w^2F_{3/2}$	4	2460.195v	20	40,634.89	$b^4P_{3/2} - 32p_{3/2}$
4	2572.234v	50w	38,865.08	$b^4F_{3/2} - x^2F_{3/2}$	5	2456.237	20w	40,700.36	$b^4F_{3/2} - w^4C_{3/2}$
10	2570.762	<1	38,887.33	$a^2F_{3/2} - w^4D_{3/2}$	4	2453.382v	4	40,747.72	
11	2567.742	1	38,933.06	$a^2F_{3/2} - w^4D_{3/2}$	4	2451.747v	3	40,774.89	$a^2F_{3/2} - w^4D_{3/2}$
4	2567.344v	50r	38,939.10	$a^4F_{3/2} - x^4D_{3/2}$	4	2451.237v	1	40,783.37	
4	2565.985v	1	38,959.72	$a^2D_{3/2} - 31p_{3/2}$	4	2448.505v	2	40,828.87	$b^4F_{3/2} - x^4P_{3/2}$
4	2564.566v	0	38,981.28	$b^4P_{3/2} - 23p_{3/2}$	4	2445.756v	3	40,874.76	$a^2F_{3/2} - w^2F_{3/2}$
4	2562.124v	10r	39,018.42	$a^4F_{3/2} - x^4D_{3/2}$	4	2445.353v	2	40,881.50	$b^4F_{3/2} - x^4P_{3/2}$
4	2561.280v	25	39,031.28		4	2443.548v	5	40,911.70	$b^4F_{3/2} - w^4C_{3/2}$
4	2560.027v	1d Co II?	39,050.39		4	2443.18v	0	40,917.8	$b^4P_{3/2} - 34p_{3/2, 3/2}$
4	2559.595v	0	39,056.98	$b^4F_{3/2} - x^4C_{3/2}$	4	2442.888v	4	40,922.75	
4	2556.762v	50w Co II?	39,100.25	$b^4F_{3/2} - w^4D_{3/2}$	4	2442.62v	2 Co II?	40,927.2	$b^4F_{3/2} - x^4P_{3/2}$
4	2555.074v	6	39,126.08	$b^4F_{3/2} - w^4F_{3/2}$	4	2441.040v	20	40,953.73	$a^2G_{3/2} - 36p_{3/2, 3/2}$
4	2553.337v	10r	39,152.69	$b^4F_{3/2} - w^4F_{3/2}$	4	2440.141v	4w	40,968.81	$b^4F_{3/2} - w^2H_{3/2}$
4	2553.004v	40r	39,157.80	$b^4F_{3/2} - w^4F_{3/2}$	4	2439.495v	8h	40,979.66	
4	2551.230v	0	39,185.03		4	2439.038v	20R	40,987.34	$a^4F_{3/2} - x^4F_{3/2}$
4	2549.296v	4	39,214.75	$a^4F_{3/2} - w^2S_{3/2}$	5	2438.411	2	40,997.87	$a^2F_{3/2} - w^2D_{3/2}$
4	2548.875v	3	39,221.23	$b^4F_{3/2} - x^2D_{3/2}$	4	2438.201v	1	41,001.41	$a^2F_{3/2} - w^2D_{3/2}$
4	2548.333v	20 Co II?	39,229.57	$a^2F_{3/2} - w^2D_{3/2}$	4	2436.786v	3	41,025.21	$a^4P_{3/2} - 27p_{3/2}$
4	2548.194v	0	39,231.71	$b^4F_{3/2} - x^2D_{3/2}$	5	2436.657	50R	41,027.38	$a^4F_{3/2} - x^4F_{3/2}$
4	2544.862v	4	39,283.07	$b^4F_{3/2} - x^2F_{3/2}$	4	2435.823v	10	41,041.43	$a^4F_{3/2} - 1p_{3/2}$
4	2544.252v	50r Co II?	39,292.49	$a^4F_{3/2} - x^4D_{3/2}$	4	2435.094v	20w	41,053.71	
4	2543.232v	1	39,308.25	$a^4P_{3/2} - w^2F_{3/2}$	4	2433.75v	0	41,076.4	$b^4F_{3/2} - x^2G_{3/2}$
10	2538.70	<1	39,378.41	$a^2F_{3/2} - 6p_{3/2}$	4	2432.213v	40R	41,102.34	$a^4F_{3/2} - x^4F_{3/2}$
4	2538.339v	6	39,384.02	$b^4F_{3/2} - w^2S_{3/2}$	4	2431.74v	1	41,110.3	$b^4F_{3/2} - w^2D_{3/2}$
4	2536.503v	1	39,412.52	$b^4F_{3/2} - x^2F_{3/2}$	4	2430.176v	10	41,136.79	$a^4F_{3/2} - 26p_{3/2}$
4	2535.961v	10r Co II?	39,420.94	$a^4F_{3/2} - x^4D_{3/2}$	4	2429.226v	25	41,152.88	$a^4F_{3/2} - w^2P_{3/2}$
4	2535.359v	5	39,430.30	$a^2F_{3/2} - w^4D_{3/2}$	4	2428.596v	10	41,163.55	
4	2532.176v	10 Co II?	39,479.86	$b^4F_{3/2} - w^4F_{3/2}$	4	2428.997v	12	41,190.67	$b^4F_{3/2} - x^4P_{3/2}$
4	2531.354v	5	39,492.68	$b^4F_{3/2} - w^4C_{3/2}$	4	2425.593v	8	41,214.51	$b^4F_{3/2} - x^4F_{3/2}$
					4	2424.932v	250R	41,225.74	$a^4F_{3/2} - x^4F_{3/2}$
					4	2422.568v	30w	41,265.97	$a^4P_{3/2} - 27p_{3/2}$

