

Compton,⁶

$$R_c = Z^2 f^2 + Z(1-f^2), \quad (9)$$

where f is the common value of the structure factor for all of the electrons. This is no longer identical with the first two terms of Eq. (3), and is found⁸ to be in somewhat less satisfactory agreement with the experiments.

Though we are accustomed to think of the Schrödinger ψ_n functions as distributed continuously throughout space, these functions are strictly speaking in $3n$ -dimensional space. The apparent overlapping of the functions is merely a convenient 3-dimensional approximation. Thus the discreteness of the electrons in the classical theory corresponds on the wave-mechanics theory to equally discrete ψ_n functions, which are completely separated by being in different dimensions.

The closest classical analog to the wave-mechanical atom is thus one composed of discrete

⁸ G. Herzog, Zeits. f. Physik **69**, 207 (1931); E. O. Wollan, Rev. Mod. Phys. **4**, 241 (1932).

electrons, each of which has its own characteristic probability $\psi_n \psi_n^* d\tau$ of occurring within a given volume element.⁹ It is accordingly proper not only to speak of electrons occurring within the atom, but also to distinguish each individual electron by the name of the corresponding quantum state. That is, K electrons are distinguishable from L electrons, etc. Thus for treatment of scattering problems, individual electrons grouped within the atom form the most nearly adequate classical picture corresponding to the continuous de Broglie waves of the wave-mechanics atom.

⁹ Cf. A. H. Compton, Phys. Rev. **35**, 931 (1930), and Tech. Rev. Mass. Inst. **33**, 19 (1930). The conclusion there drawn was that the observed presence of incoherent scattering indicated that the discrete electron interpretation of $\psi\psi^*$ was necessary to bring agreement between theory and experiment. This argument was criticized by G. Herzog (reference 8), because of a supposed lack of agreement between the classical and quantum formulas, and because the concept of discrete electrons does not enter into the quantum theory of scattering. The statement that the best *classical* interpretation of $\psi\psi^*$ is the probability of occurrence of discrete electrons seems to be the legitimate conclusion from the considerations here advanced.

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The Arc Spectrum of Samarium and Gadolinium. Normal Electron Configurations of the Rare Earths

WALTER ALBERTSON, *George Eastman Research Laboratory of Physics, Massachusetts Institute of Technology*

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A partial analysis which includes most of the low temperature lines is presented for Sa I and Gd I: 453 lines, 175 levels for Sa I; 71 lines, 35 levels for Gd I. The normal configuration and lowest state of Sa I is $4f^6 6s^2 {}^7F$; for Gd I is $4f^7 5d 6s^2 {}^9D$. It is also shown that the normal configuration for Tm I is probably $4f^{13} 6s^2$. There exists in the rare earth group the same type of variation of relative binding between the $4f$ and $5d$ electrons as exists between the s and d electrons in the long periods. In the rare earth group the $5d$ electron is most tightly bound at the beginning and middle of the group and has a minimum just before the middle and at the end of the group.

INTRODUCTION

THE region of the periodic table least investigated by spectroscopists is that occupied by the fourteen elements from cerium to lutecium, inclusive,—the so-called rare earths. With the exception of thulium, ytterbium and lutecium, the arc and spark spectra of the rare earths are of extreme complexity. Indeed, the number of

lines obtained appears to depend only on the amount of exposure given. Even if one adheres to the strictest selection rules for L , S , J and parent terms, a fundamental electron transition in neutral gadolinium can yield more than 20,000 lines, and if only the J selection rule is retained, there is a possibility of more than 18,000,000 lines, whereas the identical electron jump in

caesium gives two lines. These figures indicate the apparent futility of an attempt by any worker to push the observation of a rare earth spectrum to its limit.

With the exception of the three elements mentioned above, by far the greater number of the intense lines of an arc exposure belong to the ionized rare earth atom. The work of King¹ on the furnace spectra of the rare earths has shown that the spectrum of the neutral atom is very poorly developed in an arc source. Many neutral lines that are comparatively well developed in the furnace appear so faint in the arc that they have not been measured, while a large number more are masked in the arc by the more intense ionized lines. It is practically impossible to analyze the spectrum of the neutral atom with only the use of arc and spark exposure data. Additional data from the furnace or from absorption measurements must be added.

The most characteristic rare earth spectra are shown by the end-group, thulium, ytterbium and lutecium, and by europium, which precedes the middle. Many of the lutecium and ytterbium lines have already been explained by Meggers and Scribner² and by Meggers and Russell³ as resulting from transitions involving *s*, *p* and *d* electrons. The *4f* shell is completely filled and contributes nothing to the term types. The europium spectrum is quite complex, but it does have a special character due to a small group of lines of outstanding intensity. These lines have been explained by the writer⁴ and by Russell and King.⁵ They result from transitions involving *s*, *p* and *d* electrons and configurations built on the parent term $4f^7\ ^8S$, which does not contribute to the *L* value of the resulting terms. Thus, although the most intense rare earth lines have been classified, no terms have been found for which the *4f* electrons contribute to the *L* value.

¹ Numerous articles in *Astrophys. J.*, Spectroscopic bibliography, R. C. Gibbs, *Rev. Mod. Phys.* **4**, 278 (1932).

² W. F. Meggers and B. F. Scribner, *Bur. Standards J. Research* **5**, 73 (1930).

³ W. F. Meggers and H. N. Russell, unpublished material. C. E. Moore, *Term Designations for Excitation Potentials*, Princeton Observatory and Carnegie Institute at Mt. Wilson.

⁴ W. E. Albertson, *Phys. Rev.* **45**, 499 (1934).

⁵ H. N. Russell and A. S. King, *Phys. Rev.* **46**, 1023 (1934).

