

## Elasticity Effects in Type-II Superconductors

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A phenomenological theory of strain and stress effects in Ginzburg-Landau superconductors is given. The theory provides formulas for the elastic constants and the specific volume in the mixed state, and it is shown how to obtain a complete set of appropriate phenomenological parameters. We also obtain correct expressions for the interaction energy between fluxoids and localized strain fields which are only partly in agreement with the expressions used by previous authors.

## INTRODUCTION

BY application of thermodynamic principles, the changes in elastic constants and specific volume of type-I superconductors at the transition to the normal state have been related to the stress or strain dependence of the critical magnetic field.<sup>1</sup> Similar relations for the transition at the upper critical field  $H_{c2}$  and for the zero-field superconducting state below  $H_{c1}$  of type-II superconductors were derived by Hake.<sup>2</sup> In order to obtain a more detailed description of the mixed state between  $H_{c1}$  and  $H_{c2}$ , we derive in this paper a set of modified Ginzburg-Landau equations with strain-dependent parameters. Solving these equations by means of a perturbation calculation we obtain expressions for the elastic constants and the specific volume in the mixed state. These results provide formulas for determination of the strain dependence of the Ginzburg-Landau parameter and the thermodynamic critical field from measurements of elastic constants.

A perturbation calculation of the free energy gives us correct expressions for the interaction energy between fluxoids and slowly varying strain fields. These expressions provide the correct starting point for calculation of the pinning of fluxoids by the localized strain fields of dislocations and coherent precipitates. The basis for the existing first- and second-order calculations by Kramer and Bauer,<sup>3</sup> by Webb,<sup>4</sup> and by Toth and Pratt<sup>5</sup> is confirmed but additional terms are found. For the second-order calculation the additional term is negligible in the one material for which experimental information on its coefficient exists.

## DERIVATION OF THE MODIFIED GINZBURG-LANDAU EQUATIONS

We choose for convenience  $H_{c2}$  the upper critical field and  $\kappa^2$  the square of the Ginzburg-Landau parameter as independent material parameters. Their strain dependence is characterized by the following phenomenological coefficients, which correspond to the first and second derivatives of  $H_{c2}$  and  $\kappa^2$  with respect to

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<sup>1</sup> D. P. Seraphim and P. M. Marcus, IBM J. Res. Develop. **6**, 94 (1962).

<sup>2</sup> R. R. Hake, in Proceedings of the Conference on the Physics of Type-II Superconductivity, Cleveland, Ohio, 1964, Vol. 1, p. 15 (unpublished).

<sup>3</sup> E. F. Kramer and C. L. Bauer, Phil. Mag. **15**, 1189 (1967).

<sup>4</sup> W. W. Webb, Phys. Rev. Letters **11**, 191 (1963).

<sup>5</sup> L. E. Toth and J. P. Pratt, Appl. Phys. Letters **4**, 75 (1964).

the strain  $\epsilon_{ij}$ :

$$\begin{aligned} a_{ij} &= \partial H_{c2} / H_{c2} \partial \epsilon_{ij}, \\ a_{ijkl} &= \partial^2 H_{c2} / H_{c2} \partial \epsilon_{ij} \partial \epsilon_{kl}, \\ b_{ij} &= \partial(\kappa^2) / \kappa^2 \partial \epsilon_{ij}, \\ b_{ijkl} &= \partial^2(\kappa^2) / \kappa^2 \partial \epsilon_{ij} \partial \epsilon_{kl}. \end{aligned} \quad (1)$$

These parameters are second- and fourth-rank tensors, respectively, and their symmetry properties are determined by the crystal symmetry of the superconductor. In the case of cubic symmetry, which is of most practical interest, we have  $a_{ij} = a \delta_{ij}$ ,  $b_{ij} = b \delta_{ij}$  and the  $a_{ijkl}$ 's and  $b_{ijkl}$ 's are reduced to two sets of three independent components each.  $\delta_{ij}$  is the Kronecker delta. For a more detailed discussion of the symmetry properties, see Refs. 1 and 6.