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE NO. VAC.	MULTIPL DESIGNATION
4	2419.828v	6	41,312.69	$b^4F_{23} - x^4P_{023}$	4	2347.657v	4	42,582.60	$a^4F_{23} - w^4D_{023}$
4	2419.324v	10d‡	41,321.30		4	2346.161v	7	42,609.75	$a^4F_{23} - x^2F_{023}$
4	2419.122v	20w	41,324.75		5	2342.793	2	42,671.00	$a^4F_{13} - y^4P_{023}$
4	2418.580v	1	41,334.01		4	2341.784v	4	42,689.38	
4	2418.476v	1 Co II?	41,335.78		4	2340.99v	5	42,703.8	$b^4F_{23} - w^4D_{023}$
4	2417.329v	25	41,355.40		4	2339.92v	?	42,723.5	$a^2F_{23} - 15^0_{23}$
4	2417.045v	10	41,360.25		4	2339.550v	5	42,730.15	$b^4F_{23} - w^4D_{023}$
4	2415.516v	3	41,386.43	$a^2F_{23} - 7^0_{23}$	4	2339.048v	4 Co II?	42,739.32	$a^4F_{23} - x^2F_{023}$
4	2415.32v	2w	41,389.8	$a^4F_{23} - x^4F_{013}$	4	2338.656v	10d	42,746.48	$a^4F_{13} - w^4F_{013}$
4	2415.29v	4	41,390.3	$a^4F_{13} - x^4G_{023}$	4	2337.95v	3w Co II?	42,759.4	$a^4F_{13} - w^4G_{023}$
4	2414.458v	40R	41,404.56	$a^4F_{23} - x^4G_{023}$	4	2337.477v	4	42,768.04	
4	2413.580v	15	41,419.63	$a^4F_{13} - 32^0_{13}$	4	2336.00v	10d	42,795.0	$a^4F_{23} - w^4F_{023}$
4	2413.187v	15	41,426.37	$b^4F_{13} - v^4D_{13}$	4	2335.102v	15	42,811.53	$a^4F_{13} - x^4G_{023}$
4	2412.896v	6	41,431.37		4	2334.12v	5 Co II?	42,829.6	$b^4F_{13} - w^4D_{013}$
4	2412.762v	12r	41,433.67	$a^4F_{13} - w^4D_{023}$	4	2333.980v	3	42,832.11	
4	2411.618v	250R	41,453.32	$\{ a^4F_{23} - x^4G_{023} \}$ $\{ (a^4F_{13} - v^4D_{013}) \}$	4	2333.071v	6	42,848.79	$a^4F_{13} - y^4P_{013}$
4	2410.504v	40w	41,472.48	$a^4F_{13} - 30^0_{13}$	4	2332.087v	10	42,866.88	
4	2409.654v	8	41,487.11	$b^4F_{13} - y^4S_{013}$	4	2329.089v	6 Co II?	42,922.05	$b^4F_{23} - w^4D_{013}$
4	2409.123v	20	41,496.25	$b^4F_{23} - v^4D_{013}$	4	2328.861v	10	42,926.25	
4	2407.249v	100	41,528.58	$a^4F_{23} - x^4G_{023}$	4	2328.298v	6	42,936.63	
4	2406.266v	25	41,545.52	$b^4F_{23} - w^4D_{023}$	4	2327.539v	5	42,950.63	
4	2404.84v	10	41,570.1	$b^4F_{23} - v^4D_{013}$	5	2325.80	6	42,982.7	$b^4F_{13} - x^2S_{03}$
4	2403.637v	15	41,590.95		5	2325.615	50w	42,986.16	$b^4F_{23} - w^2F_{023}$
4	2403.337v	15	41,596.14	$b^4F_{13} - v^2D_{023}$	4	2325.531v	12	42,987.73	$a^4F_{23} - w^4G_{023}$
4	2402.559v	15	41,609.61	$b^4F_{13} - y^2P_{013}$	4	2325.131v	15d	43,032.12	$a^4F_{23} - w^4F_{023}$
4	2402.164v	30r	41,616.46	$a^4F_{13} - x^2F_{023}$	4	2322.260v	4	43,048.26	$a^4F_{13} - y^4P_{03}$
4	2402.058v	10r	41,618.29	$a^4F_{23} - x^4F_{023}$	4	2320.906v	4	43,073.37	$a^4F_{13} - y^4P_{03}$
4	2401.595v	30	41,626.31	$a^4F_{13} - w^4D_{013}$	4	2320.41v	1	43,082.5	$b^4F_{23} - w^2F_{023}$
4	2401.102v	30	41,634.86		4	2319.152v	4	43,105.94	$a^4F_{23} - x^2D_{023}$
4	2400.833v	30	41,639.52	$b^4F_{23} - v^4D_{023}$	4	2317.516v	5	43,136.37	$a^2F_{23} - w^2F_{023}$
4	2400.588v	30	41,644.29	$a^2F_{23} - 12^0_{13}$	4	2316.843v	5	43,148.90	$\{ a^4F_{23} - v^4F_{013} \}$ $\{ b^4F_{23} - 6^0_{23} \}$
4	2398.544v	4	41,679.08		4	2316.733v	5	43,150.95	$a^2F_{23} - w^2D_{023}$
4	2397.25v	4	41,701.7	$a^4F_{13} - 31^0_{13}$	4	2316.157v	10w	43,161.68	$a^4F_{23} - w^4G_{023}$
5	2397.03	6	41,705.6		4	2311.35v	10	43,251.4	$\{ a^4F_{23} - y^4P_{013} \}$ $\{ b^4F_{23} - w^4D_{023} \}$
4	2396.770v	90	41,709.95		5	2310.962	12	43,258.69	$b^4F_{13} - x^2P_{013}$
4	2396.588v	5	41,713.27	$a^4P_{23} - 30^0_{23}$	4	2310.36v	1	43,270.0	$a^2F_{23} - w^2F_{023}$
4	2396.232v	10	41,719.47	$a^2G_{43} - 36^0_{23}, 13$	5	2309.020	10R	43,295.09	$a^4F_{23} - w^4F_{023}$
4	2395.390v	6	41,734.13		4	2308.98v	?	43,295.9	$a^2F_{23} - 13^0_{23}, 43$
5	2394.227	4	41,754.40		4	2305.169v	15	43,367.40	$a^4F_{23} - w^4F_{023}$
10	2393.635	1	41,764.73	$b^4F_{23} - w^2D_{013}$	4	2304.182v	10	43,385.97	$a^4F_{23} - w^4F_{023}$
4	2392.029v	2	41,792.76	$a^4F_{23} - x^4G_{023}$	4	2303.966v	12	43,390.04	$b^4F_{43} - w^4D_{023}$
4	2391.369v	9	41,804.30		4	2303.504v	9	43,398.74	$a^4F_{43} - w^4D_{023}$
4	2390.426v	4	41,820.79		4	2303.31v	?	43,402.3	$a^2F_{23} - 16^0_{23}$
4	2389.984v	8	41,828.52	$b^4F_{23} - v^4D_{023}$	4	2298.356v	15	43,495.93	$b^4F_{13} - 14^0_{13}$
5	2389.540	12 Co II	41,836.29	$(a^4F_{23} - w^4D_{023})$	4	2296.704v	18	43,527.22	$b^4F_{23} - 14^0_{23}$
