

INTENSITY MEASUREMENTS IN THE SPECTRUM
OF NICKEL AND COBALT

BY L. S. ORNSTEIN AND T. BOUMA

PHYSICAL LABORATORY OF THE UNIVERSITY OF UTRECHT

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ABSTRACT

Quantitative intensity measurements have been carried out in the Ni I and Ni II, and the Co I spectrum. The spectrographic outfit for the intensity measurements consisted of a stigmatic concave grating mounting used with step weakeners, and a Hilger E 1 used with the method of slit width variation. The *summation rules* have been tested both for *multiplets* and *supermultiplets*, also the intensity ratio for singlets and triplets, doublets and quartets. Serious divergencies have been found everywhere. In the Ni II spectrum an extension of the summation rules to supermultiplets gives better results in several cases. Intensity tables are given of the lines measured.

QUANTITATIVE intensity measurements have been carried out in the nickel I and II and the cobalt I spectrum. In the Ni I spectrum the analysis of Becher and Sommer¹ has been utilized; later on also the very extensive analysis by Russell, obtained through the courtesy of Professor Harrison.² For Ni II the analysis has been given by Shenstone,³ for Co I by Catalan and Bechert.⁴

In the Co II spectrum no intensity measurements have been carried out, the classified multiplets⁵ being situated in the far ultraviolet where intensity measurements meet with special difficulties.

Although the material used was the purest Ni and Co that could be obtained, the Ni contained some Fe, and the Co some Fe and Ni as impurities.

THE EXPERIMENTAL METHODS

In the first measurements for the Ni I spectrum an image of the light source through step-reducers was formed on the slit of a stigmatic concave grating-mounting; the line intensities was determined by the usual method.⁶ For the subsequent investigation a Hilger E 1 quartz-spectrograph was used. The density curves were obtained by the method of variable slit width.⁷

Frequently the photometer curves of two or more lines lying close together coalesced. In such cases it is necessary to change the photometer curve accurately point for point into the intensity curve of the complex of

¹ K. Bechert and L. A. Sommer, Ann. d. Physik **77**, 351 (1925) and **77**, 537 (1925).

² Afterwards published, Phys. Rev. **34**, 821 (1929).

³ A. G. Shenstone, Phys. Rev. **30**, 255 (1927).

⁴ Catalan and Bechert, Zeits. f. Physik **32**, 336 (1925).

⁵ Meggers and Walters. Scientific Papers of the Bureau of Standards No. 551.

⁶ L. S. Ornstein, Intensity of Multiple Spectrallines, Proc. Phys. Soc. **37**, 334 (1925).

⁷ L. S. Ornstein, Proc. Phys. Soc. **37**, 337 (1925).

lines. The same thing is done for a neighbouring isolated line. It may be assumed that the shape of the intensity curve for all these lines is the same⁸ and that therefore the intensity curve of the complex can be analysed into a few separate curves of this shape.

THE FIRST MEASUREMENTS

The Ni I quintet $z^5G^0 - e^5F$ was photographed with the above mentioned concave grating in second order. The results will be found in Table I, and for 0.95 amp. also in an intensity scheme (Table II).

TABLE I. *Intensities of the lines of the $z^5G^0 - e^5F$ multiplet of Ni I.*

Line λ	Intensity		Line λ	Intensity	
	1.4 amp.	0.95 amp.		1.4 amp.	0.95 amp.
4900.97	1	~ 1	4714.416	100	100
4874.803	1.1	~ 1	4686.209	11	11
4814.59	0.95	~ 1	4648.656	40	44
4786.541	38	41	4604.990	27	25
4756.529	26	29	4600.364	10	9.5
4715.757	22	24.5	4592.532	17	16

TABLE II. *Intensity scheme for the $z^5G^0 - e^5F$ multiplet of Ni I.*

Statistical Weight	z^5G^0					Sum	Quotient
	5	7	9	11	13		
3	9.5					9.5	3.2
5	11	16				27	5.4
e^5F 7	~ 1	24.5	25			50.5	7.2
9		~ 1	29	44		74	8.2
11			~ 1	41	100	142	12.9
Sum	21.5	41.5	55	85	100		
Quotient	4.3	5.9	6.1	7.7	7.7		

According to the summation rule the quotients in Table II ought to be equal. The divergencies are serious, as will be seen. Self-reversal cannot be the cause of this divergency for it would diminish the contrasts, whereas the divergencies lie in the opposite direction.

Although in the case under consideration the summation rule does not determine the intensity of each line separately, it gives the ratio of the extreme diagonal terms; this ought to be 27:91 i.e. 29.7:100. As this is a sensitive test, the intensity ratio between these two lines has been measured several times. (Table III).

TABLE III.

Current	Int. proportion
2.4	10. 9:100
1.4	10.15:100
1.4	9.9 :100
0.95	9.3 :100
0.95	9.6 :100

⁸ L. S. Ornstein and M. Minnaert, Zeits. f. Physik **43**, 404 (1927).

As blending with impurity lines is out of question, the experimental ratio 9.6:100 differs from the theoretical 29.7:100.

In order to get more facts the measurements have been continued with the Hilger E 1 in the ultraviolet. Here fairly large regions could be photographed at once and with a sufficient dispersion.

The current used was the smallest possible (about 0.45 amp.) A preliminary examination with 0.80 and 0.45 amp. showed that difference between the intensities found for these currents is comparatively small.

A few intensity measurements have also been carried out in an arc with a pressure of 50 and 28 cm of air. These also did not show any appreciable difference for the intensity. Therefore the definitive measurements for Ni I and CO I have been carried out with a current of 0.45 amp. in air.

In the Ni II investigation a Leyden jar was charged by the secondary tension of an induction coil. The spark discharge of the jar took place via a self-induction between two small bars of nickel. Variations of the conditions of discharge could not be used here. Only, to get a current of small density, a Leyden jar of the smallest possible capacity was chosen.

THE DEFINITIVE MEASUREMENT

In each of the three spectra mentioned a region has been chosen in which a number of multiplets, suitable for intensity measurements was situated. The region was situated for Ni I between 2900 and 3800A, for Ni II between 2450 and 3770A for Co I between 2500 and 4500A.

Besides the multiplets the intensities of all the lines appearing in the photographs have been measured. In the tables the intensities found by analysis of the photograms have been marked (1) when the analysis was certain, (2) when it was less certain and (3) when the analysis was very doubtful. Intensities marked (4) are inexact, owing to the slight density and the great influence of the irregularities which the photometer curve shows in the unexposed plate for that case. The tables are the least complete on the side of the largest wave-lengths where the dispersion was so small that several lines had to be omitted. The experimental facts have been used for testing: (1) the multiplet summation rules; (2) the supermultiplet summation rules; and (3) the intensity ratio for singlets and triplets, doublets and quartets. Generally the theoretical expectations are not fulfilled. For this reason we have limited our measurements to the spectral regions given below. Perhaps our material will be of some help in developing the intensity rules for the complicated spectra.

THE NI I SPECTRUM

Besides the quintet $z^5G^0 - e^5F$ already mentioned 13 multiplets have been examined.

The intensities in horizontal and vertical direction have been formed and the quotients of intensity sums and statistical weights have been calculated in the same way as has been done for $z^5G^0 - e^5F$, the results are collected in Table IV.

TABLE IV. Intensity quotients in multiplets of Ni I.