Taking into account all terms up to the second order in  $\epsilon_{ij}$  we obtain for the free energy of the superconductor<sup>7</sup>

$$\begin{aligned} G = \frac{H_c^2}{4\pi} \int \left\{ (H - H_a)^2 + \psi^* \left( \frac{i\nabla}{\kappa} + \mathbf{A} \right)^2 \psi \right. \\ \left. - (1 + a_{ij}\epsilon_{ij} + \frac{1}{2}a_{ijkl}\epsilon_{ij}\epsilon_{kl}) |\psi|^2 \right. \\ \left. + \frac{1}{2}(1 + b_{ij}\epsilon_{ij} + \frac{1}{2}b_{ijkl}\epsilon_{ij}\epsilon_{kl}) |\psi|^4 \right\} d^3r \\ + \int \left( \frac{1}{2}C_{ijkl}n^i\epsilon_{ij}\epsilon_{kl} + u_i K_i \right) ds^3 + \oint C_{ij\ell} u_i dr^2. \end{aligned} \quad (2)$$

<sup>6</sup> See for example C. S. Smith, Solid State Phys. **6**, 215 (1958). This equation becomes obvious if one goes back to an expansion of the free energy  $G_{s0}(n, \epsilon)$  in zero magnetic field in powers of  $n$  and  $\epsilon$  at  $n=0$ ,  $\epsilon=0$ , where  $n$  is the super electron density. The terms of first and second order in  $n$  and  $\epsilon$  are

$$\begin{aligned} \frac{\partial G}{\partial n} n + \frac{1}{2} \frac{\partial^2 G}{\partial n^2} n^2 + \frac{\partial G}{\partial \epsilon_{ij}} \epsilon_{ij} + \frac{1}{2} \frac{\partial^2 G}{\partial \epsilon_{ij} \partial \epsilon_{kl}} \epsilon_{ij} \epsilon_{kl} \\ + \frac{\partial^2 G}{\partial n \partial \epsilon_{ij}} \epsilon_{ij} n + \frac{1}{2} \frac{\partial^2 G}{\partial \epsilon_{ij} \partial n^2} \epsilon_{ij} n^2 + \frac{1}{2} \frac{\partial^2 G}{\partial \epsilon_{ij} \partial \epsilon_{kl} \partial n} \epsilon_{ij} \epsilon_{kl} n \\ + \frac{1}{4} \frac{\partial^4 G}{\partial \epsilon_{ij} \partial \epsilon_{kl} \partial n^2} \epsilon_{ij} \epsilon_{kl} n^2. \end{aligned}$$

Since we expand at  $n=0$ , we have  $\partial G / \partial \epsilon_{ij} = 0$  if the system in the normal state is in equilibrium with respect to  $\epsilon_{ij}$ . For the same reason  $\partial^2 G / \partial \epsilon_{ij} \partial \epsilon_{kl}$  is identical with the elasticity tensor in the normal state. The connection to Eq. (2) is made by adding the field-dependent typical Ginzburg-Landau terms and by introducing

$$\begin{aligned} n &= - \frac{\partial G / \partial n}{\partial^2 G / \partial n^2} |\psi|^2, & \frac{H_c^2}{4\pi} &= \frac{(\partial G / \partial n)^2}{(\partial^2 G / \partial n^2)^2}, \\ \lambda^2 &= - \frac{\partial^2 G / \partial n^2}{\partial G / \partial n} \frac{mc^2}{4\pi e^2}, & \kappa^2 &= \frac{mc^2}{4\pi \hbar^2 e^*} \frac{\partial^2 G}{\partial n^2}, \end{aligned}$$

and

$$H_{c2} = +\sqrt{2} \kappa H_c = - \frac{mc}{\hbar e^*} \frac{\partial G}{\partial n}.$$

Equations (1) are self-evident from the definitions of  $\kappa$  and  $H_{c2}$ .