4	2388.374v	3	41,856.72	$a^4F_{23} - w^4D_{013}$	4	2296.038v	18	43,539.84	$b^4F_{13} - 12^0_{13}$
4	2388.175v	5	41,860.21	$b^4F_{23} - x^4P_{023}$	4	2295.223v	15	43,555.30	$a^4F_{23} - x^2F_{023}$
4	2387.460v	10	41,872.74	$b^4F_{23} - y^4S_{013}$	4	2294.003v	10	43,578.46	$a^4F_{23} - w^4G_{023}$
5	2386.509	3	41,889.42	$b^4F_{23} - x^2G_{043}$	4	2291.450v	12	43,627.01	$b^4F_{23} - v^2F_{023}$
4	2385.813v	9	41,901.65		4	2290.541v	10	43,644.32	$b^4F_{23} - x^2P_{013}$
4	2384.858v	10R	41,918.42	$a^4F_{43} - x^4F_{023}$	4	2289.495v	9	43,664.26	$a^4F_{23} - y^4P_{023}$
4	2381.26v	4	41,981.8	$b^4F_{23} - v^2D_{023}$	4	2288.774v	15	43,678.01	$b^4F_{13} - x^4S_{013}$
4	2380.696v	4	41,991.70	$a^4F_{23} - w^4D_{023}$	4	2287.804v	12d	43,696.53	$b^4F_{23} - 6^0_{23}$
4	2380.483v	20d	41,995.46	$\{ a^4F_{23} - x^4G_{023} \}$ $\{ b^4F_{23} - y^2P_{013} \}$	4	2285.408v	12	43,742.34	$b^4F_{43} - w^2F_{023}$
4	2379.357v	4	42,015.33	$b^4F_{13} - y^2P_{03}$	4	2284.86v	30	43,752.8	$a^4F_{23} - w^4G_{043}$
4	2379.160v	4	42,018.81	$a^4F_{23} - x^2F_{023}$	4	2284.81v	3	43,753.8	$b^4F_{23} - 14^0_{23}$
4	2378.905v	5	42,023.31	$a^4F_{23} - 32^0_{13}$	4	2284.375v	8	43,762.25	$b^4F_{13} - w^2S_{03}$
4	2377.215v	12	42,053.18	$b^4F_{13} - w^2F_{023}$	5	2281.34	5	43,820.3	
4	2376.975v	6	42,057.43	$b^4F_{43} - w^2H_{023}$	4	2279.927v	10Fe	43,847.48	$(a^4F_{43} - w^4F_{023})$
5	2374.456	4	42,102.04	$a^4F_{13} - x^2D_{013}$	4	2279.480v	15	43,856.08	$b^4F_{23} - 14^0_{23}$
4	2373.862v	9	42,112.58	$a^4F_{13} - x^2D_{023}$	5	2278.298	9	43,878.83	$a^4F_{13} - w^2D_{023}$
4	2373.56v	0	42,117.9	$a^2F_{23} - w^2F_{023}$	4	2276.523v	20r	43,913.04	
4	2373.370v	20	42,121.30		4	2275.884v	9	43,925.37	$b^4F_{23} - w^2F_{023}$
4	2372.832v	15	42,130.86	$a^4F_{23} - w^2P_{013}$	4	2274.617v	8	43,949.83	$a^4F_{13} - w^2P_{013}$
4	2371.845v	6 Co II?	42,148.38	$a^4F_{23} - x^2F_{023}$	4	2274.495v	9	43,952.19	$a^4F_{43} - w^4G_{013}$
4	2371.458v	15	42,155.26	$a^2G_{23} - 37^0_{23}, 33$	4	2273.58v	2	43,969.9	$a^4F_{43} - 4^0_{43}$
4	2370.514v	10	42,172.05	$a^4F_{23} - 3^0_{23}$	4	2268.742v	12	44,063.63	$b^4F_{23} - x^4S_{013}$
4	2369.924v	9	42,182.54	$b^4F_{23} - v^4D_{023}$	4	2268.163v	15	44,074.88	$b^4F_{23} - 14^0_{23}$
4	2369.674v	15	42,187.00	$b^4F_{23} - v^4D_{013}$	4	2267.113v	12	44,095.29	$a^4F_{13} - x^4P_{013}$
4	2366.046v	5	42,251.68	$a^2F_{23} - w^2F_{023}$	4	2264.880v	15	44,138.76	$a^4F_{23} - 7^0_{23}$
4	2365.057v	18d	42,269.34	$a^4F_{43} - x^4G_{043}$	4	2264.41v	10	44,148.0	$a^4F_{13} - x^4P_{013}$
5	2364.251	3	42,283.76	$b^4F_{43} - x^2G_{043}$	4	2262.592v	10	44,183.39	$a^4F_{43} - w^4G_{043}$
4	2362.327v	8	42,318.19	$b^4F_{43} - 14^0_{43}$	10	2262.07	0 Co II?	44,193.6	$a^4F_{13} - x^4P_{013}$
4	2360.789v	9	42,345.76	$a^2F_{23} - 14^0_{23}$	5	2258.328	9	44,266.81	
4	2358.676v	10	42,383.69	$a^4F_{23} - x^4G_{023}$	4	2257.582v	10	44,281.43	$a^4F_{23} - w^2D_{023}$
4	2358.177v	20	42,392.65	$a^4F_{23} - w^4F_{023}$	4	2256.565v	10	44,301.39	$b^4F_{23} - 14^0_{23}$
4	2357.507v	10	42,404.70	$a^2F_{13} - 11^0_{13}$	4	2254.82v	10	44,335.6	$a^2F_{23} - 12^0_{23}$
4	2356.267v	10	42,427.02	$a^4F_{23} - w^4L_{013}$	5	2253.776	10	44,356.20	$b^4F_{43} - 6^0_{43}$
4	2355.611v	7	42,438.83	$b^4F_{23} - w^2F_{023}$	10	2253.587	3	44,359.92	$a^4F_{23} - x^2G_{013}$
4	2355.480v	30	42,441.19	$a^4F_{23} - w^4F_{023}$	4	2252.712v	10	44,377.15	$a^4F_{13} - w^2D_{013}$
5	2354.41	5	42,460.5		4	2251.83v	8	44,394.5	$a^4F_{43} - w^4G_{023}$
4	2354.18v	2	42,464.6	$a^2F_{23} - w^2P_{013}$	4	2250.496v	10	44,420.84	$a^2F_{23} - 16^0_{23}$
4	2353.36v	10	42,479.4	$a^4F_{23} - w^4F_{043}$	4	2248.981v	5	44,450.78	$a^4F_{13} - v^4D_{013}$
4	2352.864v	15d	42,488.37	$b^4F_{43} - v^4L_{043}$	4	2248.80v	1	44,454.3	$a^2F_{23} - 12^0_{23}$
4	2351.98v	4	42,504.4	$a^4F_{23} - x^2L_{013}$	4	2247.86v	4	44,472.8	$b^4F_{23} - w^2F_{023}$
4	2351.385v	10	42,515.10	$a^4F_{23} - x^2D_{023}$	4	2246.599v	25	44,497.91	$a^4F_{23} - x^4P_{013}$
4	2350.596v	6	42,529.36	$b^4F_{23} - w^2D_{023}$	5	2245.600	10	44,517.68	
4	2350.284v	12	42,535.01	$b^4F_{23} - w^2F_{023}$	4	2245.463v	5	44,520.42	$a^4F_{13} - v^4D_{023}$