ANALYSIS OF THE ARC SPECTRUM OF SAMARIUM EXPERIMENTAL DATA

Following the above-mentioned elements, the next most characteristic spectra are those of samarium, gadolinium, dysprosium and holmium. An extensive temperature classification of samarium has recently been completed by King.⁶ The author is greatly indebted to Dr. King, who was generous enough to send a duplicate list of the neutral lines prior to publication. The list contains 422 Class I and II lines, many of which are comparatively intense in the arc and reversed in the furnace, and more than 1200 Class III, IV and V lines. The latter classes appear in two distinct wavelength regions; one from the long waves to about 5100 Å, the other, from 3900 Å to short waves. King's data have been supplemented with absorption data recorded by Paul.⁷ These data for 337 lines extend from 7755 Å to 3527 Å. Although absorption lines were found out to 8700 Å, none of them belonged to samarium. Nearly all the Class I and the strong Class II lines in this region and strong Class III lines of wavelength less than 3900 Å appear in absorption.

RESULTS

The results of the analysis of the data are given in Tables I and II. Table I contains all the classified lines (453) that involve levels which are probably real. Over 200 lines are omitted from the list as they involve levels that do not show enough combinations to be accepted with confidence as being real. Most of these levels are no doubt real but they are all omitted as at present there is no way of telling which ones are spurious. Table I also contains all unclassified Class I lines of wavelength less than 7756 Å. Column 1 gives the wavelength from King's data; Column 2 the arc intensity; Column 3 the furnace intensity with temperature class; Column 4, absorption intensity; Column 5, the wave number in vacuum; Column 6, term combinations. The absorption intensities can be compared only over a small wavelength range. Table II contains the level number, energy of level in cm^{-1} and tentative *J* value.

⁶ A. S. King, unpublished material.

⁷ F. W. Paul, M.Sc. Thesis, M. I. T. (1934).

As is seen from Table II, the analysis has yielded a set of seven low levels, each having a different J value, increasing in order. A systematic search has shown that there are no other levels below 12,000 cm⁻¹ that combine readily with the middle and high levels already found. This is quite in agreement with the fact that only a few absorption lines remain to be explained.

At the present time all books on the subject state that the normal electron configuration for a rare earth is $4f^n5d6s^2$ where n increases progressively from 1 for cerium to 14 for lutecium. If such were the fact, then the normal configuration for samarium should be $4f^55d6s^2$. $4f^5$ gives rise to the following terms:

²PDFGH1KLMNO ⁴SPDFGH1KLM ⁶PDH.

Most of the quartet and doublet terms appear several times for each value of L . Let us consider just the ⁶H multiplet, since it will be the lowest and most important. The addition of the $5d$ electron to ⁶H gives rise to a pentad of septet and quintet multiplets, all expected to be fairly low in Sa I. Since only a single septet multiplet accounts for nearly all the low temperature lines and no other low levels could be found, the normal configuration of Sa I is obviously not $4f^55d6s^2$. Another configuration likely to be found low is $4f^66s^2$. This configuration yields only one septet multiplet, ⁷F. Furthermore it is known that when a d shell lacks a single electron of being half filled, i.e., d^4 , there is but a single multiplet of highest multiplicity, and it lies far below all other levels from the same configuration. These facts suggest quite strongly that the normal configuration of Sa I is $4f^66s^2$.

The chief electron configurations and transitions of Sa I are expected to be

- | | |
|-----|----------------------------|
| (1) | $4f^66s^2 - 4f^66s6p,$ |
| (2) | $4f^66s^2 - 4f^55d6s^2,$ |
| (3) | $4f^55d6s^2 - 4f^55d6s6p,$ |
| (4) | $4f^66s6p - 4f^55d6s6p.$ |

In (1) the chief multiplets will be built on the ⁷F parent term. The upper configuration will yield the triads ⁷F6s6p⁽⁹⁾, ⁷DFG, ⁷, ⁵DFG. Although the identification is uncertain, it is believed that most of the nonet and septet levels have been found. They occur at energy values

quite near those for the corresponding multiplets built on ⁸S of Eu I⁶. Table III gives a typical multiplet ⁷FG, the first complete septet multiplet yet found.

The configurations involving the $5d$ electron will yield an enormous number of multiplets. Most of the middle and high levels in Table II, probably belong to $4f^55d6s^2$.

Numerous recurring frequency differences among the intense long wavelength Class III and IV lines have been found with the aid of the mechanical interval sorter.⁸ Thus far they have defied attempts to link them together. These intervals probably belong to the configurations involving a $5d$ electron.

THE NORMAL ELECTRON CONFIGURATION FOR THE RARE EARTHS

The normal configuration of Eu I has already been shown by Russell and King⁵ to be $4f^76s^2$ instead of the previously supposed $4f^65d6s^2$. This result, with that of Sa I, suggested that the normal configuration of Gd I is $4f^86s^2$ giving identical multiplets with Sa I but inverted. King's data for gadolinium⁹ is not complete (4680–3840A) but it does cover the most important region of the spectrum. The results of an analysis of these data are presented in Tables IV and V. Table IV contains all the Class I and II lines and Table V the energy values of the levels with tentative J values. It is seen that nearly all of King's lines result from transitions between middle levels and a low regular multiplet of five levels. The low multiplet eliminates $4f^86s^2$ and answers quite well for ⁹D, the expected normal state from $4f^75d6s^2$.

The unpublished data of King for Tm I¹⁰ indicate an extremely simple structure for the low levels. Only a few lines appear, most of which are strong and reversed. The two most probable configurations are $4f^{12}5d6s^2$ and $4f^{13}6s^2$. The former configuration yields 107 levels and the latter only 2. The experimental data, although they have thus far defied analysis favor $4f^{13}6s^2$.

⁸ G. R. Harrison, R. S. I., **4**, 581 (1933).

⁹ A. S. King, Astrophys. J., **72**, 221 (1930).

¹⁰ A. S. King, unpublished material; Phys. Rev. **38**, 583 (1931).

TABLE I. Classified lines of Sa I.