The first integral in Eq. (2) is the Ginzburg-Landau expression for the free energy in Abrikosov's units,<sup>8</sup> with strain effects explicitly included.  $\epsilon_{ij}$  is defined to be zero in the unconstrained crystal in the normal state. The material parameters  $\kappa$  and  $H_c^2 = H_{c2}^2/2\kappa^2$  are the values at zero strain. Although the correct measurement of these parameters should be done at constant volume and not as it is usually done in experiments at constant pressure, in fact the difference is very small so that it can always be neglected and the usual values may be taken. The second integral in Eq. (2) contains the elastic energy and the work that is done by volume forces  $K_i$  and the third integral, extending over the surface of the superconductor, gives the work done by the applied surface stresses  $\sigma_{ij}$ .  $C_{ijkl}^n$  is the tensor of the elastic constants in the normal state,  $u_i$  is the displacement vector, and  $e_j$  is the surface normal vector. In Eq. (2) and throughout this paper we use the Einstein convention of summation over repeated indices. By variation of  $G$  with respect to  $\psi^*$  and  $A$ , we obtain the modified Ginzburg-Landau equations

$$-\text{curl curl} \mathbf{A} = \mathbf{A} |\psi|^2 + (i/2\kappa) (\psi^* \nabla \psi - \psi \nabla \psi^*), \quad (3a)$$

$$(i\nabla/\kappa + \mathbf{A})^2 \psi = \psi \left[ 1 + a_{ij} \epsilon_{ij} + \frac{1}{2} a_{ijkl} \epsilon_{ij} \epsilon_{kl} - |\psi|^2 (1 + b_{ij} \epsilon_{ij} + \frac{1}{2} b_{ijkl} \epsilon_{ij} \epsilon_{kl}) \right]. \quad (4a)$$

Variation with respect to  $u_i$  yields the modified elasticity equations

$$\begin{aligned} \frac{\partial}{\partial x_j} \left( \frac{\partial u_k}{\partial x_l} \left[ C_{ijkl}^n - \frac{H_c^2}{4\pi} (a_{ijkl} |\psi|^2 - \frac{1}{2} b_{ijkl} |\psi|^4) \right] \right) \\ - \frac{H_c^2}{4\pi} \left( a_{ij} \frac{\partial |\psi|^2}{\partial x_j} - \frac{1}{2} b_{ij} \frac{\partial |\psi|^4}{\partial x_j} \right) \\ = K_i + \delta(r-s) e_j [\sigma_{ij} - (H_c^2/4\pi) (a_{ij} |\psi|^2 - \frac{1}{2} b_{ij} |\psi|^4)], \end{aligned} \quad (5a)$$

where  $\delta(r-s)$  is a Dirac  $\delta$  function located at the surface.

For the sake of simplicity we have confined ourselves in Eq. (5a) to symmetries for which a fourth-rank tensor  $T$  obeys the relations  $T_{ijkl} = T_{jikl} = T_{klij}$ . This includes cubic and hexagonal symmetry. The extension to any other symmetry is straightforward. For  $|\psi|^2 = 0$  Eqs. (5a) are the familiar elasticity equations of the normal state.

#### RELATIONS FOR THE SPECIFIC VOLUME CHANGE

For the macroscopic part of the strain fields, that is slowly varying compared with  $|\psi|^2$  in the mixed state, it is convenient to introduce the local averages  $\langle u_k \rangle$ ,  $\langle |\psi|^2 \rangle$ , and  $\langle |\psi|^4 \rangle$  over a unit cell of the periodic

functions  $|\psi|^2$  and  $|\psi|^4$ . Equation (5a) can then be rewritten as

$$\begin{aligned} \frac{\partial}{\partial x_j} \left( \frac{\partial \langle u_k \rangle}{\partial x_l} \left[ C_{ijkl}^n - \frac{H_c^2}{4\pi} (a_{ijkl} \langle |\psi|^2 \rangle - \frac{1}{2} b_{ijkl} \langle |\psi|^4 \rangle) \right] \right) \\ - \frac{H_c^2}{4\pi} \left( a_{ij} \frac{\partial \langle |\psi|^2 \rangle}{\partial x_j} - \frac{1}{2} b_{ij} \frac{\partial \langle |\psi|^4 \rangle}{\partial x_j} \right) \\ = K_i + \delta(r-s) e_j [\sigma_{ij} - (H_c^2/4\pi) (a_{ij} \langle |\psi|^2 \rangle - \frac{1}{2} b_{ij} \langle |\psi|^4 \rangle)]. \end{aligned} \quad (5b)$$