‡ Partly Ni—Burns.

TABLE VIII.—Continued.

REF.	λ IA	INT.—TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.—TC	WAVE No. VAC.	MULTIPL DESIGNATION
4	2244.12v	?	44,547.0	$a^2F_{3/2} - 1^2D_{3/2}$	13	2154.24	3	46,405.4	$a^4F_{3/2} - w^2F_{3/2}$
4	2243.254v	10	44,564.26	$a^4F_{3/2} - w^4D_{3/2}$	5	2154.074	10	46,409.01	$a^4F_{3/2} - w^2F_{3/2}$
4	2241.65v	9	44,596.1	$a^4F_{3/2} - w^2D_{3/2}$	13	2153.50	12	46,421.4	$a^4F_{3/2} - w^2F_{3/2}$
4	2240.74v	6	44,614.1	$a^2F_{3/2} - w^2D_{3/2}$	13	2152.83	2	46,435.8	$b^4F_{3/2} - w^2F_{3/2}$
4	2239.30v	1	44,643.0	$a^2F_{3/2} - w^2F_{3/2}$	5	2152.148	10	46,450.54	$b^4F_{3/2} - w^2G_{3/2}$
4	2237.125v	10	44,686.31	$\{a^2F_{3/2} - w^2F_{3/2}$ $b^4F_{3/2} - 7^0_{3/2}$	13	2151.69	3N	46,460.4	$b^4F_{3/2} - w^2F_{3/2}$
4	2236.796v	15	44,692.88	$a^4F_{3/2} - w^4D_{3/2}$	13	2151.26	2 Co II?	46,469.7	$b^4F_{3/2} - w^2F_{3/2}$
4	2234.710v	12	44,734.60	$b^4F_{3/2} - w^4D_{3/2}$	13	2150.11	5	46,494.6	$b^4F_{3/2} - 1^5_{3/2}$
4	2233.750v	10	44,753.64	$b^4F_{3/2} - w^4S_{3/2}$	5	2148.708	6	46,524.90	$a^4F_{1/2} - w^2F_{3/2}$
5	2233.09v	9	44,766.87	$a^4F_{1/2} - 1^1_{3/2}$	13	2147.77	5N	46,545.2	$b^4F_{3/2} - w^2F_{3/2}$
4	2232.88v	4	44,771.4	$b^4F_{1/2} - 1^1_{3/2}$	13	2146.65	0	46,569.5	$b^4F_{3/2} - w^2F_{3/2}$
4	2232.460v	8 Co II?	44,779.68	$a^4F_{3/2} - w^2D_{3/2}$	5	2146.264	12	46,577.87	$a^4F_{3/2} - w^4D_{3/2}$
5	2231.74v	6	44,793.95	$b^4F_{3/2} - 1^0_{3/2}$	5	2145.45	12	46,595.5	$b^4F_{3/2} - 1^3_{3/2}$
13	2230.07	8	44,827.7	$b^4F_{3/2} - 1^0_{3/2}$	5	2143.679	3	46,634.03	$a^4F_{1/2} - w^4D_{3/2}$
4	2229.734v	10	44,834.42	$b^4F_{3/2} - w^2F_{3/2}$	13	2142.34	2N	46,663.2	$b^4F_{3/2} - 1^4_{3/2}$
5	2228.806	12	44,853.09	$a^4F_{3/2} - w^4D_{3/2}$	5	2138.971	15	46,736.67	$a^4F_{1/2} - w^4D_{3/2}$
5	2228.334	4	44,862.59	$a^4F_{1/2} - w^2D_{3/2}$	5	2137.780	15	46,762.70	$a^4F_{1/2} - w^4D_{3/2}$
4	2227.853v	10	44,872.27	$a^4F_{3/2} - w^2D_{3/2}$	13	2137.38	0	46,771.4	$b^4F_{1/2} - w^4D_{3/2}$
4	2227.666v	12	44,876.04	$a^4F_{1/2} - w^2P_{3/2}$	5	2135.798	4	46,806.09	$a^4F_{1/2} - w^2F_{3/2}$
5	2225.848	5	44,912.69	$a^2F_{3/2} - w^2G_{3/2}$	5	2135.59	3	46,810.64	$a^4F_{3/2} - w^2F_{3/2}$
5	2225.350	12	44,922.74	$a^4F_{3/2} - w^4D_{3/2}$	13	2134.92	6	46,825.3	$a^4F_{3/2} - w^4D_{3/2}$
4	2223.97v	0	44,950.5	$a^4F_{3/2} - w^2G_{3/2}$	13	2134.10	8N	46,843.3	$a^4F_{3/2} - w^4D_{3/2}$
5	2219.154	9	45,048.15	$a^4F_{3/2} - w^2D_{3/2}$	5	2132.767	10	46,872.60	$a^4F_{3/2} - w^4D_{3/2}$
5	2218.813	10	45,055.08	$b^4F_{3/2} - 9^0_{3/2}$	13	2131.84	0	46,893.0	$b^4F_{3/2} - w^2F_{3/2}$
5	2213.86	4 Co II?	45,155.9	$\{a^4F_{3/2} - w^4S_{3/2}$ $a^4F_{3/2} - w^4D_{3/2}$	5	2131.052	3	46,910.32	$a^4F_{3/2} - w^2F_{3/2}$
5	2213.819	7	45,156.70	$b^4F_{3/2} - 1^1_{3/2}$	13	2130.91	tr	46,913.4	$b^4F_{1/2} - 1^7_{3/2}$
5	2212.354	9	45,186.60	$a^4F_{3/2} - 1^1_{3/2}$	5	2130.276	8	46,927.40	$a^4F_{3/2} - w^2P_{3/2}$
13	2212.23	15	45,189.1	$a^4F_{3/2} - 1^1_{3/2}$	5	2129.508	5	46,944.32	$a^4F_{1/2} - w^4S_{3/2}$
13	2210.89	2	45,216.5	$a^4F_{3/2} - w^2G_{3/2}$	5	2127.147	10	46,996.42	$b^4F_{3/2} - w^4D_{3/2}$
4	2208.508v	12	45,265.28	$a^4F_{3/2} - w^2D_{3/2}$	5	2126.199	5	47,017.37	$b^4F_{3/2} - w^4P_{3/2}$
4	2207.853v	9	45,278.70	$a^4F_{3/2} - w^2P_{3/2}$	5	2125.949	5	47,022.90	$a^4F_{3/2} - 6^0_{3/2}$
5	2207.697	10	45,281.90	$a^4F_{1/2} - w^2P_{3/2}$	5	2125.322	5	47,036.77	$a^4F_{3/2} - w^4D_{3/2}$
4	2204.796v	18	45,341.48	$b^4F_{3/2} - 1^0_{3/2}$	5	2125.116	10	47,041.33	$b^4F_{3/2} - 1^5_{3/2}$
13	2203.96	3N	45,358.7	$b^4F_{3/2} - 1^0_{3/2}$	13	2124.80	0	47,048.3	$a^2F_{3/2} - 3^0_{3/2}$
13	2203.53	4	45,367.5		13	2124.13	8	47,063.2	
13	2202.59	3	45,386.9		13	2122.64	10	47,096.2	$b^4F_{1/2} - w^2F_{3/2}$
13	2201.79	4	45,403.4		13	2121.99	6N	47,110.6	$b^4F_{1/2} - w^2G_{3/2}$
13	2201.55	6	45,408.3		5	2121.391	3	47,123.92	
13	2201.41	6	45,411.2		5	2120.705	10	47,139.16	$a^4F_{3/2} - w^4D_{3/2}$
5	2201.235	4	45,414.82	$b^4F_{3/2} - 1^2_{3/2}$	5	2119.904	10	47,156.97	$b^4F_{3/2} - w^4D_{3/2}$