No.	Multiplet Designation	Quotients									
1	$a^3D - y^3D^0$	35	28	17				36	29	16	
2	$a^3F - y^3D^0$	11.7	6.2	5.8				9.1	3.9	3.8	
3	$a^3D - y^3F^0$	34	18	7.4				25	25	23	
4	$a^3F - y^3F^0$	10	7.5	3.2				2.4	7.0	7.8	
5	$a^3F - z^3G^0$	3.2	6.5	4.2				2.6	8.5	6.1	
6	$a^3P - v^3D^0$	0.4	0.4	0.4				0.8	0.8	0.7	
7	$a^3D - z^3G^0$	4.5	1.7					6.2	2.3		
8	$a^3D - z^3F^0$	31	22	10				30	28	24	
9	$a^3D - z^3D^0$	23	[25]	18				[37]	29	10	
10	$a^3F - z^3D^0$	22	21.6	10.3				23.3	10.1	6.6	
11	$a^3F - z^3F^0$	21	12.1	5.9				12	17.6	6.7	
12	$a^3D - z^3P^0$	70	51	33				49	28	14	
13	$a^3F - z^3P^0$		4.3	2.4				3.1	1.4		
14	$z^3G^0 - e^5F$	3.2	5.4	7.2	8.2	12.9	4.3	5.9	6.1	7.7	7.7

The quotients [25] and [37] have been deduced from sums containing a line, ordered doubly, so that they are too high by an unknown amount.

Only the multiplet 6 is in accordance with expectation (and multiplet 3 in one direction). In the case of all other multiplets the summation rules do not apply. In the case of the incomplete multiplets, e.g. $2^5G^0 - e^5G$ it also appears from the intensities of the lines present that the summation rule will not hold.

Supermultiplets. If singlet, triplet and singlet-triplet intercombinations are taken together, no satisfactory results are reached (Table V).

TABLE V. Supermultiplet sums and quotients of intensity.

Statistical weight	a^3D			a^1D	Sum	Quotient
	3	5	7			
y^3D^0	3	61	43	39	143	48
	5	47	55	20	162	32
	7		48	71	162	23
y^1D^0	5	8.7	23	72	103.7	21
Sum	116.7	169	111	174		
Quotient	39	34	16	35		

In the same way the quotients in Table VI are found.

TABLE VI.

Combinations	Quotients							
$a^3D, a^1D - z^3D^0, z^1D^0$	24	[35]	28	22	[38]	32	11	42
$a^3D, a^1D - y^3F^0, y^1F^0$	34	25	7	15	25	25	28	25
$a^3D, a^1D - z^3F^0, z^1F^0$	36	33	10	33	30	39	31	46

Again, when either the multiplets or all the lines, coming from the same term, are taken together the summation rules do not apply, e.g. for y^5D^0 : (Table VII).

TABLE VII.

Statistical weight	a^3F			a^3D			a^1D 5	Sums	Quotient
	5	7	9	3	5	7			
y^3D^0	35			61	43		39	178	59
5	5.2	26		47	55	40	20	193.2	39
7	5.2	1.3	34		48	71	43	202.5	29

Now we add up in Tables VIII and IX the spectral lines originating from the same level.

TABLE VIII.

TABLE IX.

	a^3F			a^3D		
	5	7	9	3	5	7
z^1G^0		31		z^1G^0		42
z^3G^0	13	59.3	54.8	z^3G^0	31	15.8
z^5G^0	1.6	11.8	22.2	z^5G^0	1.7	20.7
z^1F^0	30	51	32	z^1F^0	55	50
z^3F^0	60.4	123.3	60	z^3F^0	91	139
z^5F^0	41.4	46.5	57.9	z^5F^0	36	93.3
y^1F^0	1.7	5.0	4.7	y^1F^0		31
y^3F^0	12	49.2	70	y^3F^0	74	125
z^1D^0	1	54		z^1D^0	2.4	13
z^3D^0	116.3	71	59	z^3D^0	[110]	145
z^5D^0		0.65	2.1	z^5D^0	0.8	3.7
y^1D^0	10.5	4.2		y^1D^0	8.7	23
y^3D^0	45.4	27.3	34	y^3D^0	108	146
z^1P^0	3.8			z^1P^0	17	40
z^3P^0	15.5	9.5		z^3P^0	146.6	140
Sum	352.6	543.8	396.7		596.1	974.7
Quotient	71	78	44		199	195

Here the divergencies are smaller than for the separate multiplets. Still it is not very likely that the few multiplets still wanting will be able to equalize the quotients.

According to Mack⁹ the multiplets arranged in Table X belong together. Equal quotients are not obtained in this way either. Especially the first column shows a great divergence.

Finally we shall consider the ratio between the sums of the intensities for the corresponding singlet-triplet multiplets. When intercombinations are absent a ratio of 1:3 can be expected.¹⁰ The values found for our case are shown in Table XI; the last column contains the ratios after dividing the intensities by the fourth power of the frequency. There is a fairly great difference between the experimental and the theoretical ratios. However, fairly strong intercombinations are present in all 5 cases.

Table XII contains the intensities for all the lines in the spectral region investigated; an (arbitrary) intensity of 100 has been awarded to the line 3524.543.

⁹ J. E. Mack, Phys. Rev. **34**, 17 (1929).

¹⁰ L. S. Ornstein and H. C. Burger, Zeits. f. Physik **40**, 403 (1926).

TABLE X.

Statistical weight	a^3D			a^1D 5	Sum	Quotient
	7	5	3			
z^3F^0	93 7 5	86 53	91	78 [27]	93 230 180	10 33 36
z^3D^0	7 5 3	66 5.4 80 1	64 41 69	65 50 3	195 176.4 73	28 35 24
z^3P^0	5 3 1	100	9.6 67 70	4 9.5	167.6 162.5 70	34 54 70
z^1F^0 z^1D^0 z^1P^0	7 5 3	50 2.8 40	55 13 17	124 93 106	229 111.2 163	33 22 54
Sum Quotient	392.2 56	532 106	367 122	559.5 112		

TABLE XI.

Combinations	Ratio	
$a^1D - y^1D^0$ and $a^3D - y^3D^0$	1:5.1	1:5.1
$a^1D - y^1F^0$ and $a^3D - y^3F^0$	1:4.8	1:4.5
$a^1D - z^1F^0$ and $a^3D - z^3F^0$	1:3.1	1:2.6
$a^1D - z^1D^0$ and $a^3D - z^3D^0$	1:3.5	1:3.2
$a^1D - z^1P^0$ and $a^3D - z^3P^0$	1:3.6	1:4.4

TABLE XII. Intensities of Ni I lines. Intensities marked (1) are certain, (2) less certain, (3) doubtful, (4) inexact because of small intensity and the influence of irregularities in the plate.