In this equation the oscillating parts of  $u_k$ ,  $|\psi|^2$ , and  $|\psi|^4$  have been omitted because the corresponding terms can be interpreted as rapidly oscillating forces of zero average, which do not influence the average of  $u_i$  or  $\epsilon_{ij}$  on a large scale. Integrating Eq. (5b) with respect to  $x_j$  we obtain for uniform  $\langle |\psi|^2 \rangle$  a difference in strain between the superconducting and the normal state:

$$\epsilon_{ij}^s - \epsilon_{ij}^n = -S_{ijkl} (H_c^2/4\pi) (a_{kl} \langle |\psi|^2 \rangle - \frac{1}{2} b_{kl} \langle |\psi|^4 \rangle), \quad (6a)$$

where  $S_{ijkl}$  is the tensor of elastic compliances. Higher-order terms in the very small parameter  $S_{ijkl}(H_c^2/4\pi)$  have been omitted in this result.

In the case of cubic symmetry this strain difference is equivalent to a specific volume difference

$$\Delta V/V = 3K (H_c^2/4\pi) (a \langle |\psi|^2 \rangle - \frac{1}{2} b \langle |\psi|^4 \rangle), \quad (6b)$$

where  $K = \frac{1}{3}(S_{1111} + 2S_{1122})$  is the compressibility.

Substituting for  $a$  and  $b$  the definitions Eq. (1), we obtain at zero magnetic field the same result as for type-I superconductors<sup>1</sup>:

$$(\Delta V/V)_{H=0} = {}^3K (H_c/4\pi) (\partial H_c / \partial V). \quad (6c)$$

#### CHANGE OF ELASTIC CONSTANTS

The natural way to solve Eqs. (3), (4), and (5b) is a perturbation calculation with the solutions of the unmodified Ginzburg-Landau equations and the elasticity equations of the normal state as zero-order solutions. The perturbation parameters are  $\epsilon_{ij}$  for the calculation of  $|\psi|^2$  and  $\mathbf{A}$ , and  $S_{ijkl}(H_c^2/4\pi)$  for the calculation of  $\epsilon_{ij}$ .  $S_{ijkl}(H_c^2/4\pi)$  is always very small (of the order of  $10^{-7}$ ) and by the requirement that  $\epsilon_{ij}$  be also small compared to 1, we are only restricted to the validity range of linear elasticity theory, and the lowest nonvanishing order of the perturbation is always a very good approximation.

In order to obtain the linear response of the system to applied volume forces and surface stresses, we have only to calculate the first-order perturbations of  $\langle |\psi|^2 \rangle$  for some selected values of the applied magnetic field.

(a)  $H_a < H_{c1}$ :

$$\langle |\psi|^2 \rangle = |\psi|^2 = 1 + a_{kl} \epsilon_{kl} - b_{kl} \epsilon_{kl},$$

<sup>8</sup> N. A. Abrikosov, Zh. Eksperim. i Teor. Fiz. **32**, 1442 (1957) [English transl.: Soviet Phys.—JETP **5**, 1174 (1957)].

TABLE I. Coefficients of the strain dependence of  $H_{c2}$  and  $\kappa^2$  in Pb-Tl alloys at 4.2°K from experimental data of Alers.<sup>a</sup>

	$(\Delta C_L/C_L)_{H_{c2}}$ <sup>b</sup>	$(C^s - C^n)/C^n$	$(\partial C/\partial H_a)_{H_{c2}} H_{c2}/C$	$a_{11}$	$a_{1111} - a_{1122}$	$b_{1111} - b_{1122}$
Pb-1.7 at.% Tl	$6 \times 10^{-6}$			11.9		
Pb-6 at.% Tl	$4.3 \times 10^{-6}$	$5.7 \times 10^{-6}$	$6.6 \times 10^{-6}$	11.8	11.6	1.7
Pb-17.4 at.% Tl	$\approx 0$	$5.5 \times 10^{-6}$	$7.6 \times 10^{-6}$	$\approx 0$	13.6	3.3

