The radiation observed without the grids contains also a doubly scattered ingredient which may be calculated from Eq. (7) by putting $r=L$, $P=1$, and $h / L=3.17$. Correction factors for absorption and recoil losses are obtained by squaring those applied in the single scattering case. This is equivalent to assuming that the effective path in the scatterer is $2 L$ and that $90^{\circ}$ is a proper effective scattering angle to represent both primary and secondary scattering for the purposes of this correction.

The radiation observed with the grids is calculated as explained in Section III for the case of double scattering by co-axial disks. For each primarily irradiated section as many as six emergence slots pass appreciable doubly scattered radiation. All such calculated contributions, corrected as in the preceding paragraph, are combined to give the total measurable radiation. Traces of higher order scattering will be
present in the observed radiation both with and without the grids but no calculation of such intensities has been made.

## Results

The calculated ratio of observable intensities without and with the grids, carried through as outlined above, is 47 . The ratio as observed was 44 at an x-ray tube potential of $40 \mathrm{kv}, 46$ to 50 kv , and 44 at 60 kv , the agreement being somewhat closer than might reasonably have been expected.

The methods of calculation outlined in this paper will subsequently be utilized for the correction of conclusions now in print concerning the polarization of primary x -rays, and for the interpretation of experiments in progress. The author is greatly indebted to Mr. Keith Harworth for assistance in the experimental part of this investigation.

# Preliminary Analysis of the First Spark Spectrum of Cerium-Ce II 

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#### Abstract

By applying the spectral interval sorter and a newly designed interval recorder to new data obtained with the automatic recording spectrum comparator on the M.I.T.-W.P.A. wavelength program, a preliminary term array for Ce II has been set up in which 584 lines have been accounted for as transitions between 31 lower and 51 upper states. The term diagram is found to be the most complex yet observed for a three-electron spectrum. Both configurations $4 f 5 d 6 s$ and $4 f 5 d^{2}$ appear to be low in Ce II, contrary to the analysis of Haspas. Most of the differences between observed wave numbers and those computed from the term array are less than $0.02 \mathrm{~cm}^{-1}$, and 60 percent of the lines are found to be consistent to within 0.002 A . Several of the term assignments have been checked with partially resolved Zeeman patterns recorded by King and Albertson, and the absolute $J$ values have been determined by this means. An inclusive description of the spectra of the cerium atom is being undertaken in the range 10,000 to 1000A.


THAT the spectra emitted by rare earth atoms would be unusually difficult to analyze has been expected by spectroscopists for some time, but fortunately a number of these atoms whose spectra are so complex emit outstanding groups of lines. By attacking such lines the beginnings of term arrays have been constructed in a number of cases. ${ }^{1}$ Cerium (58), the

[^0]first element of the rare earth group, which is of unusual interest spectroscopically because of its position in the periodic table, presents no such suggestive features for attack. When we made

[^1]preliminary attempts to analyze Ce I and Ce II several years ago ${ }^{2}$ we came to the conclusion that more precise wave-length values, or more highly resolved Zeeman patterns, or both, would be required before the term arrays of these spectra could successfully be unravelled.

A comprehensive resurvey of the cerium spectrum was then undertaken, and with the improved wave-length values so obtained we have developed a quadratic array for Ce II which in its present status accounts for 584 lines, including a majority of the stronger lines, as transitions between 31 lower and 51 upper states. This array is of special interest because it shows a new order of complexity in three-electron spectra. For example, about 700 lines due to Ti II are known, whereas more than 3000 lines have already been ascribed to Ce II on the basis of studies not yet complete. The difficulty of starting a term array is now explained, since we find more than two dozen low energy levels within $6000 \mathrm{~cm}^{-1}$ of the lowest, while Fe I, for example, shows only five levels in the same range.

Haspas ${ }^{3}$ has published a term array for Ce II with which we can find no point of agreement. He assigns 430 lines to 137 states, and the deviation between his observed and calculated wave numbers $(\mathrm{O}-\mathrm{C})$ is sometimes as great as 0.70 $\mathrm{cm}^{-1}$, which he justifies on the basis that the wave-lengths used, as measured by different observers, disagreed among themselves by as much as 0.3 A . Haspas' average value of $(\mathrm{O}-\mathrm{C})$ for his lines is over $0.2 \mathrm{~cm}^{-1}$, while our average is something under one-tenth this, as discussed below.

We calculate the probability of finding by accident a solid array of even four columns and 10 rows with the tolerance which we have used as being less than one in a million, starting with any random interval and the actual density of Ce II lines. If the tolerance were doubled the probability would increase to 1 in 10 . With the use of Haspas' tolerance, ten times ours, such chance arrays become very numerous in a spectrum so complex.

The present note illustrates the application of

[^2]the spectral interval sorter ${ }^{4}$ and the spectral interval recorder ${ }^{5}$ to the analysis of a complex term array, where the combination principle has little power for analysis unless precise wavelengths are available. Our results also show the internal consistency to be expected of wavelength values obtained by means of the automatic recording comparator ${ }^{6}$ in the program undertaken in this laboratory, with the assistance of the Works Progress Administration, on a systematic resurvey of atomic spectra.

## Procedure

A revised master-list of all known Ce II lines in the range $5500-2850 \mathrm{~A}$ was prepared, using the M.I.T.-W.P.A. wave-length values. The wave numbers of all lines on this list were then punched on a tape for the interval recorder, using a scale of 7.5 mm per $\mathrm{cm}^{-1}$. A similar tape was then prepared for the interval sorter, containing only the 337 strongest lines, to cut down the probability of accidental coincidences. ${ }^{4}$ No quadratic arrays grew from the intervals which were shown by the machine to occur most frequently, so the 700 strongest lines were punched on the tape. From this tape were recorded all intervals in the range 57 to $1000 \mathrm{~cm}^{-1}$, in four settings covering $300 \mathrm{~cm}^{-1}$ each. The most probable number of chance occurrences of any specified interval within a tolerance of $\pm 0.10$ $\mathrm{cm}^{-1}$ was calculated to be about 10 , but many intervals were found occurring on the developed chart from 14 to 20 times. The interval recorder was then set for each of these highly recurrent intervals in turn, and with it all pairs of lines in the master list which gave these intervals to within $\pm 0.10 \mathrm{~cm}^{-1}$ were automatically recorded. With the intervals thus determined a quadratic array was set up which was soon demonstrated to be valid by the ease and precision with which other intervals found from the record fitted into it.

Once a quadratic array has been started, both its validity and the mutual consistency of the wave-length values used can be tested by calculation of the differences ( $\mathrm{O}-\mathrm{C}$ ) mentioned

[^3]Table I. Difference between observed and computed wave numbers for lines measured on M.I.T.-W.P.A. program.

| $(\mathrm{O}-\mathrm{C}) \pm \mathrm{Cm}^{-1}$ | Percent in Range | Total Percent |
| :---: | :---: | :---: |
| 0.00 | 20.7 | 20.7 |
| .01 | 28.8 | 49.5 |
| .02 | 23.3 | 73.0 |
| .03 | 11.9 | 84.9 |
| .04 | 6.6 | 91.5 |
| .05 | 4.1 | 95.6 |
| .06 | 2.5 | 98.1 |
| .07 | .9 | 99.0 |
| .08 | .6 | 99.6 |

above. From Table I it will be seen that our average value of $(\mathrm{O}-\mathrm{C})$ is somewhat under 0.02 $\mathrm{cm}^{-1}$, and the agreement is such as to indicate that over 60 percent of the wave-length values used are mutually consistent to within 0.002 A .