λ (Kayser) ¹	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
2798.78	2798.651	23	3012.11	3012.007	72	3165.64	3165.513	0.8
2802.40	2802.28	3.1	3018.09	3017.96	0.3 (4)	3170.86	3170.73	0.3
2803.25	2803.15	1.4	3019.28	3019.150	42	3176.44	3176.30	0.4
2805.20	2805.081	4.7	3029.36	3029.30	0.6	3181.89	3181.75	3
2814.48	2814.37	0.5	3031.98	3031.869	28	3183.14	3183.05	0.8 (3)
2821.42	2821.296	31	3038.04	3037.940	55	3183.40	3183.26	1.9 (3)
2834.66	2834.550	4.2	3045.15	3045.012	26	3184.50	3184.372	11
2839.05	2838.97	1.3	3048.98		0.4	3191.97	3191.89	0.2
2849.93	2849.84	0.5	3050.92	3050.828	67	3195.67	3195.577	5.2
2865.61	2865.508	8.7	3054.42	3054.317	53	3197.22	3197.121	17
2868.85	2868.76	0.9	3057.76	3057.647	61	3199.44	3199.36	0.2
2905.85	2905.76	0.5	3064.75	3064.626	48	3200.50	3200.433	2.8
2907.58	2907.462	10.5	3066.59	3066.46	0.4	3202.21	3202.149	1.7
2914.12	2914.013	5.0	3080.91	3080.758	47	3207.05	3206.963	0.2
2916.95	2916.85	0.2 (4)	3097.27	3097.120	39	3210.00	3209.910	0.9
2917.60	2917.53	0.2 (4)	3099.25	3099.117	31	3213.53	3213.435	0.5
2931.03	2930.93	0.3 (4)	3101.67	3101.563	72 (1)	3214.17	3214.064	3.7
2932.74	2932.63	0.3 (4)	3101.99	3101.881	76 (1)	3216.93	3216.823	1.3
2944.06	2943.922	40	3105.60	3105.466	35	3217.93	3217.828	5.8
2958.39	2958.29	0.7	3107.83	3107.717	1.3	3219.92	3219.810	0.4
2969.30	2969.20	1.2	3114.26	3114.128	40	3221.41	3221.28	1.9 (1)
2973.84	2973.73	0.4	3116.84	3116.700	0.2 (4)	3221.81	3221.661	32
2981.80	2981.652	43	3129.42	3129.310	5.2	3223.66	3223.542	0.7
2983.56	2983.42	3.1	3132.68		0.3 (4)	3225.19	3225.030	39
2984.28	2984.129	34	3134.22	3134.106	74	3227.11	3226.992	8.4
	2991.103	1.7	3145.23	3145.117	0.4 (1)	3233.06	3232.945	46
2992.71	2992.597	42	3145.82	3145.707	9.5 (1)	3234.00	3233.88	0.7
2994.58	2994.458	42	3151.33	3151.29	0.15	3234.78	3234.658	31
3002.58	3002.492	71	3154.68	3154.58	0.5	3235.86	3235.764	1.0
3003.70	3003.628	55	3159.65	3159.524	0.7	3243.20	3243.064	50
3010.96		0.3	3164.30	3164.17	0.3	3245.47	3245.35	0.2

¹ H. Kayser. Handbuch der Spektroskopie.

TABLE XII (continued)

λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
3248.56	3248.44	15	3443.14	3443.00	0.2 (4)	3670.60	3670.424	9.5
3249.55	3249.440	3.8	3444.36	3444.247	0.8	3674.30	3674.105	27
3250.90	3250.749	20	3446.40	3446.263	80	3688.59	3688.413	9.4
3264.56	3264.44	0.1 (4)	3453.02	3452.891	59	3694.07	3693.933	2.8
3268.21	3268.09	0.3	3458.60	3458.467	91	3697.05	3696.904	0.25
3269.08	3268.96	0.08 (4)	3461.80	3461.660	78	3713.84	3713.696	0.2 (4)
3271.25	3271.118	13	3464.25	3464.12	0.3 (4)	3715.65	3715.498	0.2 (4)
3273.62	3273.50	0.15 (2)	3467.61	3467.505	23	3722.64	3722.484	9.6
3276.66		0.15	3469.65	3469.484	30	3724.95	3724.815	0.25
3277.35	3277.23	0.15	3472.71	3472.545	64	3729.06	3728.919	0.2 (4)
3282.03	3281.876	0.5	3476.80	3476.66	0.4	3730.90	3730.745	0.5
3282.81	3282.701	9.3	3478.00	3477.876	0.2 (4)	3736.98	3736.811	20
3284.56	3284.432	0.4	3478.42	3478.302	0.4	3739.40	3739.229	5.2
3287.08	3286.953	9.0	3479.36	3479.263	0.5	3739.94	3739.787	1.5
3293.83	3293.674	0.4	3480.30	3480.170	0.4	3744.72	3744.560	0.5
3296.42	3296.264	0.15	3483.98	3483.776	66	3749.19	3749.042	2.1
3305.10	3304.951	0.7	3486.09	3485.892	14	3762.76	3762.62	0.3
3307.16	3307.014	0.2	3488.43	3488.293	0.4	3769.60		0.15 (4)
3309.56	3309.44	0.2	3493.11	3492.965	86	3772.67	3772.518	0.7
3310.35	3310.206	1.9	3496.47	3496.352	0.8	3775.75	3775.562	50
3312.49	3312.319	2.8	3501.02	3500.852	58	3778.20	3778.048	0.9
3313.15	3312.992	0.7	3502.73	3502.604	4.9	3783.72	3783.521	51
3315.82	3315.668	55	3507.85	3507.695	6.5	3792.48	3792.325	1.1
3320.42	3320.259	54	3510.52	3510.340	70	3793.79	3793.599	2.5
3322.50	3322.316	43	3512.08	3511.94	0.4	3807.35	3807.135	65
3326.80	3326.673	0.4	3514.10	3513.947	22	3811.46	3811.32	0.08 (4)
3327.52	3327.402	0.6	3515.21	3515.057	86	3831.89	3831.685	9.5
3328.85	3328.720	1.0	3516.33	3516.220	3.5	3833.00	3832.865	0.65
3332.31	3332.19	0.5	3518.80	3518.635	2.3	3844.40	3844.27	0.2 (3)
3335.72	3335.59	0.06	3519.97	3519.776	51	3844.71	3844.58	0.15 (3)
3337.15	3337.015	0.4	3523.23	3523.075	4.6 (2)	3858.51	3858.284	78
3338.90	3338.763	0.1 (2)	3523.61	3523.445	11 (2)	3863.21	3863.08	0.3
3339.20	3339.049	0.4 (2)	3524.68	3524.543	100	3889.84	3889.673	0.9
3359.30	3359.104	1.4	3526.67	3526.53	1.0	3909.10	3908.93	0.3
3361.75	3361.557	53	3528.13	3527.988	13	3912.47	3912.31	0.2 (2)
3362.97	3362.808	2.4	3529.02	3528.890	0.6 (1)	3913.14	3912.975	0.15 (2)
3363.76	3363.612	0.6	3529.76	3529.625	0.5 (1)	3942.00	3941.86	0.1
3364.75	3364.590	1.1	3530.73	3530.588	0.9	3944.29	3944.10	0.4
3365.92	3365.771	48 (1)	3537.35	3537.243	0.3 (4)	3954.70	3954.53	0.1
3366.32	3366.169	51 (1)	3537.72	3537.634	0.4 (2)	3962.25	3962.10	0.1
3366.95	3366.808	4.5 (1)	3542.14	3542.00	0.3 (4)	3970.65	3970.49	0.35
3368.05	3367.892	5.4	3545.30	3545.16	0.3 (4)	3972.32	3972.157	1.4
3369.71	3369.576	59	3548.32	3548.189	41	3973.71	3973.547	4
3372.19	3371.995	50	3551.71	3551.563	5.3	3974.82	3974.681	0.35
3374.42	3374.228	33 (1)	3553.64	3553.483	1.7	3984.29	3984.17	0.2
3374.82	3374.637	11 (1)	3560.05	3559.925	0.4	3994.15	3993.97	0.1
3375.70	3375.560	0.5	3561.90	3561.752	8.2	4006.30	4006.14	0.01
3376.46	3376.330	0.8	3566.51	3566.373	93	4010.14	4009.99	0.007 (4)
3380.71	3380.577	106 (3)	3572.02	3571.871	63	4017.67	4017.56	0.15
3381.01	3380.885	13 (3)	3576.08	3575.94	0.4	4019.20	4019.055	0.06
3387.54	3387.467	0.3	3577.36	3577.23	0.4	4025.60	4025.44	0.1
3391.20	3391.051	48	3578.07	3578.928	12	4057.45	4057.30	0.1
3393.10	3392.993	66	3588.07	3587.928	12	4064.55	4064.380	0.05
3396.31	3396.174	0.6	3597.86	3597.699	67	4069.39	4069.24	0.015 (4)
3397.37	3397.28	0.1	3599.66	3599.530	0.3	4073.08	4072.93	0.01 (4)
3401.31	3401.164	1.9	3602.41	3602.278	17	4075.00	4074.897	0.015 (4)
3403.58	3403.427	2.2	3607.00	3606.853	0.4	4086.30	4086.15	0.01 (4)
3409.74	3409.579	12	3609.48	3609.312	19	4098.30		0.01 (4)
3413.66	3413.478	55 (1)	3610.61	3610.45	54	4116.11	4115.980	0.04
3414.12	3413.943	34 (1)	3612.90	3612.732	50	4121.48		0.015 (4)
3414.91	3414.771	93 (1)	3619.52	3619.391	124	4123.94	4123.79	0.01 (4)
3420.88	3420.742	1.0	3624.89	3624.733	14	4138.67	4138.52	0.01 (4)
3421.49	3421.339	2.3	3630.01	3629.891	14	4150.53	4150.37	0.03
3422.47	3422.334	0.7	3635.10	3634.943	3.0	4164.80	4164.636	0.02
3423.00	3422.870	1.3	3641.75	3641.632	0.3	4167.07	4166.96	0.02
3423.87	3423.713	69	3642.52	3642.383	0.2 (1)	4184.65	4184.473	0.07
3433.74	3433.565	66	3662.10	3661.938	1.7	4195.72	4195.533	0.1
3435.63	3435.495	0.5	3664.27	3664.089	13	4200.60	4200.466	0.15
3437.45	3437.283	53	3666.16		0.2 (4)	4201.89	4201.728	0.15
3442.17	3442.017	0.9	3668.36	3668.200	0.4 (1)			
3442.67	3442.540	0.4	3669.40	3669.233	6.6			