5	2198.764	2	45,465.85	$a^4F_{3/2} - w^4D_{3/2}$	5	2119.192	5	47,172.82	$b^4F_{3/2} - 1^6_{3/2}$
13	2197.98	3	45,482.1		5	2118.505	6	47,188.11	$b^4F_{1/2} - w^4D_{3/2}$
5	2197.633	5	45,489.25		13	2117.68	15s	47,206.5	$b^4F_{3/2} - w^2F_{3/2}$
13	2197.34	8	45,495.3		5	2116.842	10	47,225.17	$a^4F_{3/2} - w^2F_{3/2}$
5	2196.904	3	45,504.34		13	2116.29	8	47,237.5	
4	2196.458v	15	45,513.58	$a^4F_{3/2} - w^4D_{3/2}$	13	2115.49	2?	47,255.4	$b^4F_{1/2} - 1^3_{3/2}$
13	2196.02	3	45,522.7		5	2115.338	12	47,258.74	$b^4F_{3/2} - w^4D_{3/2}$
13	2195.17	3	45,540.3	$a^4F_{3/2} - w^2F_{3/2}$	5	2114.41	4	47,279.5	$b^4F_{1/2} - w^4P_{3/2}$
13	2191.16	3	45,623.6	$a^2F_{3/2} - 2^1_{3/2}$	5	2114.1	12	47,299.03	$b^4F_{3/2} - 1^7_{3/2}$
5	2189.350	3	45,661.34	$\{a^4F_{3/2} - 1^1_{3/2}$ $b^4F_{3/2} - w^2F_{3/2}$	13	2113.536	12	47,306.6	
5	2187.284	5	45,704.45	$\{a^2F_{3/2} - 2^3_{3/2}$ $b^4F_{3/2} - 1^1_{3/2}$	13	2113.20	3	47,320.6	$b^4F_{3/2} - w^4P_{3/2}$
4	2186.777v	12	45,715.1	$b^4F_{3/2} - 9^0_{3/2}$	13	2112.40	12	47,324.5	$a^4F_{3/2} - w^4S_{3/2}$
13	2186.45	8	45,721.9	$b^4F_{3/2} - w^2F_{3/2}$	5	2111.416	10	47,346.52	$a^4F_{3/2} - w^4S_{3/2}$
5	2186.030	3	45,730.67	$b^4F_{3/2} - 1^4_{3/2}$	13	2111.08	5N	47,354.1	
5	2184.950	10	45,753.28	$a^2F_{3/2} - w^2D_{3/2}$	13	2110.89	tr	47,358.3	$a^2F_{3/2} - 3^2_{3/2}$
5	2184.314	8	45,766.59	$a^4F_{3/2} - w^2G_{3/2}$	5	2109.206	5	47,396.12	
13	2183.33	3N	45,787.2		5	2108.980	15	47,401.20	$a^4F_{3/2} - w^4D_{3/2}$
5	2182.587	15	45,802.80	$a^4F_{1/2} - w^4D_{3/2}$	13	2108.16	0	47,419.6	$b^4F_{3/2} - w^2F_{3/2}$
5	2181.121	12	45,833.58	$a^2F_{3/2} - w^2G_{3/2}$	13	2108.05	0	47,422.1	$\{a^4F_{3/2} - 7^0_{3/2}$ $b^4F_{1/2} - 1^9_{3/2}$
13	2180.23	7	45,852.3		5	2106.798	25 Co II?	47,450.29	$b^4F_{1/2} - 2^0_{3/2}$
4	2180.060v	10	45,855.88	$a^4F_{3/2} - w^2D_{3/2}$	13	2105.02?	?N	47,490.4	$a^2F_{3/2} - 2^6_{3/2}$
13	2178.59	25N	45,886.8		5	2104.730	25	47,496.90	
13	2178.06	8Fe?	45,898.0		13	2104.50	12Nd?	47,502.1	
5	2176.968	2	45,921.00	$b^4F_{3/2} - w^2G_{3/2}$	13	2103.85	5	47,516.8	
5	2176.494	4	45,931.01	$a^2F_{3/2} - w^2G_{3/2}$	13	2103.10	4N	47,533.7	
13	2176.03	3	45,940.8		13	2102.62	10	47,544.6	
13	2174.90	8	45,964.7		13	2101.70	3	47,565.4	
4	2174.589v	30r	45,971.24	$a^4F_{3/2} - w^4D_{3/2}$	13	2100.66	6	47,588.9	
5	2173.845	10	45,986.98	$a^4F_{3/2} - w^4D_{3/2}$	5	2099.35	10	47,618.6	$a^4F_{3/2} - w^2P_{3/2}$
5	2173.173	10	46,001.19	$b^4F_{3/2} - 1^0_{3/2}$	5	2098.942	12	47,627.87	$a^4F_{3/2} - w^4D_{3/2}$
5	2172.175	4	46,022.33	$b^4F_{3/2} - w^2F_{3/2}$	5	2097.511	20	47,660.35	
13	2171.68	0N	46,032.8	$a^4F_{3/2} - w^2G_{3/2}$	5	2095.77	15	47,699.9	
5	2170.565	10	46,056.45	$a^4F_{3/2} - w^4D_{3/2}$	13	2094.86	15	47,720.7	$\{b^4F_{1/2} - w^2F_{3/2}$ $b^4F_{3/2} - 1^6_{3/2}$
5	2168.711	18	46,095.83	$a^4F_{3/2} - w^4D_{3/2}$	5	2093.40	15	47,753.9	$b^4F_{3/2} - w^2F_{3/2}$
13	2167.75	3	46,116.3	$b^4F_{3/2} - 1^4_{3/2}$	13	2091.98	12	47,786.3	$b^4F_{3/2} - 1^8_{3/2}$
13	2164.36	6	46,188.5		13	2091.40	10	47,799.6	$a^4F_{3/2} - w^2F_{3/2}$
13	2163.96	5NN	46,197.0		13	2091.05	15	47,807.6	$b^4F_{3/2} - 1^9_{3/2}$
13	2163.78	3?	46,200.9		13	2089.83	10	47,835.5	$b^4F_{3/2} - 2^0_{3/2}$
5	2163.574	12	46,205.26	$a^4F_{3/2} - w^4D_{3/2}$	13	2089.67	10	47,839.2	$a^4F_{3/2} - 6^0_{3/2}$
5	2163.034	15	46,216.79	$a^4F_{1/2} - w^2S_{3/2}$	13	2089.35	15	47,846.5	$b^4F_{3/2} - 1^7_{3/2}$
5	2162.196	6	46,234.70	$b^4F_{3/2} - w^2P_{3/2}$	13	2087.55	15	47,887.7	
13	2161.58	3N	46,247.9		13	2085.67	15N	47,930.9	
13	2158.87	4	46,305.9		13	2085.04	9	47,945.4	$a^4F_{1/2} - w^2P_{3/2}$
5	2158.542	10	46,312.96	$a^4F_{3/2} - w^2F_{3/2}$	13	2084.09	10	47,967.2	
13	2158.30	8	46,318.2		13	2082.11	12	48,012.8	$a^4F_{3/2} - 7^0_{3/2}$
13	2157.20	5N	46,341.8		13	2081.04	10	48,037.5	$a^4F_{1/2} - 1^1_{3/2}$
13	2156.33	5NN	46,360.5		13	2079.55	tr	48,071.9	$b^4F_{1/2} - w^4D_{3/2}$
13	2155.29	12	46,382.8		13	2079.32	12	48,077.3	$a^4F_{3/2} - 1^0_{3/2}$
					13	2078.06	2	48,106.4	$b^4F_{3/2} - w^2F_{3/2}$
					13	2077.76	25NN	48,113.3	
					13	2077.44	1N	48,120.8	$b^4F_{1/2} - w^2D_{3/2}$