I.A.	Int. and Temp. Arc Fur. Abs. ν (vac)	Class Designa- tion	I.A.	Int. and Temp. Arc Fur. Abs. ν (vac)	Class Designa- tion	I.A.	Int. and Temp. Arc Fur. Abs. ν (vac)	Class Designa- tion	
8027.5	1 - 15 IIA	12,453.8	6 - 15	5989.68	50 150 IA	2 16,690.72	1 - 19	5060.916	15 30 IIA
7907.48	5 40 IA	12,642.78	5 - 11	5979.38	200 200 IA	4 16,719.52	4 - 32	5049.503	10 30 IA
7787.02	8 60 IA	12,838.35	7 - 20	5936.92	2 8 IIA	16,839.10	4 - 35	5044.275	80 40 I
7755.32	? 80 IA	13,005.91	6 - 17	5927.89	20 60 IIA	16,864.75	6 - 54	5010.88	3 10 IA
7686.70	8 60 IA	13,187.40	3 - 8	5916.36	80 150 IA	3 16,897.61	2 - 22	4975.949	60 60 I
7580.91	5 60 IA	13,234.14	5 - 13	5914.91	12 40 IA	16,901.76	5 - 45	4946.305	40 60 II
7554.14	8 60 IA	13,306.1	5 - 15	5909.04	80 40 I	1 16,918.54	5 - 46	4924.044	30 30 II
7513.2	2 8 IIA	13,426.0	4 - 11	5906.05	50 40 I	1 16,927.11	4 - 37	4918.994	125 100 I
7446.2	1 - 5 IIA	13,503.78	7F - 9G	5902.60	80 40 I	1 16,937.00	5 - 47	4910.400	150 100 II
7403.30	8 60 IA	13,550.01	4 - 12	5895.35	4 20 IA	16,957.83	3 - 28	4907.81	2 2 III
7378.04	5 60 IA	13,550.01	4 - 12	5883.68	10 50 IIA	1 16,991.47	5 - 49	4904.963	80 80 II
7367.9	1 - 4 IIA	13,568.6	3 - 9	5875.92	40 100 IA	1 17,013.91	4 - 39	4883.971	200 100 II
7332.65	60 100 I	13,633.88	7 - 27	5874.21	200 150 I	3 17,018.86	3 - 29	4883.763	100 100 II
7279.25	80 100 I	13,733.90	6 - 20	5871.06	150 125 I	2 17,027.99	6 - 56	4848.309	100 100 I
7262.69	3 20 II	13,765.21	6 - 21	5868.61	200 125 I	2 17,035.10	7 - 63	4841.701	400 150 I
7213.82	80 100 I	13,858.47	5 - 17	5876.79	250 80 II	2 17,037.48	6 - 57	4789.977	50 50 II
7172.67	40 30 I	13,937.88	5 - 18	5866.23	1 - 20 III	17,042.01	7 - 64	4785.884	150 125 I
7141.13	30 100 I	13,999.53	1 - 8	5860.78	4 40 IIA	17,057.86	6 - 58	4783.125	300 200 II
7131.80	100 150 I	14,017.84	4 - 13	5822.61	5 40 IA	17,169.68	2 - 23	4770.20	30 20 I
7114.50	10 80 I	14,051.93	3 - 10	5802.84	300 100 I	4 17,228.17	5 - 50	4760.291	300 150 rII
7106.23	100 150 I	14,068.29	7F - 9G	5790.91	8 50 IA	17,263.67	3 - 31	4760.033	50 60 II
7104.54	150 200 I	14,071.63	7F - 9G	5798.38	200 80 I	3 17,271.21	6 - 59	4750.725	60 50 II
7101.46	10 50 I	14,077.74	4 - 14	5779.24	200 100 I	3 17,298.53	4 - 40	4728.433	300 100 II
7096.33	100 150 I	14,087.91	2 - 17	5746.50	5 50 IIA	17,397.08	3 - 32	4718.641	40 30 I
7095.50	150 200 I	14,089.56	4 - 15	5741.19	3 4 I	17,413.18	3 - 33	4717.071	150 125 I
7091.16	100 150 I	14,098.19	7F - 9G	5732.95	300 150 II	2 17,438.20	7 - 68	4716.097	250 80 I
7088.30	150 250 I	14,103.87	3 - 11	5726.06	3 10 IIA	17,459.18	4 - 42	4688.733	150 100 II
7056.55	40 40 I	14,167.33	2 - 26	5720.19	125 60 II	2 17,477.10	2 - 28	4684.196	1 4 II A
7026.62	100 200 IA	14,227.67	3 - 12	5711.45	40 60 II	1 17,503.84	5 - 53	4681.551	50 40 II
7002.03	2 60 IA	14,277.64	7 - 34	5707.22	3 25 IA	17,516.82	3 - 35	4678.084	3 4 I
6912.79	3 100 IIA	14,461.96	6 - 26	5706.75	80 80 I	1 17,518.56	2 - 26	4670.834	60 80 I
6880.86	20 200 II	14,529.07	6 - 27	5706.20	300 100 rII	2 17,519.95	4 - 44	4670.747	50 60 I
6860.93	300 300 I	14,571.27	2 - 10	5698.68	20 20 I	17,579.16	7 - 69	4664.509	2 10 II A
6853.92	15 150 IIA	14,586.17	5 - 20	5678.74	3 15 IIA	17,604.67	3 - 37	4663.556	100 80 rI
6839.23	10 100 IIA	14,617.50	2 - 21	5659.86	400 200 rII	3 17,663.39	3 - 38	4649.491	100 80 rI
6827.81	40 150 IA	14,641.95	4 - 17	5652.84	30 40 I	2 17,685.33	4 - 45	4648.078	40 40 I
6802.96	50 150 IA	14,695.43	3 - 13	5642.67	6 20 II A	17,717.20	5 - 54	4645.405	100 100 rI
6790.88	30 60 IA	14,721.57	4 - 18	5641.59	8 10 II	17,720.59	4 - 47	4640.518	3 8 IA
6779.16	100 200 IA	14,747.03	2 - 12	5626.01	250 150 rII	3 17,769.67	1 - 28	4632.770	1 8 IA
6775.30	60 150 IA	14,755.43	3 - 14	5621.79	200 100 I	17,783.00	2 - 31	4629.430	5 20 IA
6759.25	60 15 III	14,790.46	7 - 41	5591.17	20 40 IA	17,880.39	5 - 56	4618.228	2 10 II A
6725.88	300 200 I	14,863.85	1 - 10	5588.20	100 30 II	1 17,889.90	5 - 57	4616.615	1 12 II A