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Eight doublets and 4 quartets have been measured; the quotients of intensity sums and statistical weights are found in Table XIII.

TABLE XIII.

Multiplet Designation		Quotients							
1	$a^4D^1 - d^4F^1$	—	1.2	1.0	1.3	—	1.7	1.4	1.65
2	$a^2P^1 - b^2P$	5	4.95			5.8	4.55		
3	$a^2P^1 - b^2D^1$	0.5	0.05			0.07	0.5		
4	$a^4G^1 - d^4F^1$	1.6	2.0	2.35	2.9	1.9	1.7	2.0	1.8
5	$a^2G^1 - d^2F^1$	1.6	2.1			1.7	1.3		
6	$a^4F - d^4F^1$	2.85	1.9	1.5	1.15	1.85	1.4	1.7	1.7
7	$a^2F - d^2F^1$	1.6	1.0			1.3	1.2		
8	$a^2D^1 - d^2F^1$	0.87	0.85			1.3	1.1		
9	$a^2G - b^2F$	0.6	0.9			0.5	0.7		
10	$a^2D - a^2D^1$	2.8	1.1			2.6	1.3		
11	$a^2D - a^2F$	0.47	0.04			0.15	0.4		
12	$a^4P^1 - a^4D^1$	3.2	2.15			5.0	3.25	0.85	—

For some of the multiplets the disagreement with the summation rule is not very great, for others, however, the divergencies are wide, e.g. in the case of Nos. 3 and 11, where the diagonal terms are by far the weakest.

Adding up the doublet and quartet systems and the intercombinations, we get the quotients of Table XIV.

TABLE XIV.

Combinations	Quotients											
$a^4D^1, a^4D^1 - d^4F^1, d^2F$	—	1.5	1.65	1.3	0.9	0.85	—	1.7	1.4	1.65	1.7	2.0
$a^4G^1, a^2G^1 - d^4F^1, d^2F^1$	1.6	2.0	2.35	2.9	1.6	2.1	1.9	1.7	2.0	1.8	1.7	1.3
$a^4F, a^2F - d^4F^1, d^2F^1$	2.85	1.9	1.7	1.16	1.6	1.15	1.85	1.4	1.7	1.8	1.3	1.5

If we add the multiplets which in the quartet systems start from a^4D^1 , we find the quotients shown in Table XV.

TABLE XV.

Statistical weight	a^4D^1				a^4F^1				a^4G^1				Sum	Quotient
	1	2	3	4	2	3	4	5	3	4	5	6		
2					3.7	2.0			3.2				8.9	4.5
d^4F^1 3		3.4	0.3			2.3	3.5		2.5	3.5			15.5	5.2
4			4.0				3.3	2.6		3.3	6.1		19.3	4.8
5				6.6				5.8			3.8	10.7	26.9	5.4
Sum		3.4	4.3	6.6	3.7	4.3	6.8	8.4	5.7	6.8	9.9	10.7		
Quotient		1.7	1.4	1.7	1.9	1.4	1.7	1.7	1.9	1.7	2.0	1.8		

There is comparatively little difference between these quotients. If we add to them the small number of intercombinations that occur, we find $4.5|5.4|5.7|5.4|$.

In the same way we find:

TABLE XVI.

Q	a^2D^1			a^2F		a^2G^1		Sum	Quotient
	2	3	3	4	4	5			
d^2F^1 3	2.6							12.1	4.03
4		3.4		3.8	0.9	4.8		15.9	3.98
Q	1.3	1.1	1.3	1.2	1.7	1.3			

These results are satisfactory if the occurring intercombinations are added, the quotients become 4.03 and 4.12.

In our material these two multiplets are the only ones which start from the same level. The quartet $a^4P^1 - a^4D^1$ has the same original level as number of intercombinations. But we cannot conclude from these measurements, as there are other lines in the part of the spectrum that has not been examined which start from the same level. However, it is remarkable that the intensity ratios of this quartet are largely corrected by the additions of the intercombinations.

TABLE XVII.

	a^4P^1		a^2F^1		a^2D		Sum	Quotient
	1	2	3	4	2	3		
1	2.7	0.5			0.5		3.7	3.7
2	2.3	2.0		0.4	1.0	0.4	6.1	3.6
a^4D^1 3		4.0		0.9	1.1	3.9	11.2	3.7
4			2.6	2.7		7.2	12.5	3.1

In combining lines with a common final level we again meet with the difficulty that our materials are not complete; various lines that ought to be included do not occur in the spectral region that has been examined. Still the influence of the additions of the other intensities can be seen from Table XVIII.

TABLE XVIII.

	a^2D		a^2P^1		a^4P^1			
	2	3	1	2	1	2	3	
a^2F	0.3	1.25	b^2D^1	0.07	1.05	a^4D^1 5	6.5	2.6
a^2D^1	5.2	3.8	b^2P	5.8	9.1	a^2D^1	1.7	2.7
a^4D^1	2.8	11.5	b^4D^1	1.2		a^2F		1.2
a^4F	0.5	0.3	b^4P	1.0	2.8	a^4F	0.3	
Sum	8.8	16.85	a^2F		0.2	Sum	5	8.5
Quotient	4.4	5.6	b^2F		0.4	Quotient 5	4.3	2.2
			Sum	8.07	13.55			
			Quotient	8.1	6.8			

We have considered also the intensity ratio for doublet-quartet systems.

TABLE XIX.

Combinations	Ratio
$a^2D - d^2F^1$ and $a^4D^1 - d^4F^1$	1:1.6
$a^2G^1 - d^2F^1$ and $a^4G^1 - d^4F^1$	1:2.4
$a^2F - d^2F^1$ and $a^4F - d^4F^1$	1:2.4

The last column is found after division by ν^4 . The ratio 1:2 is found only approximately; this cannot be attributed to the occurring intercombination lines (3, 2 and 0 respectively) as in the last case where they do not occur, the divergency is the same as in the other two.

In the following intensity table (Table XX) an intensity of 100 has been awarded to line 2437.884.

TABLE XX. Intensities of the lines of Ni II. Intensities marked (1) are certain, (2) less certain, (3) doubtful, (4) inexact because of small intensity and irregularities in the plates.

λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
2416.21	2416.13	29	2834.66		0.7	3366.31		4.3 (1)
2419.40		0.8		2836.58	1.0	3366.92		1.7 (1)
2429.17		0.5 (4)	2842.55	2842.41	1.9	3369.71		20
2431.65	2431.57	1.2	2863.84	2863.69	5.2	3372.14		4.6
2433.64	2433.57	6.7	2864.4	2864.16	2.6	3374.13	3373.98	3.9 (3)
2437.98	2437.884	100	2865.63		0.6	3374.36		2.9 (3)
2441.77		1.0		2881.24	0.3	3374.77		1.6 (3)
2441.90		0.6		2882.54	0.8	3380.74		21.5 (2)
2451.05		0.8	2907.10		0.4	3381.04		6.5 (2)
2454.09		0.6	2913.71	2913.59	3.4	3391.20		11.4
2455.60	2455.51	1.8	2914.11		0.2 (3)	3393.16		23
	2459.32	0.3		2942.71	0.15 (4)	3396.25		0.5
2465.34		0.2	2944.03		4.8		3397.82	0.2 (4)
2472.27		1.0	2947.56	2947.45	1.7	3401.30		0.5
2473.28	2473.13	13.4	2969.32		0.6	3401.90	3401.76	0.5
2476.96		0.8	2981.81		5.7	3403.45		0.8
2484.41	2484.32	6.6	2984.30		2.8	3407.43	3407.30	2.7
2497.92	2497.80	1.0	2988.21	2988.05	1.2	3409.70		0.9
2503.47		0.8	2992.75		4.2	3413.61		5.0
2505.94	2505.84	7.3	2994.60		6.6	3414.05		2.5
2511.00	2510.87	98	3002.65		19	3414.91		34
2514.85	2514.75	3.4	3003.76		15	3421.47		0.6
	2520.33	0.15	3012.14		19	3423.88		14
	2525.42	4.0	3019.27		3.7	3433.70		17
2539.20	2539.09	2.6	3032.00		1.3	3437.42		14
2540.14		2.0		3032.44	0.3	3446.41		22.5
2546.01	2545.90	21	3038.09		13	3453.06		12.5
	2547.16	0.5 (4)	3045.16		1.2	3454.29	3454.16	1.3
	2549.56	1.8	3050.99		21	3458.62		28
	2551.04	1.1	3054.46		12	3461.84		23
	2555.13	3.5	3057.79		16	3465.77	3465.62	2.0
2557.98	2557.88	0.9	3064.12	3063.93	0.5	3467.63		1.1
	2560.30	3.2	3064.76		5.0	3469.61		2.0
	2565.36	0.6 (4)	3080.90		3.5	3471.50	3471.35	2.3
2566.12	2566.08	6.1	3087.20	3087.07	2.7	3472.71		13.4
2584.10	2584.01	3.2	3097.26		2.0	3483.95		7.2
	2587.25	0.4	3099.26		1.5	3486.05		0.6
2588.40	2588.31	0.4	3101.70		21 (3)	3493.13		25.5
	2592.54	0.07	3102.02		12 (3)	3501.04		5.6
2601.22	2601.126	3.8	3105.60		1.7	3502.74		0.3 (4)
	2605.45	2.5	3114.25		2.2	3507.84		0.5
2606.50	2606.40	4.8	3129.40		0.2	3510.52		15
2610.20	2610.08	10.7	3134.21		16	3511.8	3513.95	0.3 (4)
2611.78	2611.66	1.6	3197.24		1.4	3514.13		7.2
2615.29	2615.20	6.6	3214.21		1.2	3515.21		30
2623.25	2623.10	0.3 (4)	3216.95		1.0	3516.32		0.8
	2626.57	3.3	3217.95		2.0	3518.76		0.5
2630.40	2630.29	2.7	3221.43		1.0	3519.90		3.4
	2631.52	2.0	3221.80		2.2	3524.69		33
2632.98	2632.86	3.5	3225.18		3.0	3528.10		0.7
2647.15	2647.04	2.6	3227.14		1.0	3548.32		2.4
2648.85	2648.72	0.9	3233.05		9.8	3551.70		0.4 (4)
2655.6	2655.46	0.9 (2)	3234.76		2.5	3553.65		0.4 (4)
2656.05	2655.90	3.7 (1)	3243.20		6.0	3561.92		0.5
2659.8		2.5	3248.57		1.1	3566.55		23
2665.39	2665.25	2.0	3249.55		0.8	3572.06		7.5
2666.00	2665.86	0.8	3250.90		1.7	3576.91	3576.76	4.0
2670.45	2670.33	1.0	3271.26		0.8	3588.07		0.5
2679.35	2679.25	2.3	3275.03	3274.90	0.4	3597.86		7.7
2684.57	2684.41	5.8	3282.85		0.8	3602.44		0.9
2690.8	2690.62	1.9	3282.97		0.3 (3)	3609.49		1.5
2708.9	2708.78	3.3	3287.06		0.5	3610.68		8.1
2743.1	2743.01	4.0	3290.70	3290.54	0.3 (2)	3612.91		3.9
2746.85		1.4	3290.83	3290.69	0.5 (2)	3619.54		25
2759.15	2759.02	3.8	3305.10		0.3 (4)	3624.89		0.9
2760.82	2760.67	1.1	3312.46		1.0	3664.26		1.1
2768.9	2768.78	3.4	3313.12		0.6	3670.59		1.0
2775.45	2775.31	2.6	3315.80		7.0	3674.29		1.2
2794.93		0.7 (4)	3320.41		4.4	3688.57		0.5
2798.75		1.8	3322.46		3.1	3722.62		0.5
2802.4		0.2 (4)	3326.85		0.2 (4)	3736.96		0.8
2805.20		0.2 (4)	3350.56	3350.42	1.0	3739.38		0.4 (4)
2805.80	2805.67	3.6	3359.24		0.4	3769.62	3769.45	2.6
2808.47	2808.35	0.4	3361.73		5.0	3775.74		3.1
2821.45		2.3	3362.94		0.2 (4)	3783.67		3.6
	2825.23	1.1	3365.90		4.0 (1)	3807.29		5.1
						3858.50		9.7

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In Table XXI the computed quotients are given for all the multiplets measured. The indication of the multiplets is that of Catalan and Bechert. The quotients with question marks between brackets are too large, owing to lines which are ordered doubly in the multiplets to which they refer. In quartet No. 30 one of the lines in the multiplet itself has been ordered doubly; 4 quotients had therefore to be left out.

TABLE XXI

No.	Level	Quotients													
4	F^1-D^1	40	46							29	34				
5	F^1-D^2	108	56							73	42				
6	F^1-F^1	35	34							26	41				
7	F^1-f^2	75	67							102	47				
8	F^1-G^1	72	61							77	90				
9	F^1-G^2	98	47							95	85				
15	f^2-d^3	6.1	6.5	7.5	8.0					10.3	8.3	15.5			
19	f^1-d^1	99	80	78	41					89	83	41	13		
20	f^1-d^2	16	16	15	10					10	12	11	6		
21	f^1-d^3	20	20	16	11					23	15	8	4.4		
22	f^2-d^1	35	76	71	52					29	54	51	38		
23	f^2-d^2	155	115	83	51					135	78	62	18		
24	f^2-d^3	4.4	4.8	7.4	7.6					5.7	5.9	6.4	2.4		
25	f^1-f^1	89	72	[82]	30					75	70	60	[55]		
26	f^1-f^2	59	30	22	17					38	36	29	17		
28	f^2-f^1	[2.3]	2.4	3	7.7					1.0	[2.1]	3.5	8		
29	f^2-f^2	132	118	[98]	49					157	[127]	79	49		
30	f^2-f^3	11	—	11.5	—					21	—	12	—		
31	f^1-g^1	33	23	18	15					50	28	25	18		
32	f^1-g^2	38	30	10	7					25	30	29	14		
34	f^2-g^1	4.4	7.5	9.6	6.5					0.5	3.8	8.7	17.6		
35	f^2-g^2	142	89	61	26					88	97	93	80		
36	f^2-g^3	2.2	5.5	2.8	3.8					3.0	3.9	6.2	4.6		
81	$\phi^1-\phi^1$	1.6	2.6	2.6	3.3	4.4	1.1			2.2	2.2	3.0	3.4	5.3	
82	$\phi^1-\phi^1$	2.9	3.0	3.8	2.8	2.3	12			4.3	4.6	3.7	1.5	7.5	8.2

None of the 25 multiplets follows the summation rule. Neither are equal quotients obtained when doublet and quartet systems are taken together with their intercombinations. For a few of these systems the results are found in Table XXII.