<sup>a</sup> See Refs. 11-13.<sup>b</sup>  $C_L = \frac{1}{2}(C_{1111} + C_{1122} + 2C_{1212})$ .<sup>c</sup>  $C = \frac{1}{2}(C_{1111} - C_{1122})$ .

and therefore

$$a_{ij} \frac{\partial |\psi|^2}{\partial x_j} - \frac{1}{2} b_{ij} \frac{\partial |\psi|^4}{\partial x_j} = (a_{ij} - b_{ij})(a_{kl} - b_{kl}) \frac{\partial^2 u_k}{\partial x_j \partial x_l}.$$

Thus the system responds according to Eq. (5b) with an effective elastic tensor

$$(C_{ijkl}^s)_{H=0} = C_{ijkl}^n - (H_c^2/4\pi) \times [a_{ijkl} - \frac{1}{2} b_{ijkl} + (a_{ij} - b_{ij})(a_{kl} - b_{kl})]. \quad (7a)$$

This can be rewritten by means of the definitions (1) as

$$(C_{ijkl}^s - C_{ijkl}^n)_{H=0} = -(1/8\pi) [\partial^2 (H_c^2) / \partial \epsilon_{ij} \partial \epsilon_{kl}], \quad (7b)$$

which is again the same relation as for type-I superconductors.

(b)  $H_a$  near  $H_{c2}$ : For simplicity we assume that the second-order coefficient of an expansion of  $\langle |\psi|^2 \rangle$  in powers of  $(1 - H_a/H_{c2})$  is negligibly small compared with the first-order coefficient  $2\kappa^2/(2\kappa^2 - 1)\beta$ . This was implicitly shown to be true by Lasher<sup>9</sup> in a calculation of the free energy and the magnetic moment near  $H_{c2}$ . We have, then

$$\langle |\psi|^2 \rangle = \left[ \left( 1 - \frac{2\kappa^2}{2\kappa^2 - 1} b_{kl} \epsilon_{kl} \right) \left( 1 - \frac{H_a}{H_{c2}} \right) + a_{kl} \epsilon_{kl} \right] \times 2\kappa^2 / (2\kappa^2 - 1)\beta, \\ \langle |\psi|^4 \rangle = \beta \langle |\psi|^2 \rangle^2,$$

with  $\beta = 1.16$  for the triangular flux line lattice.<sup>10</sup> Inserting this in (5b) and keeping only the linear terms in  $(1 - H_a/H_{c2})$ , we get the effective elastic tensor

$$C_{ijkl}^s = C_{ijkl}^n - \frac{H_c^2}{4\pi} \left[ a_{ijkl} \left( 1 - \frac{H_a}{H_{c2}} \right) + a_{ij} a_{kl} - a_{ij} b_{kl} \left( 1 - \frac{H_a}{H_{c2}} \right) \frac{4\kappa^2}{2\kappa^2 - 1} \right] \times \frac{2\kappa^2}{(2\kappa^2 - 1) \times 1.16}. \quad (8)$$

Equation (8) indicates a jump of the elastic constants at  $H_{c2}$ ,

$$(\Delta C_{ijkl})_{H=H_{c2}} = (H_c^2/4\pi) a_{ij} a_{kl} [2\kappa^2/(2\kappa^2 - 1) \times 1.16], \quad (9)$$

<sup>9</sup> G. Lasher, Phys. Rev. **140**, A523 (1965).<sup>10</sup> W. H. Kleiner, L. M. Roth, and S. H. Autler, Phys. Rev. **133**, A1227 (1964).

and a change of the elastic constants with field,

$$\left( \frac{\partial C_{ijkl}}{\partial H} \right)_{H=H_{c2}} = \frac{1}{H_{c2}} \times \frac{H_c^2}{4\pi} \left[ a_{ijkl} - \frac{4\kappa^2}{2\kappa^2 - 1} a_{ij} b_{kl} \right] \times 2\kappa^2 / (2\kappa^2 - 1) \times 1.16. \quad (10)$$

Equation (9) is correct independent of our assumption that  $\langle |\psi|^2 \rangle$  is linear in  $(1 - H_a/H_{c2})$ .