TABLE VIII.—Continued.

REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ IA	INT.-TC	WAVE No. VAC.	MULTIPL DESIGNATION
5	2073.27	10	48,217.5	$a^4F_{3/2} - u^4D_{3/2}$	13	1972.82	tr?	50,688.9	$a^4F_{3/2} - 19^0_{3/2}$
13	2071.95	4N	48,248.3		13	1972.52	30N	50,696.6	$b^4F_{3/2} - 29^0_{3/2}$
13	2069.91	12	48,295.8	$a^4F_{3/2} - 12^0_{3/2}$	13	1971.75	15	50,716.4	$a^4F_{3/2} - 20^0_{3/2}, 23$
5	2068.99	10	48,317.3	$a^4F_{3/2} - v^2F_{3/2}$	13	1971.16	30N	50,731.6	$b^4F_{3/2} - 25^0_{3/2}$
13	2067.58	5	48,350.2		13	1970.71	50	50,743.1	$\{b^4F_{3/2} - 32^0_{3/2}$ $(a^4F_{3/2} - s^4D^0_{3/2})$
13	2067.42	6NN	48,354.0		13	1969.68	3	50,769.7	
13	2066.22	12	48,382.0	$a^4F_{3/2} - 9^0_{3/2}, 43$	13	1968.93	25N	50,789.0	$b^4F_{3/2} - 26^0_{3/2}$
13	2066.12	0 Co II?	48,384.4	$b^4F_{3/2} - u^2D^0_{3/2}$	13	1968.69	25N	50,795.2	
5	2064.86	4	48,413.9	$\{b^4F_{3/2} - l^2F_{3/2}$ $(b^4F_{3/2} - s^2F_{3/2})$	13	1967.78	10	50,818.7	$b^4F_{3/2} - 30^0_{3/2}$
13	2062.92	6	48,459.4		13	1966.96	10	50,839.9	
13	2061.39	6	48,495.4		13	1966.68	9	50,847.1	$b^4F_{3/2} - 33^0_{3/2}, 23$
13	2059.90	3	48,530.5		13	1964.03	20	50,915.7	$b^4F_{3/2} - 24^0_{3/2}$
13	2058.51	3NN	48,563.2		13	1963.92	8?	50,918.6	$b^4F_{3/2} - 27^0_{3/2}$
13	2055.46	4N	48,635.3		13	1963.55	20	50,928.2	$a^2F_{3/2} - 37^0_{3/2}, 23$
5	2054.07	10	48,668.2	$a^4F_{3/2} - 10^0_{3/2}$	13	1963.38	12	50,932.6	$b^4F_{3/2} - v^4F_{3/2}$
13	2053.46	5N	48,682.6		13	1961.59	25	50,979.0	
13	2053.27	6	48,687.1		13	1961.26	8	50,987.6	$a^4F_{3/2} - l^2F_{3/2}?$
13	2052.82	6	48,697.8	$a^4F_{3/2} - 12^0_{3/2}$	13	1961.00	15	50,994.4	$b^4F_{3/2} - v^4F_{3/2}$
13	2048.59	5	48,798.3		13	1958.94	15	51,048.0	$\{b^4F_{3/2} - 31^0_{3/2}$ $(a^4F_{3/2} - 16^0_{3/2})$
13	2043.70	8?	48,915.1		13	1958.55	25	51,058.2	
13	2043.37	8	48,923.0	$b^4F_{3/2} - 21^0_{3/2}, 43$	13	1958.10	8	51,069.9	$a^4F_{3/2} - 18^0_{3/2}$
5	2043.00	8	48,931.8		13	1957.69	12N	51,080.6	$a^4F_{3/2} - l^2F_{3/2}$
13	2042.72	8N	48,938.6		13	1956.22	15	51,119.0	$a^4F_{3/2} - 20^0_{3/2}, 23$
13	2041.76	3	48,961.6	$b^4F_{3/2} - s^2F_{3/2}$	13	1955.17	30	51,146.4	$b^4F_{3/2} - 35^0_{3/2}, 23$
13	2041.11	20	48,977.1		13	1954.22	30	51,171.3	$b^4F_{3/2} - v^4F_{3/2}$
13	2039.95?	25 Co II?	49,005.0	$b^4F_{3/2} - s^2F_{3/2}?$	13	1953.71	8	51,184.7	$a^4F_{3/2} - 15^0_{3/2}$
13	2038.86	0 Co II?	49,031.2	$a^4F_{3/2} - 11^0_{3/2}$	13	1953.50	4	51,190.2	
13	2037.92	2 Co II?	49,053.8	$b^4F_{3/2} - u^2D^0_{3/2}$	13	1951.90	25	51,232.1	$b^4F_{3/2} - 33^0_{3/2}, 23$
13	2035.35	5	49,115.7	$a^4F_{3/2} - b^2P^0_{3/2}$	13	1951.44	12	51,244.2	$b^4F_{3/2} - 29^0_{3/2}$
13	2035.05	7N	49,123.0		13	1949.00	15	51,308.4	$b^4F_{3/2} - v^4F_{3/2}$
13	2034.49	8N	49,136.5	$a^4F_{3/2} - v^2P^0_{3/2}$	13	1948.09	10	51,332.3	
13	2031.96	15	49,197.7	$a^4F_{3/2} - 9^0_{3/2}, 43$	13	1947.58	5	51,345.8	
13	2029.99	8	49,245.4		13	1946.79	25	51,366.6	$b^4F_{3/2} - 30^0_{3/2}$
13	2029.78	8	49,250.5		13	1945.86	0	51,391.2	$b^4F_{3/2} - 25^0_{3/2}$
13	2027.77	3	49,299.3		13	1945.09	12	51,411.5	$b^4F_{3/2} - 34^0_{3/2}, 23$
10	2026.794	—	49,323.0	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1943.64	12	51,449.9	$b^4F_{3/2} - 26^0_{3/2}$
13	2026.51	6	49,330.0	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1940.16	15 Co II?	51,542.1	$b^4F_{3/2} - v^4F_{3/2}$
13	2026.35	8d?	49,333.8		13	1939.75	10	51,553.0	
13	2024.68	10	49,374.5		13	1938.94	10	51,574.6	
13	2023.17	4	49,411.4		13	1936.58	30 Co II?	51,637.4	$b^4F_{3/2} - 28^0_{3/2}$
13	2020.56	trN	49,475.2	$b^4F_{3/2} - 23^0_{3/2}$	13	1935.72	0N	51,660.4	$a^4F_{3/2} - 18^0_{3/2}$
13	2020.18	2	49,484.5	$a^4F_{3/2} - 10^0_{3/2}$	13	1935.46	0N	51,667.3	$a^4F_{3/2} - u^2D^0_{3/2}$
5	2017.26	4	49,556.1		13	1934.34	12	51,697.2	$a^4F_{3/2} - s^2F_{3/2}$
13	2016.17	15 Co II?	49,582.9	$b^4F_{3/2} - 21^0_{3/2}, 43$	13	1934.03	3	51,732.3	
5	2015.99	4	49,587.3		13	1933.03	3	51,762.8	
5	2014.58	20v	49,622.03		13	1931.89	8	51,786.6	
13	2011.77	8N?	49,691.3		13	1931.00	10N	51,789.3	$a^4F_{3/2} - u^2D^0_{3/2}$
5	2011.07	5 Co II?	49,708.6	$b^4F_{3/2} - 24^0_{3/2}$	13	1930.90	6?	51,803.3	
5	2010.10	8	49,732.6	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1930.38	10	51,831.2	$b^4F_{3/2} - v^4F_{3/2}$
13	2009.24	9	49,753.9	$a^4F_{3/2} - u^4P^0_{3/2}?$	13	1929.34	15	51,896.8	$a^4F_{3/2} - l^2F_{3/2}$
13	2008.85	8	49,763.6		13	1926.90	10	51,946.7	$a^2F_{3/2} - 37^0_{3/2}, 23$
5	2008.28	5	49,777.7	$a^4F_{3/2} - 15^0_{3/2}$	13	1925.05	12	51,962.6	
13	2008.04	15	49,783.6		13	1924.46	15	51,962.6	
13	2004.00	10N	49,884.0		13	1911.86	8	52,305.1	
13	2002.44	6?	49,922.8	$a^4F_{3/2} - 13^0_{3/2}, 43$	13	1906.72	5	52,446.1	
13	2002.32	25 Co II?	49,925.8	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1905.87	20	52,469.5	
13	2002.01	3	49,933.6		13	1905.41	6	52,482.2	
13	2000.12	12N	49,980.7	$b^4F_{3/2} - 22^0_{3/2}$	13	1904.75	5	52,500.3	
13	1999.89	8	49,986.5		13	1902.15	10	52,572.1	
13	1998.49	25l	50,037.8	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1901.75	20	52,583.1	
13	1994.98	15N	50,125.8		13	1897.73	8	52,694.6	
13	1993.25	10N	50,169.3		13	1897.48	10	52,701.5	
13	1992.79	20	50,180.9		13	1895.78	4	52,748.7	
13	1991.80	3	50,205.8		13	1894.07	3	52,796.4	
13	1990.34	30 Co II?	50,242.7	$a^4F_{3/2} - v^4P^0_{3/2}?$	13	1893.43	3	52,814.2	
13	1989.80	25 Co II?	50,256.3	$b^4F_{3/2} - 26^0_{3/2}?$	13	1889.87	10	52,913.7	
13	1989.28	10	50,269.4	$b^4F_{3/2} - 24^0_{3/2}$	13	1889.60	6	52,921.2	
13	1987.65	20	50,310.7		13	1887.89	12	52,969.2	
13	1987.24	10?	50,321.0	$b^4F_{3/2} - 29^0_{3/2}$	13	1884.56	10N	53,062.8	
13	1987.15	12?	50,323.3		13	1884.45	10	53,065.9	$a^4F_{3/2} - 21^0_{3/2}, 43$
13	1987.03	15	50,326.4		13	1881.09	5	53,160.7	
13	1986.31	6	50,344.6		13	1880.82	15	53,168.3	
13	1985.88	4	50,355.5	$a^4F_{3/2} - v^4P^0_{3/2}$	13	1880.34	4	53,181.9	
13	1985.36	10	50,368.7		13	1878.28	25	53,240.2	
13	1985.25	10	50,371.5	$a^4F_{3/2} - 15^0_{3/2}$	13	1877.40	15	53,265.1	
13	1982.81	8	50,433.5	$b^4F_{3/2} - 27^0_{3/2}$	13	1876.88	8	53,279.9	
13	1982.52	20	50,440.8	$b^4F_{3/2} - 30^0_{3/2}$	13	1876.48	7	53,291.2	
13	1981.97	20	50,454.9	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1876.01	10	53,304.6	
13	1980.89	40N	50,482.4	$a^4F_{3/2} - s^4D^0_{3/2}$	13	1875.22	4	53,327.1	
13	1980.59	15	50,490.0		13	1872.37	8	53,408.3	
13	1978.53	12	50,542.6	$a^4F_{3/2} - l^2F_{3/2}$	13	1870.45	5	53,463.1	
13	1978.36	10	50,546.9	$b^4F_{3/2} - v^4F_{3/2}$	13	1869.16	5	53,500.0	
13	1976.97	30	50,582.5	$a^4F_{3/2} - 17^0_{3/2}$	13	1866.45	3	53,577.7	$a^4F_{3/2} - 29^0_{3/2}$
13	1975.94	6	50,608.8	$b^4F_{3/2} - v^4F_{3/2}$	13	1866.27	6	53,582.8	$a^4F_{3/2} - 24^0_{3/2}$
13	1975.67	20	50,615.7		13	1864.92	4	53,621.6	
13	1975.36	6N	50,623.7	$b^4F_{3/2} - v^4F_{3/2}$	13	1862.31	25	53,696.8	
13	1974.39	15	50,648.6	$b^4F_{3/2} - v^4F_{3/2}$	13	1858.26	3	53,813.8	$a^4F_{3/2} - v^4F_{3/2}$
13	1973.85	25	50,662.4	$b^4F_{3/2} - 31^0_{3/2}$	13	1856.13	15 Co II?	53,875.5	$a^4F_{3/2} - v^4F_{3/2}$
13	1973.62	5	50,668.3		13	1855.05	40 Co II?	53,906.9	$a^4F_{3/2} - v^4F_{3/2}$
					13	1854.28	8	53,929.3	$a^4F_{3/2} - 31^0_{3/2}$