TABLE XXII.

Terms	Quotients											
f^1, F^1 and g^2G^2	101	57	39	44	59	7	25	32	34	22	112	148
f^1, F^1 and g^1G^1	73	66	33	23	19	15	50	28	31	18	77	91
f^1, F^1 and f^2-F^2	78	73	65	33	53	46	38	38	34	17	150	83
f^1, F^1 and d^2-D^2	109	58	16	16	16	19	10	14	12	6	74	51

If we take together the lines which originate from the same level we find the quotients of Table XXIII.

TABLE XXIII.

Term	Quotient			
g^1	38	31	28	21
G^1	110	84		
g^2	181	133	120	33
G^2	138	84		

Although for the level mentioned here the system is complete, the results are not appreciably better than for the separate multiplets; sometimes (for G^1) even worse.

For the other terms the system is incomplete; of these only for d^3 a considerable improvement is found. Here we combine f^1-d^3 , f^2-d^3 , F^1-d^3 and p^2-d^3 and find the quotients 31, 32, 32 and 28. However, p^1-d^3 , p^2-d^3 and P^1-d^3 could not be taken into account as they did not occur in spectral region we investigated.

TABLE XXIV.

Final level	Quotients			
f^1	315	293	235	144
f^2	431	488	413	264
F^1	467	450		

Finally we can add all the lines with a common final level. In each of these 3 cases a few systems of lines are wanting (2, 2 and 3 respectively), but it is highly improbable that the quotients given, which have been derived from 16, 16 and 13 lines respectively, would be greatly influenced by these.

For the ratio of intensities of doublet and quartet systems the following values (after division by ν^4) are tabulated here:

TABLE XXV.

Multiplet	Ratio
F^1-D^1 and f^1-d^1	1:2
F^1-D^2 and f^1-d^2	1:0.22
$F^1-\bar{F}^1$ and $f^1-\bar{f}^1$	1:2.1
$F^1-\bar{F}^2$ and $f^1-\bar{f}^2$	1:0.4
F^1-G^1 and f^1-g^1	1:0.3
F^1-G^2 and f^1-g^2	1:0.22

In 4 of the 6 cases the doublet is even stronger than the quartet. This cannot be ascribed to the existing intercombinations as the divergencies in the case of the systems F^1-D^2 and F^1-G^1 , where the intercombinations are weak, is much the same as in that of F^1-F^2 and F^1-G^2 with their strong intercombinations. Whereas the division by ν^4 yields a fairly correct ratio in 2 cases, it increases the error in the other 4 cases.

All the intensity values found are shown in Table XXVI in which an intensity of 100 has been awarded to the line 3334.151.

TABLE XXVI. *Intensities of the lines of Co I.* Intensities marked (1) are certain, (2) less certain, (3) doubtful, (4) inexact because of small intensity and irregularities in the plates.

λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
2441.15		9.4	2451.84		1.2	2464.30		2.8
2443.00		2.7	2453.50		2.0	2464.58		2.8 (2)
2443.63	2443.55	5.1	2456.31		12	2464.71		4.5(2)
2443.89		2.2	2460.28		2.2	2467.80	2467.71	11
2446.60		0.9	2460.90	2460.81	11	2470.38		16
2449.24		1.4	2462.22		3.8	2473.02		10
2450.10		2.4	2463.85		6.0	2474.01	2473.92	8.7

TABLE XXVI (continued)

λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
2476.73	2476.64	17	2650.04	2650.271	11	2929.62		5.1
2483.70		15	2650.40		11		2936.551	0.5 (1)
2485.44		0.9	2653.84		0.5 (4)		2942.630	0.5
2486.53		3.4	2661.80		1.0	2943.60		1.9
2488.55		3.0	2663.61		0.6	2955.50		1.6
2489.36		3.3	2669.65		1.0	2957.79		3.1 (2)
2494.05		5.2	2674.04		1.3	2969.70		0.7
2494.83		9.5	2676.06	2675.987	10	2975.56		0.6
2495.65	2495.56	13	2679.83		12	2977.56		0.5
2496.80		17	2680.20		2.6	2978.10		1.5
2500.60	2500.51	3.2	2685.44	2685.340	17	2982.37		1.0
2504.63		17	2694.50		2.1	2984.24		0.3 (4)
2505.2		1.4	2694.76		2.2	2987.28	2987.172	33
2506.55		7.7	2695.93	2695.853	20	2989.70	2989.599	36
2507.26		1.0	2705.50		1.5	2996.67		1.0
2511.12	2511.03	18	2705.94		3.7	2999.84		1.0 (2)
2513.01		9.3	2708.88		1.4	3000.66	3000.554	2.7
2513.20		6.4	2716.05		13	3005.86		3.2 (1)
2517.90	2517.81	23	2719.65		1.1	3006.10		0.8 (1)
2519.90		5.4	2722.20		1.4	3013.70	3013.598	24
2521.03		1.1	2728.86		1.0	3015.77		3.8
2521.49	2521.40	22	2731.20		5.7	3017.33		1.0 (3)
2525.09		6.5	2740.54		7.2	3017.66	3017.552	31
2528.67		11	2745.17		8.0	3019.23		0.7
2529.06	2528.97	23	2746.10		1.3	3022.47		3.2
2530.22	2530.13	21	2750.20		3.5	3023.66		0.5
2530.65		6.8	2752.21		1.7	3026.49		10.7
2531.45		4.0	2758.67		1.0	3028.31		0.6
2532.26		21	2761.49	2761.375	9.6	3031.43		2.4
2535.45		5.6	2763.19		1.0	3034.55	3034.426	15
2536.02	2535.93	21	2764.30	2764.193	12	3038.42	3038.304	2.1
2536.55		19	2766.31		1.0 (1)	3039.66		3.3
2538.45		2.7	2766.47	2766.37	4.2 (1)	3040.93		14
2542.05		5.2	2768.80		1.2	3042.60	3042.482	30
2544.34	2544.25	20	2772.80		1.6	3044.11	3044.007	50
2544.94		12	2775.06	2774.964	4.4	3045.13		0.7
2548.40		20	2775.29		0.7 (1)	3048.21		2.0 (2)
2549.37		14	2775.67		1.5	3049.00	3048.892	46
2553.09	2553.00	16	2778.92		8.7	3050.64		3.6 (2)
2553.44	2553.35	18	2786.00		2.2	3054.84	3054.724	4.4
2555.15	2555.06	17	2790.40		0.7	3060.17		7.9
2556.85		12	2791.13		1.7	3061.15		1.5 (1)
2559.48		4.6	2791.57		0.6	3061.94	3061.825	49
2561.37		2.0	2792.55		2.2	3062.33	3062.198	8.8 (1)
2562.22	2562.13	19	2796.33	2796.236	5.4	3064.49	3064.375	16
2564.14		8.3	2797.18		4.0	3070.94		1.3 (1)
2567.42	2567.33	20	2803.87	2803.775	11	3072.06	3071.954	9.4 (2)
2572.32		8.8	2804.25		1.0 (2)	3072.45	3072.346	56
2574.45	2574.36	18	2811.23		1.5	3073.64		3.3
2574.94		1.2	2811.64		2.6	3079.49	3079.390	4.9
2575.82		4.2	2815.06	2814.979	1.1	3082.73	3082.614	42
2578.99		2.5	2815.65	2815.557	16	3086.46		9.0 (2)
2580.43		20	2818.69	2818.596	2.2	3086.89	3086.778	71
2580.95		16	2820.11	2820.003	3.6	3087.86		2.1
2582.35		7.8	2821.86		1.6	3088.76	3088.676	0.9
2585.45	2585.36	11	2823.78		1.2	3089.68	3089.593	38
2587.30		9.0	2825.29		2.5	3090.36		3.0
2590.70		11	2826.91		1.9	3095.81		2.7
2591.78		12	2828.55		0.8	3096.50		2.9 (1)
2594.26	2594.176	6.6	2834.02	2833.928	1.9	3096.80		1.8 (1)
2595.31		1.9	2834.55	2834.425	1.7	3098.30	3098.195	35
	2596.000	0.6	2837.26		4.7	3099.76		2.1
2601.07	2600.991	4.9	2842.46		1.8	3102.49		4.0
2606.22		9.0	2850.15		4.3	3103.82		7.2 (1)
2610.86	2610.770	4.7	2851.05	2850.956	1.1	3104.12	3103.990	4.0 (1)
2613.60		1.4	2859.75	2859.660	2.4	3106.03	3105.920	1.4 (2)
2613.98		10	2861.48		0.5	3106.22	3106.136	1.5 (2)
2614.23	2614.132	5.4	2862.70	2862.610	7.0	3107.15		2.5
2614.45		0.9 (2)	2867.57		0.4	3107.65		1.3
2615.45		2.4	2872.60		3.7	3109.60		3.3
2616.34		4.1	2878.65		1.4	3110.12		3.0
2617.95		6.7	2879.71		3.1	3110.94	3110.817	3.3
2619.36		5.0	2882.34	2882.221	1.8	3111.45		1.4
2622.15	2622.064	14 (1)	2886.55	2886.448	20	3113.58		7.3
2622.35	2622.252	5.9 (1)	2892.37		1.8	3118.35	3118.240	4.8
2622.54	2622.434	11	2895.46		0.7 (3)	3118.76	3118.630	0.4 (1)
2623.54	2623.450	11	2895.57		1.6 (3)	3121.54	3121.414	30 (3)
2623.85		4.0	2899.91	2899.801	3.3	3121.69	3121.560	36 (3)
2627.13		3.5	2903.30		1.9	3126.85		3.4
2627.71	2627.641	23	2904.40		0.6	3127.35	3127.244	4.6
2630.05		2.3	2907.75		0.5	3129.10	3128.997	1.5
2640.33		1.5	2911.70	2911.560	0.7	3129.57		2.3
2642.97		2.1	2919.66	2919.041	0.2 (4)	3132.33	3132.212	2.4
2644.89		4.9	2927.78		1.3	3136.81	3136.721	2.2
2646.51	2646.420	24	2927.78		5.0	3137.47	3137.325	49
2648.79	2648.648	51	2928.91	2928.819	4.4	3140.08	3139.943	42