Our wave-length data were supplemented by King's temperature classification of the 337 strongest lines. ${ }^{7}$ Partially resolved Zeeman patterns for both the $n$ and $p$ components in the range $3750-2900 \mathrm{~A}$ were also made available to us through the kindness of Drs. A. S. and R. B. King. In addition, $n$ components for the range 4700-3850A were photographed by A. S. King
${ }^{7}$ A. S. King, Astrophys. J. 68, 194 (1928).
and one of us (W. A.), who desires to record here his thanks to the National Research Council for the award of a fellowship which made this work possible. These cerium Zeeman effect plates were taken in the physical laboratory of the Mt. Wilson Observatory in Pasadena, using a 15 ft . concave grating and a large Weiss electromagnet.

While the Zeeman patterns were not sufficiently resolved to enable this powerful means of starting a term analysis to be used, our application of the combination principle, together with the selection principle for inner quantum numbers, served to determine the relative $J$ values of the terms. Several of the patterns were sufficiently resolved to rule out certain $J$ values, and by this means the absolute scale for $J$ was determined. The partially resolved pattern types served also to check our assignments in a number of cases, with very satisfactory agreement.

## Term Analysis of Ce II

Various considerations indicate that the electron configurations $4 f 5 d 6 s$ and $4 f 5 d^{2}$ both give rise to low lying terms in Ce II, with the former probably the lower. If $4 f 5 d 6 s$ is lower the ground

Table II. Energy levels of $C e I I$.

| Level | $\begin{gathered} \text { Term Value } \\ \text { WAve } \\ \text { Numbers } \end{gathered}$ | $\underset{\text { VALUE }}{J}$ | $\begin{aligned} & \text { No. of } \\ & \text { COMbINA- } \\ & \text { TIONS } \end{aligned}$ | Level | $\begin{gathered} \text { Term Value } \\ \text { Wave } \\ \text { Numbers } \end{gathered}$ | $\underset{\text { VALUE }}{J}$ | $\begin{aligned} & \text { No. of } \\ & \text { COMBINA- } \\ & \text { TIONS } \end{aligned}$ | Level | $\begin{gathered} \text { Term Value } \\ \text { Wave } \\ \text { Numbers } \end{gathered}$ | $\underset{\text { Value }}{J}$ | No. of CombinaTION |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.00 | $3 \frac{1}{2}$ | 19 | 29 | 6,638,25 | $4 \frac{1}{2}$ | 12 | 125 | 29,984.08 | $1 \frac{1}{2}$ | 7 |
| 2 | 1,410.30 | $4 \frac{1}{2}$ | 20 | 30 | 7,259.08 | $3 \frac{1}{2}$ | 16 | 126 | 30,065.19 | $3 \frac{1}{2}$ | 15 |
| 3 | 1,873.95 | $3 \frac{1}{2}$ | 23 | 31 | 8,280.96 | $3 \frac{1}{2}$ | 13 | 127 | 30,166.08 | $1 \frac{1}{2}$ | 5 |
| 4 | 2,382.26 | $4 \frac{1}{2}$ | 22 | 101 | 24,663.05 | $4 \frac{1}{2}$ | 9 | 128 | 30,245.89 | $4 \frac{1}{2}$ | 14 |
| 5 | 2,563.26 | $5 \frac{1}{2}$ | 11 | 102 | 25,359.69 | $2 \frac{1}{2}$ | 7 | 129 | 30,425.37 | $2 \frac{1}{2}$ | 10 |
| 6 | 2,581.27 | $4 \frac{1}{2}$ | 27 | 103 | 25,681.50 | $1 \frac{1}{2}$ | 4 | 130? | 30,576.84 | $4 \frac{1}{2}$ | 7 |
| 7 | 2,595.65 | 13 | 12 | 104 | 25,945.40 | $3 \frac{1}{2}$ | 13 | 131 | 30,637.17 | $4 \frac{1}{2}$ | 12 |
| 8 | 2,634.68 | $2 \frac{1}{2}$ | 21 | 105 | 26,841.40 | $4 \frac{1}{2}$ | 13 | 132 | 30,702.64 | $4 \frac{1}{2}$ | 16 |
| 9 | 2,641.57 | $3 \frac{1}{2}$ | 29 | 106 | 26,900.37 | $3 \frac{1}{2}$ | 13 | 133 | 30,829.13 | $3 \frac{1}{2}$ | 15 |
| 10 | 2,879.71 | $5 \frac{1}{2}$ | 14 | 107 | 27,187.06 | $3 \frac{1}{2}$ | 15 | 134 | 31,075.60 | $5 \frac{1}{2}$ | 8 |
| 11 | 3,363.44 | $2 \frac{1}{2}$ | 21 | 108 | 27,249.69 | $2 \frac{1}{2}$ | 13 | 135 | 31,207.96 | $4 \frac{1}{2}$ | 14 |
| 12 | 3,593.89 | $4 \frac{1}{2}$ | 25 | 109 | 27,379.95 | $5 \frac{1}{2}$ | 9 | 136 | 31,558.64 | $3 \frac{1}{2}$ | 13 |
| 13 | 3,703.61 | $3 \frac{1}{2}$ | 23 | 110 | 27,514.68 | $3 \frac{1}{2}$ | 11 | 137 | 31,738.50 | $5 \frac{1}{2}$ | 8 |
| 14 | 3,995.48 | $3 \frac{1}{2}$ | 30 | 111 | 27,811.52 | $4 \frac{1}{2}$ | 13 | 138 | 31,851.42 | $2 \frac{1}{2}$ | 9 |
| 15 | 4,266.41 | $3 \frac{1}{2}$ | 29 | 112 | 27,812.41 | $2 \frac{1}{2}$ | 12 | 139 | 32,138.73 | $2 \frac{1}{2}$ | 12 |
| 16 | 4,322.70 | $3 \frac{1}{2}$ | 21 | 113 | 27,835.23 | $1 \frac{1}{2}$ | 4 | 140 | 32,318.21 | $3 \frac{1}{2}$ | 14 |
| 17 | 4,459.89 | $3 \frac{1}{2}$ | 24 | 114 | 27,934.66 | $4 \frac{1}{2}$ | 19 | 141 | 32,862.80 | $3 \frac{1}{2}$ | 16 |
| 18 | 4,511.26 | $2 \frac{1}{2}$ | 20 | 115 | 28,297.49 | $3 \frac{1}{2}$ | 14 | 142 | 33,552.59 | $2 \frac{1}{2}$ | 11 |
| 19 | 4,523.01 | $4 \frac{1}{2}$ | 25 | 116 | 28,334.77 | $4 \frac{1}{2}$ | 11 | 143 | 33,808.31 | $2 \frac{1}{2}$ | 12 |
| 20 | 4,844.63 | $1 \frac{1}{2}$ | 8 | 117 | 28,337.82 | $2 \frac{1}{2}$ | 16 | 144 | 33,977.16 | $3 \frac{1}{2}$ | 16 |
| 21 | 4,910.98 | $5 \frac{1}{2}$ | 10 | 118 | 28,634.51 | $5 \frac{1}{2}$ | 11 | 145 | 34,155.33 | $3 \frac{1}{2}$ | 19 |
| 22 | 5,010.88 | $2 \frac{1}{2}$ | 15 | 119 | 28,725.16 | $4 \frac{1}{2}$ | 14 | 146 | 34,333.12 | $2 \frac{1}{2}$ | 11 |
| 23 | 5,118.81 | $2 \frac{1}{2}$ | 18 | 120 | 29,166.61 | $4 \frac{1}{2}$ | 16 | 147 | 34,426.07 | $2 \frac{1}{2}$ | 11 |
| 24 | 5,437.46 | $3 \frac{1}{2}$ | 25 | 121 | 29,281.37 | $2 \frac{1}{2}$ | 10 | 148 | 34,920.78 | $3 \frac{1}{2}$ | 11 |
| 25 | 5,716.22 | $3 \frac{1}{2}$ | 20 | 122 | 29,438.83 | $5 \frac{1}{2}$ | 9 | 149 | 34,934.46 | $2 \frac{1}{2}$ | 10 |
| 26 | 5,819.12 | $4 \frac{1}{2}$ | 25 | 123 | 29,807.09 | $4 \frac{1}{2}$ | 11 | 150 | 35,346.30 | $3 \frac{1}{2}$ | 14 |
| 27 | 5,942.79 | $3 \frac{1}{2}$ | 19 | 124 | 29,908.92 | $4 \frac{1}{2}$ | 18 | 151 | 35,558.70 | $3 \frac{1}{2}$ | 12 |
| 28 | 6,389.93 | 41 | 10 |  |  |  |  |  |  |  |  |