TABLE VIII.—*Concluded.*

REF.	λ <i>IA</i>	INT.—TC	WAVE No. VAC.	MULTIPL DESIGNATION	REF.	λ <i>IA</i>	INT.—TC	WAVE No. VAC.	MULTIPL DESIGNATION
13	1852.71	30 Co II?	53,975.0	$a^4F_{3/2} - v^4F_{0_{1/2}}$	13	1837.82	8	54,412.3	$\{a^4F_{1/2} - 35^0_{1/2}, 2\}$
13	1852.52	15?	53,980.5	$a^4F_{2/2} - 29^0_{2/2}$	13	1837.13	3	54,432.7	$\{a^4F_{2/2} - 32^0_{1/2}, 2\}$
13	1851.49	8	54,010.6		13	1836.97	3	54,437.5	
13	1850.80	4	54,030.7		13	1834.99	10 Co II?	54,496.2	$a^4F_{2/2} - v^4F_{0_{1/2}}?$
13	1847.89	30	54,115.8	$a^4F_{3/2} - 26^0_{3/2}$	13	1834.34	10	54,515.5	$a^4F_{2/2} - 33^0_{1/2}, 2\}$
13	1846.94	4	54,143.6		13	1832.47	15	54,571.2	$a^4F_{2/2} - 29^0_{2/2}$
13	1843.45	8	54,246.1	$a^4F_{2/2} - 27^0_{2/2}$	13	1828.35	12	54,694.2	$a^4F_{2/2} - 34^0_{1/2}, 2\}$
13	1842.34	25 Co II?	54,278.8	$a^4F_{2/2} - v^4F_{0_{1/2}}?$	13	1825.17	1 Co II?	54,789.4	$a^4F_{4/2} - v^4F_{0_{1/2}}?$
13	1841.88	3	54,292.4	$a^4F_{1/2} - 34^0_{1/2}, 2\}$	13	1822.03	3	54,883.8	
13	1841.47	10	54,304.5	$a^4F_{3/2} - 28^0_{3/2}$	13	1820.42	12	54,932.4	$a^4F_{4/2} - 26^0_{3/2}$
13	1840.79	10	54,324.5		13	1814.20	12	55,120.7	$a^4F_{4/2} - 28^0_{3/2}$
13	1840.55	10	54,331.6	$a^4F_{2/2} - 31^0_{1/2}$					
13	1838.28	15	54,398.7	$a^4F_{4/2} - 24^0_{3/2}$					

Notes in intensity column: *d*, double; *g*, ghost; *h*, hazy; *l*, shaded to longer wave-length (asymmetrical); *n*, diffuse; *N*, very diffuse; *r*, narrow self-reversal; *R*, wide self-reversal; *s*, shaded to shorter wave-length (asymmetrical); *w*, wide or complex; *W*, very wide or complex.