TABLE XXVI (continued)

λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
3140.83		1.4	3342.10		3.2	3495.83	3495.685	176
	3143.812	0.6	3342.88		11	3496.80	3496.682	38 (2)
3145.16		1.8	3344.36		1.0 (4)	3496.90		38 (2)
3147.19	3147.060	56	3347.10		7.1	3502.45	3502.281	89 (2)
3149.43	3149.304	28	3348.28		11	3502.80	3502.620	159 (2)
3150.82		5.3 (2)	3351.70		1.6	3503.85		2.4 (3)
3150.93		6.3 (2)	3354.51	3354.386	92	3504.89		2.4 (3)
3152.84		6.8	3355.27		2.3	3506.47	3506.315	138
3154.91		42	3356.59		3.8	3510.00	3509.844	122 (1)
3157.23		1.3	3356.97		1.3	3510.59	3510.419	92 (1)
3158.92	3158.769	48	3358.13		0.7 (4)	3512.80	3512.643	128
3159.80	3159.660	16	3359.42		5.6	3513.61	3513.483	89
3161.78		4.6	3361.72		6.0	3518.50	3518.353	215
3164.66		0.3	3362.93		6.7	3520.23	3520.087	78
3168.19		4.5	3363.41		3.1	3521.73	3521.572	186
3169.90		10	3363.89		2.2	3523.55	3523.438	155
3173.30		0.6	3364.38		3.0	3526.97	3526.856	99
3174.29		1.3	3365.13		1.2	3529.19	3529.037	83
3175.06		3.2	3367.25	3367.114	94	3529.92	3529.815	151
3177.40		7.0	3368.72		1.2	3533.51	3533.363	100
3179.98		0.5	3370.48	3370.330	15	3534.91		12
3180.42		1.7	3373.40		5.9	3543.43		27
3182.25		6.6	3374.42		4.4	3546.85		2.6
3186.05		0.8	3376.34		1.5	3548.60		5.8
3186.46	3186.346	6.4	3377.20		4.7	3550.78	3550.599	64
3188.50		8.8	3378.86		5.4	3552.90	3552.719	3.0 (2)
3189.87	3189.756	3.6	3381.65		2.2	3553.16		15 (1)
3191.44	3191.300	1.8	3383.07		16	3553.31		3.0 (3)
3193.30	3193.162	3.2	3384.09		2.2	3558.93	3558.780	15
3198.79	3198.664	2.3	3385.38	3385.227	81	3561.03	3560.896	103
3199.44	3199.325	1.4	3388.29	3388.175	95	3562.25		5.0
320.15	3203.030	2.0	3390.54		2.5 (2)	3563.09		5.3
3210.35		3.4	3390.92		3.8 (2)	3565.09	3564.955	103
3210.96		1.6	3395.55	3395.378	135	3569.59	3569.382	185
3219.31	3219.155	12	3398.96		1.4	3575.13	3574.964	99 (2)
3224.80		2.0	3402.14		3.9	3575.53	3575.361	114 (2)
3227.15		1.8	3403.33		0.6 (4)	3578.21		4.5
3235.69		9.2	3405.27	3405.120	144	3579.04		4.5 (3)
3237.18	3237.028	24	3407.02		1.0 (4)	3579.15		3.6 (3)
3239.08		1.1 (4)	3409.29	3409.176	124	3582.02		1.7
3243.99		22	3412.50	3412.335	128	3584.94	3584.796	7.2 (3)
3250.17	3249.994	10	3412.79	3412.636	64 (1)	3585.33	3585.159	109
3254.37		20	3415.66	3415.527	3.0 (1)	3587.30	3587.188	223
3258.16		2.3	3417.32	3417.158	118	3595.03	3594.869	101
3260.99		13	3417.84		8.0 (3)	3596.67		2.4
3263.35		2.4	3417.93	3417.796	8.0 (3)	3602.22	3602.081	114
3264.96	3264.842	7.4	3420.64		1.9 (3)	3605.52	3605.367	74
3271.92		9.8	3420.95		4.7 (3)	3611.89		14
3276.60		2.8	3421.77		1.4	3615.54		4.3
3277.44		2.3 (2)	3423.03		3.1	3618.15	3618.006	2.5
3277.80		2.3 (2)	3424.67		11	3620.56		2.7
3278.96		5.1	3426.60		1.3	3624.54		2.6 (1)
3279.39		4.2	3428.34		5.2	3625.18	3624.955	11 (1)
3280.74		18	3428.89		1.8	3627.98	3627.807	90
3283.60		38	3431.76	3431.579	71	3631.59	3631.340	50
3287.34		7.7	3433.18	3433.043	170	3633.01		7.4
3292.24		1.3 (4)	3437.10		1.4	3634.86		7.0
3298.83		4.6	3437.83		5.8	3637.44		1.7
3304.03		0.8 (3)	3439.05		5.8	3636.84		4.7
3304.29		1.7 (1)	3443.06	3442.924	84 (1)	3639.60		17
3305.27		1.0 (4)	3443.79	3443.646	140 (1)	3641.94		7.0
3305.87		1.0 (4)	3449.26	3449.171	170 (3)	3643.35		14
3306.54		0.8 (4)	3449.54	3449.443	153 (3)	3645.34		3.6
3307.31		7.9	3452.44		3.8	3647.85	3647.663	37
3308.65		3.0	3453.66	3453.513	155	3649.49		7.8
3308.96		4.7	3455.33	3455.236	99	3651.41		2.3
3312.33		10	3457.05	3456.936	9.3	3652.70	3652.544	45
3312.99		1.6	3460.86	3460.732	2.4	3654.59		4.0
3314.21		9.9	3461.33		15	3657.10	3656.965	7.5
3315.20		1.1 (4)	3462.94	3462.807	144	3658.06		1.0 (4)
3318.55		1.8	3465.96	3465.796	87	3662.32		22
3319.31		2.2 (1)	3469.11		1.5	3670.20		1.0 (4)
3319.66		14 (1)	3471.53		4.7	3676.72		17
3320.00		4.9 (1)	3472.85		2.0	3683.22		41
3322.41		15	3474.17	3474.019	169	3684.63		5.2
3325.44		15	3476.50		2.1	3690.91		4.1
3327.14		14	3478.00		1.8	3693.63		15 (3)
3328.34		1.1	3478.60		8.7 (3)	3702.39		16
3329.16		0.8 (4)	3478.90		5.2 (3)	3704.22	3704.061	83
3329.63		4.3	3480.17		3.5	3707.61		3.9
3333.55	3333.390	13	3483.58	3483.415	99	3709.00		21
3334.31	3334.151	100	3485.51		21	3712.35		2.9
3337.34	3337.175	6.4	3487.84		4.8	3726.79		1.2
3338.68		0.6 (4)	3489.57	3489.406	166	3730.63		27
3339.97		9.0	3490.89	3490.741	20	3732.59		55
3341.52		5.0	3491.49	3491.324	76	3733.65		22