6671.51	800 400 I	14,984.98	5 - 58	5581.83	10 20 II	17,910.31	5 - 58	4611.248	20 50 IA
6588.91	500 300 I	15,172.83	6 - 34	5575.59	15 20 I	17,930.36	6 - 63	4602.024	1 10 IA
6580.53	50 200 IA	15,192.16	2 - 26	5574.89	80 30 II	2 17,932.61	2 - 33	4598.285	4 8 IA
6566.36	80 100 I	15,224.94	6 - 36	5573.42	100 60 II	2 17,937.34	6 - 64	4596.743	60 100 rI
6563.52	150 200 I	15,231.53	5 - 24	5561.37	50 20 II	17,976.20	3 - 40	4581.729	150 80 I
6562.64	10 80 IA	15,233.57	7 - 48	5550.40	300 200 rII	4 18,011.73	4 - 50	4581.581	100 100 rI
6558.18	8 50 IA	15,243.95	7 - 49	5548.95	150 125 I	3 18,016.44	4 - 58	4580.188	1 12 II A
6551.80	200 300 I	15,258.77	1 - 4 III	5517.87	1 100 I	18,117.91	6 - 66	4569.579	6 20 IA
6544.95	40 150 IA	15,274.75	2 - 14	5516.09	500d 300 rII	4 18,123.76	5 - 59	4566.767	12 25 IA
6536.83	30 150 IA	15,293.73	5 - 25	5512.10	200 100 I	4 18,136.88	3 - 42	4556.628	4 40 IA
6533.96	200 300 I	15,300.44	5 - 27	5511.09	60 40 I	18,140.18	5 - 60	4539.830	1 - 5 II A
6532.25	200 300 I	15,304.44	5 - 28	5513.44	20 20 II	18,173.81	3 - 43	4537.570	2 10 IA
6528.02	200 250 I	15,314.36	5 - 26	5500.90	10 25 IIA	18,182.70	2 - 38	4536.161	1 20 IA
6509.44	50 300 IA	15,358.07	2 - 16	5498.21	200 150 II	3 18,182.70	2 - 38	4531.869	1 20 IA
6501.00	25 100 IA	15,378.01	6 - 39	5493.72	300 200 rII	3 18,197.56	3 - 44	4534.869	1 20 IA
6492.05	5 25 IIA	15,399.11	3 - 18	5485.42	150 100 rII	2 18,225.09	1 - 33	4533.799	50 50 I
6491.28	15 100 IA	15,401.03	4 - 21	5466.72	250 125 rII	3 18,287.44	4 - 53	4532.444	8 40 IA
6425.90	200 250 I	15,557.73	5 - 29	5453.00	300 150 rII	3 18,333.45	6 - 68	4527.418	5 15 IA
6387.79	4 100 IA	15,655.05	1 - 16	5433.82	30 20 II	2 18,398.16	3 - 47	4523.182	30 30 I
6373.50	10 100 IIA	15,685.64	6 - 41	5421.57	80 30 I	2 18,439.73	5 - 61	4522.546	20 30 I
6373.29	4 60 IA	15,686.16	5 - 30	5411.39	100 50 II	1 18,474.42	6 - 69	4511.327	40 40 I
6371.01	150 150 I	15,691.77	7 - 52	5411.15	10 40 IIA	1 18,475.24	1 - 38	4504.321	1 - 6 II A
6367.41	250 250 I	15,700.64	4 - 22	5405.23	200 125 rII	3 18,495.47	2 - 40	4503.378	80 125 rI
6295.97	15 80 IIA	15,878.80	2 - 19	5403.70	200 80 I	3 18,500.71	4 - 54	4499.108	100 150 RI
6273.29	15 100 IA	15,936.20	3 - 22	5368.32	150 80 II	2 18,622.52	7 - 76	4490.758	1 - 10 II A
6258.94	4 30 IIA	15,972.74	4 - 23	5353.701	1 5 IIA	18,673.49	4 - 57	4490.019	4 30 IIA
6242.39	60 200 IA	16,015.08	4 - 24	5349.116	15 40 IA	2 18,689.49	3 - 50	4480.316	30 60 I
6229.07	3 20 IIA	16,049.33	5 - 35	5348.067	10 30 IA	2 18,693.16	2 - 43	4477.505	6 15 IA
6226.70	100 20 II	16,055.44	5 - 35	5341.265	100 50 I	3 18,716.96	2 - 44	4471.504	1 8 II A
6222.55	15 30 IA	16,066.15	6 - 46	5320.575	100 100 I	4 18,789.75	5 - 64	4470.886	100 100 rI
6218.23	50 150 IA	16,077.31	{ 5 - 36	5299.21	4 15 IA	18,865.50	3 - 51	4470.475	1 4 II A
6198.37	30 125 IA	16,128.82	6 - 48	5271.388	200 125 I	3 18,965.07	3 - 53	4459.290	80 60 I
6196.83	2 25 IIA	16,132.83	7 - 56	5269.90	5 10 IA	18,970.21	5 - 66	4456.708	3 40 IA
6194.39	200 200 I	16,139.18	6 - 49	5265.646	20 25 I	2 18,985.75	1 - 43	4452.953	60 50 I
6174.45	150 150 I	16,191.30	5 - 49	5251.912	150 100 I	5 19,035.40	5 - 67	4445.153	80 125 rI
6159.56	150 200 I	16,230.45	5 - 39	5210.738	10 12 I	18,198.51	5 - 68	4443.270	6 15 IA
6117.79	40 150 IA	16,341.26	4 - 29	5200.592	200 100 I	3 19,223.24	4 - 61	4442.276	80 100 rI
6103.95	3 15 IIA	16,378.31	3 - 22	5187.131	10 15 I	2 19,273.13	4 - 62	4441.812	100 150 RI
6099.90	40 200 IA	16,389.19	2 - 19	5185.550	2 6 IA	19,279.00	3 - 55	4433.344	3 50 IIA
6096.55	6 80 IA	16,398.19	2 - 19	5175.443	150 80 I	3 19,316.65	4 - 56	4433.076	15 30 IA
6084.12	400 250 I	16,431.69	4 16,469.75	5172.750	80 40 I	2 19,326.71	5 - 69	4429.664	60 80 rI
6070.06	300 200 I	16,469.75	4 - 30	5157.260	20 30 I	2 19,384.75	2 - 51	4423.383	10 20 IA
6045.00	300 150 I	16,538.03	5 - 41	5145.834	10 12 I	1 19,427.80	5 - 70	4419.332	80 150 RIA
6027.52	40 100 IA	16,585.99	4 - 31	5122.159	125 60 I				