If  $\kappa$  and the thermodynamic critical field  $H_c$  are known for a material, all the coefficients introduced in Eq. (1) can be obtained by elasticity measurements and a specific volume measurement. For cubic symmetry,  $a_{11}^2 = a_{22}^2 = a_{33}^2$  are directly given by the jump of the bulk modulus at  $H_{c2}$  as shown in Eq. (9). According to Eq. (6b) a measurement of the volume difference between the normal state and the zero-field superconducting state provides then  $b_{11} = b_{22} = b_{33}$ . After the  $a_{ij}$ 's and  $b_{ij}$ 's are known, any pair of coefficients  $a_{ijkl}$  and  $b_{ijkl}$  is obtained through Eqs. (7a) and (10) by a measurement of the field dependence near  $H_{c2}$  and the total change between the normal and the zero-field superconducting state of the elastic constant  $C_{ijkl}$  with the same indices  $i, j, k, l$ . This method is of interest from the experimental point of view because direct measurement of the strain dependence of  $H_{c2}$  and  $\kappa$  is very difficult.

The only existing experiments from which some of our parameters can be obtained are the measurements of the sound velocity in Pb-Tl alloys by Alers.<sup>11,12</sup> From his data we obtain the numbers given in Table I.

#### INTERACTIONS BETWEEN FLUXOIDS AND ELASTIC DEFECTS

We start with an exact solution  $\psi_0$ ,  $A_0$ ,  $\epsilon_{0ij}$  of the modified Ginzburg-Landau equations (3) and (4) and the modified elasticity equations (5a). The introduction of an internal strain source like a dislocation or other defects imposes new boundary conditions on the elasticity equations. Writing the total strain field  $\epsilon_{ij}$  under these boundary conditions as  $\epsilon_{ij} = \epsilon_{0ij} + \eta_{ij}$ ,

<sup>11</sup> G. A. Alers, in Proceedings of the Conference on the Physics of Type-II Superconductivity, Cleveland, Ohio, 1964, Vol. 1, p. 82 (unpublished).<sup>12</sup> G. A. Alers (private communication).

we obtain for  $\eta_{ij}$  the equation

$$(\partial/\partial x_j)[\eta_{kl}(C_{ijkl} - (H_c^2/4\pi)(a_{ijkl}|\psi|^2 - \frac{1}{2}b_{ijkl}|\psi|^4))] - (H_c^2/4\pi)(\partial/\partial x_j)[\epsilon_{0kl}(a_{ijkl}(|\psi|^2 - |\psi_0|^2) - \frac{1}{2}b_{ijkl}(|\psi|^4 - |\psi_0|^4))] - (H_c^2/4\pi)(\partial/\partial x_j)[a_{ij}(|\psi|^2 - |\psi_0|^2) - \frac{1}{2}b_{ij}(|\psi|^4 - |\psi_0|^4)] = 0. \quad (5c)$$

By inserting  $\epsilon = \epsilon_0 + \eta$  in Eqs. (3) and (4), new equations for  $A$  and  $\psi$  are obtained. In these equations we consider the terms containing  $\eta_{ij}$  as a perturbation. The solution is obtained as a perturbation series

$$\psi = \psi_0 + \sum_{n=1}^{\infty} \varphi_n,$$

$$A = A_0 + \sum_{n=1}^{\infty} \alpha_n,$$

where  $\varphi_n$  and  $\alpha_n$  are proportional to the  $n$ th power of  $\eta_{ij}$ . The equations for  $\varphi_1$  and  $\alpha_1$  are, for example,