Table III. List of classified Ce II lines.

| WaveLength | Int. | Wave Number | Сомв. | WaveLENGTH | Int. | Wave Number | Сомв. | Wave- <br> Length | Int. | Wave Number | Сомв. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4984.42 | 1 | 20,056.94 | 31-117 | 4390.59 | 1 | 22,769.61 | 17-1 | 4197.511 | 3 | 23,816.95 | 14-112 |
| 4914.938 | 8 V | 20,340.47 | 16-101 | 4384.44 | 1 | 22,801.54 | 22-112 | 4196.335 | 75 V | 23,823.63 | 11-107 |
| 4865.12 | 1 | 20,548.76 | 29-107 | 4381.779 | 4 | 22,815.39 | 26-118 | 4195.819 | 3 | 23,826.56 | 18-117 |
| 4795.22 | 2 | 20,848.29 | 18-102 | 4380.057 | 3 | 22,824.36 | 22-113 | 4193.875 | 5 | 23,837.60 | 17-115 |
| 4755.51 | 2 | 21,022.38 | 26-105 | 4375.932 | 60 V | 22,845.88 | 14-105 | 4192.757 | 2 | 23,843.96 | 24-121 |
| 4744.91 | 3 | 21,069.34 | 12-101 | 4373.820 | 50 V | 22,856.91 | 19-109 | 4189.176 | 2 | 23,864.34 | 27-123 |
| 4742.22 | 1 | 21,081.29 | 26-106 | 4373.220 | 3 | 22,860.04 | 24-115 | 4187.324 |  | 23,874.90 | 17-116 |
| 4739.49 | 25 V | 21,093.44 | 15-102 | 4372.401 | 4 | 22,864.33 | 16-107 | 4185.334 | 5 | 23,886.25 | 11-108 |
| 4722.31 |  | 21,170.17 | 18-103 | 4365.520 | 2 | 22,900.36 | 24-117 | 4179.291 | 2 | 23,920.79 | 12-110 |
| 4705.85 | 1 | 21,244.22 | 27-107 | 4364.659 | 125 IV | 22,904.88 | 14-106 | 4176.081 | 3 | 23,939.17 | 14-114 |
| 4692.02 | 2 | 21,306.84 | 27-108 | 4364.502 |  | 22,905.71 | 26-119 | 4174.386 | 2 | 23,948.89 | 30-135 |
| 4678.61 |  | 21,367.91 | 26-107 | 4361.661 | 6 | 22,920.63 | 15-107 | 4172.152 |  | 23,961.71 | 10-105 |
| 4670.76 | 2 | 21,403.82 | 24-105 | 4360.444 | 3 | 22,927.02 | 16-108 | 4171.384 |  | 23,966.13 | 27-124 |
| 4666.70 | 1 | 21,422.44 | 19-104 | 4360.444 | 35 | 22,927.02 | 31-135 | 4169.878 | 30 V | 23,974.78 | 16-115 |
| 4664.11 | 1 | 21,434.34 | 18-104 | 4352.733 | 75 IV | 22,967.64 | 20-112 | 4162.89 | 1 | 24,015.04 | 16-117 |
| 4657.85 | 1 | 21,463.14 | 24-106 | 4349.790 | 100 IV | 22,983.18 | 15-108 | 4160.107 |  | 24,031.09 | 15-115 |
| 4657.22 | 1 | 21,466.05 | 30-119 | 4348.190 |  | 22,991.63 | 19-110 | 4159.033 | 50 IV | 24,037.30 | 31-140 |
| 4644.22 | 2 | 21,526.13 | 31-123 | 4345.963 | 5 | 23,003.42 | 18-110 |  |  |  | 3-104 |
| 4636.72 | 1 | 21,560.95 | 26-109 | 4344.920 | 1 | 23,008.94 | 25-119 | 4153.130 | 4 | 24,071.46 | 15-117 |
| 4623.47 | 1 | 21,622.74 | 16-104 | 4342.137 | 125 | 23,023.68 | 21-114 |  | 50 V | 24,089.99 | 26-124 |
| 4589.37 | 1 | 21,783.40 | 10-101 | 4337.777 | 125 IV | 23,046.83 | 8-103 | 4149.936 | 60 V | 24,089.99 | 25-123 |
| 4571.47 | 1 | 21,868.69 | 27-111 | 4330.444 | 30 IV | 23,085.85 | 7-103 | 4146.235 |  | 24,111.49 | 19-118 |
| 4567.12 | 1 | 21,889.52 | 22-106 | 4320.723 | 60 IV | 23,137.78 | 13-105 | 4137.475 |  | 24,162.54 | 23-121 |
| 4563.35 | 1 | 21,907.60 | 28-115 | 4315.404 | 3 | 23,166.31 | 30-129 | 4132.633 |  | 24,190.85 | 29-133 |
| 45 |  | 21,949.98 | $30-120$ $14-104$ | 4314.939 4313.100 | 2 | 23,168.80 | $\xrightarrow{29-128}$ | 4131.099 | 100 V | $\begin{aligned} & 24,199.82 \\ & 24.202 .14 \end{aligned}$ | -9-105 |
| 4545.878 | 2 | 21,991.8 | 27-114 | 4310.700 | 5 | 23,191.59 | 14-107 | 4128.067 |  | 24,217.60 | 12-111 |
| 4544.961 | 5 | 21,996.25 | 11-102 | 4309.740 | 50 IV | 23,196.75 | 13-106 | 4125.776 | 2 | 24,231.05 | 13-114 |
| 4544.961 | 5 | 21, | 29-118 | 4305.609 | 2 | 23,219.11 | 23-117 | 4123.230 | 5 | 24,246.01 | 26-126 |
| 4539.755 | 200 IV | 22,021.46 | 9-101 | 4304.723 | 0 | 23,223.79 | 27-120 | 4121.595 | 1 | 24,255.63 | 21-120 |
| 4527.354 | 200 V | 22,081.78 | 6-101 | 4300.331 | 60 IV | 23,247.51 | 12-105 | 4120.829 | 150 V | 24,260.14 | 6-105 |
| 4524.590 |  | 22,095.27 | 25-107 | 4299.362 | 60 IV | 23,252.75 | 2-101 | 4119.886 | 5 | 24,265.70 | -106 |
| 4520.410 |  | 22,115.71 | 26-114 | 4299.092 |  | 23,254.21 | 14-108 | 4114.141 | 2 | 24,299.58 | 30-136 |