- ¹ Meggers, unpublished material, 1935.
² Meggers and Kiess, J. Research Nat. Bur. Stand. **9**, 319 (1932), (RP 473).
³ Meggers and Kiess, Sci. Pap. Bur. Stand. **14**, 645 (1918); (No. 324).
⁴ Burns, unpublished material. Three-place measures in heavy type are interferometer measures; "v" denotes vacuum source.
⁵ M. I. T. *Wave-Length Tables* (The Technology Press; John Wiley and Sons, New York, 1939).
⁶ Russell, unpublished material.
⁷ Dhein, Zeits. f. Wiss. Ptg. **19**, 289 (1920).
⁸ Stütting, Zeits. f. Wiss. Ptg. **7**, 73 (1909).
⁹ Exner and Haschek, see Kayser, *Handbuch der Spectroscopie*, Vol. 5 (1910), p. 310; also reference 10 below; also King, Mt. Wilson Contr. No. 108; *Astrophys. J.* **42**, 347 (1915).
¹⁰ Catalan and Antunes, Anal. Soc. Española de Física y Química **34**, 207 (1936).
¹¹ Krebs, Zeits. f. Wiss. Ptg. **16**, 292 (1917).
¹² Hasselberg, see Kayser, *Handbuch der Spectroscopie*, Vol. 5 (1910), p. 310.
¹³ C. E. Moore, unpublished material.

There are a few conspicuous cases of sharing of *g* values between neighboring terms, as shown in Table VII. The most remarkable group is $y^4S_{1/2}^0$, $v^4D_{1/2}^0$, $v^2D_{1/2}^0$. The designations of the first two might almost as well be interchanged. Those here given depend on the intensities in the multiplets with a^4P , b^4P ; but these also indicate such an extensive sharing of properties by the three levels that it is hardly more than a formality to give them definite names. The intermixture of $b^4P_{1/2}$ and $a^2D_{1/2}$ is less complete, and they may be definitely labeled. A somewhat better agreement with the theoretical *g* values could also be obtained by interchanging the designations e^4P_3 and e^4D_3 , and also $e^6P_{1/2}$ and $e^6D_{1/2}$, without much disturbing the energy levels or intensities.

9. LINE LIST

Table VIII includes all the classified lines, and all unclassified lines of intensity exceeding 5 on the M.I.T. scale or 2 on that of other observers. Fainter unclassified lines are included for which King gives a temperature class or Burns has an interferometer measure. Lines which are very probably due to impurities, or to Co II, are also omitted.

The wave-lengths in column 2 have been collected from many sources, as described in the notes, and indexed in column 1. The values printed in heavy type are Burns' interferometer

measures. They greatly exceed the rest in accuracy. For other lines, we have entered what appears to us to be the best available wave-length, but it has been impracticable to secure a strictly homogeneous system. The intensities in the third column are King's estimates for all lines to which he has assigned a temperature class (column 4). For the other lines the values of the M.I.T. catalog are entered, when available, except in the red ($\lambda 8648-11,894$) where the values of Meggers and Kiess were adopted. For the remaining lines the intensity assigned by the measurer is given.

All these intensities are estimates of the strength of the lines on the negatives, and different observers have used extremely different scales—the older lists going usually from 1 to 10 and some recent ones from 1 to 3000, so that great caution is necessary in comparing them.

King's estimates are much more nearly homogeneous, but fall off at both ends with the sensitivity of his plates. His temperature classes show the usual close correlation with the energy levels, and have been of great aid in the analysis. The wave number and the adopted designation are given in the last two columns.

Of the 3007 lines in this table 282 have not been classified. Only one, $\lambda 3177.266$, is of any considerable strength. This, and some other low-temperature lines between $\lambda 3500$ and $\lambda 3150$ are probably the principal components of the missing

combinations of a^2G and a^2H (§4); but, since the faint components of the multiplets have not been found, they cannot be classified.

This spectrum may now be regarded as pretty well analyzed. Between $\lambda 11,900$ and $\lambda 2500$ there are 90 unclassified lines out of 2388; between $\lambda 2500$ and $\lambda 2200$, 52 out of 279; and between $\lambda 2200$ and $\lambda 1810$, 140 out of 340.

The classification is therefore fairly complete except in the remoter ultraviolet. Here many of the lines we list may belong to Co II, a spectrum still very incompletely analyzed. Some of these

are noted by "Co II?" following the intensity in Table VIII.

It is a pleasure to express our gratitude to Dr. M. T. Antunes for making the important work of Catalan and himself accessible to us; to Dr. Keivin Burns for the communication of his extensive and accurate measures,—especially with the interferometer—; to Dr. A. S. King for the loan of a set of plates of the spectrum, and for Zeeman data; and to Dr. A. G. Shenstone for taking the spectrogram which permitted the extension of our work beyond $\lambda 2230$.

The Effect of an Activator on the Absorption Spectrum of Zinc Sulphide Powders

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(Received May 24, 1940)

The absorption of zinc sulphide powders, both pure and with various concentrations of activator, was measured in the region 3200–4800A by the diffuse reflection method. It was found that the long wave-length limit of the absorption band for a pure ZnS powder was at 3800A and that this limit moved to longer wave-lengths with increasing concentration of Ag activator. No evidence could be found of a secondary absorption peak characteristic of the activator.

IF pure zinc sulphide is to luminesce under ultraviolet light, it must be activated. This is usually done by heating the powder with a trace of the salt of a foreign atom, such as silver or copper. In order to get a clearer picture of the nature of this activating process, it seems desirable to find out what effect the heat treatment and the presence of foreign atoms have on the absorption spectrum of the pure powder. Gisolf,¹ studying the transmission of thin layers of ZnS powder, has reported that, within an accuracy of 10 angstrom units, no difference is found between the wave-lengths of the absorption edge for both pure ZnS and for ZnS activated with traces of Cu or Ag. He also claims to have found a secondary absorption peak, characteristic of the impurity, on the long wave-length side of the principal absorption edge.² These results were not confirmed, however, in the experiments about to be described.

¹ J. H. Gisolf, *Physica* **6**, 87 (1939).

² See reference 1, Fig. 2 on page 87, and remarks on page 88.

The absorption spectra of the ZnS powders were obtained by the diffuse reflection method. The source of radiation was a 120-watt tungsten lamp with a quartz window.³ The ZnS powder⁴ was sprinkled in a thin layer over the corrugated end of a black wooden rod, held at an angle of approximately 45° in front of the slit of a small Littrow quartz spectrograph. During preliminary experiments a quartz mercury arc was used as a source of radiation. The appearance on the photographic plate, with small but uniformly diminished intensity, of the mercury lines in the region 3342 to 2537A was interpreted as indicating that a little light enters the spectrograph after one surface reflection from the crystals. Most of the reflected light, however, is apparently totally reflected internally, perhaps several times, so that it arrives at the slit of the

³ Kindly loaned by Professor George Winchester of Rutgers University.

⁴ Thanks are due to Dr. G. R. Shaw, Dr. L. B. Headrick and Mr. H. W. Leverenz of the RCA Manufacturing Company, for supplying the samples of ZnS used in these experiments.