$$-\text{curl curl} \alpha_1 = \alpha_1 |\psi_0|^2 + 2A_0 \text{Re}(\varphi_1 \psi_0) + (1/\kappa) \text{Im}(\psi_0^* \nabla \varphi_1 + \varphi_1^* \nabla \psi_0) \quad (3b)$$

and

$$[(i\nabla/\kappa) + A_0]^2 \varphi_1 + 2A_1 [(i\nabla/\kappa) + A_0] \psi_0 = \varphi_1 [1 + a_{ij} \epsilon_{0ij} + \frac{1}{2} a_{ijkl} \epsilon_{0ij} \epsilon_{0kl}] - (\varphi_1 |\varphi_0|^2 + 2\psi_0 \text{Re}(\varphi_1 \psi_0)) \times [1 + b_{ij} \epsilon_{0ij} + \frac{1}{2} b_{ijkl} \epsilon_{0ij} \epsilon_{0kl}] + \eta_{ij} [(a_{ij} + a_{ijkl} \epsilon_{0kl}) - |\psi_0|^2 (b_{ij} + b_{ijkl} \epsilon_{0kl})] \psi_0. \quad (4b)$$

Inserting  $\epsilon = \epsilon_0 + \eta$ ,  $\psi = \psi_0 + \sum \varphi_n$ , and  $A = A_0 + \sum \alpha_n$  in the free-energy equation (2), we obtain the energy of the solution with no defect and additional terms which we arrange in rising powers of  $\eta$ . Using the fact that  $A_0, \psi_0, \epsilon_{0ij}$  are a solution of Eqs. (3), (4), and (5), we obtain the first-order term

$$\Delta E_1 = \int \eta_{0ij} \left[ C_{ijkl} \epsilon_{0kl} - \frac{H_c^2}{4\pi} (a_{ij} |\psi_0|^2 + \frac{1}{2} b_{ij} |\psi_0|^4) \right] d^3 r. \quad (11)$$

We have neglected higher orders of the very small parameter  $S_{ijkl}(H_c^2/4\pi)$  in this result, and consequently for  $\eta_{ij}$  the strain field of the defect in normal material  $\eta_{0ij}$  may be taken, because the corrections from the terms containing  $|\psi|^2$  in Eq. (5c) are also of the order  $S_{ijkl}(H_c^2/4\pi)$ .

For the second-order energy contribution we obtain a very lengthy expression containing  $\varphi_1, \alpha_1, \epsilon_0$ , and  $\eta$ . Since a solution of Eqs. (3b) and (4a) for  $\varphi_1$  and  $\alpha_1$  is not known and is very difficult to obtain, we give here only a second-order formula for the simple case where for symmetry reasons the strain field of the defect  $\eta_{ij}$  is a pure shear. Then  $a_{ij} \eta_{ij}$  and the cross products  $a_{ijkl} \epsilon_{0ij} \eta_{kl}$  and  $b_{ijkl} \epsilon_{0ij} \eta_{kl}$  are zero, and therefore the first-order corrections  $\varphi_1$  and  $\alpha_1$  are zero. The second-order energy contribution in this case is

$$\Delta E_2 = \int \eta_{ij} \eta_{kl} \left( \frac{1}{2} C_{ijkl} \eta^2 - (H_c^2/8\pi) (a_{ijkl} |\psi_0|^2 - \frac{1}{2} b_{ijkl} |\psi_0|^4) \right) d^3 r, \quad (12)$$

where  $\eta_{ij}$  is the solution of Eq. (5c) with  $\psi = \psi_0$ . Higher orders of  $S_{ijkl}(H_c^2/4\pi)$  have again been neglected in this result.