| 4508.084 | 1 | 22,176.17 | 22-107 | 4296.069 | 6 | 23,270.57 | 29-124 | 4113.722 |  |  | 14-115 |
| 4499.52 | 1 u | 22,218.38 | 25-114 | 4294.756 | 3 | 23,277.68 | 31-136 | 4113.722 | 4 | 24,302.05 | 27-128 |
| 4495.389 | , | 22,238.80 | 22-108 | 4292.905 | 1 | 23,287.72 | 24-119 | 4111.923 | 2 | 24,312.69 | 28-132 |
| 4494.226 | 4 | 22,244.55 | 28-118 | 4292.767 |  | 23,288.47 | 19-111 | 4110.840 |  | 24,319.09 | 106 |
| 4486.909 | 150 V | 22,280.83 | 4-101 | 4290.435 | 2 | 23,301.13 | 18-112 | 4107.426 | 200 V | 24,339.31 | 14-116 |
| 4483.900 | 100 V | 22,295.78 | 31-130 | 4289.937 | 300 IV | 23,303.84 | 9-104 | 4106.881 | 5 d | 24,342.54 | 14-117 |
| 4479.35 | 30 V | 22,318.39 | 11-103 | 4289.453 |  | 23,306.46 | 12-106 | 4092.715 |  | 24,426.79 | 26-128 |
| 4472.716 | 50 | 22,351.53 | 19-105 | 4288.671 | 1 2 | 23,310.71 | $8-104$ $27-121$ | 4090.942 4089.006 | 4 | $24,437.37$ $24,448.94$ | 29-134 |
| 4472.11 | 1 | 22,354.56 | 27-115 | 4281.914 | 1 | 23,347.49 | 26-120 | 4087.371 | 4 d | 24,458.72 | 15-119 |
| 4468.023 | 2 u | 22,375.01 | 24-112 | 4281.156 | 3 | 23,351.63 | 17-111 | 4087.297 | 4 | 24,459.17 | 4-105 |
| 4467.537 | 5 | 22,377.44 | 19-106 | 4280.998 | 3 | 23,352.49 | 17-112 | 4085.232 | 100 V | 24,471.53 | 24-124 |
| 4463.87 | 1 u | 22,395.82 | 23-110 | 4278.865 | 5 | 23,364.12 | 6-104 | 4080.435 | 5 | 24,500.30 | 10-109 |
| 4462.03 | 1 | 22,405.06 | 20-108 | 4270.189 | 60 IV | 23,411.60 | 19-114 | 4077.470 | 75 V | 24,518.11 | 4-106 |
| 4454.984 | 3 | 22,440.49 | 17-106 | 4264.372 | I | 23,443.54 | 30-132 | 4075.853 | 125 IV | 24,527.84 | 21-122 |
| 4449.337 | 200 V | 22,468.97 | 21-109 | 4258.699 | 1 | 23,474.77 | 17-114 | 4074.646 | 2 | 24,535.11 | 2-104 |
| 4443.752 | , | 22,497.21 | 24-114 | 4257.120 | 4 | 23,483.47 | 13-107 | 4066.910 | 1 | 24,581.78 | 31-141 |
| 4442.43 | 1 | 22,503.90 | 22-110 | 4256.156 | 5 | 23,488.79 | 16-111 | 4065.164 | 3 | 24,592.33 | 30-138 |
| 4440.13 | 1 | 22,515.56 | 26-116 | 4255.992 | 4 | 23,489.70 | 16-112 | 4064.904 | 3 | 24,593.91 | 13-115 |
| 4439.50 | 1 | 22,518.76 | 16-105 | 4255.359 | 3 | 23,493.19 | 20-117 | 4062.941 | 3 | 24,605.79 | 6-107 |
| 4437.612 | 4 | 22,528.34 | 29-120 | 4250.651 | 1 | 23,519.21 | 14-110 | 4061.421 | 2 | 24,615.00 | 8-108 |
| 4433.708 | 2 | 22,548.18 | 31-133 | 4245.976 |  | 23,545.10 | 15-111 | 4059.314 | 1 | 24,627.77 | 24-126 |
| 4428.437 | 5 | 22,575.01 | 15-105 | 4242.726 | 7 | 23,563.14 | 4-104 | 4058.76 | 4 | 24,631.13 | 13-116 |
| 4427.917 | 6 | 22,577.66 | 16-106 | 4241.403 | 2 | 23,570.49 | 31-138 | 4058.245 | 4 | 24,634.26 | 13-117 |
| 4427.070 | 5 | 22,581.98 | 11-104 | 4234.726 | 2 | 23,607.65 | 29-128 | 4054.944 | 50 IV | 24,654.01 | 7-108 |
| 4419.89 |  | 22,618.67 | 25-116 | 4233.949 |  | 23,611.99 | 16-114 | 4053.508 | 100 IV | 24,663.05 | 1-101 |
| 4419.298 | 3 | 22,621.70 | 25-117 | 4232.569 | 4 | 23,619.68 | 26-122 | 4049.80 | ${ }^{1}$ | 24,685.63 | 28-134 |
| 4416.904 | 4 | 22,633.96 | 15-106 | 4223.882 | 4 | 23,668.26 | 15-114 | 4048.367 | 1 | 24,694.37 | 27-131 |
| 4413.805 | 2 | 22,649.85 | 30-124 | 4214.041 | 50 IV | 23,723.53 | 21-118 | 4046.341 | 100 V | 24,706.73 | 17-120 |
| 4400.872 | 3 | 22,716.41 | 23-113 | 4213.035 | 3 u | 23,729.20 | 24-120 | 4045.976 |  | 24,708.96 | 25-129 |
| 4400.545 4399 | 60 IV | 22,718.09 | 9-102 | 4202.944 | 150 IV | 23,786.17 | 12-109 | 4042.584 4040.758 | 200 IV | 24,729.69 | 14-119 |
| 4399.204 4398.790 | 60 IV | 22,725.02 | -8-102 | 4198.431 | 150 | 23,811.74 | 18-115 | 4040.758 4037.664 | 300 IV | $24,740.87$ $24,759.83$ | 12-116 |
| 4396.585 | 3 | 22,738.56 | 18-108 | 4197.998 | 5 | 23,814:19 | 21-119 | 4031.339 | 150 I | 24,798.67 | 6-109 |
| 4391.663 | 250 IV | 22,764.04 | 7-102 | 4197.668 | 4 | 23,816.06 | 14-111 | 4030.343 | 4 | 24,804.80 | 4-107 |