TABLE I—(Continued.)

I.A.	Int. and Temp. Arc	Class Fur.	Temp. Abs.	Class ν (vac)	Designa- tion	I.A.	Int. and Temp. Arc	Class Fur.	Temp. Abs.	Class ν (vac)	Designa- tion	I.A.	Int. and Temp. Arc	Class Fur.	Temp. Abs.	Class ν (vac)	Designa- tion
4397.341	60	60 I	2	22,734.65	3-86	3960.501	1	8 IIIA	1	25,242.21	3-116	3481.523	4	10 III		28,714.87	7-166
4393.354	60	30 II	1	22,755.28	4-96	3951.887	100	60 rI	3	25,297.23		3466.796	30	20 III		28,836.85	3-141
4393.170	1	20 IIIA		22,756.23	7-122	3949.849	4	10 IA	1	25,310.29	5-128	3465.466	60	30 III		28,847.92	4-149
4386.219	40	60 I	2	22,792.30	5-106	3945.252		8 IIIA		25,339.78	6-128	3457.788	1	2		28,911.47	5-156
4381.257	1	8 IIIA		22,818.11	3-88	3926.325	20	20 II	1	25,461.92	5-131	3447.790	20	15 III		28,995.81	5-158
4380.423	100	100 rI	2	22,822.45	4-97	3925.216	400	60 rI	2	25,469.12	3-118	3446.58	1	4		29,005.99	3-143
4365.954	4	25 IA	1	22,893.09	3-89	3909.946	50	12 I	1	25,568.58	6-136	3431.890	20	20 III		29,130.14	4-151
4362.912	150	150 RI	2	22,914.05	1-80	3901.046	3	4		25,626.92	6-138	3427.855	2	6		29,164.44	6-163
4357.896	2	40 IIIA	1	22,940.42	6-117	3891.955	8	8 II		25,686.78	2-115	3421.903	1	5		29,215.16	6-164
4355.835	2	40 IA	2	22,951.28	2-83	3877.486	200	rII	2	25,782.62	7-142	3421.304	5	8 III		29,220.27	5-159
4350.815	6	50 IA	2	22,977.76	4-99	3858.737	200	100 rII	4	25,907.90	5-132	3416.198	20	12 III		29,263.94	4-152
4339.924	5	20 IIIA	2	23,035.42	3-90	3858.849	80	40 rII	1	25,909.37	4-126	3411.22	1	5		29,306.65	4-153
4338.965	25	60 IA	3	23,040.52	3-91	3854.556	150	rII		25,936.00	4-127	3410.037	20	12 III		29,316.82	3-146
4336.137	150	125 RI	2	23,055.54	6-137	3853.295	200	50 rII	1	25,944.49	6-139	3408.049	4	6 III		29,333.92	4-154
4331.447	40	50 I	3	23,080.51		3846.761	30	15 II	2	25,988.56	2-118	3394.815	5	6		29,448.26	4-155
4330.016	125	150 RI	3	23,088.13	2-85	3834.945	5	8		26,068.63	7-144	3391.024	3	5 III		29,418.18	5-161
4326.145	4	30 IIIA		23,108.79	7-124	3834.476	300	80 rII	3	26,071.81	7-145	3385.970	8	12 III		29,525.19	2-143
4325.163	3	30 IIIA	2	23,114.07	5-105	3832.808	150	20 III	3	26,083.16	5-133	3376.246	1	2		29,610.22	6-166
4324.460	60	60 rI	1	23,117.80	5-108	3824.811	8	8 III	1	26,137.69	4-129	3366.522	1	4		29,695.75	4-156
4319.530	100	100 rI	2	23,144.18	4-101	3822.972	100	15 III	3	26,150.27	3-123	3352.727	6	8		29,817.93	1-143
4313.871	3	30 IIIA	2	23,174.54	3-92	3818.363	80	20 III	3	26,181.83	4-130	3350.664	12	10 III		29,836.28	2-146
4312.854	60	30 I	2	23,180.00	5-109	3816.846	8	8 III		26,192.23	5-134	3338.864	8	8		29,941.72	3-152
4301.275	8	15 IIIA	1	23,242.41	3-94	3813.827	150	30 III	3	26,212.97	7-147	3334.119	3	2		29,984.34	3-153
4299.141	20	40 IA	2	23,253.94	2-86	3809.954	100	30 III	4	26,239.61	6-140	3331.935	4	4		30,003.98	4-159
4296.743	300	300 RI	2	23,266.92	rF-rC	3806.467	60	20 III	1	26,263.68	7-148	3331.074	6	6		30,011.75	3-154
4293.743	4	15 IIIA	1	23,283.18	4-103	3803.942	300	100 rII	4	26,281.09	1-118	3330.508	4	4		30,016.85	5-163
4290.832	1-	8 IIIA		23,298.97	5-110	3783.804	30	20 III	1	26,420.95	5-136	3324.872	2	4		30,067.73	5-164
4283.772	5	8 I		23,337.37	2-88	3775.459	10	15 III		26,479.35	5-138	3309.885	1	3		30,203.87	7-171
4283.500	80	80 rI	2	23,338.85	3-95	3773.331	150	80 rII	3	26,494.23		3307.346	1	3		30,227.05	4-160
4282.833	80	80 rI	1	23,342.49	5-111	3766.923	20	20 III	1	26,539.35	7-150	3291.429	15	10 III		30,373.22	3-156