## DISCUSSION

$\Delta E_1$  can be interpreted as the first-order interaction energy between a fluxoid or a configuration of fluxoids characterized by  $\psi_0, A_0, \epsilon_{0ij}$  and an elastic defect characterized by its strain field  $\eta_{0ij}$ .  $\Delta E_2$  contains the elastic energy of the defect itself, and therefore the energy  $\Delta E_{2\infty}$  of the defect at a large distance from the fluxoid configuration has to be subtracted from  $\Delta E_2$  to obtain the second-order interaction energy. We compare now our general results with the explicit calculations of the interaction between defects and single fluxoids by previous authors. The expression in brackets in Eq. (11) can be interpreted as the stress field  $\sigma_{0ij}$  of a fluxoid. The first-order interaction energy is then

$$\Delta E_1 = \int \eta_{0ij} \sigma_{0ij} d^3 r.$$

This form, and the appropriate calculation of  $\sigma_{0ij}$  from Eq. (5a), is identical with the formalism used by Kramer and Bauer in their calculation of the first-order interaction between a fluxoid and an edge dislocation. But their result for  $\sigma_{ij}$  is only obtained from Eq. (5a) if the coefficient  $b_{ij}$  is assumed to be zero. Whether or not the corresponding difference in  $\Delta E_1$  is significant cannot be decided because no measurements are available from which  $a_{ij}$  and  $b_{ij}$  can be determined separately. Equation (5c) with  $\psi = \psi_0$  and Eq. (12) are identical with the problem of a defect in a medium with local variations  $\delta C_{ijkl}(\mathbf{r})$  of the elastic constants  $C_{ijkl}$ , where in our case  $\delta C_{ijkl} = -(H_c^2/4\pi) (a_{ijkl} |\psi_0|^2 - \frac{1}{2} b_{ijkl} |\psi_0|^4)$ . The formalism used by Webb<sup>4</sup> to calculate the interaction between a fluxoid and a screw dislocation and, following the same scheme, by Toth and Pratt<sup>5</sup> to calculate the interaction between a fluxoid and the shear

stress field around a coherent precipitate, correspond to use of our Eqs. (5c) and (12) with the additional assumption  $b_{ijkl}=0$ . Alternatively these calculations may be regarded as relying on the assumption that  $|\psi|^2=|\psi|^4$  everywhere. Then the same factor  $a_{ijkl}-\frac{1}{2}b_{ijkl}$  appears in Eqs. (5c) and (12) and in Eq. (7a) for  $C_{ijkl}^s-C_{ijkl}^n$ . Under either of these assumptions, the appropriate coefficients are available for niobium, vanadium, and tantalum from the measurements by Alers and Waldorf<sup>13</sup> on the changes of elastic constants between the normal and superconducting states  $C_{ijkl}^s-C_{ijkl}^n$ . More recent measurements by Alers on some lead-indium alloys have shown that in fact the terms in  $b_{ijkl}$  are much smaller than the terms in  $a_{ijkl}$  for these alloys (see Table I). However, the coefficients may be quite different in other materials and should be measured for each material separately. The basis of the aforementioned detailed calculations is confirmed by our more general approach although additional terms have been found. It should be pointed out however that if the strain field of a defect has dilatational components, the second-order interaction involves terms containing the first-order corrections  $\varphi_1$ ,  $\alpha_1$  of  $\psi_0$  and  $A_0$  which are then nonzero. These terms can be comparable in magnitude with those given in Eq. (12). Since the first- and second-order interactions seem to be of the same magnitude for small fluxoid-

defect distances,<sup>3</sup> reliable values of the total interaction energy for these defects, i.e., essentially for all defects *except* screw dislocations, cannot be obtained from the existing calculations. (Since our equations indicate no exact cancellation between the various terms contributing to the total energy, these calculations may then still give the right order of magnitude.)

#### VALIDITY OF THE METHOD

It should be emphasized that the validity of our calculations is not only restricted by the limitations of the two-parameter local Ginzburg-Landau theory but also by our implicit assumption that the local value of the free-energy parameters depends on only the local value of the strain and not on its derivatives. We expect this to hold only if the strain is nearly constant over regions of the size of the coherence length. Thus for instance the calculation of the interaction force between a fluxoid and a dislocation by means of this method is not correct if the fluxoid is near the dislocation core, but nevertheless may give a good estimate of the true interaction.

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<sup>13</sup> G. A. Alers and D. L. Waldorf, Phys. Rev. Letters **6**, 677 (1961).