Table III.-Continued.

| Wave- <br> Length | Int. | Wave Number | Сомв. | Wave- <br> Length | Int. | Wave Number | Сомв. | Wave- <br> Length | Int. | Wave <br> Number | Сомв. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4029.75 | 1 | 24,808.45 | 24-128 | 3898.949 | ? | 25,640.70 | 3-110 | 3769.046 | 5 | 26,524.41 | 2-114 |
| 4028.413 | 150 IV | 24,816.68 | 5-109 | 3898.674 | 1 | 25,642.51 | 15-124 | 3766.514 | 4 u | 26,542.23 | 13-128 |
| 4028.198 | 2 | 24,818.01 | 26-131 | 3896.804 | 100 IV | 25,654.81 | 18-127 | 3765.044 | 4 | 26,552.60 | 19-134 |
| 4028.198 | 2 | 24,818.01 | 28-135 | 3896.637 | 1 | 25,655.91 | 9-115 | 3764.117 | 150 IV | 26,559.14 | 10-122 |
| 4027.633 | 2 | 24,821.49 | 17-121 | 3895.114 | 125 IV | 25,665.93 | 21-130 | 3763.612 | 3 | 26,562.70 | 15-133 |
| 4020.542 | 2 | 24,865.27 | 23-125 | 3890.986 |  | 25,693.17 | 9-116 | 3760.404 | 2 | 26,585.36 | 6-120 |
| 4019.274 | 2 | 24,873.11 | 9-110 |  |  |  | 9-117 | 3757.858 | 4 | 26,603.37 | 5-120 |
| 4018.213 |  | 24,879.68 | 30-139 | 3890.519 | 2 | 25 | 31-144 | 3755.425 | 75 IV | 26,620.61 | 11-125 |
| 4017.596 | 2 | 24,883.54 | 26-132 | 3889.478 | 3 | 25,703.13 | 8-117 | 3752.453 | 2 | 26,641.69 | 14-131 |
| 4014.899 | 125 V | 24,900.22 | 15-120 | 3888.388 | 4 u | 25,710.34 | 23-133 | 3751.002 | 1 | 26,652.00 | 12-128 |
| 4012.389 | 300 IV | 24,915.79 | 19-122 | 3886.495 | 3 | 25,722.86 | 19-128 | 3746.373 | 2 d | 26,684.93 | 19-135 |
| 4011.559 | 2 | 24,920.95 | 25-131 | 3883.983 |  | 25,739.50 | 26-136 | 3746.260 | 2 | 26,685.73 | 7-121 |
| 4003.168 |  | 24,973.18 | 22-125 | 3883.583 | 4 | 25,742.15 | 7-117 | 3744.05 | 1 |  | 11-126 |
| 4002.975 | 4 | 24,974.38 | 11-117 | 3881874 | 4 | 25,753.48 | 6-116 | 3744.05 | 1 | 26,701.48 | 24-139 |
| 4001.049 | 4 | 24,986.41. | 25-132 | 3881.675 | 5 | 25,754.80 | 10-118 | 3741.721 | 3 | 26,718.10 | 30-144 |
| 3999.242 | 500 IV | 24,997.69 | 4-109 | 3879.313 | 3 | 25,770.48 | 24-135 | 3739.691 | 2 | 26,732.61 | 23-138 |
| 3996.481 | 4 | 25,014.97 | 15-121 | 3878.372 | 150 IV | 25,776.73 | 2-107 | 3737.540 | 3 | 26,747.99 | 17-135 |
| 3995.429 | 2 | 25,021.55 | 13-119 | 3876.975 | 6 | 25,786.02 | 17-128 | 3729.918 | 4 | 26,802.65 | 11-127 |
| 3992.385 | 125 IV | 25,040.63 | 12-118 | 3876.129 | 4 | 25,791.65 | 21-132 | 3726.462 | 3 | 26,827.50 | 21-137 |
| 3991.317 | 3 | 25,047.33 | 23-127 | 3875.036 | 6 d | 25,798.91 | 15-126 | 3724.639 | 5 | 26,840.63 | 22-138 |
| 3990.105 | 5 | 25,054.94 | 10-114 | 3873.117 | 1 | 25,811.71 | 14-123 | 3722.291 | 4 | 26,857.56 | 6-122 |
| 3989.444 | 30 V | 25,059.09 | 30-140 | 3872.137 | 1 | 25,818.24 | 22-133 | 3719.797 | 3 | 26,875.57 | 5-122 |
| 3982.901 | 60 V | 25,100.25 | 29-137 | 3868.516 | 2 | 25,842.41 | 25-136 | 3719.091 | 1 | 26,880.67 | 24-140 |
| 3980.895 | 100 V | 25,112.90 | 25-133 | 3868.138 | 4 | 25,844.93 | 12-122 | 3718.190 | 150 IV | 26,887.19 | 2-115 |
| 3977.807 | 4 | 25,132.40 | 4-110 | 3863.741 | 4 | 25,874.34 | 31-145 | 3716.938 | 4 | 26,896.24 | 30-145 |
| 3976.67 | 1 |  | 20-125 | 3857.928 | 2 u | 25,913.33 | 14-124 | 3716.365 | 600 IV | 26,900.39 | 1-106 |
| 3976.6 | 1 |  | 24-130 | 3857.813 | 2 | 25,914.10 | 18-129 | 3713.648 | 2 | 26,920.07 | 27-141 |
| 3974.201 | 2 | 25,155.20 | 22-127 | 3857.644 | 5 | 25,915.24 | 4-115 | 3711.783 | 3 | 26,933.59 | 13-131 |
| 3972.071 | 6 | 25,168.69 | 28-136 | 3857.240 | 4 | 25,917.95 | 11-121 | 3710.684 | 2 | 26,941.57 | 15-135 |
| 3971.873 | 3 | 25,169.95 | 9-111 | 3857.032 | 5 | 25,919.35 | 26-137 | 3704.979 | 4 | 26,983.06 | 12-130 |
| 3971.684 | 100 V | 25,171.14 | 14-120 | 3854.322 | 100 IV | 25,937.57 | 3-111 | 3702.785 | 5 | 26,999.05 | 13-132 |
| 3970.646 | 5 | 25,177.72 | 8-112 | 3854.187 | 100 IV | 25,938.48 | 3-112 | 3701.730 |  | 27,006.74 | 20-138 |
| 3967.185 | 4 | 25,199.68 | 24-131 | 3853.158 | 125 IV | 25,945.41 | 1-104 | 3699.920 | 50 V | 27,019.95 | 23-139 |