4282.208	100	100 rI	2	23,345.89	6-120	3760.169	60	15 III	2	26,587.02	3-126	3287.693	2	3		30,407.73	3-157
4274.011	2	12 IIIA		23,390.66	5-112	3756.411	600	100 rII	3	26,613.62	3-127	3283.728	2	3		30,444.45	4-162
4271.862	40	40 I	2	23,402.43	5-113	3748.521	100	80 rII	3	26,669.64	2-123	3281.775	5	4		30,462.57	5-166
4266.309	30	20 I	2	23,432.89	3-96	3747.360	20	15 III		26,677.90	6-142	3277.354	5	6 III		30,503.66	2-153
4258.168	1	6		23,477.69	4-104	3745.463	100	80 rII	3	26,691.40	4-132	3274.430	1	4		30,530.90	2-154
4256.209	2	12		23,488.50	4-105	3730.737	100	25 III	2	26,796.75	5-139	3245.802	30	10		30,800.17	4-163
4244.246	3	12 IA	1	23,554.70	2-90	3728.126	.50	20 III	2	26,815.27	3-129	3234.850	1	3		30,904.45	3-160
4240.450	6	40 IA	1	23,575.79	4-106	3722.026	60	40 III	3	26,859.48	3-130	3232.489	6	6		30,927.01	2-157
4230.727	4	10 IA	1	23,629.97	1-88	3721.028	150	50 III	3	26,866.68	4-133	3218.260	2	2		31,063.75	6-170
4226.858	2	10 IIIA		23,651.60	6-122	3707.850	150	40 III	4	26,962.16	1-123	3217.706	1	2		31,069.10	4-165
4226.178	50	60 rI	5	23,655.30	3-99	3707.629	10	12 III		26,963.77	6-144	3214.613	2	4		31,098.99	6-171
4219.306	8	40 IA	2	23,693.93	2-92	3707.167	100	30 III	3	26,967.13	6-145	3212.224	1	3		31,122.12	3-162
4207.250	1	6 IIIA		23,761.72	2-94	3705.995	1	10 IIIIA		26,975.66	4-134	3205.636	6	1		31,186.92	6-172
4205.779	40	40 I	4	23,770.13		3690.084	300	50 III	2	27,091.98	5-140	3202.201	3	4		31,219.53	1-157
4201.766	1	4		23,792.83	5-117	3688.129	30	10 III		27,106.33	2-126	3181.386	2	2		31,423.78	2-160
4183.333	60	50 rI	4	23,897.67	4-107	3687.878	200	20 III	1	27,108.17	6-147	3177.748	3	3		31,459.76	5-169
4164.790	1	8 IIIA		24,004.07	6-124	3680.983	100	15 III		27,158.95	6-148	3159.497	1	2		31,641.48	2-162
4151.213	4	8 IA		24,082.58	4-110	3668.887	20	10 III		27,248.49	7-158	3157.688	1	1		31,659.61	7-174
4151.135	1	5 IA		24,083.03		3666.972	2	6 IIIIA		27,262.82	4-138	3149.027	1	2		31,746.67	3-165
4147.974	1	6 IA	1	24,101.38		3657.312	100	15 III	2	27,334.73	2-129	3135.985	2	2		31,878.70	6-173
4146.636	1	4 IA	1	24,109.16	5-119	3651.823	4	8 III		27,375.80	5-141	3132.751	10	5		31,911.61	7-175
4145.594	1	6 IA		24,115.22		3643.997	30	15 III	1	27,434.61	6-150	3132.288	1	1		31,916.32	5-170
4145.239	20	30 I	3	24,117.28		3636.106	30	8 III		27,494.14	6-151	3128.864	1	2		31,951.25	5-171
4142.969	1	4 IIIA		24,130.50	6-125	3629.480	80	40 III	3	27,544.33	3-133	3130.254	2	2		32,039.41	5-172
4138.734	3	12 IIIA	1	24,155.19	3-104	3604.714	4	8 III		27,733.57	7-161	3118.862	2	2		32,053.71	3-167
4135.505	10	20 IA	3	24,174.05	4-112	3594.508	2	4 III		27,812.31	6-155	3102.867	2	2		32,218.94	3-168
4106.284	1	8 IIIA		24,346.07	5-121	3594.004	20	12 III		27,816.21	5-144	3100.500	1	1		32,243.54	4-169
4087.505	1	10 IIIA		24,457.92	6-128	3592.894	10	8 III		27,824.80	3-135	3098.328	1	1		32,266.14	2-165
4079.834	20	40 IIIA	2	24,503.91	5-122	3586.360	80	40 III	3	27,875.40	4-140	3070.874	3	3		32,554.59	6-174
4069.751	1	8 IIIA		24,564.62	4-116	3562.224	15	15 III		28,064.36	5-149	3069.144	1	1		32,572.94	2-167
4062.320	15	40 IIIA	2	24,609.55	6-131	3552.206	8	10 III		28,143.51	6-158	3057.229	2	2		32,699.88	4-170
4051.822	1	6 IIIA		24,673.31	7-136	3550.216	50	40 II	1	28,159.29	4-141	3045.313	2	2		32,731.10	5-173
4016.111	2	4 IIIA		24,892.70	4-1												