TABLE XXVI (continued)

λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.	λ (Kayser)	λ (I.A.)	Int.
3736.08		12	3972.69		3.5 (2)	4270.60	4270.423	1.0
3740.34		2.1	3973.31	3973.148	13	4285.95	4285.787	2.8
3745.65	3745.501	107	3974.90	3974.732	17	4292.42		0.7
3750.07		14 (1)	3978.78	3978.656	11 (3)	4303.41	4303.236	1.3
3751.75		3.3	3978.99		7.1 (3)	4309.61	4309.418	0.4
3754.47		1.5	3979.67	3979.525	20 (1)	4331.43		1.2
3755.60		9.3	3987.25	3987.121	4.1	4339.81		2.8
3759.83		1.0 (3)	3990.45	3990.307	5.9	4371.31		1.4
3760.55		1.3 (3)	3991.68		7.7 (2)	4373.81		1.4 (1)
3774.75		2.9	3991.83	3991.693	7.0 (2)	4375.11	4374.940	1.4 (1)
3777.68		2.6	3994.70	3994.541	1.0 (3)	4391.70	4391.59	1.2 (1)
3783.87		0.6 (4)	3995.45	3995.312	244	4392.02		1.0 (1)
3808.25	3808.106	7.2	3998.09	3997.909	125	4402.86		1.0
3808.25		7.2	3998.69	3998.554	1.0 (3)	4417.55	4417.425	1.5
3811.23	3811.070	0.9	4003.85		0.5	4421.54	4421.359	1.3
3812.62		3.1	4011.10	4011.098	1.1	4431.79		0.8
3816.48		17 (2)	4014.09	4013.950	4.8	4445.88	4445.730	1.4
3816.61		13 (2)	4019.45	4019.300	2.7	4467.09	4466.888	4.7
3842.21	3842.056	137	4021.07	4020.904	38	4469.75	4469.569	10
3845.60	3845.474	235	4023.55		2.1	4471.76	4471.578	4.0
3850.27		1.2 (2)	4027.18	4027.044	11	4478.50	4478.345	1.6
3851.09	3850.949	7.7	4035.74		5.9	4484.11	4483.946	1.5 (2)
3852.00		2.4 (2)	4040.57		0.7 (3)	4494.94		0.6
3856.94		4.8	4040.95		0.5 (3)	4517.26	4517.121	2.8
3861.31	3861.168	80	4045.56	4045.397	51	4528.08	4527.936	0.8 (2)
3863.75		1.0	4049.43		0.6 (4)	4531.12	4530.985	48
3870.66		2.5	4053.10		1.3	4534.16	4533.998	6.1
3873.23	3873.117	188 (1)	4057.10		2.0 (1)	4543.98	4543.836	5.5
3874.09	3873.957	185 (1)	4057.36	4057.199	4.5 (1)	4549.83		11
3877.01	3876.840	37	4058.36	4058.188	9.6 (1)	4565.79		17
3882.06	3881.877	133	4058.76	4058.603	5.5 (1)	4570.21		1.4
3884.79	3884.609	11 (1)	4063.34	4063.19	2.0	4580.34	4580.133	2.6 (2)
3885.45	3885.281	5.0 (2)	4066.56	4066.378	36	4581.80	4581.618	25
3894.25	3894.086	285	4068.72	4068.553	9.4	4594.82		3.2
3895.15	3894.981	35 (1)	4076.30	4076.134	3.1	4597.09		3.0
3898.54	3898.499	1.6	4077.56		1.4	4623.20	4623.024	1.1
3904.23		1.9	4082.75	4082.606	2.0	4625.92		1.0
3906.46	3906.296	16	4086.49	4086.307	32	4629.52	4629.380	19
3910.13	3909.941	26	4092.56	4092.397	135	4657.56	4657.399	0.2
3917.80		8.6	4104.57	4104.430	0.8 (2)	4663.59	4663.411	11
3920.90		5.3	4104.91		1.8 (2)	4682.53	4682.363	6.6
3922.90	3922.764	8.1	4110.70	4110.544	77	4693.36	4693.193	2.8
3925.33		0.9	4118.96	4118.784	232	4698.56	4698.370	1.4
3929.43		1.1	4121.52	4121.329	306	4704.57		0.7
3934.07	3933.921	4.5	4132.30	4130.538	0.4 (4)	4728.14	4727.924	2.2
3934.85		1.1	4132.15		3.0	4735.04	4734.834	0.8
3936.13	3935.974	146	4150.62	4150.442	0.5 (4)	4737.95	4737.776	1.1
3939.00		0.8	4158.59		0.8	4749.89	4749.684	6.8
3941.06	3940.895	20	4162.38		1.3	4754.59	4754.372	1.3
3941.91	3941.735	39 (1)	4179.44		0.5	4756.93		0.8
3945.51	3945.323	27	4187.46	4187.248	1.5	4767.33		0.8 (2)
3946.75		1.0 (2)	4190.88	4190.709	15	4768.26	4768.096	1.2 (2)
3947.26	3947.132	1.3 (2)	4193.02		0.8 (4)	4771.27	4771.105	2.8
3952.46	3952.329	2.1 (3)	4198.56	4198.424	0.7 (4)	4776.49	4776.328	3.1
3953.10	3952.923	55	4234.17	4233.996	1.8	4780.14	4780.001	5.7
3956.42	3956.276	0.8	4242.07		1.0	4793.03	4792.867	8.5
3958.10	3957.935	26	4245.75		0.2 (4)	4813.67	4813.482	12
3961.15		3.3	4248.35		0.2 (4)	4840.42	4840.267	14
3969.28		11	4252.46	4252.303	6.9	4858.05	4867.690	18