| 3967.048 | 100 IV | 25,200.55 | 8-113 | 3852.103 | 2 | 25,952.51 | 4-116 | 3698.650 | 5 | 27,029.23 | 5-124 |
| 3964.503 | 6 | 25,216.73 | 7-112 | 3849.562 | 2 | 25,969.65 | 2-109 | 3696.673 | 2 | 27,043.68 | 26-141 |
| 3960.914 | 125 IV | 25,239.58 | 7-113 | 3848.105 | 3 | 25,979.48 | 15-128 | 3694.911 | 60 V | 27,056.58 | 4-122 |
| 3958.266 | 6 | 25,256.47 | 26-134 | 3837.210 | 3 | 26,053.24 | 6-118 | 3693.720 | 3 | 27,065.30 | 31-150 |
| 3956.901 | 4. |  | 24-132 | 3836.110 | 6 | 26,060.69 | 3-114 | 3689.165 | 3 | 27,098.72. | 17-136 |
| 3956.901 | 4. |  | 27-135 | 3834.785 | 3 | 26,069.71 | 14-126 | 3687.802 | 30 V | 27,108.73 | 12-132 |
| 3953.957 | 4 u | 25,283.99 | 19-123 | 3834.556 | 100 IV | 26,071.27 | 5-118 | 3685.516 | 2 u | 27,125.55 | 13-133 |
| 3953.660 | 5 | 25,285.89 | 14-121 | 3832.745 | 4 | 26,083.59 | 9-119 | 3682.660 | 2 | 27,146.59 | 25-141 |
| 3952.573 | $125 \mathrm{~V}$ |  | 9-114 | 3829.946 | 2 | 26,102.65 | 16-129 | 3680.084 | 4 | 27,165.59 | 9-123 |
| 3952.573 | $125 \mathrm{IV}$ | 25,292.84 | 9-114 | 3829.694 | 4 | 26,104.37 | 2-110 | 3679.92 | 1 | 27,166.80 | 30-147 |
| 3950.436 | 5 | 25,306.52 | 23-129 | 3827.227 | 3 | 26,121.19 | 24-136 | 3677.176 | 2 | 27,187.07 | 1-107 |
| 3949.412 | 5 | 25,313.11 | 3-107 | 3823.903 | 50 IV | 26,143.90 | 6-119 | 3673.739 | 2 | 27,212.50 | 14-135 |
| 3944.101 | 3 u | 25,347.11 | 17-123 | 3821.702 | 6 | 26,158.96 | 15-129 | 3672.166 | 5 d | 27,224.16 | 2-118 |
| 3943.888 | 100 IV | 25,348.54 | 28-137 | 3821.270 | 5 | 26,161.91 | 5-119 | 3671.941 | 4 | 27,225.83 | 6-123 |
| 3943.141 | 5 | 25,353.34 | 6-114 | 3820.871 | 5 | 26,164.64 | 21-134 | 3670.669 | 2 | 27,235.26 | 12-133 |
| 3942.151 | 125 IV | 25,359.71 | 1-102 | 3819.024 | 5 | 26,177.30 | 17-131 | 3668.727 | 4 | 27,249.68 | 1-108 |
| 3940.338 | 100 IV | 25,371.38 | 5-114 | 3818.688 | 5 | 26,179.60 | 19-132 | 3666.346 | 2 | 27,267.38 | 9-124 |
| 3939.662 | 3 | 25,375.73 | 3-108 | 3814-942 | 2 | 26,205.31 | 13-124 | 3664.944 | 1 | 27,277.81 | 31-151 |
| 3938.086 | 7 | 25,385.89 | 19-124 | 3808.384 | 3 | 26,250.43 | 14-128 | 3663.005 | 2 | 27,292.25 | 15-136 |
| 3937.643 | 2 | 25,388.74 | 26-135 | 3808.124 | 300 IV | 26,252.22 | 4-118 | 3659.972 | 6 | 27,314.86 | 2-119 |
| 3931.369 | 100 IV | 25,429.26 | 4-111 | 3803.097 | 200 IV | 26,286.88 | 10-120 | 3658.258 | 3 | 27,327.66 | 6-124 |
| 3931.088 | 125 IV | 25,431.08 | 2-105 | 3800.324 | 1 | 26,306.11 | 19-133 | 3656.756 | 3 | 27,338.88 | 29-144 |
| 3928.312 | 4 | 25,449.05 | 17-124 | 3799.097 | 3 | 26,314.56 | 16-131 | 3655.851 | 500 IV | 27,345.65 | 5-124 |
| 3927.383 | 4 | 25,455.07 | 10-116 | 3799.035 | 2 | 26,315.03 | 12-124 | 3655.349 | 2 | 27,349.40 | 8-125 |
| 3926.163 | 2 | 25,462.98 | 13-120 | 3792.326 | 50 IV | 26,361.58 | 13-126 | 3653.108 | 125 V | 27,366.18 | 10-128 |
| 3924.644 | 60 IV | 25,472.83 | 18-125 | 3790.342 | 3 | 26,375.38 | 27-140 | 3650.134 | 3 | 27,388.48 | 7-125 |
| 3921.731 | 100 V | 25,491.75 | 25-135 | 3786.632 | 150 IV | 26,401.22 | 2-111 | 3649.730 | 1 | 27,391.51 | 17-138 |
| 3913.995 | 2 | 25,542.14 | 19-126 | 3783.569 | 5 | 26,422.59 | 25-139 | 3645.455 | 4 | 27,423.63 | 9-126 |
| 3912.424 | 300 IV | 25,552.39 | 4-114 | 3782.524 | 75 IV | 26,429.89 | 14-129 | 3645.226 | 5 u | 27,425.36 | 24-131 |
| 3912.191 | 5 | 25,553.91 | 18-126 | 3781.620 | 150 IV | 26,436.21 | 15-132 | 3644.539 | 1 | 27,430.53 | 8-126 |
| 3909.313 | 6 | 25,572.73 | 12-120 | 3781.102 | 3 | 26,439.83 | 23-136 | 3639.868 | 1 | 27,465.73 | 11-133 |
| 3908.543 | 100 IV | 25,577.76 | 13-121 | 3777.668 | 5 | 26,463.87 | 3-117 | 3637.459 | 2 | 27,483.98 | 6-126 |
| 3908.094 | 3 | 25,580.70 | 20-129 | 3776.611 | 5 | 26,471.28 | 12-126 | 3633.391 | 3 | 27,514.68 | 1-110 |
| 3904.582 | 2 | 25,603.71 | 30-141 | 3772.650 | 4 | 26,499.07 | 26-140 | 3631.194 | 125 V | 27,531.33 | 8-127 |
| 3904.340 | 5 | 25,605.30 | 17-126 | 3771.602 | 6 | 26,506.43 | 16-133 | 3627.001 | 2 | 27,563.16 | 14-136 |