TABLE II. Energy levels of Sa I.

Symbol	Level	<i>J</i>												
1	0.00	0	30	17,959.28	4	59	20,396.67	4, 5	90	23,847.25	2	118	26,281.09	1
2	292.58	1	31	18,075.57	2	60	20,413.30	3, 4	91	23,852.43	3	119	26,382.25	3, 4
3	811.92	2	32	18,209.04	3	61	20,712.80	3, 4	92	23,986.48	1, 2	120	26,471.36	6
4	1,489.55	3	33	18,225.13	1	62	20,762.84	2	93	23,996.55	4	121	26,619.18	3, 4
5	2,273.09	4	34	18,298.29	6	63	21,055.79	6	94	24,054.32	1, 2	123	26,776.98	5
6	3,125.46	5	35	18,328.64	3	64	21,062.82	5	95	24,150.80	3	124	27,129.49	6
7	4,020.66	6	36	18,350.40	4, 5	65	21,193.68	1	96	24,244.82	3	125	27,255.97	4, 5
8	13,999.43	1	37	18,416.62	2	66	21,243.27	4	97	24,312.03	4	126	27,398.92	2
9	14,380.44	2	38	18,475.28	1	67	21,308.50	3, 4	98	24,323.51	5	127	27,425.54	3
10	14,863.85	1	39	18,503.49	4	68	21,458.89	5	99	24,467.27	2, 3	128	27,583.38	4, 5
11	14,915.83	3	40	18,788.08	2	69	21,599.84	5	100	24,467.84	4, 5	129	27,627.25	2
12	15,039.59	2	41	18,811.11	5	70	21,700.89	3	101	24,633.74	4	130	27,671.39	2, 3
13	15,507.35	3	42	18,948.80	3	71	21,813.22	2	102	24,668.79	5	131	27,735.01	6
14	15,567.32	2	43	18,985.74	1	73	22,313.63	1	103	24,772.74	4	132	28,180.95	5
15	15,579.11	4	44	19,009.52	2	74	22,491.94	2	104	24,967.14	3	133	28,356.24	4
16	15,650.55	1	45	19,174.84	4	75	22,632.34	3	105	24,977.99	3, 4	134	28,465.26	4
17	16,131.53	4	46	19,161.62	4, 5	76	22,643.12	5	106	25,065.37	4	135	28,636.67	1
18	16,211.04	3	47	19,210.10	3	77	22,844.00	2	107	25,387.19	4	136	28,694.02	5
19	16,690.76	1	48	19,254.29	6	78	22,893.07	3, 4	108	25,390.91	5	138	28,752.40	4
20	16,859.31	5	49	19,264.60	5	79	22,893.40	2	109	25,453.11	5	139	29,069.90	4, 5
21	16,890.59	4	50	19,501.27	3	80	22,914.07	1	110	25,572.10	3, 4	140	29,365.03	4
22	17,190.19	2	51	19,677.38	1, 2	82	23,230.73	3	111	25,615.57	5	141	29,648.83	3
23	17,462.31	2	52	19,712.44	6	83	23,243.80	1, 2	112	25,663.67	3, 4	142	29,803.32	6
24	17,504.63	3, 4	53	19,776.97	3	84	23,316.62	3	113	25,675.50	5	143	29,817.92	1
25	17,566.84	3, 4	54	19,990.25	4	85	23,380.72	2	114	25,840.31	6	144	30,089.27	5
26	17,587.44	5	55	20,091.03	1	86	23,546.54	2	115	25,979.35	1, 2	145	30,092.53	6
27	17,654.03	6	56	20,153.47	5	87	23,594.86	4	116	26,054.15	2, 3	146	30,128.83	2
28	17,769.68	1	57	20,162.99	4	88	23,629.98	1	117	26,065.88	5	147	30,233.63	6
29	17,830.80	3	58	20,183.36	4, 5	89	23,709.98	3	137	26,181.95	6			

TABLE III. Typical 7FG multiplet in samarium.

7F	0	1	2	3	4	5	6
7G	0.00	292.58	811.92	1,489.55	2,273.09	3,125.46	4,020.66
22,914.07	22,914.05	22,621.52	22,102.15				
	150 2	80 2	30 2				
	150 RI	150 RIA	30 I				
	4362.912	4419.332	4523.182				
23,380.72	23,088.13	22,568.76	21,891.21				
	125 3	60 2	12 1				
	150 RI	80 rI	25 IA				
	4330.016	4429.664	4566.767				
24,150.80	23,338.85	22,661.25	21,877.74				
	80 2	30 2	6 2				
	80 rI	60 rIA	20 IA				
	4283.500	4411.585	4569.579				
24,633.74	23,144.18	22,360.68	21,508.27				
	100 2	100 2	40 1				
	100 rI	100 rI	40 I				
	4319.530	4470.886	4648.078				
25,615.57	32,342.49	22,490.12	21,594.90				
	80 1	80 2	5 2				
	80 rI	125 rI	20 IA				
	4282.833	4445.153	4629.430				
26,471.36	23,345.89	22,450.72					
	100 2	60 2					
	100 rI	50 I					
	4282.208	4452.953					
27,287.58	23,266.92						
	300 2						
	300 RI						
	4296.743						