Table III.-Continued.

| Wave- <br> Length | Int. | Wave <br> Number | Сомв. | Wave- <br> Length | Int. | Wave <br> Number | Сомв. | Wave- <br> Length | Int. | Wave Number | Сомв. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3623.837 | 200 V | 27,587.22 | 28-144 | 3471.546 | 1 | 28,797.39 | 22-143 | 3286.020 | 5 d | 30,423.22 | 18-149 |
| 3618.576 | 2 | 27,627.33 | 18-139 | 3467.776 |  | 28,828.70 | 3-132 | 3285.224 | 125 V | 30,430.59 | 14-147 |
| 3613.701 | 150 V | 27,664.60 | 6-128 | 3466.952 | 4 | 28,835.55 | 2-128 | 3284.221 | 4 | 30,439.88 | 23-151 |
| 3611.331 |  |  | 4-126 | 3464.160 | 6 | 28,858.79 | 10-137 | 3283.680 | 4 | 30,444.90 | 11-143 |
| 3611.331 | 2 |  | 5-128 | 3463.138 | 1 | 28,867.31 | 14-141 | 3280.485 | 4 | 30,474.55 | 17-149 |
| 3603.355 | 3 | 27,744.03 | 23-141 | 3457.177 | 4 | 28,917.08 | 9-136 | 3279.842 | 125 V | 30,480.52 | 4-141 |
| 3600.583 | 60 V | 27,765.39 | 28-145 | 3456.772 | 3 | 28,920.47 | 29-151 | 3271.151 | 4 | 30,561.50 | 12-145 |
| 3598.196 | 50 V | 27,783.81 | 9-129 | 3456.340 | 1 u | 28,924.08 | 8-136 | 3267.245 | 2 | 30,598.08 | 16-148 |
| 3596.725 | 2 | 27,795.17 | 19-140 | 3452.623 | 3 | 28,955.22 | 3-133 | 3263.884 | 5 | 30,629.54 | 13-146 |
| 3594.61 | 3 | 27,811.52 | 1-111 | 3451.617 | 3 | 28,963.66 | 20-143 | 3263.071 | 2 | 30,637.17 | 1-131 |
| 3594.496 | 1 | 27,812.41 | 1-112 | 3449.910 | 1 | 28,977.99 | 27-148 | 3261.242 | 1 | 30,654.36 | 15-148 |
| 3593.134 | 2 | 27,822.95 | 10-132 | 3448.290 | 3 | 28,991.60 | 27-149 | 3259.784 | 3 | 30,668.07 | 15-149 |
| 3589.390 | 1 | 27,851.96 | 22-141 | 3442.955 | 3 | 29,036.53 | 23-145 | 3254.013 | 5 | 30,722.45 | 13-147 |
| 3587.639 | 4 | 27,865.56 | 27-143 | 3442.380 | 75 V | 29,041.38 | 18-142 | 3246.678 | 60 V | 30,791.86 | 11-145 |
| 3586.753 | 2 | 27,872.45 | 15-139 | 3436.304 | 4 | 29,092.73 | 17-142 | 3243.370 | 200 V | 30,823.27 | 19-150 |
| 3578.738 | 1 | 27,934.87 | 1-114 | 3428.697 | 3 | 29,157.27 | 6-137 | 3242.135 | 2 | 30,835.01 | 18-150 |
| 3574.906 | 1 | 27,964.81 | 12-136 | 3427.605 |  | 29,166.56 | 1-120 | 3236.735 | 150 V | 30,886.45 | 17-150 |
|  |  |  | ( 6-130 | 3427.605 |  | 29,166.56 | 2-130 | 3234.165 | 300 V | 30,910.98 | 9-142 |
| 3570.983 | 3 | 27,995.5 | 9-131 | 3426.583 | 4 | 29,175.26 | 5-137 | 3233.441 | 3 | 30,917.91 | 8-142 |
|  |  |  | 16-140 | 3421.556 | 2 | 29,218.12 | 25-149 | 3231.236 | 200 V | 30,939.01 | 14-149 |
| 3566.77 | 1 | 28,028.60 | 2-122 | 3420.534 | 2 | 29,226.85 | 2-131 | 3229.363 | 4 | 30,956.95 | 7-142 |
| 3563.823 | 3 | 28,051.77 | 15-140 | 3420.176 | 5 | 29,229.91 | 16-142 | 3228.024 | 1 | 30,969.79 | 11-146 |
| 3559.328 | 2 | 28,087.20 | 30-150 | 3414.168 | 2 | 29,281.34 | 1-121 | 3226.036 | 2 | 30,988.88 | 3-141 |
| 3558.706 | 3 | 28,092.11 | 25-143 | 3412.334 | 4 | 29,297.08 | 18-143 | 3221.171 | 250 V | 31,135.68 | 19-151 |
| 3555.788 | 2 | 28,115.16 | 24-142 | 3409.405 | 2 | 29,322.25 | 22-146 | 3218.380 | 5 | 31,062.59 | 11-147 |
| 3554.993 | 150 V | 28,121.45 | 6-132 | 3406.364 | 2 | 29,348.43 | 17-143 | 3207.624 | 3 | 31,166.75 | 9-143 |
| 3552.727 | 5 | 28,139.39 | 5-132 | 3394.138 | 2 | 29,454.14 | 19-144 | 3206.921 | 2 | 31,173.58 | 8-143 |
| 3552.067 | 2 | 28,144.60 | 12-137 | 3392.784 |  | 29,465.89 | 18-144 | 3202.906 | 2 | 31,212.66 | 7-143 |
| 3551.664 | 4 | 28,147.80 | 13-138 | 3390.515 | 5 | 29,485.61 | 16-143 | 3190.341 | 3 | 31,335.58 | 9-144 |
| 3546.651 | 2 | 28,187.59 | 9-133 |  |  | 29,496.95 | 9-139 | 3189.638 | 4 | 31,342.49 | 8-144 |
| 3546.190 | 150 V | 28,191.25 | 3-126 |  |  | 29,496.95 | 24-149 | 3188.787 | 6 | 31,350.85 | 14-150 |
| 3545.781 | 2 |  | 4-130 | 3388.407 | 2 | 29,503.95 | 8-139 | 3184.212 | 4 | 31,395.84 | 6-144 |
| 3545.781 | 2 |  | 8-133 | 3383.925 | 1 | 29,543.03 | 7-139 | 3178.485 | 3 | 31,452.46 | 2-141 |
| 3545.603 | 3 | 28,195.92 | 10-134 | 3373.729 | 125 V | 29,632.31 | 19-145 | 3172.299 | 4 | 31,513.79 | 9-145 |
| 3543.520 | 4 | 28,212.49 | 27-145 | 3368.690 | 5 | 29,676.64 | 9-140 | 3171.615 | 200 V | 31,520.60 | 8-145 |
| 3539.086 | 300 V | 28,247.84 | 6-133 | 3366.554 | 150 V | 29,695.46 | 17-145 | 3167.918 | 3 | 31,557.37 | 11-148 |
| 3537.43 | ? | 28,261.06 | 25-144 | 3364.821 | 4 | 29,710.76 | 15-144 | 3167.324 | 3 | 31,563.29 | 14-151 |
| 3532.878 | 3 | 28,297.48 | 1-115 | 3361.853 | 3 | 29,736.99 | 6-140 | 3166.243 | 5 | 31,574.06 | 6-145 |
| 3532.609 | 3 | 28,299.63 | 30-151 | 3361.555 | 3 | 29,739.63 | 26-151 | 3164.154 | 200 V | 31,594.91 | 4-144 |
| 3530.022 | 5 | 28,320.37 | 4-132 | 3355.011 | 7 | 29,797.63 | 2-135 | 3155.793 | 5 | 31,678.61 | 3-142 |
| 3529.043 | 2 | 28,328.23 | 10-135 | 3354.520 | 2 | 29,802.09 | 23-148 | 3154.506 | 5 | 31,691.54 | 9-146 |
| 3528.052 | 2 | 28,336.18 | 26-145 | 3352.986 | 3 | 29,815.62 | 23-149 | 3149.937 | 2 | 31,737.50 | 7-146 |
| 3527.850 | 4 | 28,337.80 | 1-117 | 3352.283 | 4 d | 29,821.88 | 18-146 | 3148.458 | 4 | 31,752.42 | 12-150 |
| 3527.607 | 2 | 28,339.76 | 19-141 | 3351.077 | 2 | 29,832.61 | 16-145 | 3146.407 | 200 V | 31,773.11 | 4-145 |
| 3520.522 | 150 V | 28,396.79 | 2-123 | 3349.967 | 5 | 29,842.49 | 25-151 | 3145.282 | 150 V | 31,784.48 | 9-147 |
| 3515.776 | 5 | 28,435.12 | 13-139 | 3346.517 | 4 | 29,873.26 | 17-146 | 3144.596 | 5 | 31,791.41 | 8-147 |
| 3509.254 | 3 | 28,487.97 | 11-138 | 3344.761 | 300 V | 29,888.94 | 15-145 | 3138.296 | 3 u | 31,855.23 | 13-151 |
| 3508.470 | 4 | 28,494.33 | 6-134 | 3342.531 | 2 | 29,908.88 | 1-124 | 3127.529 | 80 V | 31,964.89 | 12-151 |
| 3507.945 | 125 V | 28,498.60 | 2-124 | 3342.531 | 2 | 29,908.88 | 24-150 | 3125.762 | 1 | 31,982.96 | 11-150 |
| 3506.256 | 5 | 28,512.32 | 5-134 | 3341.868 | 100 V | 29,914.82 | 18-147 | 3114.055 | 1 u | 32,103.19 | 3-144 |
| 3503.978 | 3 | 28,530.86 | 28-148 | 3340.886 | 4 | 29,923.61 | 22-149 | 3097.079 | 2 | 32,279.15 | 9-148 |
| 3502.888 | 3 | 28,539.74 | 24-144 | 3339.505 | 4 | 29,935.98 | 4-140 | 3096.876 | 3 d | 32,281.27 | 3-145 |
| 3502.650 | 3 | 28,541.68 | 22-142 | 3334.896 | 1 | 29,977.35 | 3-138 | 3095.098 | 2 | 32,299.77 | 8-149 |
| 3501.453 | 60 V | 28,551.44 | 3-129 | 3331.224 | 3 | 30,010.40 | 16-146 | 3093.348 | 3 | 32,318.09 | 1-140 |
| 3495.941 | 4 | 28,596.45 | 15-141 | 3324.985 | 3 | 30,066.70 | 15-146 | 3091.292 | 3 d | 32,339.57 | 6-148 |
| 3493.728 | 5 | 28,614.56 | 13-140 | 3320.940 | 2 | 30,103.32 | 16-147 | 3079.906 | , | 32,459.12 | 3-146 |
| 3492.249 | 3 | 28,626.68 | 6-135 | 3320.781 | 2 | 30,104.77 | 13-143 | 3072.391 | 1 | 32,538.52 | 4-148 |
| 3482.355 | 6 | 28,708.01 | 20-142 | 3318.964 | 5 | 30,121.25 | 24-151 | 3071.109 3056.775 | 4 | 32,552.10 | 3-147 |
| 3482.139 | 5 | 28,709.79 | 29-150 | 3314.731 | 100 V | 30,159.71 | 14-141 | 3056.775 3051.163 | 200 V | $32,704.74$ $32,764.89$ | $9-150$ $6-150$ |
| 3481.155 | 3 | 28,717.91 | 24-145 | 3311.497 | 5 d | 30,189.16 | 11-142 | 3037.049 | 2 | 32,917.15 | 9-151 |
| 3480.382 | 4 | 28,724.29 | 12-140 | 3307.233 | 5 | 30,228.09 | 8-141 | 3032.727 | 3 | 32,964.06 | 4-150 |
| 3480.279 | 3 | 28,725.14 | 1-119 | 3303.225 | 3 | 30,264.76 | 3-139 | 3025.124 | 1 | 33,046.90 | 3-148 |
| 3475.670 | 5 | 28,763.22 | 3-131 | 3295.289 | 80 V | 30,337.65 | 14-146 | 2986.669 | 2 | 33,472.39 | 3-150 |
| 3474.216 | 6 | 28,775.26 | 11-139 | 3290.341 | 4 | 30,383.27 | 12-144 | 2862.787 | 3 | 34,920.77 | 1-148 |