Wave number
Arc abs.
Fur.
Wavelength

TABLE IV. *Classified lines of Gd I.*

I.A.	Int. and Temp.	Class	(vac)	Designation	I.A.	Int. and Temp.	Class	(vac)	Designation	I.A.	Int. and Temp.	Class	(vac)	Designation
Arc	Fur.				Arc	Fur.				Arc	Fur.			
4680.04	40	150 II	21,361.38		4286.127	100	60 II	23,324.55	5-23	4023.154	80	100 I	24,849.12	
4658.60	6	40 IIA	21,459.69		4274.167	40	60 II	23,389.81	1-15	4019.739	12	40 IIA	24,870.23	3-27
4654.765	4	20 IIIA	21,477.39	5-12	4267.010	80	80 II	23,429.04	2-16	4015.592	6	10 III	24,895.92	5-35
4647.650	30	50 II	21,510.25	5-14	4266.601	125	100 II	23,431.29	4-18	4008.339	25	50 IIA	24,940.96	4-30
4608.583	8	30 IIIA	21,692.59	3-6	4260.123	125	100 II	23,466.92	3-17	4006.975	6	30 IIIA	24,949.46	2-34
4602.932	40	60 II	21,719.22	4-9	4225.846	300	300 rI	23,657.26	5-25	3992.696	20	40 IIA	25,038.67	
4581.294	100	100 II	21,821.80	4-10	4225.028	20	50 IIA	23,661.84	5-26	3987.840	50	50 II	25,069.17	
4542.034	125	100 II	22,010.42	2-12	4191.628	125	100 I	23,850.38	4-21	3979.346	60	80 IIIA	25,122.68	2-24
4537.820	200	150 I	22,030.86	3-5	4190.779	200	200 I	23,855.21	4-22	3974.819	30	40 II	25,151.29	4-33
4519.661	200	150 I	22,119.37	2-7	4175.539	200	150 I	23,942.28	5-28	3972.713	30	40 I	25,164.62	1-34
4506.226	200	125 I	22,185.32	3-7	4167.271	12	30 IIA	23,989.78	4-32	3969.004	60	50 I	25,188.14	2-27
4503.803	8	30 IIIA	22,197.25	4-12	4157.781	15	50 IIA	24,044.53	4-23	3966.279	60	60 II	25,205.44	
4497.133	150	100 I	22,230.17	4-14	4148.864	20	40 IIA	24,096.21		3953.372	80	40 I	25,287.73	3-29
4486.908	125	100 II	22,280.83	5-17	4134.169	100	100 I	24,181.81	3-20	3945.548	150	100 I	25,337.88	1-24
4485.484	8	30 IIIA	22,287.90	3-10	4127.3	2	4 IIIA	24,221.0	5-30	3943.244	30	20 II	25,352.68	
4476.144	300	150 I	22,334.41	1-7	4111.251	2	3 IIIA	24,316.66	3-21	3942.643	60	30 I	25,356.55	
4473.282	20	40 IIA	22,348.70	2-8	4100.269	60	50 I	24,381.79	4-26	3941.802	40	25 II	25,361.95	
4430.631	300	150 I	22,563.83	1-5	4092.718	100	80 PI	24,426.77	5-31	3935.393	40	30 II	25,403.25	1-27
4422.409	300	150 I	22,605.78	2-10	4091.966	2	3 III	24,431.26	5-33	3934.790	200	50 I	25,407.18	3-30
4414.741	200	100 I	22,645.04	4-16	4090.418	40	30 I	24,440.55	2-19	3905.653	30	25 II	25,596.69	
4411.160	150	80 I	22,663.43	3-12	4087.847	2	10 IIIA	24,455.87	3-32	3904.293	20	25 II	25,605.60	2-29
4401.849	300	150 I	22,711.33	5-18	4080.534	15	30 IIA	24,499.70	2-20	3902.718	30	25 II	25,615.94	4-35
4373.831	300	150 I	22,856.85	3-15	4078.705	300	200 I	24,510.69	3-23	3874.476	8	6 II	25,802.66	
4346.624	200	150 I	22,999.92	2-13	4058.222	250	200 I	24,634.40	2-21	3867.62	8	6 II	25,848.40	
4346.460	400	250 I	23,000.78	4-17	4054.731	80	75 I	24,655.61	1-19	3811.989	30	15 II	25,852.61	
4327.106	250	200 I	23,103.66	1-11	4053.643	200	150 I	24,662.23	2-28	3843.275	40	10 I	26,012.13	
4325.691	200	200 I	23,111.21	3-16	4045.013	60	100 I	24,714.84	1-20	3840.264	6	5 II	26,032.52	
4321.202	100	100 II	23,135.23	5-22	4035.396	20	60 IIA	24,773.74	2-32					
4313.851	200	200 I	23,174.65	2-15	4027.613	12	50 IIIA	24,821.61	4-29					
4306.348	200	150 I	23,215.02	1-13	4023.355	60	100 I	24,847.88	3-26					

TABLE V. *Energy levels of Gd I.*

Symbol	Level	J												
1	0.00	2	7	22,334.40	2	13	23,215.03	2	19	24,655.64	2	34	25,164.60	2
2	215.12	3	8	22,563.83	3	14	23,229.32	6	20	24,714.82	3	24	25,337.89	2
3	532.99	4	9	22,718.33	3	15	23,389.81	3	21	24,849.52	4	25	25,376.37	7
4	999.14	5	10	22,820.91	4	16	23,644.18	4	22	24,854.34	6	26	25,380.93	5
5	1,719.09	6	11	23,103.66	1	17	23,999.92	5	32	24,988.88	5	27	25,403.24	3
6	22,225.57	2	12	23,196.43	5	18	24,430.42	6	23	25,043.67	5	28	25,661.37	6

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TABLE VI. *Normal configurations of spectra in the rare earths.*

Atomic number	Element	Normal configuration
62	Samarium	$4f^6 6s^2$
63	Europium	$4f^7 6s^2$
64	Gadolinium	$4f^7 5d 6s^2$
69	Thulium	$4f^{13} 6s^2$
70	Ytterbium	$4f^{14} 6s^2$
71	Lutecium	$4f^{14} 5d 6s^2$