state should be ${ }^{4} H_{3 \frac{1}{3}}$, whereas if $4 f 5 d^{2}$ is lower it should be ${ }^{4} I_{4 \frac{1}{2}}$. The $J$ value of the lowest state which we have thus far found is $3 \frac{1}{2}$, this possibly being ${ }^{4} H_{3\}}$. In any case the spectrum is not like that of La I, which Haspas' analysis purported to show.

Experimental $g$ values have been determined for several of the levels. While these are not very precise they do show large departures from the theoretical $g$ values, evidence of large interactions between the various levels. This perturbation is to be expected, since our term diagram, though far from complete, shows the greatest density of low levels yet observed. The fact that 13 low levels having $J$ values of $3 \frac{1}{2}$ have already been found means that at least 13 multiple terms lie within $8300 \mathrm{~cm}^{-1}$ of the lowest state. The large number of times this value of $J$ is found shows also that some of the low levels belong to $4 f 5 d^{2}$, since $4 f 5 d 6 \mathrm{~s}$ can account for only eight at the most. The two configurations probably interact so strongly that exact electron configuration assignments will have little meaning.

The energy levels found are presented in Table II. The low levels are numbered from 1 up in order of energy, and the middle levels are numbered from 101 up.

Table III contains a list of the lines which have thus far been classified. Those wave-lengths given to hundredths of an angstrom only are taken from Exner and Haschek; ${ }^{8}$ the remainder are M.I.T.-W.P.A. measurements. The second column contains the estimated intensity of the line as given by Klein ${ }^{9}$ or by Exner and Haschek, ${ }^{8}$ and, where known, King's temperature classification.
We record with gratitude assistance from a grant by the Rumford Committee of the American Academy of Arts and Sciences. We are particularly happy to acknowledge our debt to Colonel R. C. Eddy and the staff members of the W.P.A. project for their conscientious work on the wave-length determinations.

[^4]
# Pressure Effects of Homogeneous K Vapor in Absorption 

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#### Abstract

By use of the newly developed corrosion-resistant MgO windows, the K resonance lines in absorption of a homogeneous vapor, were obtained for pressures ranging from 0.001 to 20 mm Hg . The "dispersion" equation was generally adequate to describe the observed contours. The corresponding half-breadths were linear in the density, equal as between components, but of magnitude several times that predicted by the theory of the resonance interaction. The slight asymmetry which appeared at the highest pressure was attributed to van der Waals forces. But it is pointed out that, in contradistinction to the circumstance for Hg , a quantitative verification of the inverse sixth power law is probably not possible. The infrared bands of the $\mathrm{K}_{2}$ molecule were also observed.


THE strong asymmetries and shifts, characteristic of spectral lines arising from absorption by a metallic vapor in the presence of a foreign gas, have recently been the subject of extended investigation. The pressure effects in a homogeneous absorbing vapor, ${ }^{1}$ with the typical

[^5]marked symmetrical broadenings, are, however, not only less well understood, but their experimental study has been comparatively neglected. It is the purpose of this paper to describe an experimental investigation of the contours of the K resonance lines $(\lambda \lambda 7664.9,7699.0)$ for the latter case.

In what follows, it will be supposed that foreign gases are present in negligible quantity, so that the interactions among like particles only,


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